

# Finite Volume Methods for Hyperbolic Problems

## Multidimensional Finite Volume Methods

- Integral form on a rectangular grid cell
- Flux differencing form
- Scalar advection: donor cell upwind
- Corner transport upwind and transverse waves
- Wave propagation algorithms for systems
- Transverse Riemann solver

# Derivation of conservation law

$$\frac{d}{dt} \iint_{\Omega} q(x, y, t) dx dy = - \int_{\partial\Omega} \vec{n} \cdot \vec{f}(q) ds.$$

where  $\vec{f}(q) = (f(q), g(q))$ , fluxes in  $x$ - and  $y$ -directions.

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If  $\Omega$  is a rectangular grid cell  $[x_{i-1/2}, x_{i+1/2}] \times [y_{j-1/2}, y_{j+1/2}]$

Then flux in normal direction  $\vec{n}$  is

$$\vec{n} \cdot \vec{f}(q) = \begin{cases} \mp f(q) & \text{at } x_{i\pm 1/2}, \\ \mp g(q) & \text{at } y_{j\pm 1/2}. \end{cases}$$

## 2D finite volume method for $q_t + f(q)_x + g(q)_y = 0$

Evolution of total mass due to fluxes through cell edges:

$$\begin{aligned} \frac{d}{dt} \iint_{C_{ij}} q(x, y, t) dx dy &= \int_{y_{j-1/2}}^{y_{j+1/2}} f(q(x_{i+1/2}, y, t)) dy \\ &\quad - \int_{y_{j-1/2}}^{y_{j+1/2}} f(q(x_{i-1/2}, y, t)) dy \\ &\quad + \int_{x_{i-1/2}}^{x_{i+1/2}} g(q(x, y_{j+1/2}, t)) dx \\ &\quad - \int_{x_{i-1/2}}^{x_{i+1/2}} g(q(x, y_{j-1/2}, t)) dx. \end{aligned}$$

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Suggests:

$$\begin{aligned} \frac{\Delta x \Delta y Q_{ij}^{n+1} - \Delta x \Delta y Q_{ij}^n}{\Delta t} &= -\Delta y [F_{i+1/2,j}^n - F_{i-1/2,j}^n] \\ &\quad - \Delta x [G_{i,j+1/2}^n - G_{i,j-1/2}^n], \end{aligned}$$

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Where we define numerical fluxes:

$$F_{i-1/2,j}^n \approx \frac{1}{\Delta t \Delta y} \int_{t_n}^{t_{n+1}} \int_{y_{j-1/2}}^{y_{j+1/2}} f(q(x_{i-1/2}, y, t)) dy dt,$$

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Rewrite by dividing by  $\Delta x \Delta y \implies$  FV method in conservation form:

$$\begin{aligned}Q_{ij}^{n+1} &= Q_{ij}^n - \frac{\Delta t}{\Delta x} [F_{i+1/2,j}^n - F_{i-1/2,j}^n] \\ &\quad - \frac{\Delta t}{\Delta y} [G_{i,j+1/2}^n - G_{i,j-1/2}^n].\end{aligned}$$

## Dimensional splitting vs. unsplit FV method

Hyperbolic system in 2d:  $q_t + f(q)_x + g(q)_y = 0$

Split method:

$$Q_{ij}^* = Q_{ij}^n - \frac{\Delta t}{\Delta x} [F_{i+1/2,j}^n - F_{i-1/2,j}^n]$$
$$Q_{ij}^{n+1} = Q_{ij}^* - \frac{\Delta t}{\Delta y} [G_{i,j+1/2}^* - G_{i,j-1/2}^*].$$

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Unsplit method:

$$\begin{aligned} Q_{ij}^{n+1} &= Q_{ij}^n - \frac{\Delta t}{\Delta x} [F_{i+1/2,j}^n - F_{i-1/2,j}^n] \\ &\quad - \frac{\Delta t}{\Delta y} [G_{i,j+1/2}^n - G_{i,j-1/2}^n]. \end{aligned}$$

