

# BJT Small-Signal Analysis

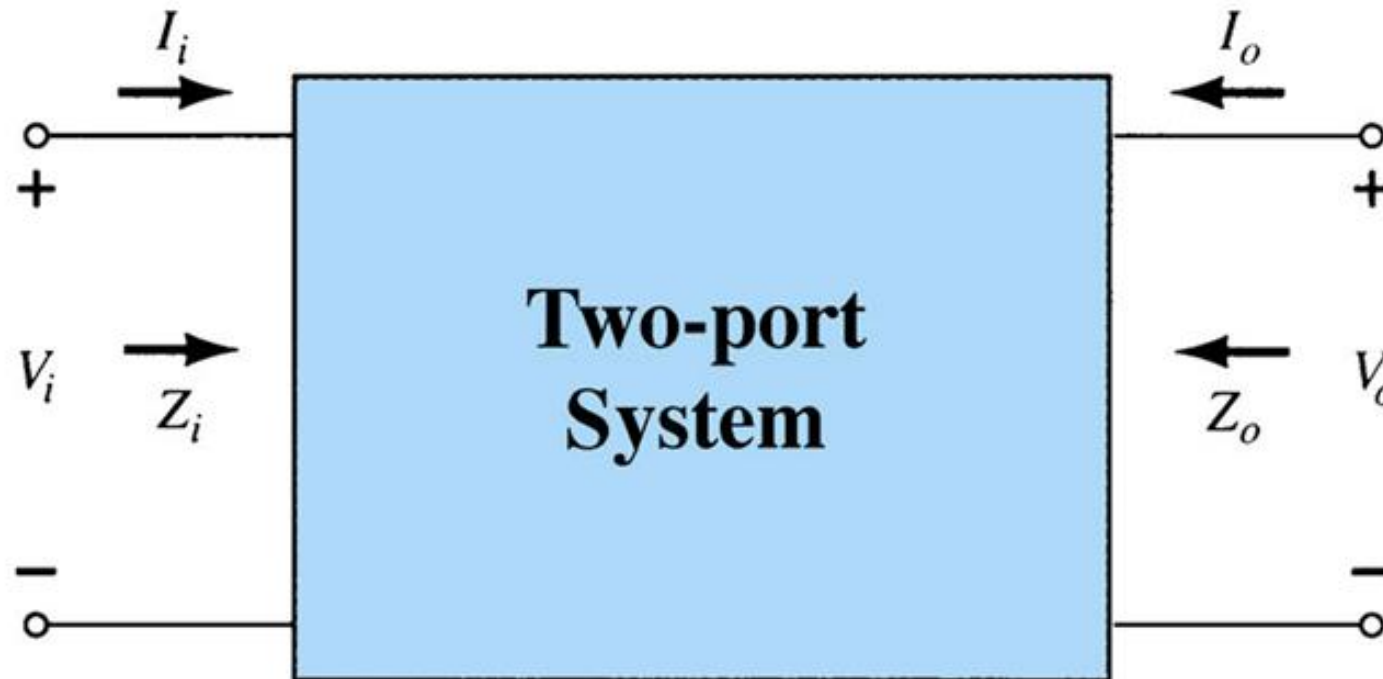
**Semiconductor Devices and Circuits**  
**(ECE 181302)**

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- BJT small-signal model is the equivalent circuit that represents the AC characteristics of the transistor.
- It uses circuit elements that approximate the behavior of the transistor.
- 2 models are commonly used in small signal AC analysis of a transistor:
  - $r_e$  model
  - hybrid equivalent model

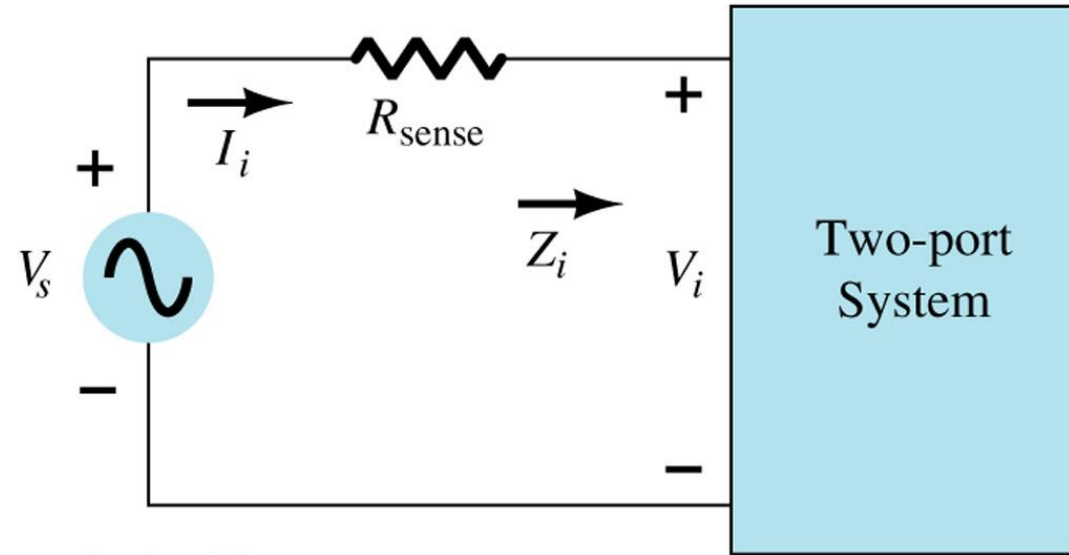
# Important Parameters

- $Z_i$ ,  $Z_o$ ,  $A_v$ ,  $A_i$  are important parameters for the analysis of the AC characteristics of a transistor circuit.



