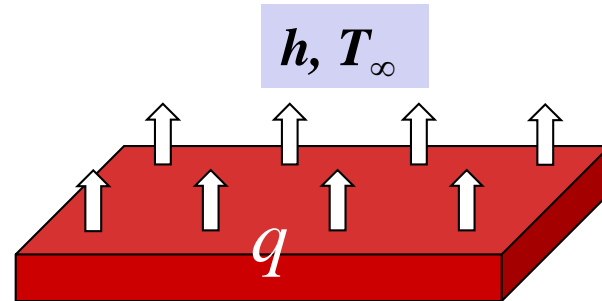


# Conduction: Theory of Extended Surfaces

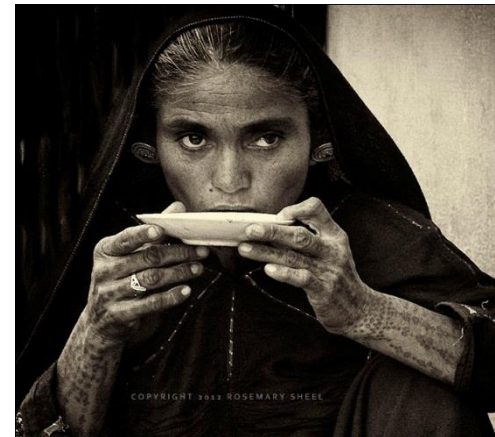
# Why extended surface?



$$q = hA(T_s - T_{\infty})$$

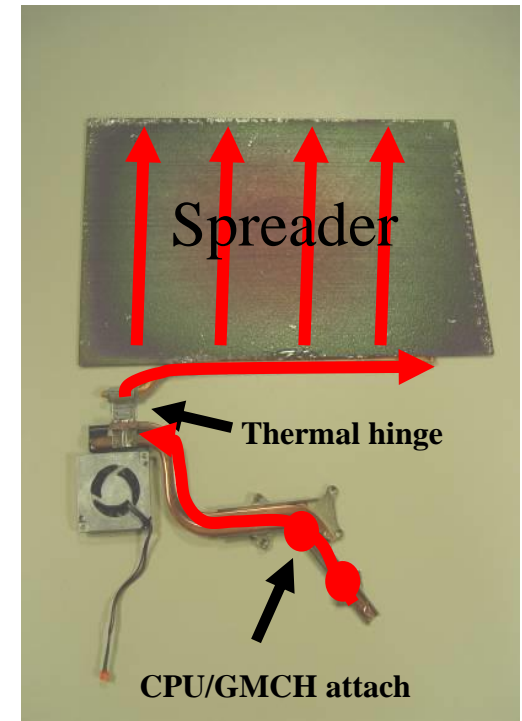
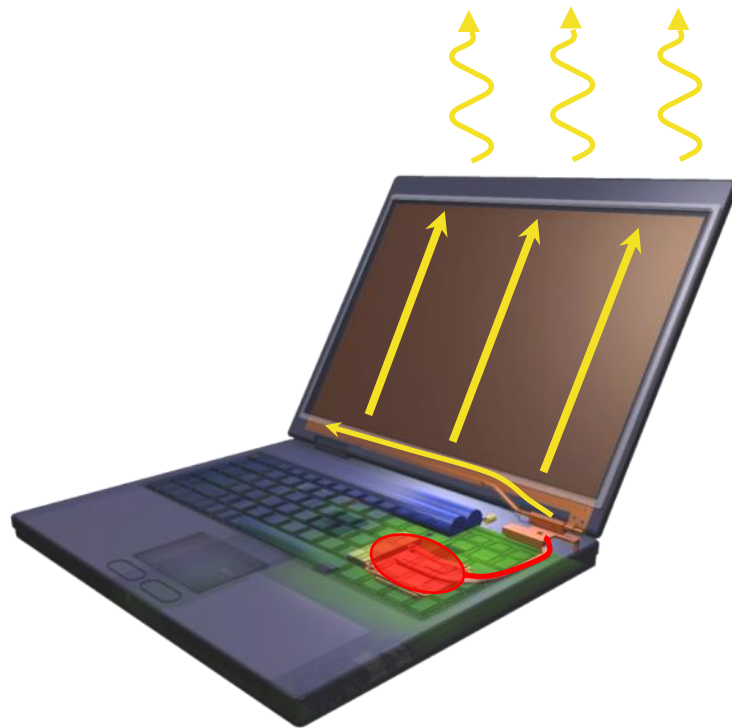