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Fluctuation form:

$$\begin{aligned} Q_{ij}^{n+1} = Q_{ij} - \frac{\Delta t}{\Delta x} (\mathcal{A}^+ \Delta Q_{i-1/2,j} + \mathcal{A}^- \Delta Q_{i+1/2,j}) \\ - \frac{\Delta t}{\Delta y} (\mathcal{B}^+ \Delta Q_{i,j-1/2} + \mathcal{B}^- \Delta Q_{i,j+1/2}) \\ - \frac{\Delta t}{\Delta x} (\tilde{F}_{i+1/2,j} - \tilde{F}_{i-1/2,j}) - \frac{\Delta t}{\Delta y} (\tilde{G}_{i,j+1/2} - \tilde{G}_{i,j-1/2}). \end{aligned}$$

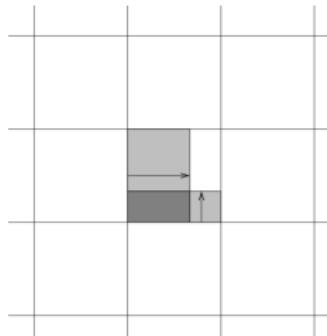
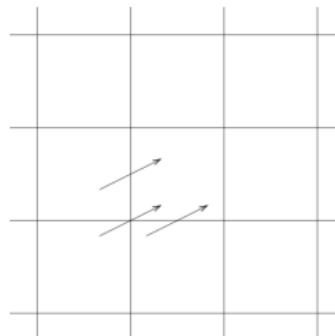
The  $\tilde{F}$  and  $\tilde{G}$  are **correction fluxes** to go beyond Godunov's upwind method.

Incorporate approximations to second derivative terms in each direction ( $q_{xx}$  and  $q_{yy}$ ) **and mixed term  $q_{xy}$ .**

# Advection: Donor Cell Upwind

With no correction fluxes, Godunov's method for advection is  
**Donor Cell Upwind:**

$$\begin{aligned} Q_{ij}^{n+1} = Q_{ij} & - \frac{\Delta t}{\Delta x} [u^+(Q_{ij} - Q_{i-1,j}) + u^-(Q_{i+1,j} - Q_{ij})] \\ & - \frac{\Delta t}{\Delta y} [v^+(Q_{ij} - Q_{i,j-1}) + v^-(Q_{i,j+1} - Q_{ij})]. \end{aligned}$$

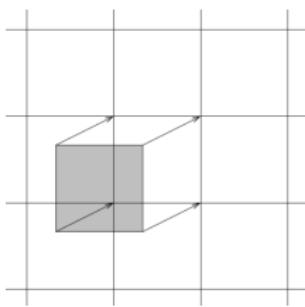
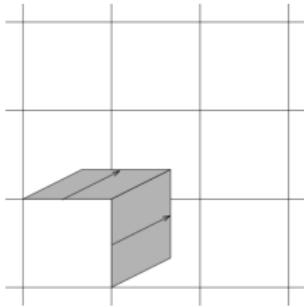
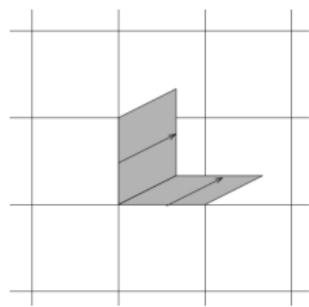


**Stable only if**  $\left| \frac{u \Delta t}{\Delta x} \right| + \left| \frac{v \Delta t}{\Delta y} \right| \leq 1.$

# Advection: Corner Transport Upwind (CTU)

Correction fluxes can be added to advect waves correctly.

Corner Transport Upwind:



Stable for  $\max \left( \left| \frac{u\Delta t}{\Delta x} \right|, \left| \frac{v\Delta t}{\Delta y} \right| \right) \leq 1$ .

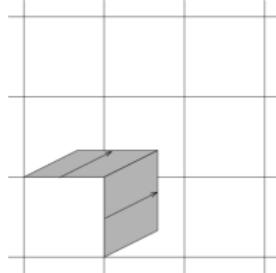
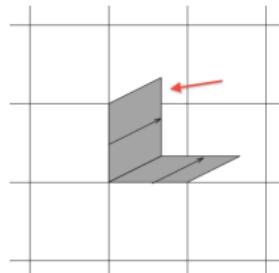
# Advection: Corner Transport Upwind (CTU)

Need to transport triangular region from cell  $(i, j)$  to  $(i, j + 1)$ :

$$\text{Area} = \frac{1}{2}(u\Delta t)(v\Delta t) \implies \left( \frac{\frac{1}{2}uv(\Delta t)^2}{\Delta x \Delta y} \right) (Q_{ij} - Q_{i-1,j}).$$

Accomplished by correction flux:

$$\tilde{G}_{i,j+1/2} = -\frac{1}{2} \frac{\Delta t}{\Delta x} uv(Q_{ij} - Q_{i-1,j})$$



$\frac{\Delta t}{\Delta y} (\tilde{G}_{i,j+1/2} - \tilde{G}_{i,j-1/2})$  gives approximation to  $\frac{1}{2}\Delta t^2 uv q_{xy}$ .