# Input Impedance, $Z_i$

- To determine  $I_i$ : insert a “sensing resistor”



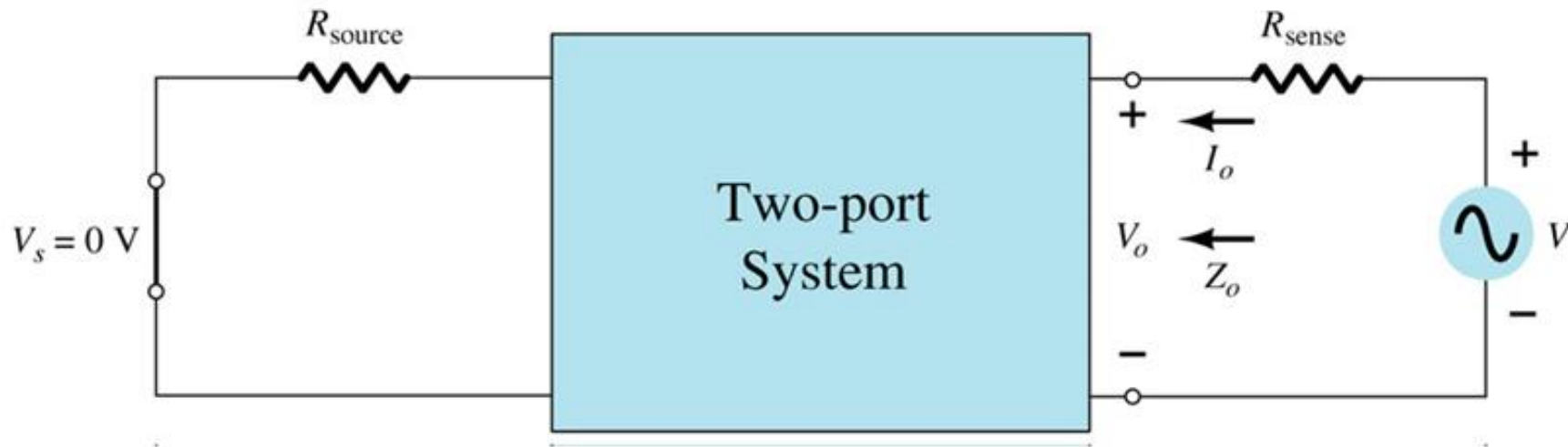
then calculate  $I_i$ :

$$I_i = \frac{V_s - V_i}{R_{\text{sense}}}$$

$$Z_i = \frac{V_i}{I_i}$$

# Output Impedance, $Z_o$

- To determine  $I_o$ : insert a “sensing resistor”



then calculate  $I_o$ :

$$I_o = \frac{V - V_o}{R_{\text{sense}}}$$

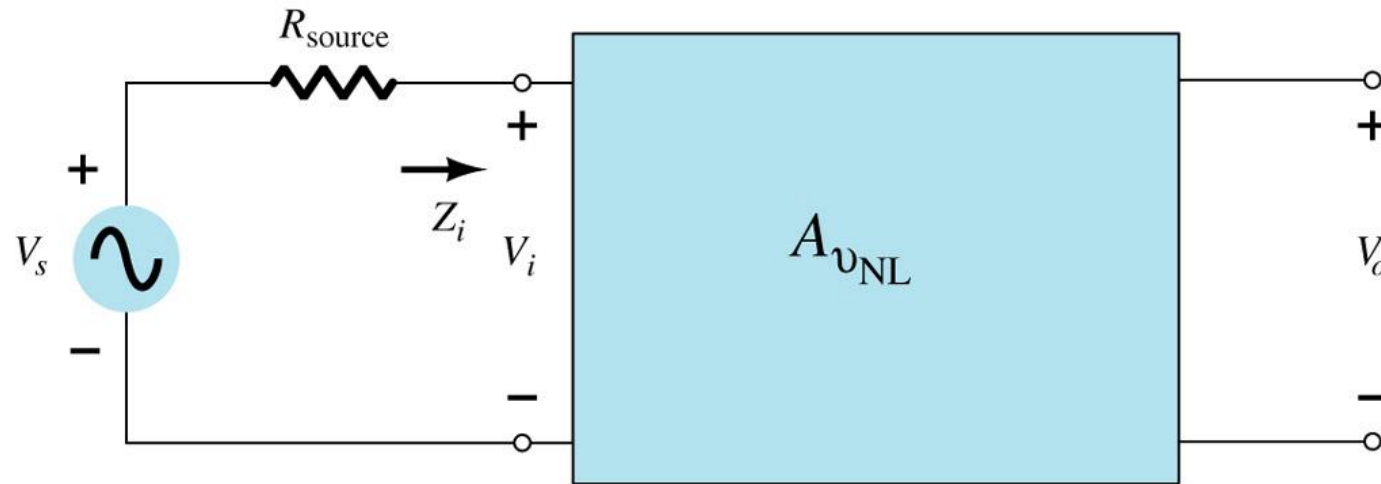
$$Z_o = \frac{V_o}{I_o}$$

# Voltage Gain, $A_v$

- For an amplifier with no load:

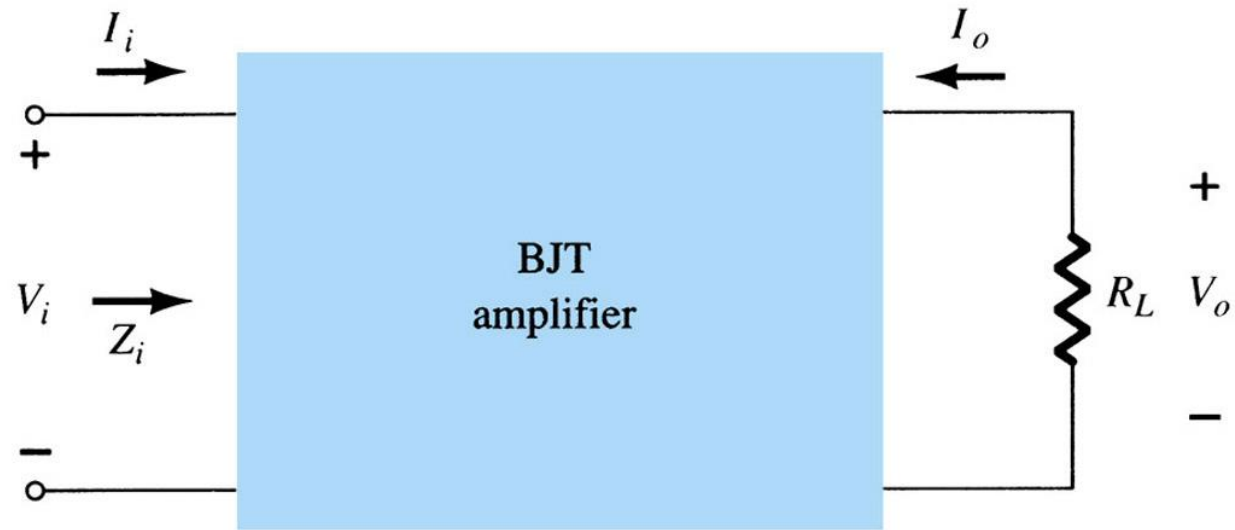
$$A_v = \frac{V_o}{V_i}$$

$$A_{vNL} = \frac{V_o}{V_i} \bigg/ R_L = \infty \Omega (\text{open circuit})$$



- Note:** the no-load voltage gain ( $A_{vNL}$ ) is always greater
  - than the loaded voltage gain ( $A_v$ ).

