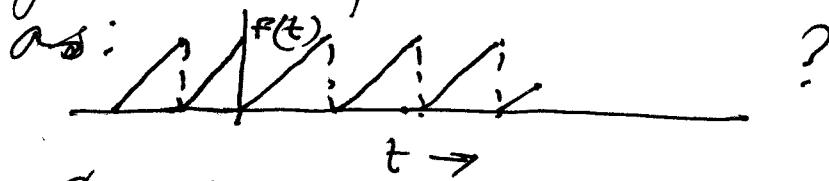


### ⑤ Periodic excitations:-

→ What happens <sup>to the forced response</sup> when we have a general periodic excitation such



Could we use our earlier experience with the special periodic excitation  $F_0 \sin \omega_f t$ ? The answer is: Yes, we could. Here two things come into play, the Fourier series and the principle of superposition and I guess you know about both. Still, we shall recapitulate for the sake of those who might have forgotten!

① The Fourier series:- for a general periodic function  $f(t)$  of period  $\tau$ ,  $f(t)$  can be represented by a Fourier series:

$$f(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} (a_n \cos n\omega_f t + b_n \sin n\omega_f t)$$

where  $a_n = \frac{2}{\tau} \int_0^{\tau} f(t) \cos n\omega_f t \, dt; n=0, 1, 2, \dots$  note

$$\& b_n = \frac{2}{\tau} \int_0^{\tau} f(t) \sin(n\omega_f t) \, dt;$$

$$n = 1, 2, 3, \dots$$

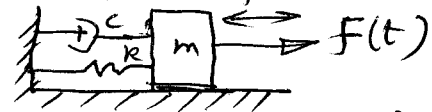
Of course, the function  $f(t)$  has to satisfy a few conditions known as the Dirichlet conditions (check).

(2)

from Engg. Maths books or the book 'Fourier Series & Integrals' by Carslaw ~~(1930)~~. Our engineering forcing period functions never fail to satisfy these conditions and hence we may proceed without further deliberations on this point.

You should note the relationship between  $\tau$  &  $\omega_f$ . Actually,  $\tau = \frac{2\pi}{\omega_f}$  or  $\omega_f = \frac{2\pi}{\tau}$ .

Hence, to obtain the forced response of the Kelvin-Voigt model



when  $F(t+\tau) = F(t)$ , i.e.,  $F(t)$  is periodic with period  $\tau$ , we write

(i) the response due to the constant term  $\frac{a_0}{2}$ , which will be  $\frac{a_0}{2k}$  only,

(ii) the response due to a general forcing term  $a_n \cos n\omega_f t$  by comparison with the response due to  $F_0 \cos \omega_f t$ ,

(iii) the response due to a general forcing term  $b_n \sin n\omega_f t$ , once again comparing with the response due to  $F_0 \sin \omega_f t$  and then finally, we add up all these responses (valid due to the principle of superposition) to get the required forced response.

(3)

## ② The principle of superposition:-

Our ~~diff~~ DEOM  $m\ddot{x} + c\dot{x} + kx = F(t)$  is a linear DEOM and hence, if it has the forced response  $x_1(t)$  with forcing function  $F_1(t)$  and response  $x_2(t)$  when the forcing function is  $F_2(t)$ , then,

When the forcing function  $c_1 F_1(t) + c_2 F_2(t)$  acts, the response will simply be  $c_1 x_1 + c_2 x_2$ . This can be shown pretty easily: ( $c_1, c_2$  are constants)  
We have,

$$\left. \begin{aligned} m\ddot{x}_1 + c\dot{x}_1 + kx_1 &= F_1(t) \\ m\ddot{x}_2 + c\dot{x}_2 + kx_2 &= F_2(t) \end{aligned} \right\}$$

$$\text{So, } m(c_1\ddot{x}_1) + c(c_1\dot{x}_1) + k(c_1x_1) = c_1 F_1(t)$$

$$\& m(c_2\ddot{x}_2) + c(c_2\dot{x}_2) + k(c_2x_2) = c_2 F_2(t)$$

Adding these, we get

$$\begin{aligned} m(c_1\ddot{x}_1 + c_2\ddot{x}_2) + c(c_1\dot{x}_1 + c_2\dot{x}_2) + k(c_1x_1 + c_2x_2) \\ = c_1 F_1 + c_2 F_2 \end{aligned}$$

$$\text{or, } m\ddot{x}_3 + c\dot{x}_3 + kx_3 = F_3$$

with  $x_3 = c_1 x_1 + c_2 x_2$  as the particular integral (response, forced)

due to forcing function  $F_3 = c_1 F_1 + c_2 F_2$ .