$\frac{\Delta t}{\Delta x} (\tilde{F}_{i+1/2,j} - \tilde{F}_{i-1/2,j})$  gives similar approximation.

# Upwind splitting of matrix product

In 1D, the upwind method is

$$Q_i^{n+1} = Q_i^n - \frac{\Delta t}{\Delta x} [A^+(Q_i^n - Q_{i-1}^n) + A^-(Q_{i+1}^n - Q_i^n)]$$

where

$$A = R\Lambda R^{-1} = R\Lambda^+R^{-1} + R\Lambda^-R^{-1} = A^+ + A^-$$

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In 2D the unsplit generalization uses

$$AB = (A^+ + A^-)(B^+ + B^-) = A^+B^+ + A^+B^- + A^-B^+ + B^-A^-,$$

$$BA = (B^+ + A^-)(B^+ + A^-) = B^+A^+ + B^+A^- + B^-A^+ + B^-A^-.$$

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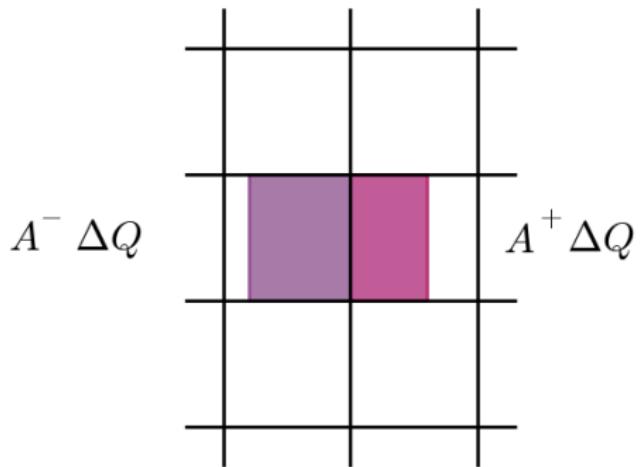
Scalar advection: only one term is nonzero in each product,

e.g.  $u > 0, v < 0 \implies uv = vu = u^+v^-$

# Wave propagation algorithm for $q_t + Aq_x + Bq_y = 0$

Decompose  $A = A^+ + A^-$  and  $B = B^+ + B^-$ .

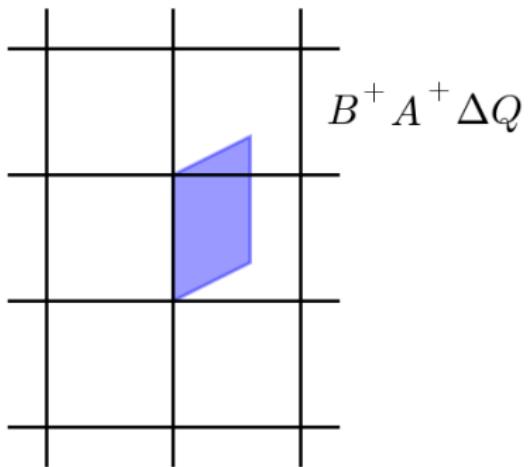
For  $\Delta Q = Q_{ij} - Q_{i-1,j}$ :