# Current Gain, $A_i$



- The current gain ( $A_i$ ) also be calculated using the voltage gain ( $A_v$ ):

$$A_i = -A_v \frac{Z_i}{R_L}$$

$$A_i = \frac{I_o}{I_i}$$

# Phase Relationship

- The phase relationship between input and output depends on the amplifier configuration circuit.
  - Common – Emitter  $\sim 180$  degrees
  - Common - Base  $\sim 0$  degrees
  - Common – Collector  $\sim 0$  degrees



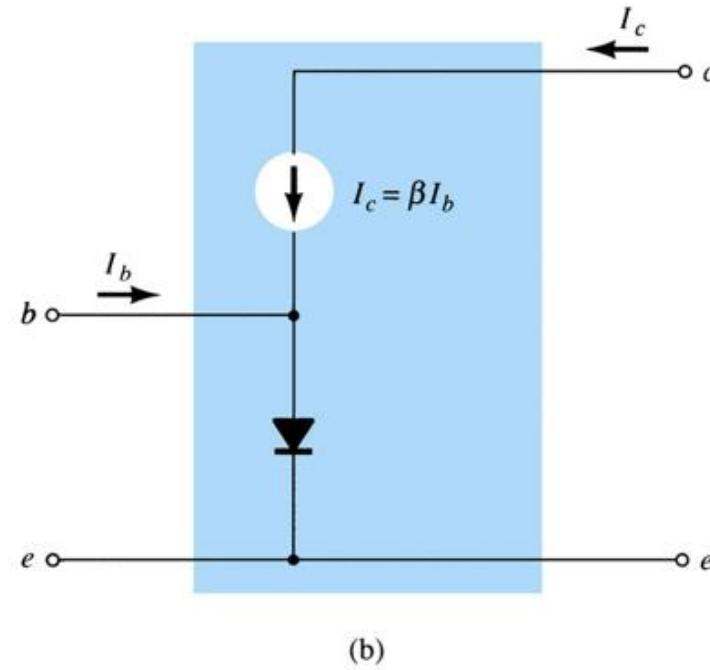
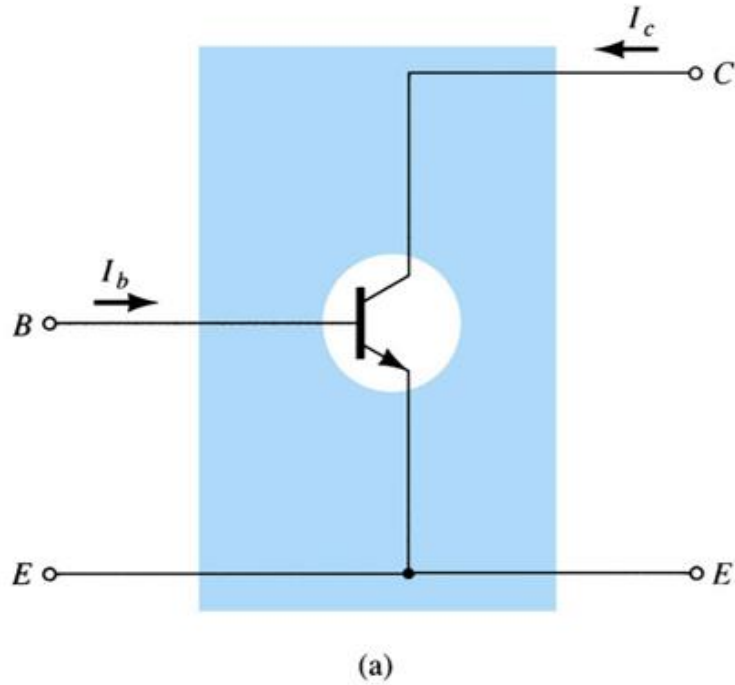
# BJT $r_e$ Model

- BJTs are basically current controlled devices, therefore the  $r_e$  model uses a diode and a current source to duplicate the behavior of the transistor.
- The  $r_e$  model employs a diode and controlled current source to duplicate the behavior of a transistor in the region of interest.
- The ac resistance of a diode can be determined by the equation  $r_{ac} = 26 \text{ mV}/I_D$ , where  $I_D$  is the dc current through the diode at the  $Q$  (quiescent) point. This same equation is used to find the ac resistance of the diode in the BJT.
- Substituting the emitter current:

$$r_e = \frac{26 \text{ mV}}{I_E}$$

- The subscript  $e$  of  $r_e$  is chosen to emphasize that it is the dc level of emitter current that determines the ac level of the resistance of the diode.
- One disadvantage to this model is its sensitivity to the DC level.