Increasing  $h$



Increasing  $A$

# Extended surface: an example

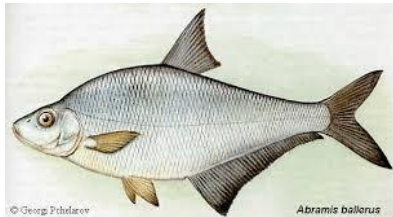


## Lid Cooling in laptop computers

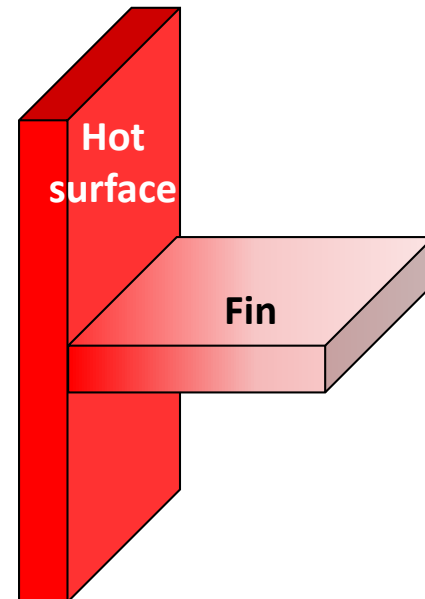
- Laptop display area (lid) used for cooling
- 7-15W of additional cooling achievable

# Fins as extended surfaces

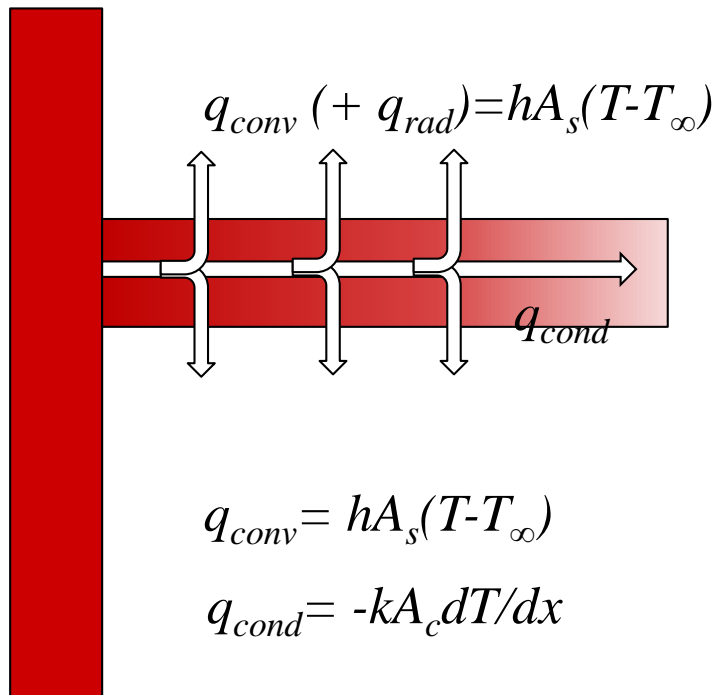
A **fin** is a thin component or appendage attached to a larger body or structure



In the context of heat transfer also, these are components protruding out of a heated (or cold) surface