This is true even when  $F(t) = \sum_{i=1}^n c_i F_i(t)$ ,  $n$  being any positive integer, the response would simply be

$$x(t) = \sum_{i=1}^n c_i x_i(t) \text{ where } x_i(t) \text{ is}$$

the response due to  $F_i(t)$  ( $i=1, 2, \dots, n$ ). ④

→ Let us now sum things up:-

(i) When  $F(t) = \frac{a_0}{2}$ , the response is, ~~is~~,  $\frac{a_0}{2k}$  (by simple observation)

(ii) When  $F(t) = a_n \cos n\omega_f t$ , the response

Compare with  $\frac{F_0/k}{\sqrt{(1-r^2)^2 + (2\zeta r)^2}} \sin(\omega_f t - \psi)$  is:

$$\frac{a_n/k}{\sqrt{(1-r^2)^2 + (2\zeta r)^2}} \cos(n\omega_f t - \psi_n)$$

where  $r = \frac{n\omega_f}{\omega_n}$  & hence, we represent it as  $r_n = \frac{n\omega_f}{\omega_n}$  for convenience, since a simple  $r$  won't do. Similarly,  $\psi = \psi_n = \tan^{-1}\left(\frac{2\zeta r_n}{1-r_n^2}\right)$

So, for  $F(t) = a_n \cos n\omega_f t$ , the response is:

$$\frac{a_n/k}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \cos(n\omega_f t - \psi_n)$$

(iii) When  $F(t) = \sum_{n=1}^{\infty} a_n \cos n\omega_f t$ , the forced response is:

$$\sum_{n=1}^{\infty} \frac{a_n/k}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \cos(n\omega_f t - \psi_n),$$

by the principle of superposition.

(iv) When  $F(t) = \sum_{n=1}^{\infty} b_n \sin n\omega_f t$ , the forced response is, in a similar manner,

$$\sum_{n=1}^{\infty} \frac{b_n/k}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \sin(n\omega_f t - \psi_n).$$

Hence, when the forcing function is

$$F(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} a_n \cos n\omega_f t + \sum_{n=1}^{\infty} b_n \sin n\omega_f t,$$

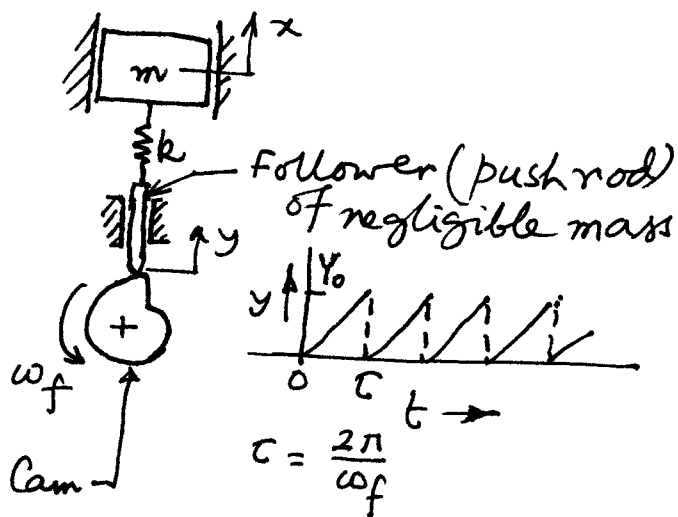
the response is (again applying principle of superposition again);

$$x(t) = \frac{a_0}{2K} + \sum_{n=1}^{\infty} \frac{a_n/K}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \cos(n\omega_f t - \psi_n) + \sum_{n=1}^{\infty} \frac{b_n/K}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \sin(n\omega_f t - \psi_n)$$

$$\text{or, } x(t) = \frac{a_0}{2K} + \frac{1}{K} \sum_{n=1}^{\infty} \frac{1}{\sqrt{(1-r_n^2)^2 + (2\zeta r_n)^2}} \left[ a_n \cos(n\omega_f t - \psi_n) + b_n \sin(n\omega_f t - \psi_n) \right]$$

& you might remember this RHS expression if you feel like!