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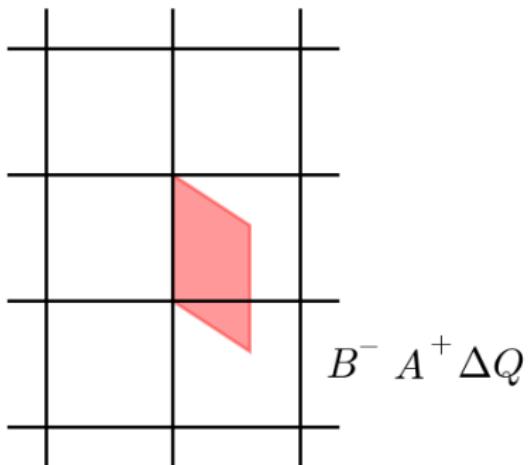
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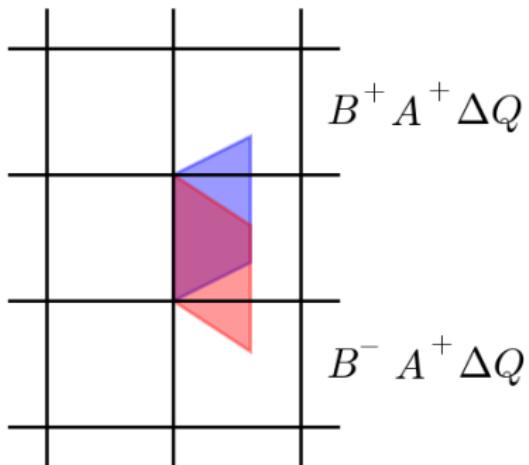
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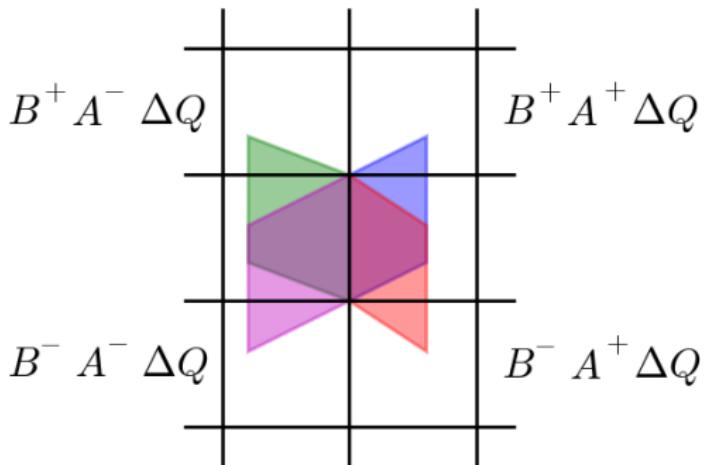
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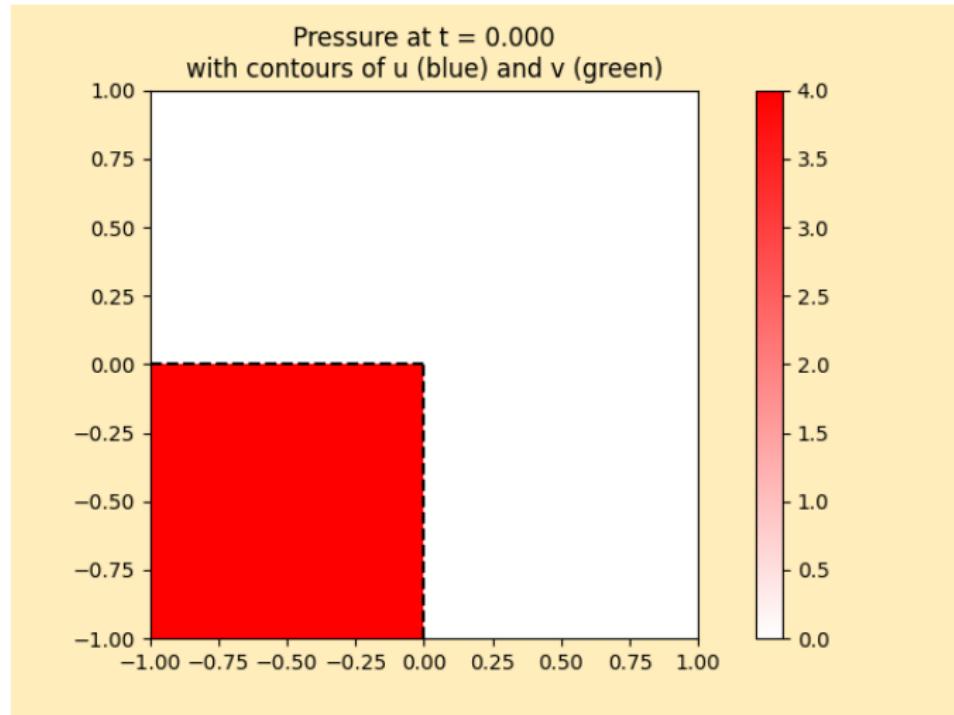
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# Acoustics near a cell corner

