

8/4/25

⇒ Poisson's and Laplace's Equations:-

$$\nabla \cdot D = \rho_v$$

wkt

$$E = -\nabla V$$

$$\nabla(\epsilon_0 E) = \rho_v$$

$$\nabla(\epsilon_0(-\nabla V)) = \rho_v$$

$$-\nabla^2 V = \frac{\rho_v}{\epsilon_0}$$

$$\nabla^2 V = -\frac{\rho_v}{\epsilon_0} \quad (1)$$

eqn (1) is Poisson's eqn

For In freespace, $\rho_v = 0$

$$\therefore \nabla^2 V = 0 \quad (2)$$

Eqn (2) is called as Laplace's Equation

Q11 Determine whether or not the following potential fields satisfy Laplace eqn.

a) $V = x^2 - y^2 + z^2$ b) $V = r \cos \phi + z$ c) $V = r \cos \theta + \phi$

Sol ✓

$\nabla^2 V$ in 3-coordinates

In cartesian

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \quad (\text{Cartesian coordinates})$$

in cylindrical C.S

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \left(\frac{\partial^2 V}{\partial \phi^2} \right) + \frac{\partial^2 V}{\partial z^2} \text{ (cylindrical C.S)}$$

in spherical

$$\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) +$$

$$\frac{1}{r^2 \sin^2 \theta} \left(\frac{\partial^2 V}{\partial \phi^2} \right) \text{ (spherical)}$$

a) $V = x^2 - y^2 + z^2$

$$\nabla^2 V = 0$$

$$\nabla^2 V = \frac{\partial^2 (x^2 - y^2 + z^2)}{\partial x^2} + \frac{\partial^2 (x^2 - y^2 + z^2)}{\partial y^2} + \frac{\partial^2 (x^2 - y^2 + z^2)}{\partial z^2}$$

$$= 2 - 2 + 2$$

$$= 2$$

$$\therefore \nabla^2 V \neq 0$$

b) $V = r \cos \phi + z$ Hence the potential field doesn't satisfy the Laplace eqn

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} [r \cos \phi] + \frac{1}{r^2} [-\cos \phi] + 0$$

$$= \frac{\cos \phi}{r} - \frac{\cos \phi}{r} = 0$$

$$\therefore \nabla^2 V = 0$$

$$= 0$$

Hence the given potential field satisfies Laplace eqn

$$q \quad \nabla r \cos \theta + \phi$$

$$1 - \cos^2 \theta$$

$$\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \cos \theta \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left[\sin^2 \theta \frac{\partial V}{\partial \theta} \right]$$

$$+ \frac{1}{r^2 \sin^2 \theta} \left[0 \right]$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial r^2} + \frac{\partial}{\partial r} \left[\cos \theta \right] \sin \theta$$

$$= \frac{\partial \cos \theta}{\partial r} - \frac{\sin \theta}{r^2 \sin \theta}$$

$$= \frac{\partial \cos \theta}{\partial r} - \frac{\partial \cos \theta}{\partial r} = 0$$

\therefore Hence the given potential satisfies eqn

Uniqueness Theorem

Under the given boundary conditions Laplace eqn has one and only one soln. The same holds good for Poisson eqn

Consider Laplace eqn

$$\nabla^2 V = 0 \quad \text{--- (1)}$$

Let there be a soln V_1, V_2 which obey the above eqn and both satisfy boundary conditions for the given case

$$\nabla^2 V_1 = 0 \quad \text{--- (2)} \quad \nabla^2 V_2 = 0 \quad \text{--- (3)}$$

Subtraction eqn (2) from (3) --- (2) - (3)

$$\nabla^2 (V_1 - V_2) = 0$$

$$\nabla^2 f = 0$$

where $f = V_1 - V_2$ is a scalar function

Let the values of a. solns at the boundary be

$$V_1 = V_2 = V_{ab}$$

$$\therefore V_1 = V_2$$

(since both satisfy boundary conditions)

$$V_1 = V_2 = V_b$$

$V_b \rightarrow$ potential at boundary

$$V_1 - V_2 = 0 = f_b = f$$

from vector calculus we have

$$\nabla(f \cdot \vec{A}) = f \cdot (\nabla \vec{A}) + \vec{A} \cdot \nabla f$$

∴ Let us choose $\vec{A} = \nabla f$
can be any vector

$$\therefore \nabla(f \cdot \nabla f) = f \cdot (\nabla \cdot \nabla f) + \nabla f \cdot \nabla f$$

Integrate above eqn throughout the volume

$$\int \nabla(f \cdot \nabla f) \cdot dV = \int f \cdot [\nabla \cdot \nabla f] dV + \int (\nabla f)^2 dV \quad (7)$$