# CE *re* Model

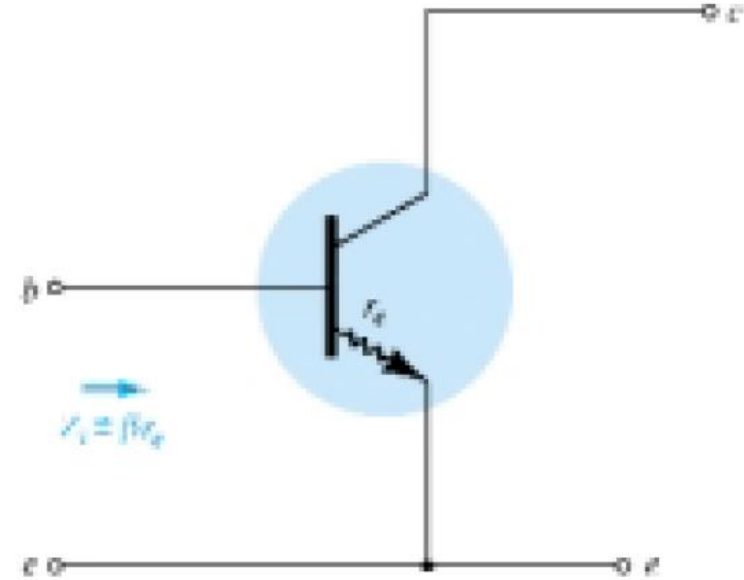
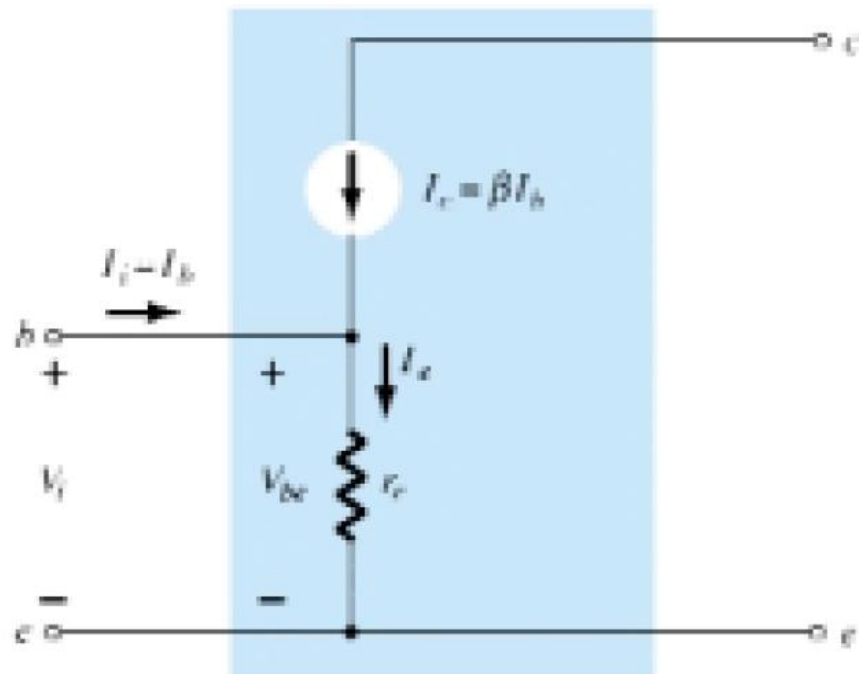


The base current is the input and the collector is the output.  
This model indicates:

$$I_c = \beta I_b$$

$$I_e = (\beta + 1) I_b$$

$$I_e \cong \beta I_b$$



$$I_c = \beta I_b$$

$$I_e = I_c + I_b = \beta I_b + I_b$$

$$I_e = (\beta + 1)I_b$$

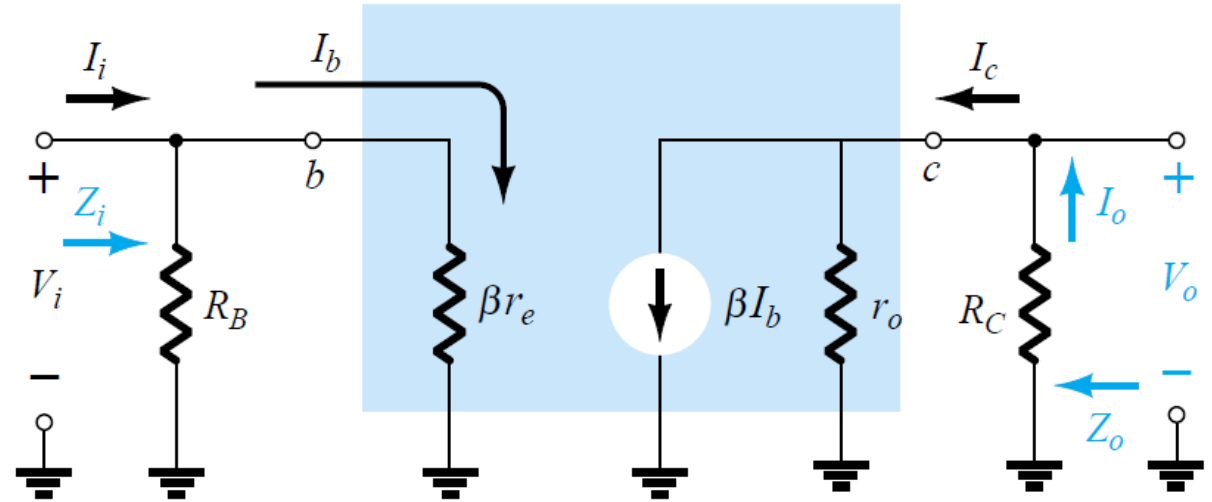
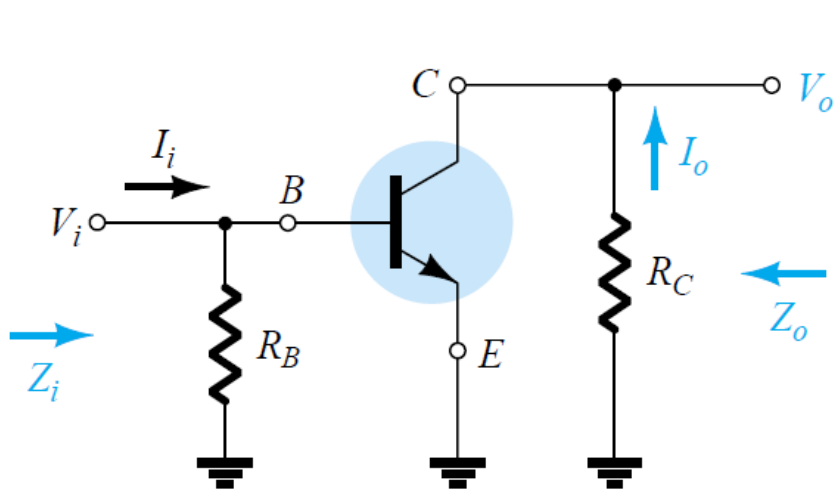
$$I_e \cong \beta I_b$$

# Impedance in Common-Emitter Configuration

$$Z_i = \frac{V_i}{I_i} = \frac{V_{be}}{I_b} \qquad V_i = V_{be} = I_e r_e \cong \beta I_b r_e$$

$$= \frac{V_{be}}{I_b} \cong \frac{\beta I_b r_e}{I_b}$$

$$\boxed{Z_i \cong \beta r_e}_{CE} = (160)(6.5 \, \Omega) = \mathbf{1.04 \, k\Omega}$$



$$Z_i = R_B \parallel \beta r_e \quad \text{ohms} \quad \text{Or}$$

$$Z_i \cong \beta r_e \quad R_B \geq 10\beta r_e$$

- $Z_o$ : The output impedance of any system is defined as the impedance  $Z_o$  determined when  $V_i = 0$ . When  $V_i = 0$ ,  $I_i = I_b = 0$ , resulting in an open-circuit equivalence for the current source. Therefore;