Solve 2D acoustics with  $\rho = K = c = Z = 1$

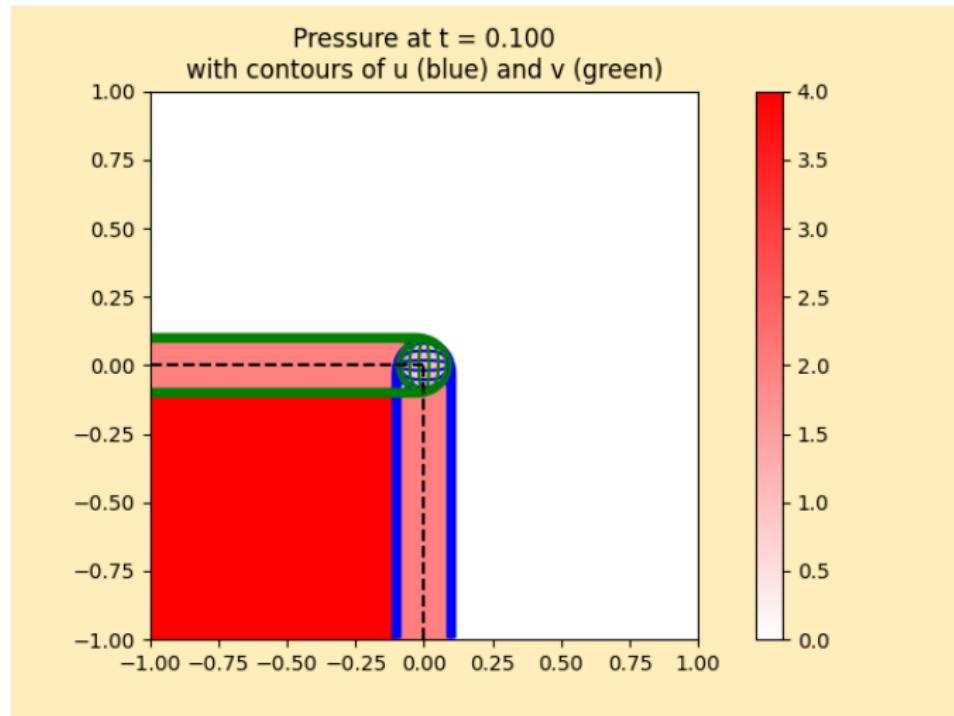
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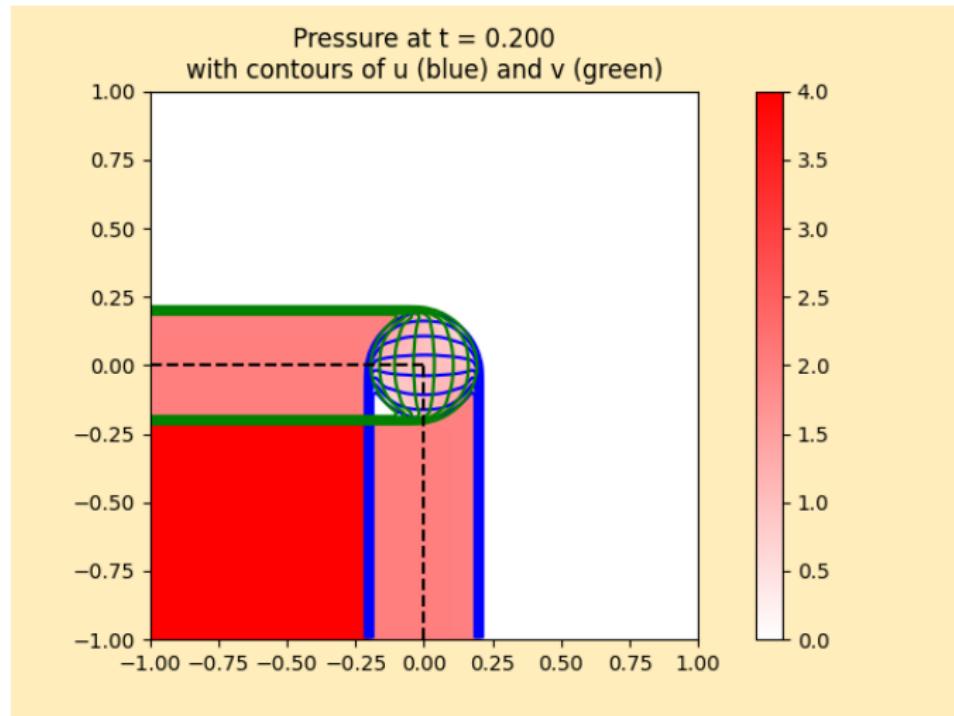