From divergence theorem

$$\int \nabla \cdot \vec{A} dV = \oint \vec{A} \cdot d\vec{S}$$

$$\int \nabla \cdot \nabla f dV = \oint \nabla f \cdot d\vec{S}$$

Multiply both sides by f

$$\int \nabla[f \cdot \nabla f] dV = \oint f \cdot \nabla f \cdot d\vec{S} \quad (8)$$

The RHS of above eqn is an integral over throughout surface that surrounds the volume. Obviously this surface involves the boundaries at which we know

$$f = f_b = 0$$

$$\therefore \text{LHS} \cdot \nabla f = 0 \text{ eqn (4)} \quad \nabla^2 f = 0$$

$$\int (\nabla f)^2 dV = 0$$

$$\int [\nabla(v_1 - v_2)]^2 dV = 0$$

An integral over certain volume can be zero under condition

- ① If the integrand has ~~to~~ the values at some points \leq -ve at some other parts of the volume. So that the sum could be zero.

- ② If the integrand is zero at every point in volume since eqn (8) integrand consists of square, it can't be \leq -ve at any point which rules out the 1st possibility

$$\therefore [\nabla(v_1 - v_2)]^2 = 0$$

$$\nabla(v_1 - v_2) = 0$$

It is possible only if $(v_1 - v_2)$ is constant

The statement $v_1 - v_2 = \text{constant}$ throughout the volume implies that the value of f has at the boundary inside volume should be equal.

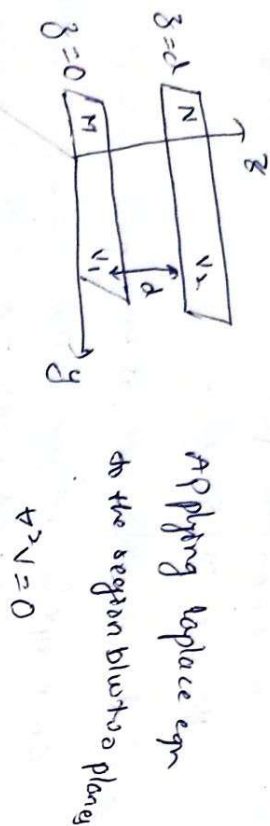
$$\therefore v_1 - v_2 = v_{1b} - v_{2b} = 0$$

$$v_1 = v_2$$

Thus v_1 and v_2 are identical and hence the uniqueness theorem.

Application of Laplace eqn:-

1) Two uniformly charged parallel plates of infinite extent (case of parallel plate capacitor)



$$\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = 0 \quad \text{--- (1)}$$

$$\therefore \frac{\partial V}{\partial y} = \frac{\partial V}{\partial x} = 0$$

$$\therefore \frac{\partial^2 V}{\partial z^2} = 0 \quad \text{--- (2)}$$

Soln of above eqn

$$V = Az + B \quad \text{--- (3)}$$

where A & B are constants apply boundary conditions

at $z=0$ $V=V_1$

$$V_1 = A(0) + B$$

$$B = V_1$$

put in eqn (3)

$$V = Az + V_1 \quad \text{--- (4)}$$

at $z=d$, $V=V_2$

Substitute in eqn (4)

$$V_2 = Ad + V_1$$

$$\frac{V_2 - V_1}{d} = A$$

$$V = \left(\frac{V_2 - V_1}{d} \right) z + V_1$$

Soln

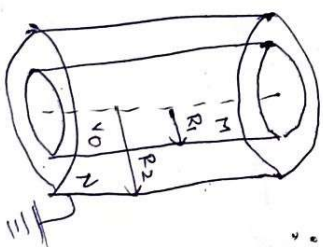
\therefore we get

$$E = -\nabla V$$

$$= - \left[\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right]$$

$$\vec{E} = - \left[\frac{V_2 - V_1}{d} \right] \hat{a}_z$$

2) Two concentric cylinders of infinite length (coaxial cable)



$$\therefore \nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left[r \frac{\partial V}{\partial r} \right] + \frac{1}{r^2} \frac{\partial^2 V}{\partial \phi^2} +$$

$$\frac{\partial^2 V}{\partial z^2} = 0$$

Since the field exists only along radial direction

$$\frac{\partial V}{\partial \phi} = \frac{\partial V}{\partial z} = 0$$

$$\therefore \frac{1}{r} \frac{\partial}{\partial r} \left[r \frac{\partial V}{\partial r} \right] = 0$$

$$\frac{\partial}{\partial r} \left[r \frac{\partial V}{\partial r} \right] = 0$$

