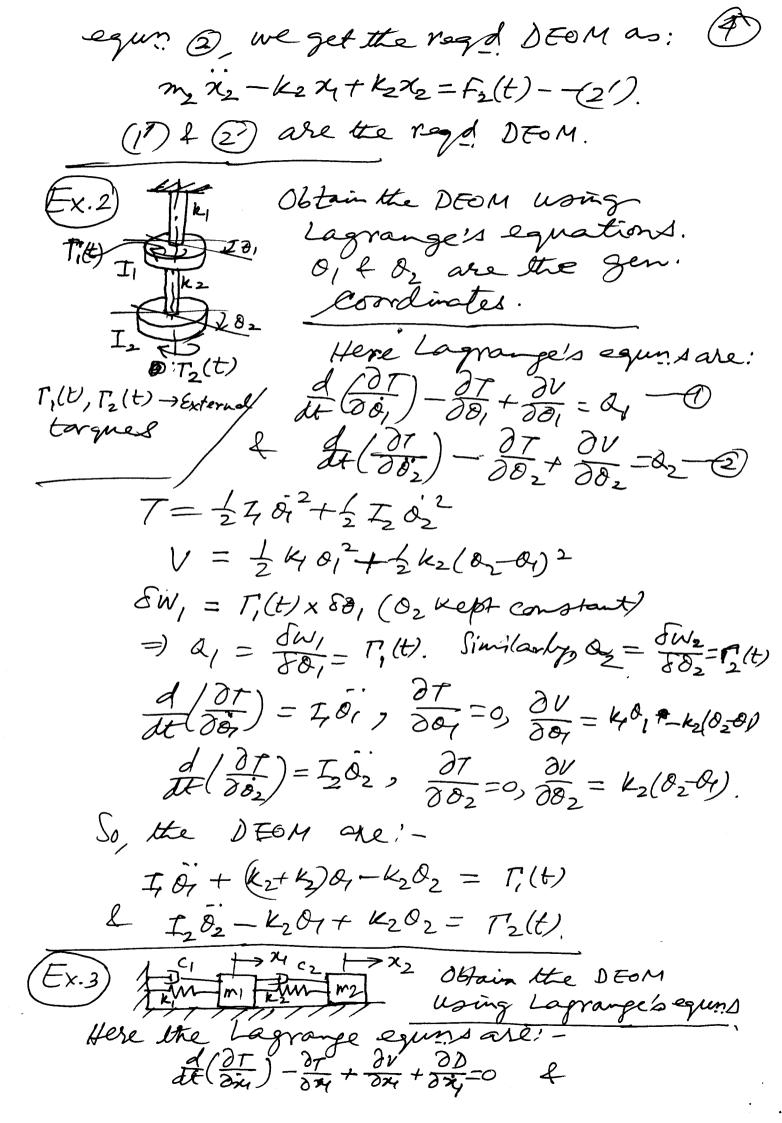
(3) Lagrangés Equations (The Lagrange equations of the 2nd kind) for a holonomic dynamic system having n degrees-of-freedom, there are n number of Lagrange's equations. These are usually written as: $\frac{\partial}{\partial t} = \frac{\partial}{\partial t} \left(\frac{\partial \tau}{\partial \dot{q}_{i}} \right) - \frac{\partial}{\partial \dot{q}_{i}} + \frac{\partial}{\partial \dot{q}_{i}} + \frac{\partial}{\partial \dot{q}_{i}} + \frac{\partial}{\partial \dot{q}_{i}} = Q_{i} ; j=1,2,\dots,n.$ Remember q_{i} %, v2, --, vn are the n generalized coordinates used to describe the system configuration at any instant of time. 9; = dy is the jtt. generalized velocity. $(v_1 = a_1(t), a_2 = a_2(t) \text{ etc. Similarly, } a_1 = a_1(t) \text{ etc.})$ T = System Kinetic energy D = The Rayleigh dissipation function V = System potential energy Qj = Generalized force corresponding to the generalized coordinate vj. To arrive at the Lagrange's equations U, one starts with the general Egnation of dynamics (See Ands Tectures in Analytical Mechanics by F. Gantmacker) Which is also called generalized D'Alembert's principle. We are not going for the der derivations of equations (2) at this moment. We shall illustrate the use of 1) through several examples. (Single DOF cases have been to already takenup) Obtain the DEOM voing Lagrangers equations. F(4) / = k2 24 Here we have a 2-Dof system. $x_1(t)$ & $x_2(t)$ are the generalized coordinates. The 2 Lagrange's equisare: $\frac{d}{dt}\left(\frac{\partial T}{\partial \dot{u}}\right) - \frac{\partial T}{\partial \dot{u}} + \frac{\partial V}{\partial \dot{u}} = 2, \quad 0$ $4 \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_0} \right) - \frac{\partial T}{\partial x_2} + \frac{\partial V}{\partial x_2} = \alpha_2 - 2$ Since D = 0 (no viscous domping). ** Contdon page 3. / Note: - The Lagrangian function, is defined as: L=T-V. Since V instres conserative forces only which are independent of geheralized velocities, $\frac{\partial V}{\partial \dot{z}_i} = 0$ \$ $\frac{\partial V}{\partial \dot{x}_{s}} = 0$. Then, $\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_{t}} \right) = \frac{d}{dt} \left(\frac{\partial (T-v)}{\partial \dot{x}_{t}} \right) = \frac{d}{dt} \frac{\partial L}{\partial \dot{x}_{t}}$, $\frac{d}{dt}\left(\frac{\partial T}{\partial \dot{x}_2}\right) = \frac{d}{dt}\left(\frac{\partial L}{\partial \dot{x}_2}\right)'' + \frac{\partial T}{\partial v_j} + \frac{\partial v}{\partial v_j} = -\frac{\partial}{\partial v_j}(T - v)$ = - OL for j=1,2. Then Of & 2 Can be written as: $\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{x}_{i}}\right) - \frac{\partial L}{\partial x_{i}} = Q_{i}$ 4 dt (2/2) - 2/2 = 02