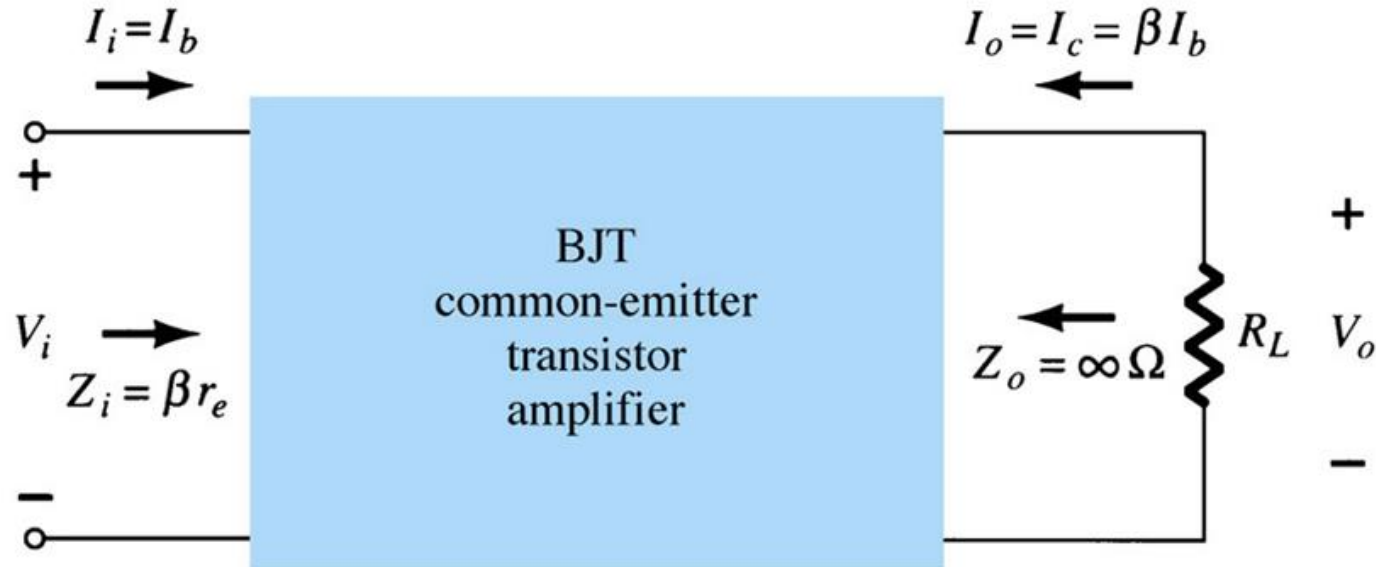
$$Z_o = r_o$$

$$Z_o \cong \infty \Omega$$

$$Z_o = R_C \parallel r_o \quad \text{ohms}$$

$$Z_o \cong R_C \quad r_o \geq 10R_C$$

# Gain calculations for the Common-Emitter using the $r_e$ model



Voltage Gain ( $A_v$ ):

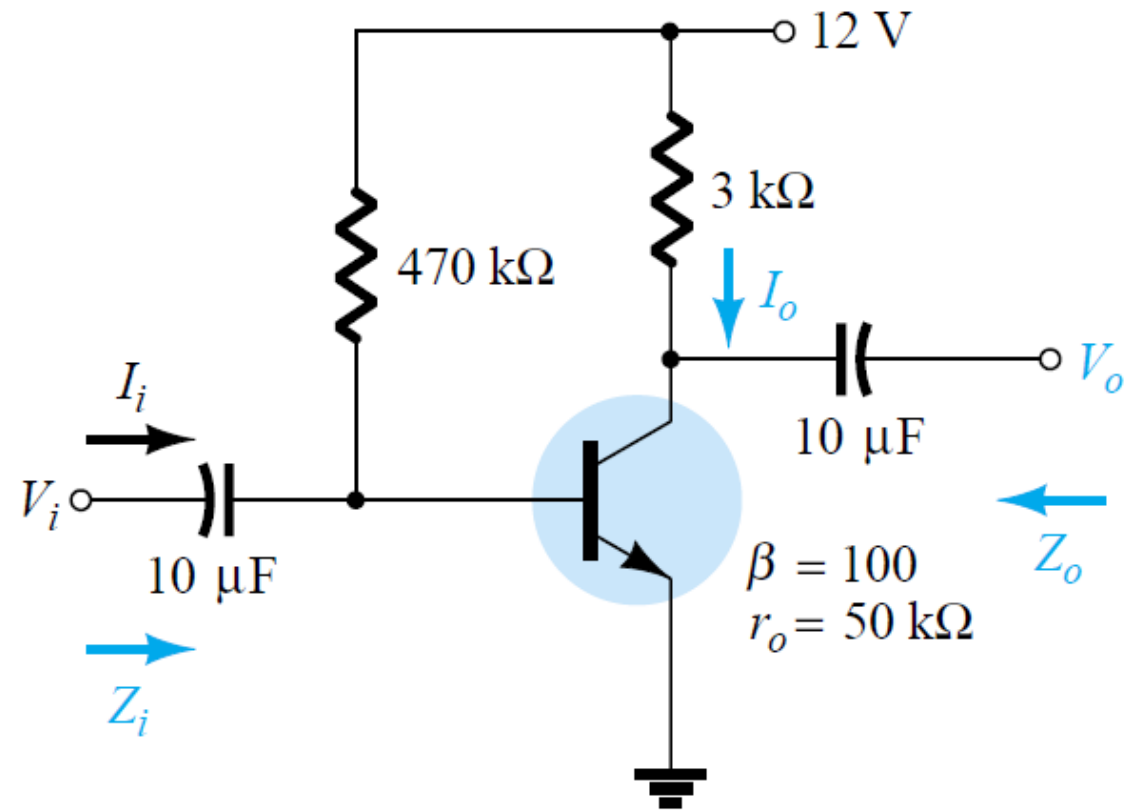
$$A_v = -\frac{R_L}{r_e}$$

Current Gain ( $A_i$ ):

$$A_i = \beta \Big/_{r_o = \infty \Omega}$$

Example: For the network;