$$r \frac{\partial V}{\partial r} = A$$

$$\frac{\partial V}{\partial r} = \frac{A}{r}$$

$$V = A \ln r + B \quad \text{--- (1)}$$

Apply boundary conditions

$$\text{at } r = R_1,$$

$$V = V_0$$

$$V_0 = A \ln R_1 + B \quad \text{--- (2)}$$

$$\text{at } r = R_2, V = 0 \quad (\text{as it is grounded})$$

$$0 = A \ln R_2 + B$$

$$B = -A \ln R_2 \quad \text{--- (3)}$$

Substitute (3) in (2)

$$V_0 = A \ln R_1 - A \ln R_2$$

$$V_0 = A \ln \left[\frac{R_1}{R_2} \right]$$

$$A = \frac{V_0}{\ln(R_1/R_2)} \quad \text{--- (4)}$$

(3) in (1)

$$V = A \ln r - A \ln R_2$$

$$= A \ln \left(\frac{r}{R_2} \right)$$

$$V = V_0 \frac{\ln(r/R_2)}{\ln(R_1/R_2)}$$

$$\text{WKT } E = -\nabla V$$

$$E = -\frac{d}{dr} \left[V_0 \frac{\ln(r/R_2)}{\ln(R_1/R_2)} \right]$$

$$E = \frac{-V_0}{\ln(R_2/R_1)} \frac{d}{dr} [\ln r - \ln R_2]$$

$$E = \frac{-V_0}{\ln(R_2/R_1)} \left[0 - \frac{1}{r} \right] = \frac{V_0}{r \ln(R_2/R_1)}$$

$$\therefore \vec{E} = \frac{V_0}{r \ln(R_2/R_1)} \hat{a}_r \quad \text{--- (5)}$$

Also we have

$$\vec{E} = \frac{\rho_L}{2\pi\epsilon_0 r} \hat{a}_r \quad \text{--- (6)}$$

Compare (5) & (6)

$$\frac{V_0}{r \ln(R_2/R_1)} = \frac{\rho_L}{2\pi\epsilon_0 r}$$

$$\frac{V_0}{\ln\left[\frac{R_2}{R_1}\right]} = \frac{Q}{L \pi \epsilon}$$

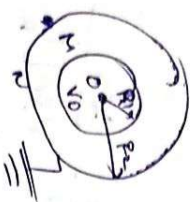
$$C = \frac{Q}{V_0} = \frac{Q \pi \epsilon L}{\ln\left[\frac{R_2}{R_1}\right]}$$

$$\Phi = CV$$

capacitance per unit length

$$\frac{C}{L} = \frac{Q \pi \epsilon}{\ln\left[\frac{R_2}{R_1}\right]}$$

3 Two concentric spheres



$$\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left[r^2 \frac{\partial V}{\partial r} \right] + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left[\sin \theta \frac{\partial V}{\partial \theta} \right]$$

$$+ \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2} = 0$$

$$\frac{\partial V}{\partial \theta} = \frac{\partial V}{\partial \phi} = 0, \text{ potential remains constant along } \theta, \phi$$

$$\frac{1}{r^2} \left[\frac{\partial}{\partial r} \left[r^2 \frac{\partial V}{\partial r} \right] \right] = 0$$

$$r^2 \frac{\partial V}{\partial r} = A$$

$$\therefore \frac{\partial V}{\partial r} = \frac{A}{r^2}$$

$$V = -\frac{A}{r} + B \quad \text{--- (1)}$$

Apply boundary conditions

$$\text{at } r = R_2, V = 0$$

$$0 = -\frac{A}{R_2} + B$$

$$B = \frac{A}{R_2} \quad \text{--- (2)}$$

$$\text{at } r = R_1, V = V_0$$

$$\therefore V_0 = -\frac{A}{R_1} + B$$

$$V_0 = -\frac{A}{R_1} + \frac{A}{R_2}$$

$$V_0 = A \left[\frac{1}{R_2} - \frac{1}{R_1} \right]$$

$$\therefore A = \frac{V_0}{\left[\frac{1}{R_2} - \frac{1}{R_1} \right]} \quad \text{--- (3)}$$

substitute in (1)

$$V = -\frac{A}{r} + \frac{A}{R_2}$$

$$V = A \left[-\frac{1}{r} + \frac{1}{R_2} \right]$$

$$V = \frac{V_0}{\frac{1}{R_2} - \frac{1}{R_1}} \left[\frac{1}{R_2} - \frac{1}{r} \right]$$

$$V = V_0 \frac{\left[\frac{1}{x} - \frac{1}{R_2} \right]}{\left[\frac{1}{R_1} - \frac{1}{R_2} \right]}$$