Thus, for free vibrations of above system, the Lagrange equis can be written as: $\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{x}_{i}}\right) - \frac{\partial L}{\partial \dot{x}_{i}} = 0$ $\frac{1}{\sqrt{2}} \int_{0}^{1} \frac{\partial L}{\partial z_{2}} dz = 0$ ** Now, T= = mpi/2+ = m2 2, V = 1 K1 x12 + 1 K2 (x2-x1)2. So, $\frac{\partial T}{\partial \dot{x}_{1}} = m_{1}\dot{x}_{1} \Rightarrow \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_{1}}\right) = m_{1}\dot{x}_{1} - 2$ $\frac{\partial T}{\partial x_{2}} = 0, \frac{\partial V}{\partial x_{1}} = \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_{1}}\right) = m_{1}\dot{x}_{1} - 2$ To Obtain Q1, = (K1th2)xy-kexe-(3) the generalized force associated with generalized coordinate & x:-Here we keep x2 fixed, give x4 a virtual variation of 5x4 4 compute the virtual work Swy done by Fi(t). For may then, $Q_1 = \frac{8Wx_1}{8Xy}$, by definition. as $8W_1$, also So, here $8W_{x_1} = F_1(t) 8xy 4Q_1 = \frac{8W_2}{8x_4} = F_1(t)$. Putting (2), (3), (2) & (4) in (1), we get the DEOM of m, as: min + (ktk2)x1-k2n2=F,(t)--(1) \rightarrow Again, $d(\frac{\partial T}{\partial \dot{x}_1}) = m_2 \dot{x}_2$, $\frac{\partial T}{\partial x_2} = 0$, $\frac{\partial V}{\partial x_2} = k(x_2 x_1)$. Virtual dipl= δn_2 , $\delta w_{n_2} = \delta w_2 = F_2(t) \cdot \delta x_2 \, d$ so, 2 = 3W2 = F2(t). Butting all this in