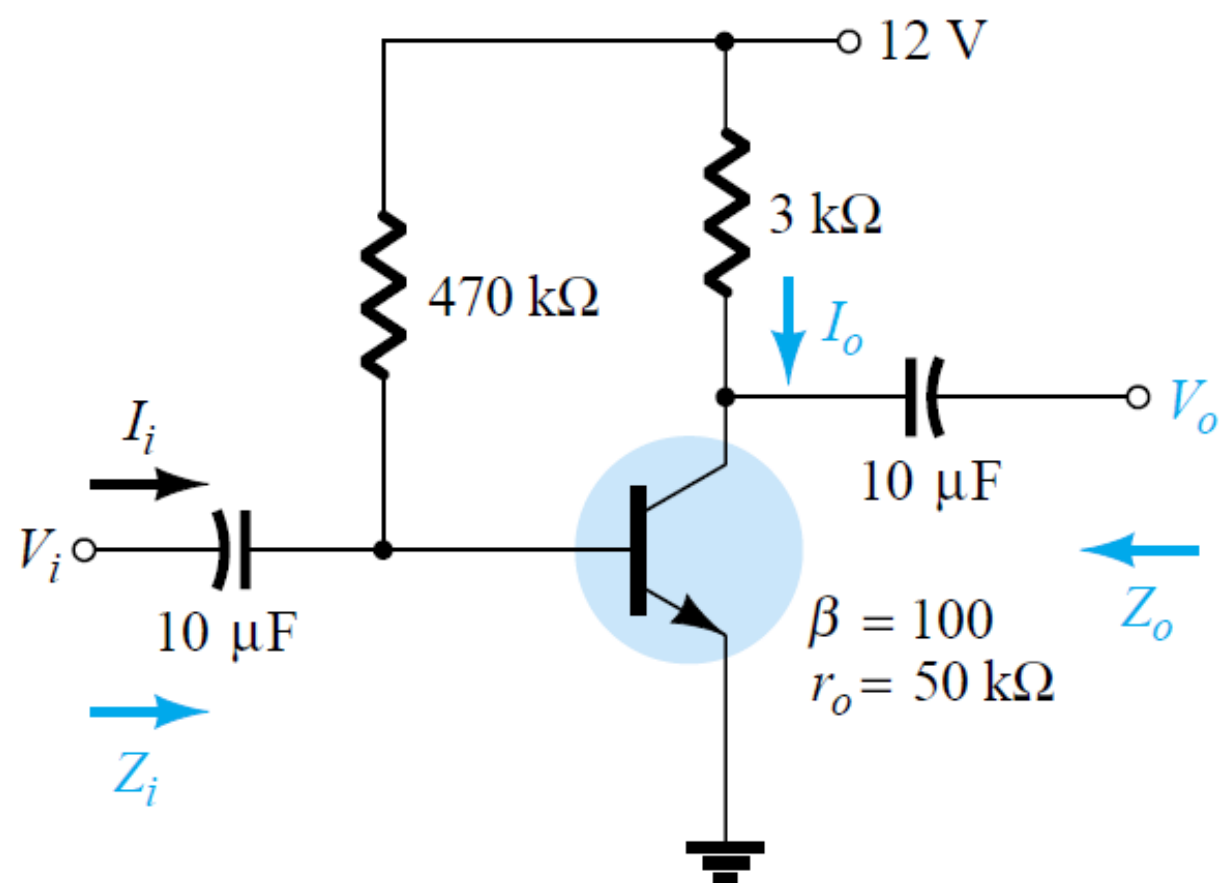
- (a) Determine  $r_e$ .
- (b) Find  $Z_i$  (with  $r_o = \infty\Omega$ ).
- (c) Calculate  $Z_o$  (with  $r_o = \infty\Omega$ ).
- (d) Determine  $A_v$  (with  $r_o = \infty\Omega$ ).
- (e) Find  $A_i$  (with  $r_o = \infty\Omega$ ).
- (f) Repeat parts (c) through (e) including  $r_o = 50\text{ k}\Omega$  in all calculations and compare results.

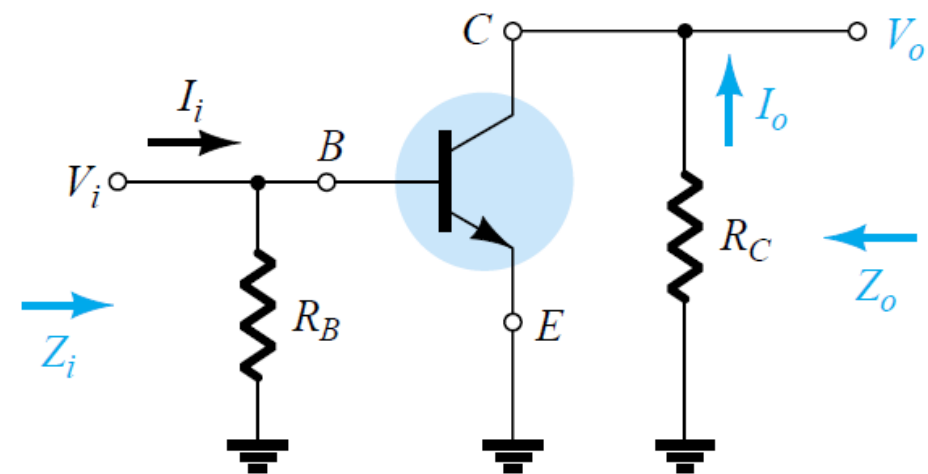
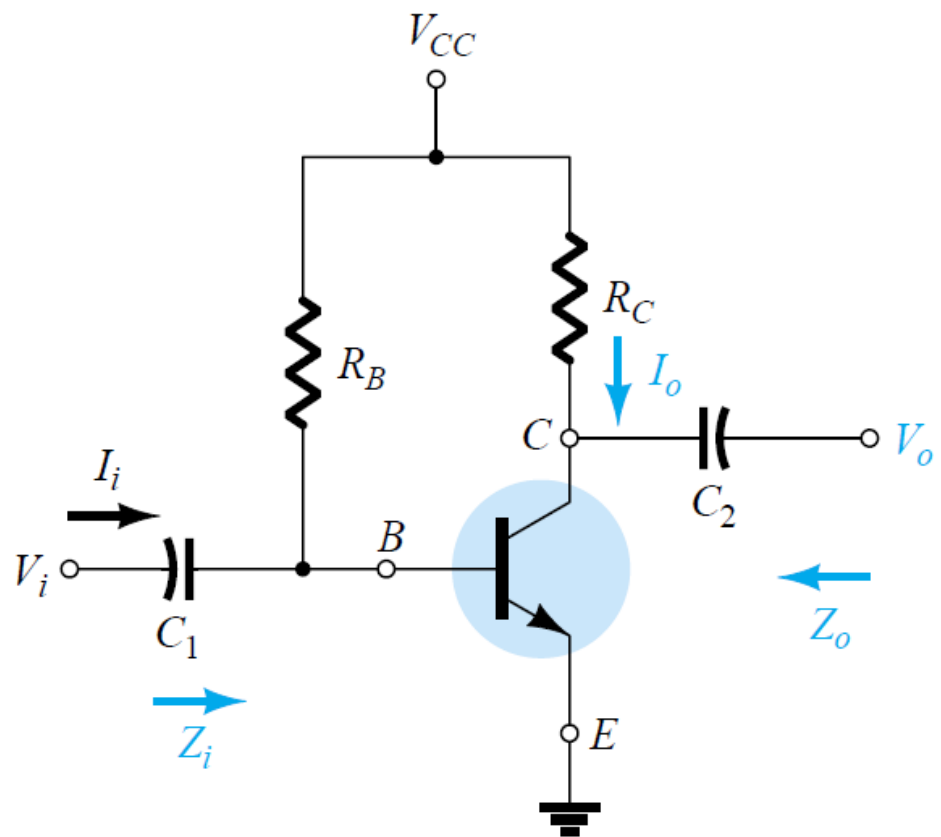