$$\epsilon = -\frac{\partial V}{\partial x} = -\frac{\partial}{\partial x} \left[\frac{V_0 \left[\frac{1}{x} - \frac{1}{R_2} \right]}{\left[\frac{1}{R_1} - \frac{1}{R_2} \right]} \right]$$

$$= -\frac{\partial}{\partial x} \left[\frac{V_0 \left[\frac{1}{x} - \frac{1}{R_2} \right]}{\left[\frac{1}{R_1} - \frac{1}{R_2} \right]} \right]$$

$$= -\frac{V_0}{\left(\frac{1}{R_1} - \frac{1}{R_2} \right)} \left[-\frac{1}{x^2} \right]$$

$$\vec{E} = -\frac{1}{x^2} \frac{V_0}{\left(\frac{1}{R_1} - \frac{1}{R_2} \right)} \hat{a}_x \rightarrow (6)$$

Also we have

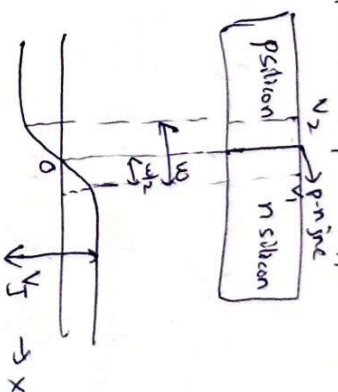
$$\epsilon = \frac{Q}{\epsilon_0 \epsilon_r} \hat{a}_x \quad (5)$$

$$\frac{Q}{\epsilon_0 \epsilon_r x^2} = \frac{1}{x^2} \frac{V_0}{\left(\frac{1}{R_1} - \frac{1}{R_2} \right)}$$

$$\therefore C = \frac{Q}{V_0} = \frac{\epsilon_0 \epsilon_r}{\left(\frac{1}{R_1} - \frac{1}{R_2} \right)}$$

Application of Poisson's eqn

(i) solution of Poisson's eqn as applicable to p-n-jnc.



→ Exactly at junction, i.e. at $x=0$, $V=0$ — (1)

→ at $x=w/2$, $\frac{dV}{dx} = 0$ — (2)

→ $\frac{dV}{dy} = \frac{dV}{dz} = 0$ all over the material — (3)

From Poisson's eqn

$$\nabla^2 V = -\frac{\rho_v}{\epsilon}$$

$$\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = -\frac{\rho_v}{\epsilon}$$

from condition (3)

$$\frac{\partial^2 V}{\partial x^2} = -\frac{\rho_v}{\epsilon} \quad (\text{partial diff})$$

Since we are differentiating only x
 \therefore it is complete differential

$$\frac{d^2 V}{dx^2} = -\frac{\rho_v}{\epsilon}$$

$$\frac{d}{dx} \left(\frac{dV}{dx} \right) = -\frac{\rho_v}{\epsilon}$$

$$d \left(\frac{dV}{dx} \right) = -\frac{\rho_v}{\epsilon} dx$$

Integrate

$$\frac{dV}{dx} = -\frac{\rho_v}{\epsilon} x + k_1 \quad \text{--- (1)}$$

$k_1 \rightarrow$ integration constant

From condition (2)

$$0 = -\frac{\rho_v}{\epsilon} \left(\frac{w}{2} \right) + k_1$$

$$k_1 = \frac{\rho_v w}{2\epsilon} \quad \text{--- (2)}$$

Substitute k_1 in eqn (1)

$$\frac{dV}{dx} = -\frac{\rho_v}{\epsilon} x + \frac{\rho_v w}{2\epsilon} \left(\frac{w}{2} \right)$$

$$dV = -\frac{\rho_v}{\epsilon} x dx + \frac{\rho_v w}{2\epsilon} dx$$

Integrate

$$V = -\frac{\rho_v}{2\epsilon} \frac{x^2}{2} + \frac{\rho_v w}{2\epsilon} x + k_2 \quad \text{--- (3)}$$

Condition (1)

$$V=0 \quad x=0$$

$$0 = k_2$$

Substitute in (3)

$$V = \frac{\rho_v w x}{2\epsilon} - \frac{\rho_v x^2}{2\epsilon}$$

$$\therefore V = \frac{\rho_v x}{2\epsilon} (w - x)$$

Let the potential at $x = \frac{w}{2}$ be V_1

$$V_1 = \frac{\rho_v w}{2\epsilon} \left(\frac{w}{2} \right) - \frac{\rho_v}{2\epsilon} \left(\frac{w}{2} \right)^2$$

$$V_1 = \frac{\rho_v w^2}{4\epsilon} - \frac{\rho_v w^2}{8\epsilon}$$

$$V_1 = \frac{\rho_v w^2}{8\epsilon}$$

Let the potential at $x = \frac{w}{2}$ be V_2

$$V_2 = \frac{\rho_v w}{2\epsilon} \left(\frac{w}{2} \right) - \frac{\rho_v}{2\epsilon} \left(\frac{w}{2} \right)^2$$