 $\frac{d}{dt}\left(\frac{\partial I}{\partial \dot{x}_1}\right) - \frac{\partial I}{\partial x_2} + \frac{\partial V}{\partial x_2} + \frac{\partial D}{\partial \dot{x}_2} = 0$ (Damped free- Ubration) T= = = 1 m 2 + 1 m 2 12 $V = \frac{1}{2} K_1 x_1^2 + \frac{1}{2} K_2 (x_2 - x_1)^2$ D=2(22-24)2 Then, $\frac{\partial D}{\partial \dot{x}_1} = G\dot{x}_1 - G_2(\dot{x}_2 - \dot{x}_1) = G + G_2\dot{x}_2 - G_2\dot{x}_2$ $+\frac{\partial D}{\partial \dot{x}_0} = c_2(\dot{x}_2 - \dot{x}_1) = -c_2\dot{x}_1 + c_2\dot{x}_2$ Other teams are as in Ex. 1. The negd DEOM are: my xi + (4+62) x4-(2x2+(k+k2)x4-k2x2=0 & mexie - gir + Ceiz - kzx1+kzx2 = 0 Hinge

Rigid bar of negligible

mass

The pendulum

2 or DEOM The block translates 4 the pendulum Oficillates. Obtain the nonlinear DEOM using Lagrange's equations. A horizontal force F(t) acts on the bob. Solution: Let x(t) & Olt) be the generalized Coordinates (This is a 2-DOF supplem). O, is measured from the vertical, the CCW.

The Lagrange equations here are: 6 $\frac{d(\frac{\partial T}{\partial \dot{x}}) - \frac{\partial T}{\partial x} + \frac{\partial V}{\partial x} = Q_1 - Q$ $4 \frac{4}{3\pi} \left(\frac{\partial T}{\partial \dot{a}} \right) \sqrt{\frac{\partial T}{\partial a}} - \frac{\partial T}{\partial a} + \frac{\partial V}{\partial a} = a_2 - 2$ ACC T= = 1 mx + 1 mv2 where V=velocity of 60% w.r.t.
ground reference. V canbe obtained in severalways. One of the ways is shown above. Then, $v^2 = \dot{x}^2 + (l\dot{o})^2 + 2\dot{x}l\dot{o} \cos\theta$ [You can also use $\overline{V_B} = \overline{V_A} + \overline{W_{AB}} \times \overline{AB}$ where $V_A = \dot{\chi} i$, $\overline{\omega}_A = A O R$, $AB = U \times mo / n + mu.$ $AB = U \times mo / n + mu.$ $X \quad You can also find <math>V = |V_B|as$ $follows: - V_B = 2igi + yji$ $(2y) \frac{3}{8}(x+15ind), lcosd) \quad When \quad X_B = x+15ind$ $So, \quad V = |V_B|^2 = x_B^2 + y_B^2 \text{ et c.}$ $So, \quad V = |V_B|^2 = x_B^2 + y_B^2 \text{ et c.}$ Thus, T= Than + Toob = 1 Mi2+ 1m[x2+10+21x0 Coxo] $V = \frac{1}{2}Kx^2 + mgl(1-coso)$ Thus, $\frac{\partial T}{\partial \dot{x}} = M \dot{x} + \frac{1}{2}m[Z\dot{x} + Zlo Coro]$ $4 \frac{d}{dt} \left(\frac{\partial \tau}{\partial \dot{x}} \right) = M \dot{x} + m \left[\dot{x} + Lo Cord - Lo Sino \right]$

De careful while differentsating. Note that the generalized to coordinates & gen. velocities are all independent of each other at this stage of obtaining the DEOM) (It (coro) = Id (coro). do = - i sind) $\frac{d}{dt}\left(\frac{\partial T}{\partial \dot{x}}\right) = (M+m)\dot{x} + mlocool-mlosino$ $\rightarrow \frac{\partial T}{\partial x} = 0, \quad \frac{\partial V}{\partial x} = kx$ $\frac{\partial T}{\partial \dot{a}} = \frac{1}{2} m \left[2 l^2 \dot{a} + 2 l \dot{x} cos \delta \right]$ $\Rightarrow \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{n}} \right) = m \left[\ell^2 \ddot{0} + \ell \ddot{x} \cos \theta - \ell \dot{x} \dot{0} \sin \theta \right]$ Now comes the interesting term. Till now, the derivatives $\frac{\partial T}{\partial x}$, $\frac{\partial T}{\partial x_1}$, $\frac{\partial T}{\partial x_2}$, $\frac{\partial T}{\partial x_3}$ used to be zero. Here it is not so, note. This is because T is a function of o (a, coro) $\rightarrow \frac{\partial T}{\partial \theta} = \frac{1}{2} m \left[\frac{\partial}{\partial \theta} (21 \dot{x} \dot{\theta} \cos \theta) \right] = -m \dot{x} \dot{\theta} \sin \theta$ $\rightarrow \frac{\partial V}{\partial \theta} = mgl \sin \theta$ Now to Abtain a, & Q2. for Obtaining by, o is to be kept constant. The block is given a virtual displacement ox. Then, Sw= F(t) 8x & so, & = & wa F(t). For (Note that while the block undergoes the Virtual displacement, the bar of the pendulum moves & the bob also undergoes a displacement 8x & hence, F(t) does virtual work = F(t) 8x.