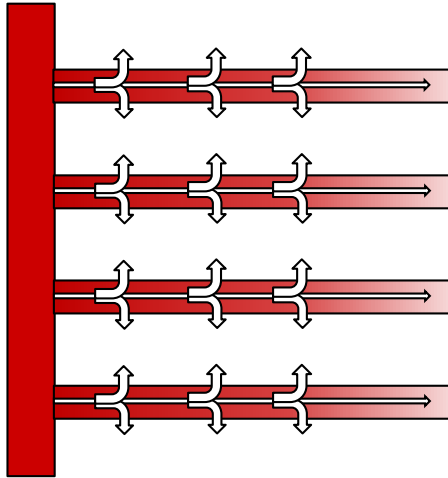


# What happens in a fin?



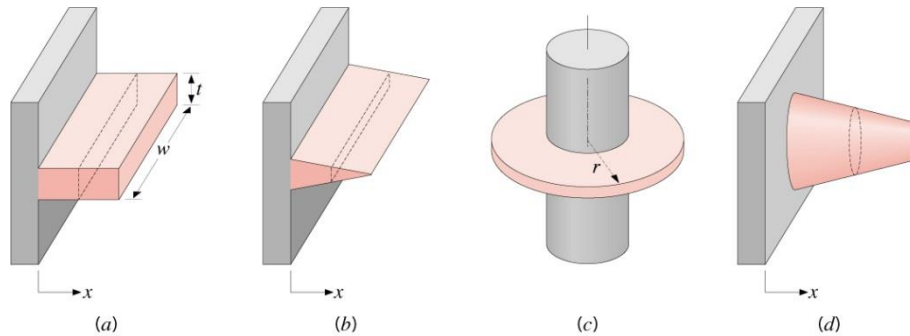
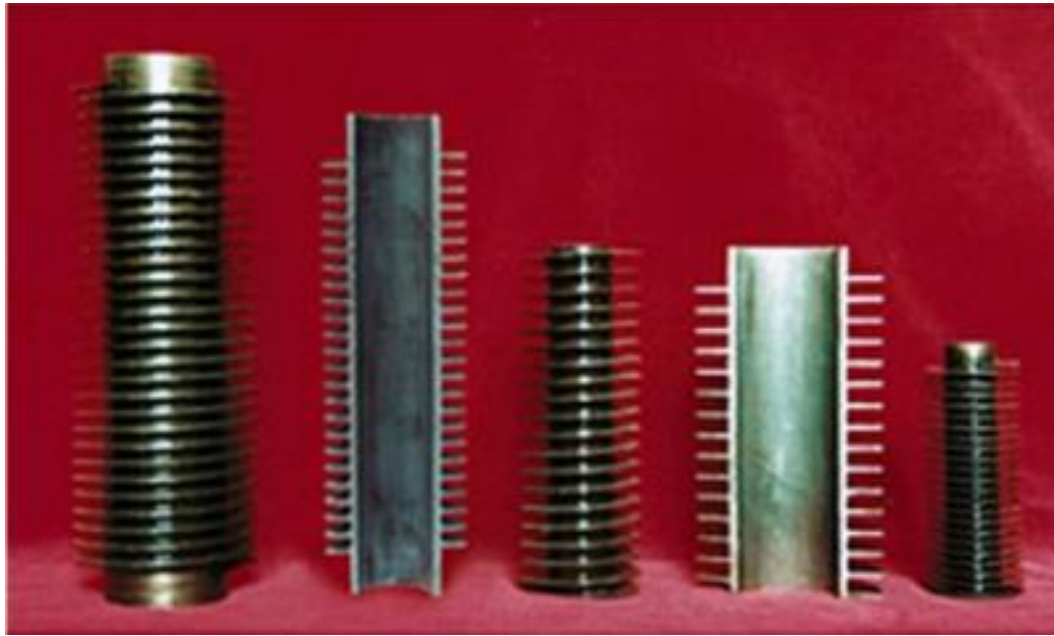
An extended surface (**combined conduction-convection system**) is a solid within which **heat transfer by conduction is assumed** to be **one dimensional**, while heat is also transferred by **convection (and/or radiation)** from the surface in a direction transverse to that of conduction.

# What happens in a fin?



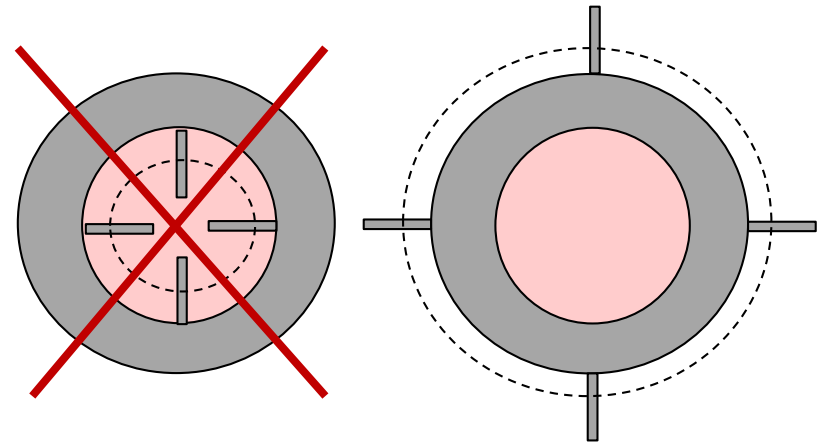
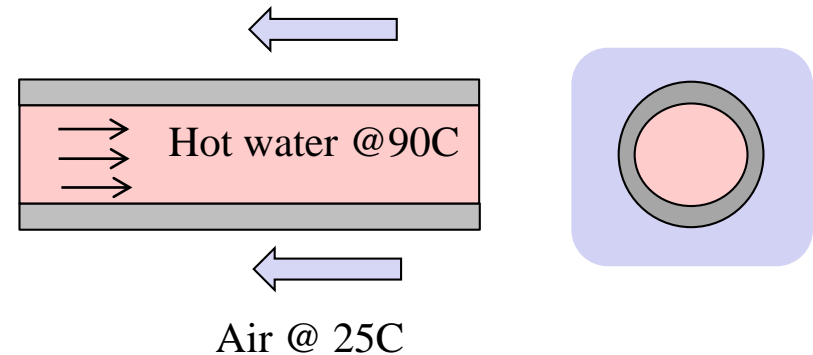
An extended surface (**combined conduction-convection system**) is a solid within which **heat transfer by conduction is assumed** to be **one dimensional**, while heat is also transferred by **convection (and/or radiation)** from the surface in a direction transverse to that of conduction.