$$V_2 = \frac{\rho_v w^2}{4\epsilon} - \frac{\rho_v w^2}{8\epsilon}$$

$$V_2 = \frac{-3\rho_v w^2}{8\epsilon}$$

\therefore The junction potential V_j

$$V_j = V_1 - V_2$$

$$= \frac{\rho_v w^2}{8\epsilon} + \frac{3\rho_v w^2}{8\epsilon}$$

$$= \frac{1}{2} \frac{\rho_v w^2}{\epsilon}$$

$$V = \frac{\rho v^2}{g z}$$

② Electric field across the junction

$$E = -\nabla V$$

$$= - \left[\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right]$$

from condition ③

$$E = - \frac{\partial V}{\partial x} \hat{a}_x$$

$$V = \frac{\rho v u x}{g z} - \frac{\rho v x^2}{g z}$$

$$E = - \left[\frac{d}{dx} \left\{ \frac{\rho v u x}{g z} - \frac{\rho v x^2}{g z} \right\} \right] \hat{a}_x$$

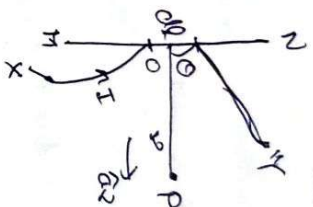
$$E = - \left[\frac{\rho v u}{g z} - \frac{2 \rho v x}{g z} \right] \hat{a}_x$$

$$E = \frac{\rho v}{g z} \left[x - \frac{\rho v u}{g} \right] \hat{a}_x$$

23/10/25

Module-3

Biot-Savart's Law



statement the magnitude of the magnetic field intensity dH at P due to current in the differential element is directly proportional to the product of the current I , the magnitude of the length of the differential element dl , and the sine of the angle b/w the tangent drawn to the element and the line joining the point P and the element and it is inversely proportional to the square of the distance b/w the point and the element.

$$\therefore dH \propto \frac{I dl \sin \theta}{r^2}$$

$$dH = k \frac{I dl \sin \theta}{r^2}$$

where k is the proportionality constant it is given by

$$k = \frac{1}{4\pi} \mu_0$$

$$dH = \frac{I dl \sin \theta}{4\pi r^2}$$

The direction of dH at P as per the law is tangent to the plane containing the tangent drawn to the element & the line joining the point and the element.

It is expressed in vector notation as

$$d\vec{H} = \frac{I d\vec{l} \times \hat{r}}{4\pi r^2}$$

where $d\vec{l}$ is directed along the direction of current and \hat{r} is the unit vector directed from point 's' towards 'p'.

Q1 Find the magnetic field at $A(2,3,-2)$ due to a current element $I d\vec{l} = \pi(0.5\hat{x} - 0.6\hat{y} + 0.8\hat{z}) \mu A$ situated at point $B(3,-2,4)$.

Sol $A(2,3,-2) \quad B(3,-2,4)$

$$I d\vec{l} = \pi(0.5\hat{x} - 0.6\hat{y} + 0.8\hat{z}) \mu A$$

$$\vec{r} = \frac{B(3,-2,4) - A(2,3,-2)}{|B(3,-2,4) - A(2,3,-2)|} \quad \hat{r} = \frac{\vec{r}}{|\vec{r}|}$$

$$\vec{r} = -\hat{x} + 5\hat{y} - 6\hat{z}$$

$$|\vec{r}| = \sqrt{1+25+36} = \sqrt{62}$$

$$\hat{r} = \frac{-\hat{x} + 5\hat{y} - 6\hat{z}}{\sqrt{62}}$$

$$\hat{a}_r = -0.18\hat{x} + 0.63\hat{y} - 0.76\hat{z}$$

$$I d\vec{l} \times \hat{a}_r = \pi \times 10^{-6} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 0.5 & -0.6 & 0.8 \\ -0.18 & 0.63 & -0.76 \end{vmatrix}$$