- An important example! [Also, see Ex. 1.12 (Cam follower mechanism) S.S. Rao, 6th Ed. pg. 73]



← This example could be a simplified system corresponding to a mechanical press, say.

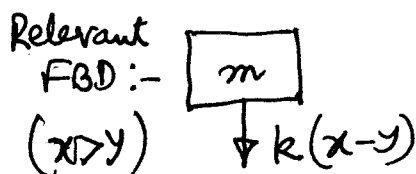
The DEOM is:

$$m\ddot{x} = -k(x-y)$$

$$\text{or, } m\ddot{x} + kx = ky \quad \text{--- (1)}$$

$y$  is periodic with period

$$T = \frac{2\pi}{\omega_f}. \text{ This is an example}$$



⑥

of a periodic base excitation. [See also ex. 1.12, (S Rao 6th Ed, pg. 73) for another practical example of periodic excitation]

$$So, \quad y(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} (a_n \cos n\omega_f t + b_n \sin n\omega_f t) \quad \text{--- (2)}$$

$$a_n = \frac{2}{\tau} \int_0^{\tau} y(t) \cos n\omega_f t dt; \quad n=0,1,2,3,\dots$$

$$b_n = \frac{2}{\tau} \int_0^{\tau} y(t) \sin n\omega_f t dt; \quad n=1,2,3,\dots$$

Note that  $y(t) = \frac{V_0}{\tau} t$  in  $[0, \tau]$ .

Hence,  $a_n = \frac{2}{\tau} \int_0^{\tau} \frac{V_0}{\tau} t \cos n\omega_f t dt$

Home work  $\left\{ \begin{array}{l} \& \text{ use integration by parts} \\ \text{to get } a_n. \end{array} \right.$

Similarly, obtain  $b_n$

Now, the RHS of (1) becomes:

$$\frac{k a_0}{2} + k \sum (a_n \cos n\omega_f t + b_n \sin n\omega_f t).$$

→ SS response (Particular integral) due to  $\frac{k a_0}{2}$  is  $\frac{a_0}{2}$

→ SS response due to  $k a_n \cos n\omega_f t$  is

$$\begin{aligned} & \frac{k a_n / k}{\sqrt{(1-r_n^2)^2 + 2\gamma r_n}} \cos(n\omega_f t - \psi_n) \quad (\psi_n = 0) \\ & = \frac{a_n}{(1-r_n^2)} \cos n\omega_f t \quad (r_n \neq 1) \quad \left\{ r_n = \frac{n\omega_f}{\omega_n} \right\} \end{aligned}$$

→ SS response due to  $k b_n \sin n\omega_f t$  is  $\frac{b_n}{(1-r_n^2)} \sin n\omega_f t$ .

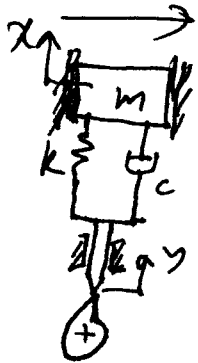
(7)

Hence, the reqd. SS response is:

$$x(t) = \frac{a_0}{2} + \sum \frac{1}{(1-r_n^2)} [a_n \cos n\omega_f t + b_n \sin n\omega_f t] \text{ etc.}$$

HW:- Obtain  $x(t)$  after substituting values of  $a_n$ 's,  $b_n$ 's in above expression.

Do a similar exercise when there is a damper parallel to the spring,  $\gamma$  being the same.