# Examples of Fins



# Question time

- Heat is transferred from hot water flowing inside a tube to cooling air flowing over the tube. To enhance heat transfer rate, **which side** should the **fins** be installed?
- Fins are most **beneficial** where  **$h$  is low**
- Fin ***dimensions*** and  **$k$**  are **critical** design parameters



*Liquid side*

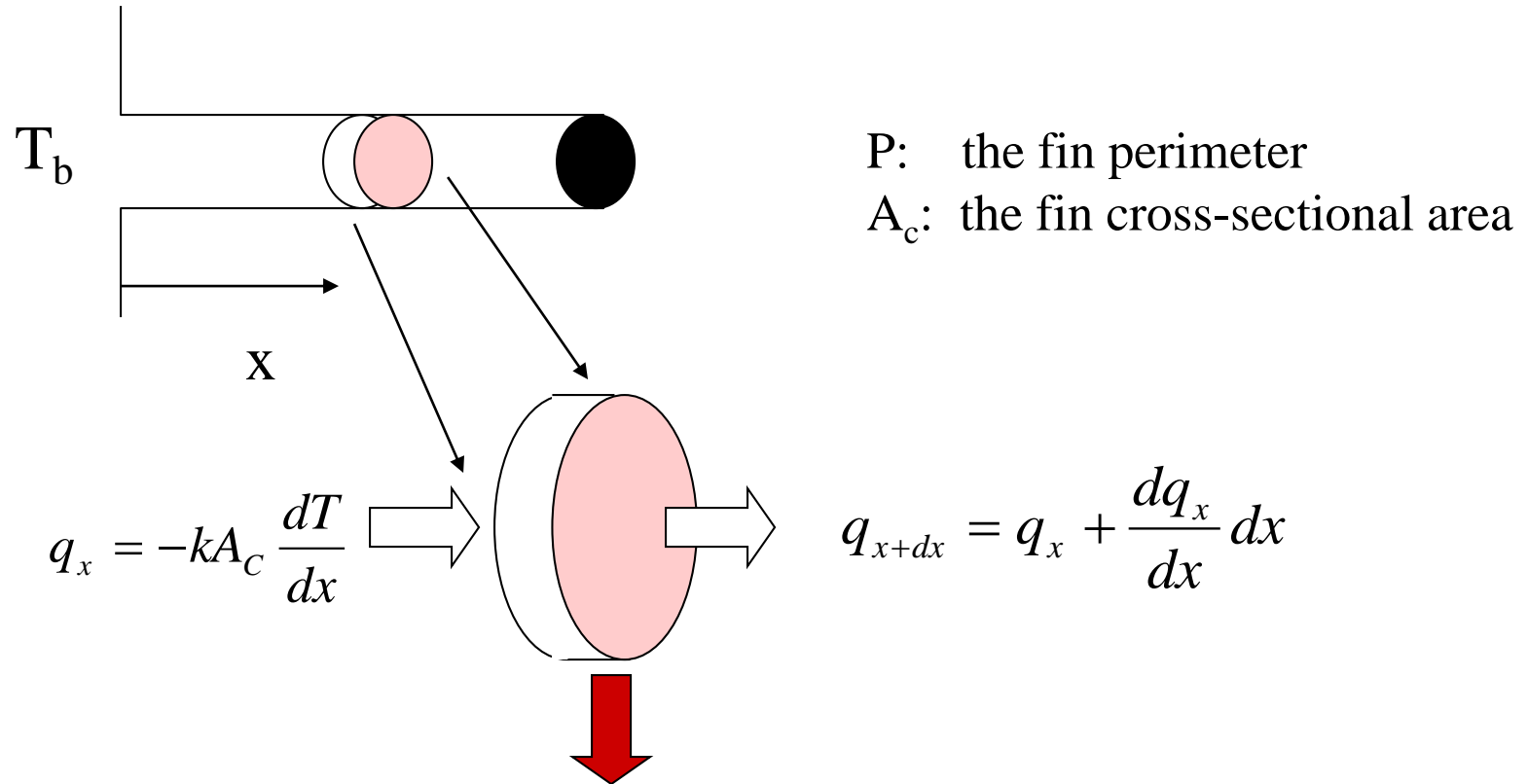
*Air side*



# Summary

- Extended surfaces help in enhancing heat dissipation
  - Increases surface area for heat exchange
- Fins: most common embodiment of extended surface
  - Can be of varied shape and forms
- Fin performance =  $f(h, \text{material}, \text{size})$

# Fin Analysis



$dq_{conv} = h(dA_s)(T - T_\infty)$ , where  $dA_s$  is the surface area of the element

Energy balance:  $q_x = q_{x+dx} + dq_{conv} = q_x + \frac{dq_x}{dx} dx + hPdx(T - T_\infty)$

# Fin Analysis (cont.)

$$\frac{d}{dx} \left( k A_c \frac{dT}{dx} \right) - hP(T - T_\infty) = 0 \quad A_c = A_c(x)$$

$$\theta = T - T_\infty \rightarrow \frac{d}{dx} \left( A_c \frac{d\theta}{dx} \right) - \frac{hP}{k} \theta = 0$$