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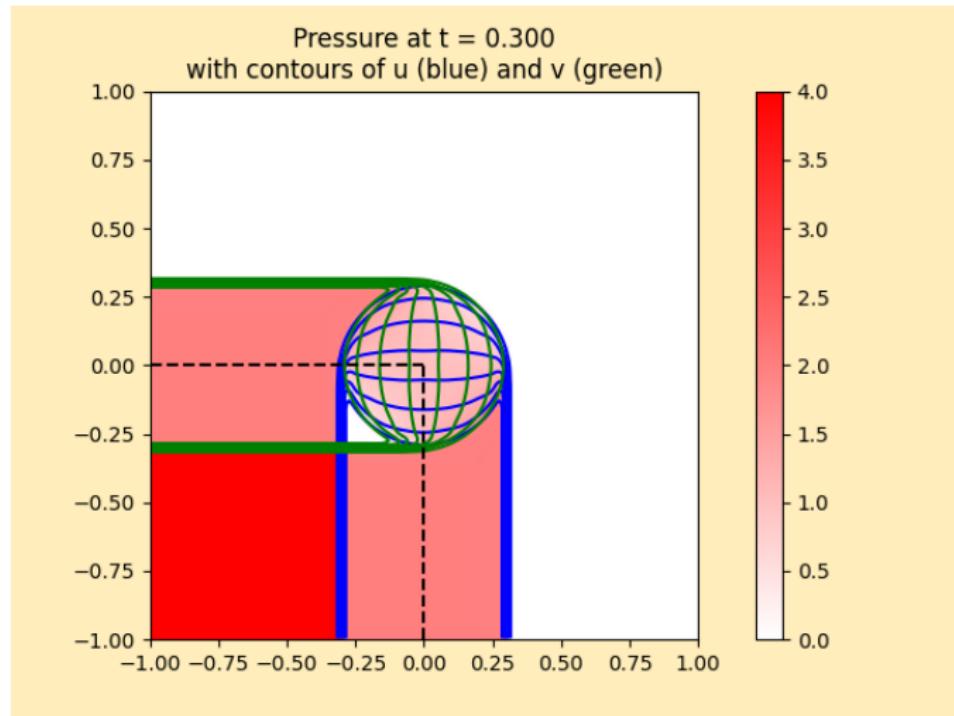
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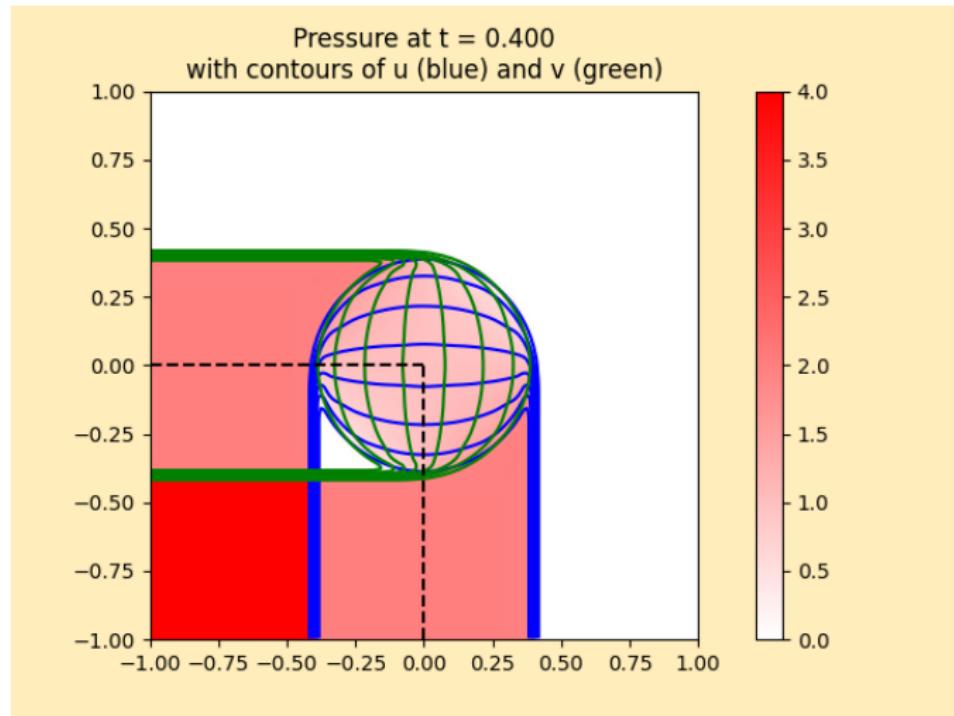
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