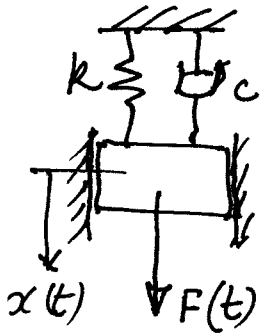


→ It is important to note that in practical computations, we take only first few  $a_n$  &  $b_n$  into account since the values of  $a_n$  &  $b_n$  for higher values of  $n$  become very small.

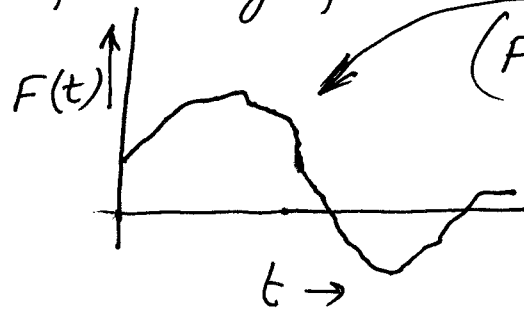
Important:- Do example problem 4.4 (SS Rao, 6th Ed., pg. 414).

Also, study § 4.3 (pg. 418) to see what is to be done when an experimentally obtained periodic excitation cannot be put in an analytical form.

# ⑤ Response to a general excitation



$F(t)$  can now be any general forcing function such as:



( $F(t)$  is applied at  $t=0$  & was zero for  $t < 0$ . This looks more practical)

We are interested in finding the steady-state (forced) response although it would be better to call it a transient response only because except for a few special  $F(t)$ 's, there won't be any 'steady state'.

→ The basic idea is to imagine the forcing function to be made of impulses of short durations. Find the response due to an impulse of this type and then add-up <sup>(superpose)</sup> such responses for all the impulses over the interval  $[0, t]$  to get the response at time  $t$ .

Step 1:- To obtain the response due to a Dirac's delta function or the unit impulse function  $\delta(t)$  :-  $\delta(t)$  is defined as follows:-

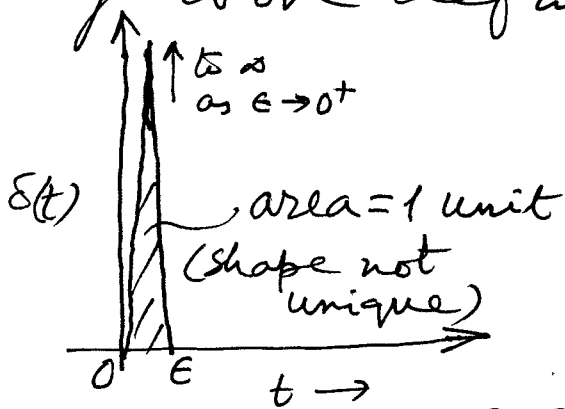


$$\delta(t) = 0 \text{ for } t \neq 0$$

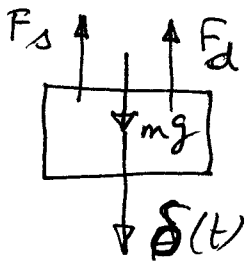
$$\int_0^{\infty} \delta(t) dt = 1$$

$$\int_0^{\infty} \delta(t) f(t) dt = f(0).$$

To visualize  $\delta(t)$ , you can't go strictly by above definition. Assume that  $\delta(t)$  occurs over a interval of time  $[0, \epsilon]$  where  $\epsilon \rightarrow 0^+$ , i.e.  $\epsilon \rightarrow 0$  from above ( $\epsilon > 0$ ) and as  $\epsilon \rightarrow 0^+$ , the maximum value of  $\delta(t) \rightarrow \infty$  such that the area under the  $\delta(t)$  &  $t$  plot  $\rightarrow 1$  unit.



$\rightarrow$  Let us find the response of the system at time  $t = \epsilon$  (as  $\epsilon \rightarrow 0^+$ ).



Since  $\epsilon$  is very small, the impulses  $\int_0^{\epsilon} F_s dt$  &  $\int_0^{\epsilon} F_d dt$  &  $\int_0^{\epsilon} mg dt$  are negligible because  $mg$ ,  $F_s$  &  $F_d$  are finite.