$$= \pi \times 10^{-6} (-0.048\hat{x} + 0.878\hat{y} + 0.238\hat{z})$$

$$d\vec{H} = \pi \times 10^{-6} (-0.048\hat{x} + 0.878\hat{y} + 0.238\hat{z})$$

$$4\pi \times 10^{-7} (60)$$

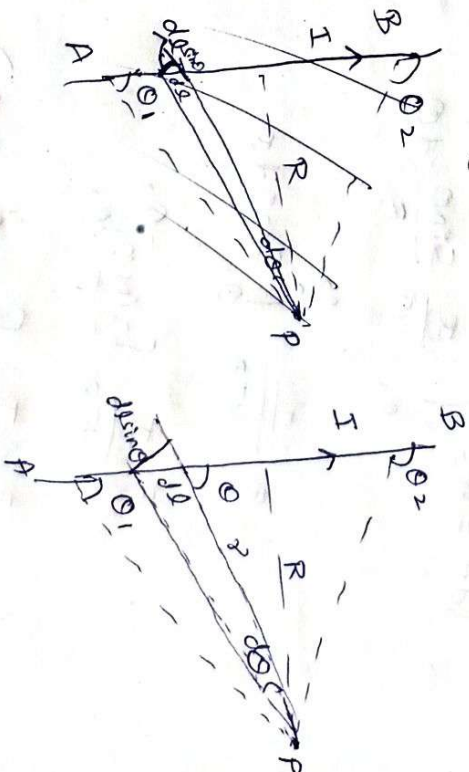
$$d\vec{H} = 10^{-6} \text{ A/m}$$

$$|d\vec{H}| = 0.004 \mu A/m$$

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Applications of Biot-Savart's Law:-

1) Magnetic field intensity at a point due to a current in a straight conductor of finite length:-



From Biot-Savart's law

$$d\vec{H} = \frac{I d\vec{l} \times \hat{r}}{4\pi r^2}$$

Its magnitude

$$dH = \frac{I dl \sin\theta}{4\pi r^2}$$

From the figure

$$d\vec{s} \sin \theta = r d\theta$$

$$\therefore dH = \frac{I r d\theta}{4\pi r^2} = \frac{I}{4\pi r} d\theta$$

from fig

$$\sin \theta = \frac{R}{r}$$

$$\therefore \frac{1}{r} = \frac{\sin \theta}{R}$$

$$\therefore dH = \frac{I}{4\pi} \frac{\sin \theta}{R} d\theta$$

\therefore Total field at point 'P' due to entire ~~conducting~~ ^{conducting} wire

$$\int dH = H = \int_{\theta_1}^{\theta_2} \frac{I}{4\pi} \frac{\sin \theta}{R} d\theta$$

$$= \frac{I}{4\pi R} \int_{\theta_1}^{\theta_2} \sin \theta d\theta$$

$$= \frac{I}{4\pi R} [-\cos \theta]_{\theta_1}^{\theta_2}$$

$$= \frac{I}{4\pi R} [\cos \theta_1 - \cos \theta_2]$$

\therefore Magnetic field intensity at a point due to a current in an infinitely long length along straight conductor is -

Ans.

Same as prev diagram

for wire length $\theta_1 = 0$ & $\theta_2 = \pi$

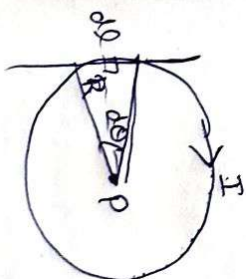
$$H = \frac{I}{4\pi R} [\cos 0 - \cos \pi]$$

$$= \frac{I}{4\pi R} [\cos 0 - \cos \pi]$$

$$= \frac{I}{4\pi R} (2)$$

$$H = \frac{I}{2\pi R}$$

3) Magnetic field intensity at the centre of circular current loop :-



From Biot-Savart's law

$$d\vec{H} = \frac{I d\vec{l} \times \vec{r}}{4\pi r^2}$$

$$dH = \frac{I dl \sin \theta}{4\pi R^2}$$

from the fig $\theta = 90^\circ$ & $dl = R d\theta$

$$\therefore dH = \frac{I \times R d\theta \sin 90^\circ}{4\pi R^2}$$

$$dH = \frac{I d\theta}{4\pi R}$$

$$H = \frac{I}{4\pi R} \int d\theta$$

$$H = \frac{I}{4\pi R} (2\pi)$$

$$H = \frac{I}{2R}$$

$$\vec{H} = \frac{I}{2R} \hat{a}_\phi$$

⇒ Ampere's Circuital Law

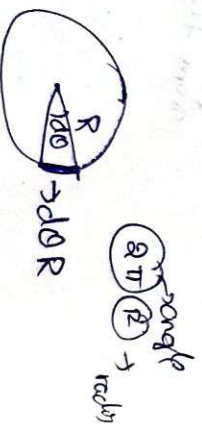
Statement:- Ampere's law states that line integral of \vec{H} about any closed path is equal to the current enclosed by the path. Its representation as integration