# BJT AC Analysis Steps

- Mark the terminals of the transistor.
- Mark the current directions and define the voltages.
- Remove the dc effects of  $V_{CC}$  by connecting it to the ground.
- Ground  $V_{CC}$ .
- Replace the dc blocking capacitors by short-circuit equivalents.
- Redraw the circuit.
- Substitute the BJT by the  $r_e$  model into the network.







- Solution:

(a) DC analysis:

$$I_B = \frac{V_{CC} - V_{BE}}{R_B} = \frac{12 \text{ V} - 0.7 \text{ V}}{470 \text{ k}\Omega} = 24.04 \text{ }\mu\text{A}$$

$$I_E = (\beta + 1)I_B = (101)(24.04 \text{ }\mu\text{A}) = 2.428 \text{ mA}$$

$$r_e = \frac{26 \text{ mV}}{I_E} = \frac{26 \text{ mV}}{2.428 \text{ mA}} = \mathbf{10.71 \text{ }\Omega}$$

(b)  $\beta r_e = (100)(10.71 \text{ }\Omega) = 1.071 \text{ k}\Omega$

$$Z_i = R_B \parallel \beta r_e = 470 \text{ k}\Omega \parallel 1.071 \text{ k}\Omega = \mathbf{1.069 \text{ k}\Omega}$$

(c)  $Z_o = R_C = \mathbf{3 \text{ k}\Omega}$

(d)  $A_v = -\frac{R_C}{r_e} = -\frac{3 \text{ k}\Omega}{10.71 \text{ }\Omega} = \mathbf{-280.11}$

(e) Since  $R_B \geq 10\beta r_e (470 \text{ k}\Omega > 10.71 \text{ k}\Omega)$

$$A_i \cong \beta = \mathbf{100}$$

$$(f) \quad Z_o = r_o \parallel R_C = 50 \text{ k}\Omega \parallel 3 \text{ k}\Omega = \mathbf{2.83 \text{ k}\Omega} \text{ vs. } 3 \text{ k}\Omega$$

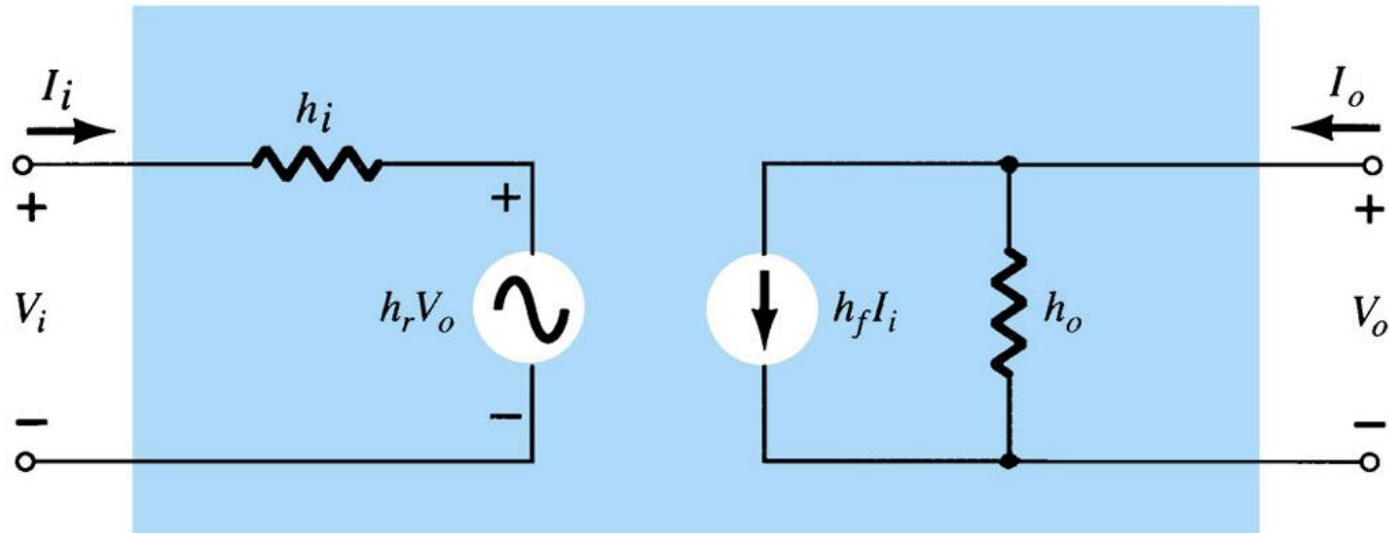
$$A_v = -\frac{r_o \parallel R_C}{r_e} = \frac{2.83 \text{ k}\Omega}{10.71 \text{ }\Omega} = \mathbf{-264.24} \text{ vs. } -280.11$$

$$A_i = \frac{\beta R_B r_o}{(r_o + R_C)(R_B + \beta r_e)} = \frac{(100)(470 \text{ k}\Omega)(50 \text{ k}\Omega)}{(50 \text{ k}\Omega + 3 \text{ k}\Omega)(470 \text{ k}\Omega + 1.071 \text{ k}\Omega)} \\ = \mathbf{94.13} \text{ vs. } 100$$

$$A_i = -A_v \frac{Z_i}{R_C} = \frac{-(-264.24)(1.069 \text{ k}\Omega)}{3 \text{ k}\Omega} = \mathbf{94.16}$$

# Hybrid Equivalent Model

- General h-Parameters:  $h_{ie}$ ,  $h_{re}$ ,  $h_{fe}$ ,  $h_{oe}$  are developed and used to model the transistor.
- The h-Parameters can be found in a specification sheet for a transistor.