$F_s \rightarrow$  spring force  
 $F_d \rightarrow$  damping force

Impulse of  $\delta(t)$  is  $\int_0^{\epsilon} \delta(t) dt = 1$  as  $\epsilon \rightarrow 0^+$  & is not negligible.

So, we now apply the impulse-momentum theorem to the block in the vertical direction (Let downward direction is positive) to get (change in momentum = force impulse)  
 $mv(\epsilon) - mv(0) = 1$  as  $\epsilon \rightarrow 0$ , i.e.,  $m(v(0^+)) = 1$   
 (since  $v(0) = 0$ )

where  $v(t)$  is the velocity of block.

Thus,  $\boxed{v(0^+) = \frac{1}{m}}$  or,  $(\dot{x}(0^+) = \frac{1}{m})$

→ What is  $x(0^+)$ ? ( $x = \text{displacement of block}$ )

Now, 
$$x(\epsilon) = \int_0^\epsilon v(t) dt \approx \epsilon v(\epsilon_1) \rightarrow 0 \text{ as } \epsilon \rightarrow 0$$
  
by mean value theorem of integral calculus, where

Hence,  $\boxed{x(0^+) = 0}$   $0 < \epsilon_1 < \epsilon$

So, Physically, When a ~~one~~ unit impulse of very short duration is applied to the block at  $t=0$  (say, by a proper blow of a hammer), all it does is causes a velocity  $= \frac{1}{m}$  without any appreciable displacement.

What happens subsequently is just free-vibration with initial conditions  $x(0^+) = 0$  &  $\dot{x}(0^+) = \frac{1}{m}$ .

→ This response for the case of an underdamped system has a special name. It is called the 'impulsive response function' or 'impulse response function' which is denoted by  $g(t)$  in many text books. Let us obtain this  $g(t)$ .

→ For an underdamped system,

$$x(t) = x_0 e^{-\zeta \omega_n t} \sin(\omega_d t + \phi) \quad \text{--- (I)}$$

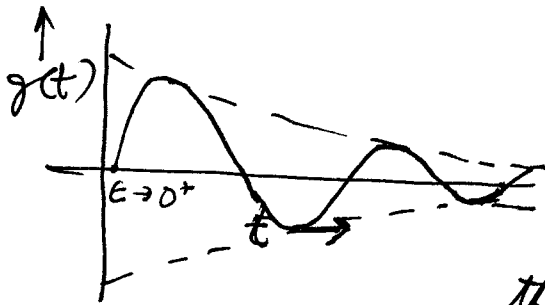
So,  $x(0^+) = 0 \Rightarrow 0 = \sin \phi$  or,  $\underline{\underline{\phi = 0}} \rightarrow$

$$\text{So, } x(t) = X_0 e^{-\gamma \omega_d t} \sin \omega_d t$$

$$\therefore \dot{x}(t) = -X_0 \gamma \omega_d e^{-\gamma \omega_d t} \sin \omega_d t + X_0 \omega_d e^{-\gamma \omega_d t} \cos \omega_d t$$

$$\therefore \dot{x}(0^+) = \frac{1}{m} \Rightarrow \frac{1}{m} = X_0 \omega_d \text{ or } X_0 = \frac{1}{m \omega_d}$$

$$\text{Hence, } \underline{g(t)} = \underline{x(t)} = \underline{\frac{1}{m \omega_d} e^{-\gamma \omega_d t} \sin \omega_d t} \text{ (Remember)}$$

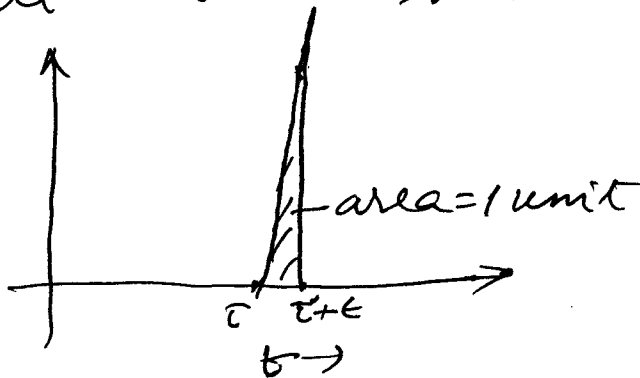


Also note that in case the impulse has magnitude  $I$ , the response would be

simply  $g(t) \times I$ , i.e.,  $I g(t)$

since ~~our~~ our system is linear.