For a constant cross-section  $A_c$

$$\frac{d^2\theta}{dx^2} - m^2\theta = 0, \quad m^2 = \frac{hP}{kA_c} \quad \longrightarrow \quad \boxed{\theta(x) = C_1 e^{mx} + C_2 e^{-mx}}$$

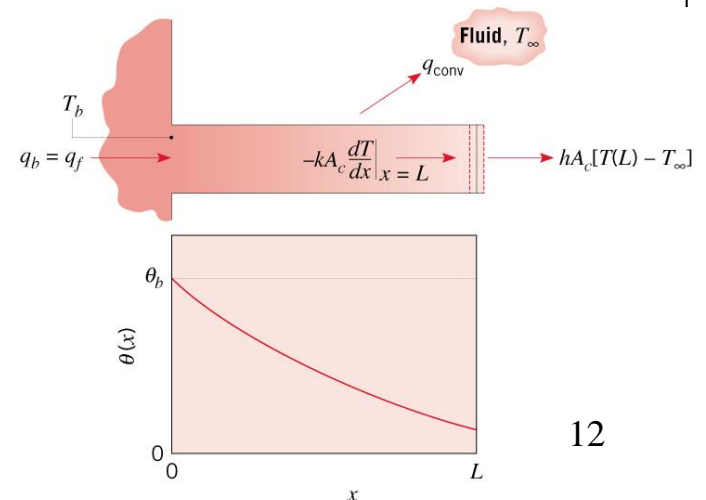
Need two boundary conditions  $\left\{ \begin{array}{l} \rightarrow \text{Base: } \theta = \theta_b \text{ at } x = 0 \\ \rightarrow \text{Tip: 4 scenarios at } x = L \end{array} \right.$

# Temperature profiles

Case	Tip Condition	Temp. Distribution	Fin heat transfer
A	Convection heat transfer: $h\theta(L) = -k(d\theta/dx)_{x=L}$	$\frac{\cosh m(L-x) + (h/mk) \sinh m(L-x)}{\cosh mL + (h/mk) \sinh mL}$	$M\theta_b \frac{\sinh mL + (h/mk) \cosh mL}{\cosh mL + (h/mk) \sinh mL}$
B	Adiabatic $(d\theta/dx)_{x=L} = 0$	$\frac{\cosh m(L-x)}{\cosh mL}$	$M\theta_b \tanh mL$
C	Given temperature: $\theta(L) = \theta_L$	$\frac{(\theta_L/\theta_b) \sinh m(L-x) + \sinh m(L-x)}{\sinh mL}$	$M\theta_b \frac{(\cosh mL - \theta_L/\theta_b)}{\sinh mL}$
D	Infinitely long fin $\theta(L) = 0$	$e^{-mx}$	$M\theta_b$