$$\oint \vec{H} \cdot d\vec{l} = I$$

or

$$\oint \frac{B}{\mu} d\vec{l} = I$$

$$\oint \vec{B} \cdot d\vec{l} = \mu I$$

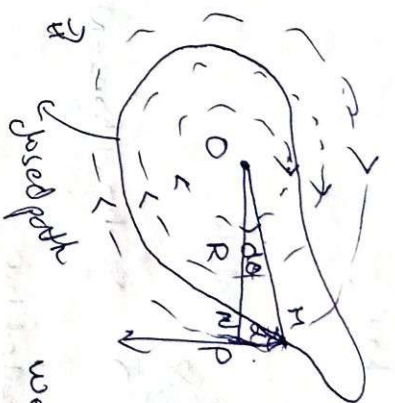


$$MN = dl$$

from fig

$$MP = dl \cos \alpha$$

$$R \sin \alpha = MP$$



where 'P' is the distance of element from 'O', we know that magnetic flux density due to a current carrying straight conductor

$$B = \frac{\mu I}{2\pi R}$$

∴ the flux through the current element = $\vec{B} \cdot d\vec{l}$
the flux through the entire closed path = $\oint \vec{B} \cdot d\vec{l}$

$$\therefore \oint \vec{B} \cdot d\vec{l} = \oint B dl \cos \alpha$$

$$\oint \vec{B} \cdot d\vec{l} = \oint B dl \cos \alpha$$

$$= \oint \frac{\mu I}{2\pi R} dl \cos \alpha$$

$$= \frac{\mu I}{2\pi} \int dl \cos \alpha$$

$$\oint \vec{B} \cdot d\vec{l} = \frac{\mu I}{2\pi} (2\pi)$$

$$\oint \vec{B} \cdot d\vec{l} = \mu I$$

2/5/15

Application of Ampere's Law:-

① toroidal coil:-



Number of turns = N

From Ampere's Circuital Law

$$\oint \vec{H} \cdot d\vec{l} = N \cdot I$$

$$H \oint dl = NI$$

$$H(2\pi R) = NI$$

$$H = \frac{NI}{2\pi R}$$

Since H remains constant
closed path is a circle of radius R

② straight solid cylindrical conductor:-



closed path inside the conductor

From Ampere's Circuital Law

$$\oint \vec{H} \cdot d\vec{l} = I$$

→ The current density through the

$$\text{cross section} = \frac{I}{\pi R^2} = \frac{\text{Current}}{\text{area}}$$

③ Coaxial cable (refer notes)

→ Area of cross section enclosed by the closed path = πr^2

→ Current enclosed by the closed path

$$= \frac{I}{\pi R^2} \times \pi r^2 = \frac{I r^2}{R^2}$$

From Ampere's Law

$$\oint \vec{H} \cdot d\vec{l} = I = \frac{I r^2}{R^2}$$

$$H \oint dl = \frac{I r^2}{R^2}$$

$$H(2\pi r) = \frac{I r^2}{R^2}$$

$$H = \frac{I r}{2\pi R^2}$$

③. If consider H at the surface

i.e. $r = R$

$$H = \frac{I R}{2\pi R^2}$$

$$H = \frac{I}{2\pi R}$$

③ Consider H outside the surface i.e. $r > R$

From Ampere's Law

$$\oint \vec{H} \cdot d\vec{l} = I$$

$$H \oint dl = I$$

$$H(2\pi r) = I$$

$$H = \frac{I}{2\pi r}$$

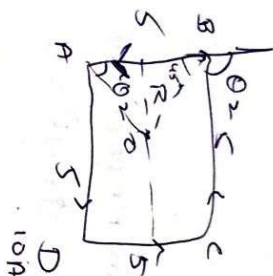
1) Find the magnetic field intensity at the centre of the square of side equal to 5 m and carrying a current of 10 A

Sol: $I = 10 \text{ A}$

$$R = 2.5$$

$$\tan \theta_1 = \frac{2.5}{2.5} = 1$$

$$\theta = 45^\circ$$



$$\theta_2 = 180^\circ - 45^\circ = 135^\circ$$

$$\boxed{\theta_2 = 135^\circ}$$

$$\vec{H} = \frac{I}{4\pi R} [\cos \theta_1 - \cos \theta_2]$$

$$\vec{H} = \frac{10}{4\pi(2.5)} [\cos 45^\circ - \cos 135^\circ]$$

$$\vec{H} = \frac{10}{4\pi(2.5)} [1.414]$$

$$\boxed{\vec{H} = 0.45 \text{ A/m}}$$

considering one side

(For sides) \therefore the field strength at centre 'O' due to all sides of square

$$\vec{H} = 4(0.45)$$

$$\boxed{\vec{H} = 1.8 \text{ A/m}}$$

2) An air core toroid having a noncircular area of 6 cm^2 and mean radius 15 cm is wound uniformly with sections carrying current of 4 A . Determine the magnetic flux density and field intensity of the toroid.