→ Let us now see what happens when the unit impulse function is applied at  $t = \tau$  instead of at  $t = 0$ .



So, what we are applying to the system is the unit impulse function  $\delta(t - \tau)$

defined as:

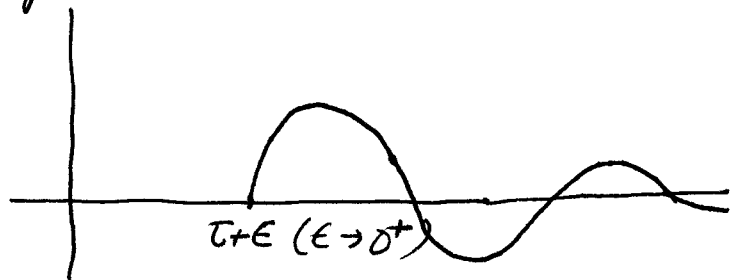
$$\delta(t - \tau) = 0 \text{ for } t \neq \tau$$

$$\int_0^{\infty} \delta(t - \tau) dt = 1$$

$$\int_0^{\infty} \delta(t - \tau) f(t) dt = f(\tau)$$

with  $0 < \tau < \infty$ .

Clearly, the system response now will simply be  $g(t-\tau)$  which looks like :

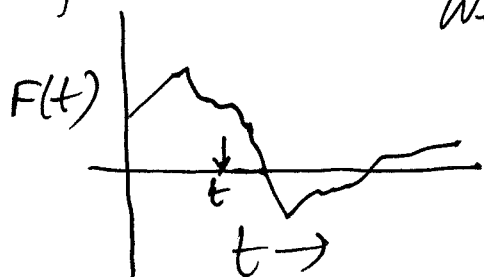


$$\text{So, } g(t-\tau) = 0 \text{ for } t < \tau$$

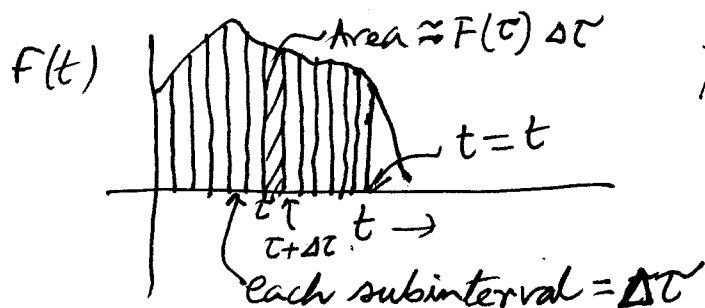
$$= \frac{1}{m\omega_d} e^{-\gamma\omega_n(t-\tau)} \sin \omega_d(t-\tau)$$

If the impulse has magnitude  $I$ , the response would be  $I g(t-\tau)$ .

→ After these preliminaries, let us go for the general forcing function  $F(t)$ ! We want  $x(t)$ , response at time  $t$ .



~~Let us~~ For response at time  $t$ , we need to take  $F(t)$  over the interval  $[0, t]$  only.



The effect of  $F(t)$  over  $[0, t]$  is the effect created by the impulses shown in the figure.

The impulse over  $[\tau, \tau+\Delta\tau)$  gives the approximate response

$$\Delta x(t) \approx \underbrace{F(\tau)\Delta\tau}_I g(t-\tau) \text{ as per}$$

our earlier discussion. So, total response  $x(t)$  at time  $t$  will be

$$x(t) \approx \sum_1^{\sum \Delta x(t)} \text{ (or } \sum F(\tau) g(t-\tau) \Delta \tau \text{)} = \sum F(\tau) g(t-\tau) \Delta \tau \quad (13)$$

where the summation is carried over all the impulses shown in the figure. (we are using the principle of superposition, see?)