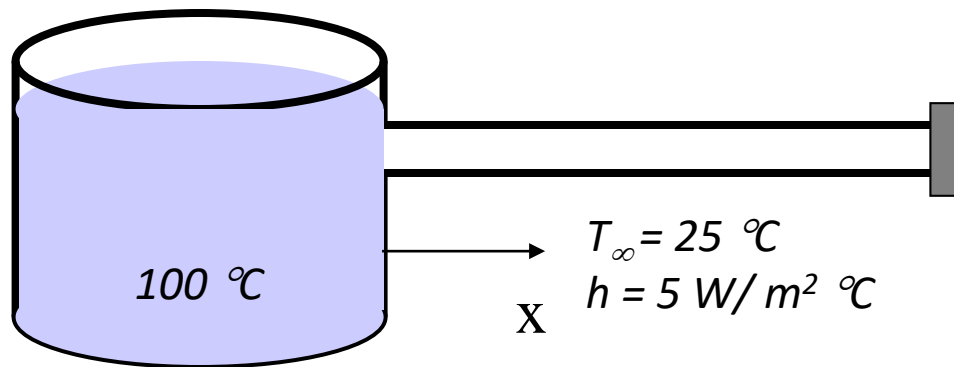
$$\theta \equiv T - T_{\infty}, \quad m^2 \equiv \frac{hP}{kA_c}$$

$$\theta_b = \theta(0) = T_b - T_{\infty}, \quad M = \sqrt{hPkA_c} \theta_b$$



# Example Problem

An Aluminum pot is used to boil water as shown below. The handle of the pot is *20-cm long, 3-cm wide, and 0.5-cm thick*. The pot is exposed to *room air at 25°C*, and the convection coefficient is *5 W/m<sup>2</sup>-K*. Assume no heat transfer at the end of the handle. Question: can you touch the handle when the water is boiling? (*k for Al = 237 W/m-K*)

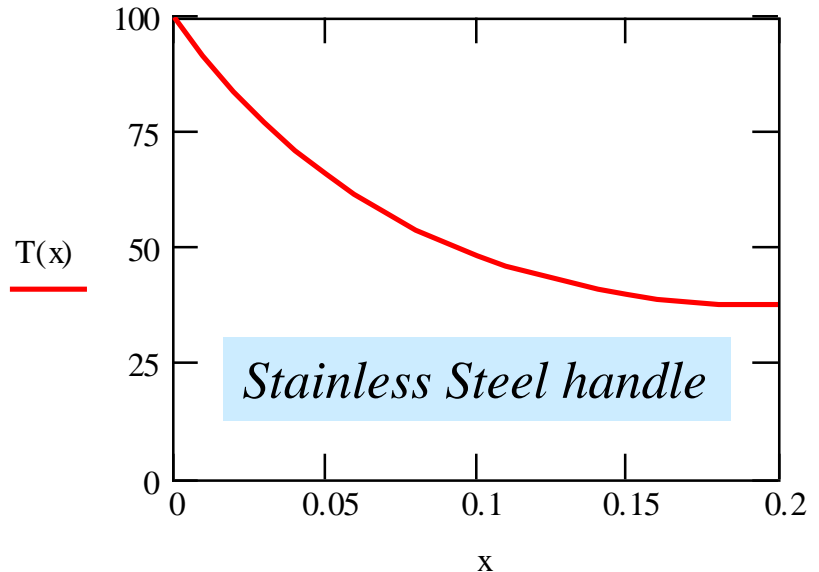
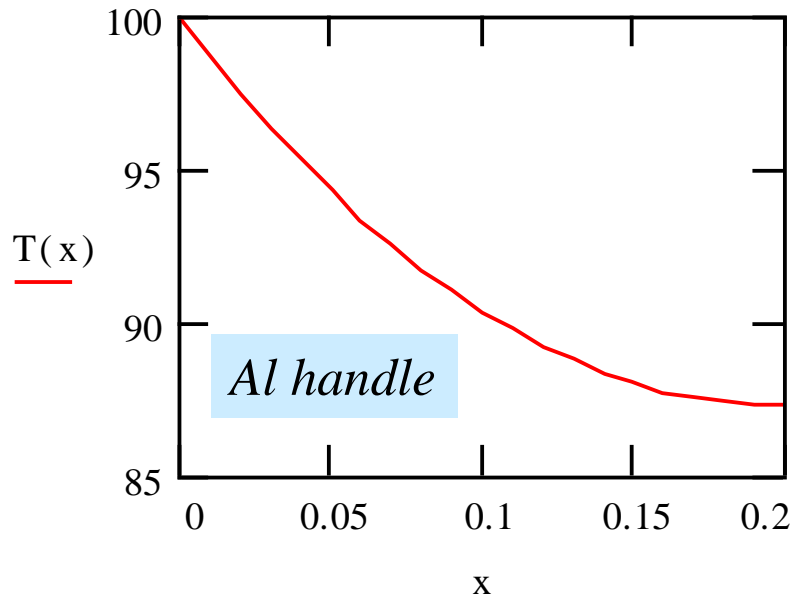