Sol: $H = \frac{NI}{2\pi R}$

Given

$N = 500, R = \text{Mean Radius} = 0.15 \text{ m}$

$I = 4$

$$H = \frac{(500)(4)}{2\pi(0.15)}$$

$$H = 2101.29 \text{ A/m}$$

$$B = \mu_0 \mu_r H$$

$$B = 400 \mu_r H$$

$$B = 4\pi \times 10^{-7} \times 1 \times 2101.29$$

$$B = 2.6 \times 10^{-3}$$

$$B = 2.6 \text{ mT or } 2.6 \times 10^{-3} \text{ T or } 2.6 \text{ A/m}^2$$

Magnetic force

A positive charge 'q' moving with a velocity 'v' in a uniform magnetic field of flux density

\vec{B} experiences force \vec{F} given by

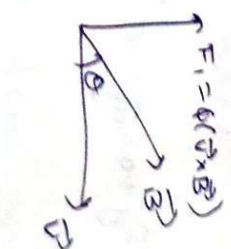
$$\vec{F} = q(\vec{v} \times \vec{B}) \rightarrow \text{①}$$

It's magnitude is given by

$$|\vec{F}| = qvB \sin \theta \quad (\text{angle b/w } \vec{v} \text{ \& } \vec{B})$$

velocity = v

B - flux density



$\theta \rightarrow$ angle b/w velocity vector 'v' and flux density B

The direction of force is seen to plane containing

u & B

of the charge is subjected to only the influence of an electric field of strength F , then the direction of force will be the sum of forces F_1 & F_2

$$F_2 = Q_2 E_2 \quad (2)$$

If it is subjected to the combined influence of a magnetic field of flux density B and electric field of strength E then the resultant force vector F will be the sum of forces F_1 & F_2

$$F = Q(E + v \times B)$$

\rightarrow Lorentz force eqn

(1) A point charge $q = 18 \text{ nC}$ has a velocity of

$v = 5 \times 10^6 \text{ m/s}$ in direction $\hat{a} = 0.6\hat{a}_x + 0.75\hat{a}_y + 0.3\hat{a}_z$. Calculate the magnitude of the force exerted on charge by the field

$B = -3\hat{a}_x + 4\hat{a}_y + 6\hat{a}_z \text{ mT}$

Sol

$$B = -3\hat{a}_x + 4\hat{a}_y + 6\hat{a}_z$$

$$v = 5 \times 10^6 \text{ m/s}$$

$$Q = 18 \text{ nC}$$

$$\hat{a} = 0.6\hat{a}_x + 0.75\hat{a}_y + 0.3\hat{a}_z$$

$$F = Q(v \times B)$$

$$v \times B = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0.6 & 0.75 & 0.3 \\ -3 & 4 & 6 \end{vmatrix} \times 5 \times 10^6$$

$$v \times B = (3.3\hat{a}_x - 4.5\hat{a}_y + 4.65\hat{a}_z) \times 5 \times 10^6$$

$$F = 18 \times 10^{-9} \times 5 \times 10^6 [3.3\hat{a}_x - 4.5\hat{a}_y + 4.65\hat{a}_z]$$

$$F = 90 \times 10^{-3} [3.3\hat{a}_x - 4.5\hat{a}_y + 4.65\hat{a}_z]$$

$$|F| = \sqrt{(10.26)^2 + (-40.5)^2 + (41.85)^2} \times 10^{-3}$$

$$|F| = 0.65374 \times 10^3$$

$$|F| = 653.74 \text{ mN}$$

(2) $Q = 18 \text{ nC}$, $v = 5 \times 10^6 \text{ m/s}$

$$\hat{a} = 0.6\hat{a}_x + 0.75\hat{a}_y + 0.3\hat{a}_z$$

$$B = -3\hat{a}_x + 4\hat{a}_y + 6\hat{a}_z \text{ mT}$$

Sol

$$v \times B = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0.6 & 0.75 & 0.3 \\ -3 & 4 & 6 \end{vmatrix} \times 5 \times 10^6$$

$$= (1.8\hat{a}_x - 3.3\hat{a}_y + 4.65\hat{a}_z) \times 5 \times 10^3$$

$$F = 90 \times 10^{-6} [1.8\hat{a}_x - 3.3\hat{a}_y + 4.65\hat{a}_z]$$

$$F = [1.62\hat{a}_x - 2.97\hat{a}_y + 4.185\hat{a}_z] \times 10^{-6}$$

$$|F| = \sqrt{(1.62)^2 + (-2.97)^2 + (4.185)^2} \times 10^{-6}$$

$$F = 538.14 \times 10^{-6} \text{ N}$$

$$F = 538.14 \text{ mN}$$