Have you noticed we take the force to remain constant at F(t) while on is given? This is so because time Congeals', that is remains unchanged While the virtual displacement is given. This is a little deep & you need to study Analytical Expression Mechanics a bit to properly understand it! To get Qz, keep x und unchanged, ie. the block remains fixed at location X and O is changed by 80 (see zig.)

[Actually 8x, 80 are infinitesimals.]

80,180 Exaggerated for clarity SO 180

Note that due to the virtual displacement SO, F(t) moves an amount lisocord in the Lorizontal displacement Alirection. Hence, SWO = F(t) x 1Cool 80 $\beta'o)$ $Q_2 = \frac{\delta Wo}{\delta \delta} = F(t)/(cos \delta)$. Thus, Q2 is not a force but the moment of a force. Hence, the name "generalized force. I We now have Stained everything needed to get the DEOM. Substitutions in 1 gives: Substitutions m (M+m) $\ddot{x}+ml$ \ddot{o} Cos0-ml \ddot{o} \ddot{s} \ddot{o} $d+kx=F(t)-\ddot{a}$ 4 (2) gives: $ml^2\ddot{o}+ml$ \ddot{x} Cos0-ml \ddot{x} \ddot{o} \ddot{s} \ddot{o} d+ml \ddot{s} \ddot{o} \ddot{s} \ddot{o} d+ml \ddot{s} \ddot{o} \ddot{s} \ddot{o} d+ml \ddot{s} \ddot{o} \ddot

DEOM and there is no way you canget a closed form analytical solution for these. The can, however, linewize these DEOM. However, to linearize, only Coro = 1 & Sind = 0 (for small 0) won't do! Because, substitution of Caso=1 & fino=0 in @ & B gives: (M+m) x + mlo - mlo 0+kn=f(t)-0 $ml^2 \dot{\theta} + ml \dot{n} + mgl\theta = f(t)l - (d)$ Although dis linear, C) is not due to the term -who 20. Hence we must additionally assume that o'd is negligible 4 this seems a bit strange, ion't it? So, the final linearized equation of motion are: $(4+m)\ddot{x} + ml\ddot{o} + kn = F(t)$ Check everything

(e)...- ml $\ddot{x} + ml^2\dot{o} + mglo = F(t)l$ (everything) OR [M+m) ml] (x) + [k 0] (x) {F(t)}

or my [of = [F(t)] 4 note that the inertia matrix is symmetric but non-diagonal but the stiffness matrix is diagonal (4 automatically symmetric). These linearized equis

can be solved as before for free (10) vibration l'esponse.

) A WORD OF CAUTION

See DEOM @, pg.9:

You might be tempted to

reduce this to:

DONOT do o this, because,
although mathematically it seems
or, doing this would destroy
the symmetric nature of the mass
matrix & pose some analysis problem
matrix & pose some analysis problem
subsequently. Also, doing so will
outsequently. Also, doing so will
otherate the nature of excitation free
(it is the moment of a force) corresponding
to gen. Coordinate o.

We have spent about 5 pages
to do this problem. This is because
quite few explanations were in order.
You should not take more than 2 pages
to complete it.

Example-5: This example will illustrate how a new set of generalized Coordinates result in a non-diagonal mass matrix.

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