## Steps

- Treat handle as fin
- Identify tip condition
  - *Adiabatic*
- Calculate P, m, M
- Get temp. profile
- Calculate T at  $x=L=20\text{ cm}$

# Example (contd...)

Temperature distribution along the pot handle



Temperature at the tip = **87.3 °C** → **Not safe** to touch

Why?

What can you do?

# Fin parameters: Effectiveness ( $\varepsilon_f$ )

**Fin effectiveness ( $\varepsilon_f$ ):** how effective is the fin

- *Ratio of heat transferred in presence of fin to in its absence*

$$\varepsilon_f \equiv \frac{q_f}{hA_{c,b}\theta_b}$$

→

>1 → fin is effective

<1 → should not include fin

$\varepsilon_f \uparrow$  with  $\downarrow h, \uparrow k$  and  $\downarrow A_c / P$

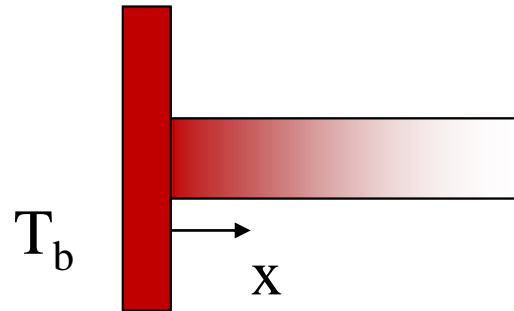
*Remember we wanted fins on the air side!!*

# Fin parameters: Efficiency ( $\eta_f$ )

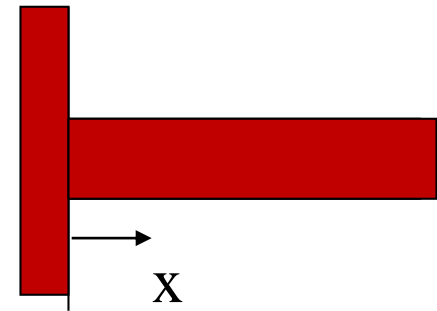
**Fin efficiency ( $\eta_f$ ):** how close to ideal scenario is the fin

- *Ratio of heat transferred to that if entire fin were at base temp*

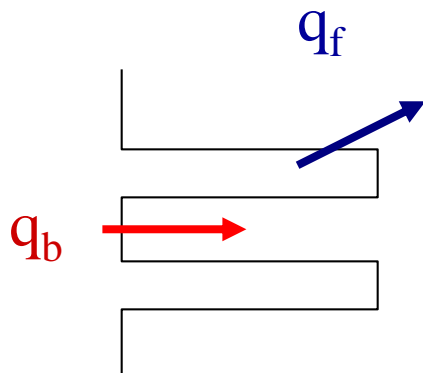
$$\eta_f \equiv \frac{q_f}{q_{f,\max}} = \frac{q_f}{hA_f\theta_b}$$



Real situation



Ideal situation



For a **fin array** with  $N$  *fins*,

$A_B$ : total base area

$A_b, A_t$ : base and tip area of fin

$A_f$ : surface area of a single fin (excluding tip)