As  $\Delta \tau \rightarrow d\tau$  & number of impulses  $\rightarrow \infty$ , the above summation gives way to integration & we get exact  $x(t)$  as:

$$\underline{x(t) = \int_0^t F(\tau) g(t-\tau) d\tau \text{ (Remember)}}$$

This is the famous Duhamel's integral or Convolution integral formula.

[It has an interesting geometrical interpretation. See Analytical Methods in vibrations by Z. Meirovitch]

→ Try to see what has been achieved.

If the above integral exists, then for any irregular  $F(t)$ , the integration can be performed numerically provided  $F(t)$  is measured for a sufficiently large number of points on the  $t$ -axis in the interval  $[0, t]$ .

Using proper instrumentation, this can be quite easily done &  $x(t)$  can be obtained.

→ We shall now consider some simple

(14)

examples to illustrate the use of above formula. In passing, note that

$$\int_0^t F(\tau) g(t-\tau) d\tau = \int_0^t F(t-\tau) g(\tau) d\tau$$

which can be established by a change of variable of integration (say, substitute  $z = t - \tau$  and use the fact that  ~~$\int_0^t F(\tau) g(t-\tau) d\tau$~~   $\int_0^t F(t-z) g(z) dz = \int_0^t F(t-\tau) g(\tau) d\tau$  etc.)

So, you can use either

$$x(t) = \int_0^t F(\tau) g(t-\tau) d\tau$$

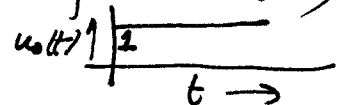
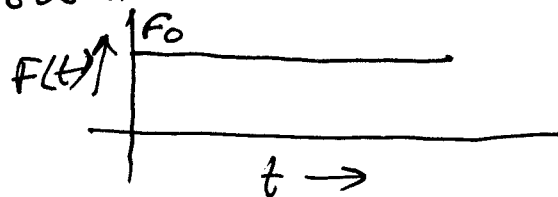
OR

$$x(t) = \int_0^t F(t-\tau) g(\tau) d\tau,$$

whichever is convenient.

Example 1:- For an undamped 1-DOF spring-mass system, obtain  $x(t)^*$

(\* When  $F(t) = F_0 u_0(t)$  ( $u_0(t)$  → unit step function) (by Duhamel's method) as shown:-

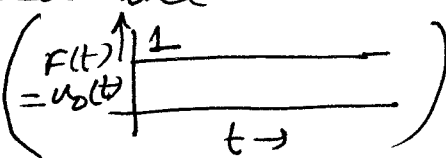


So,  $m\ddot{x} + kx = F_0$  ( $t > 0$ ) is the DEOM.

Since  $\delta = 0$ ,  $\boxed{g(t) = \frac{1}{m\omega_n} \sin \omega_n t} \rightarrow$

∴ Required response is:

$$\begin{aligned}
 x(t) &= \int_0^t F(\tau) g(t-\tau) d\tau \\
 &= \int_0^t F_0 \cdot \frac{1}{m\omega_n} \sin \omega_n(t-\tau) d\tau \\
 &= \frac{F_0}{m\omega_n} \times \frac{1}{\omega_n} \left[ \cos \omega_n(t-\tau) \right]_0^t \\
 &= \frac{F_0}{m\omega_n^2} [1 - \cos \omega_n t] \\
 &= \frac{F_0}{k} [1 - \cos \omega_n t] \quad \underline{\text{Ans.}}
 \end{aligned}$$

[Note that in some books,  $g(t)$  is denoted as  $h(t)$  and the response to  $u_0(t)$   is denoted as  $g(t)$ .

We have used the notation found in most of the textbooks.

The response to  $F(t) = u_0(t)$  has the special name 'the indicial response'. ] It can be shown that

$$g(t) = \frac{dh(t)}{dt} + h(0)\delta(t) \quad \text{(Meirovitch, Analytical....)}$$

(To be continued)  
onto VA-3, part 6