$h_i$  = input resistance

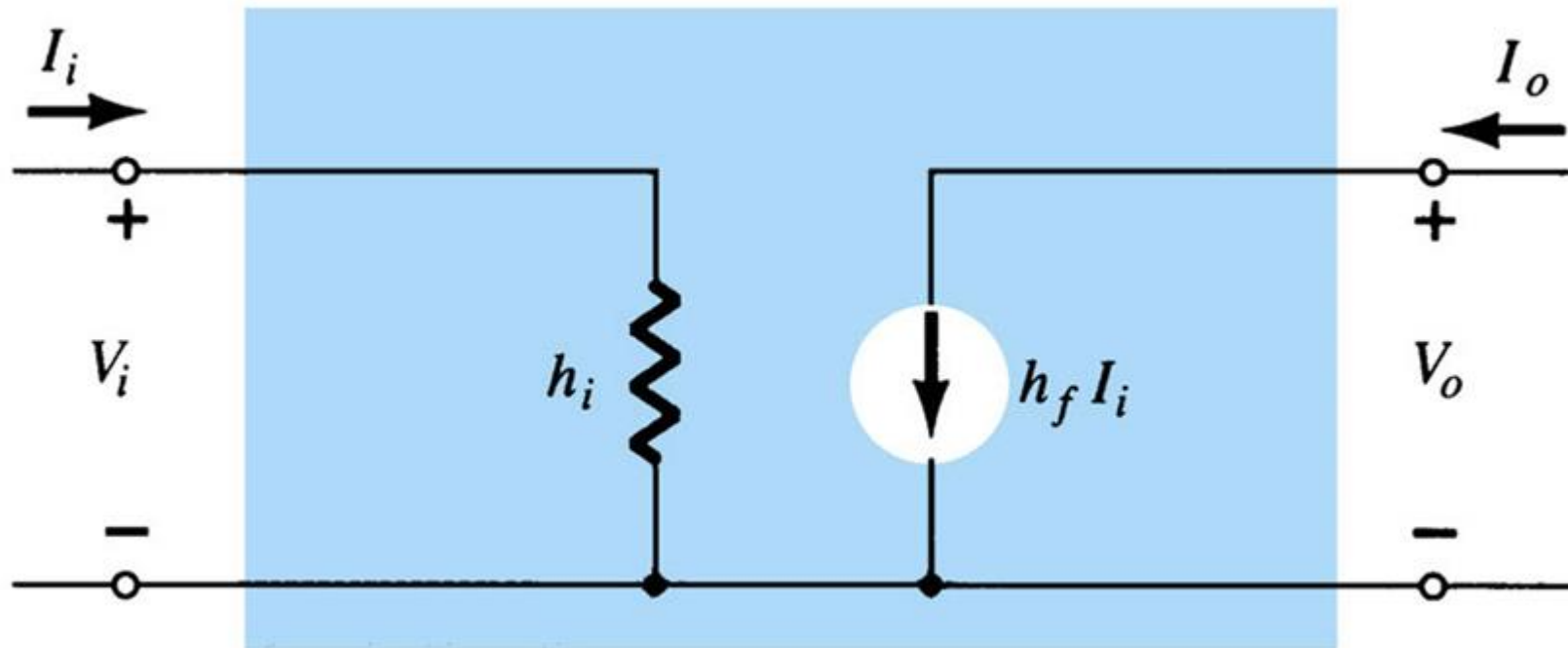
$h_r$  = reverse transfer voltage ratio ( $V_i/V_o$ )

$h_f$  = forward transfer current ratio ( $I_o/I_i$ )

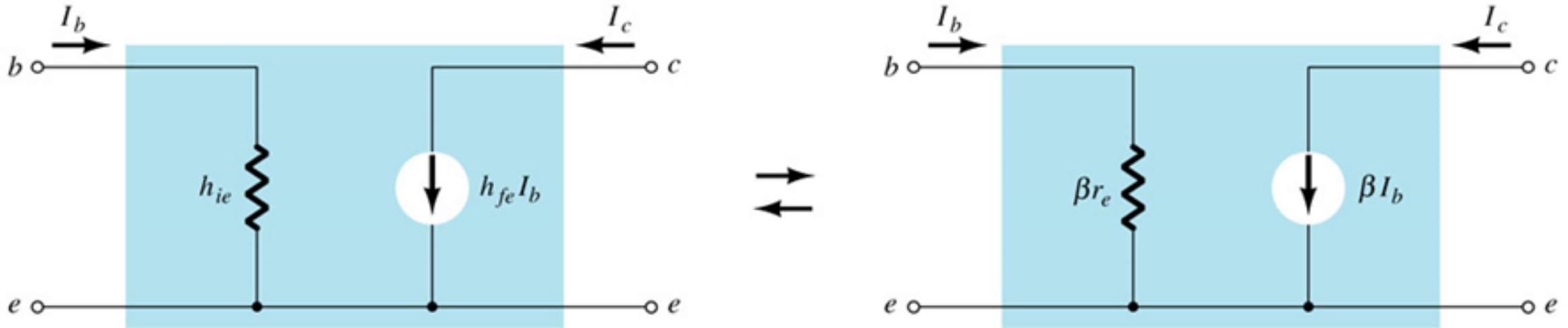
$h_o$  = output conductance

# Simplified General h-Parameter Model

- The general h-parameter model can be simplified based on approximations:
- $h_r \cong 0$  therefore  $h_r V_o = 0$  and  $h_o \cong \infty$



# Common-Emitter $r_e$ vs. h-Parameter Model



$$\begin{aligned}h_{ie} &= \beta r_e \\h_{fe} &= \beta \\h_{oe} &= 1/r_o\end{aligned}$$

Common-Emitter h-Parameters:

$$\begin{aligned}h_{ie} &= \beta r_e \\h_{fe} &= \beta_{ac}\end{aligned}$$





# References:

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