$$q_{tot,array} = h(A_s - NA_b + N\eta_f(A_f + A_t))\theta_b$$



# Fin array in heat sinks



Parallel fins



Radial fins



Pin fins

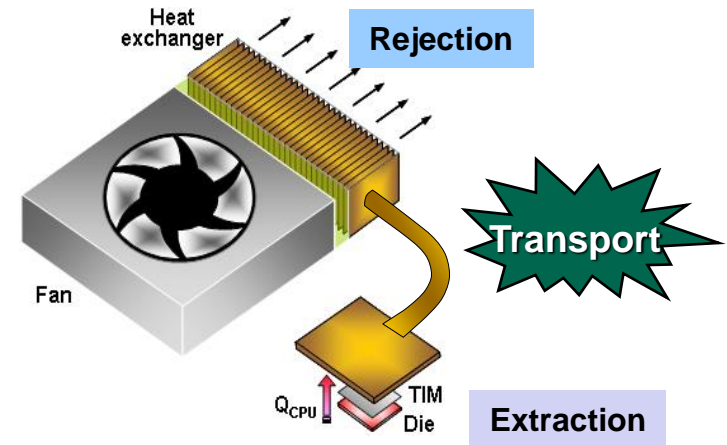
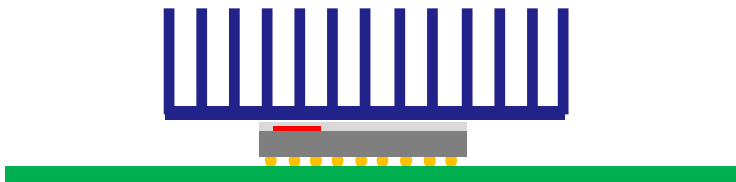


Circular heat sink

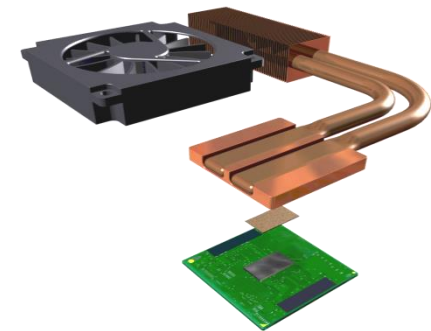


Dovetail fins

# Fins in computing products



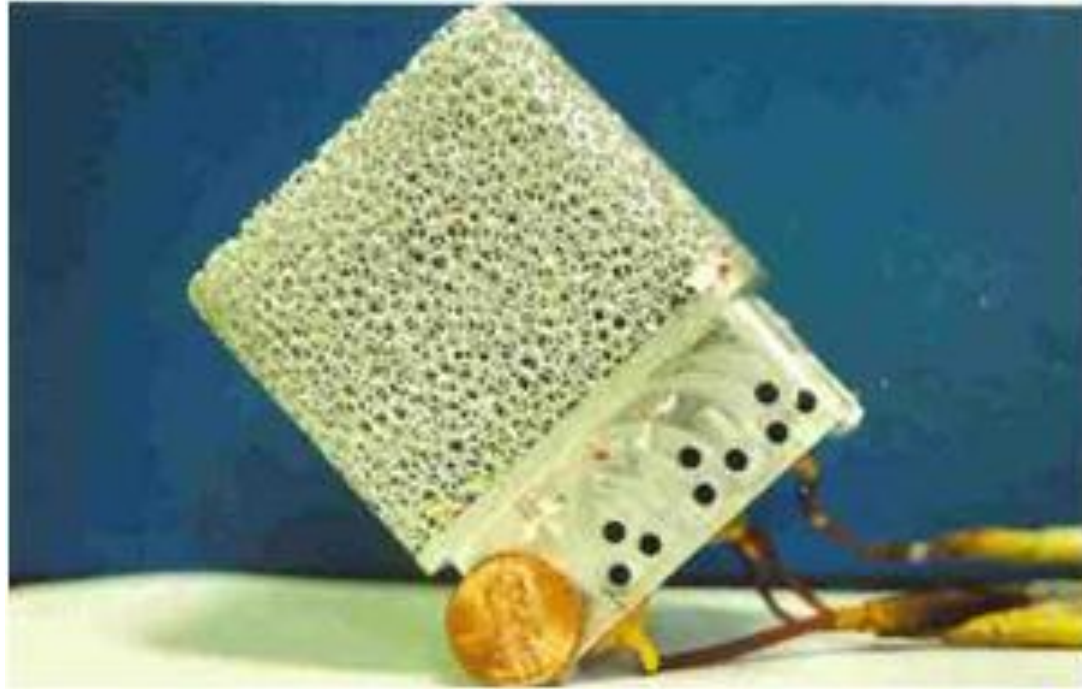
Desktop Computer



Laptop Computer

# Summary

- Solved ODE for 1-D heat conduction to get temp profile
  - 4 different tip conditions
- Fin performance metrics – Effectiveness ( $\varepsilon_f$ ) & Efficiency ( $\eta_f$ )
- Fin arrays used to design heat sinks
  - Commonly used in computing products



**Thank you!!**