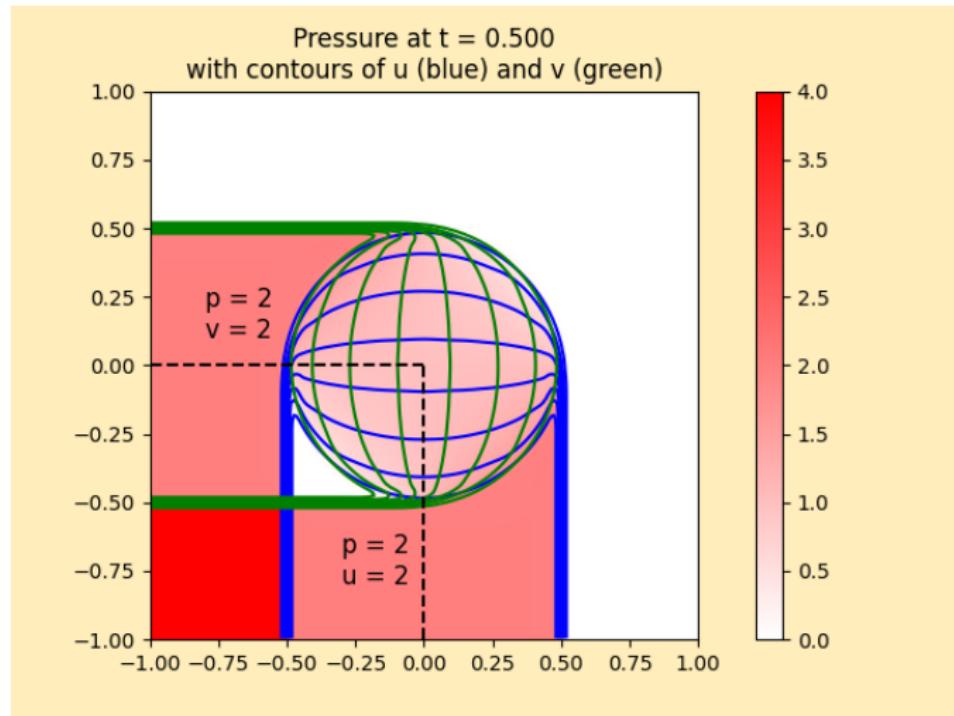
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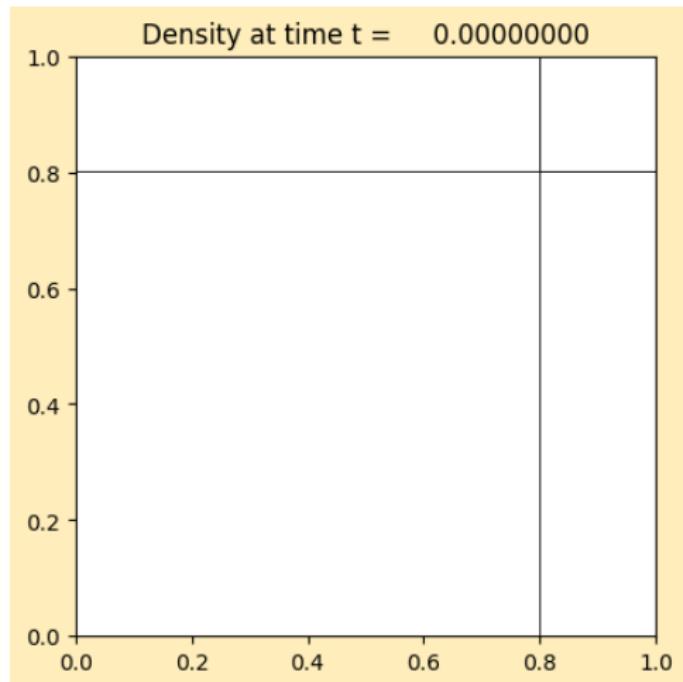
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# 2D Riemann problem for Euler

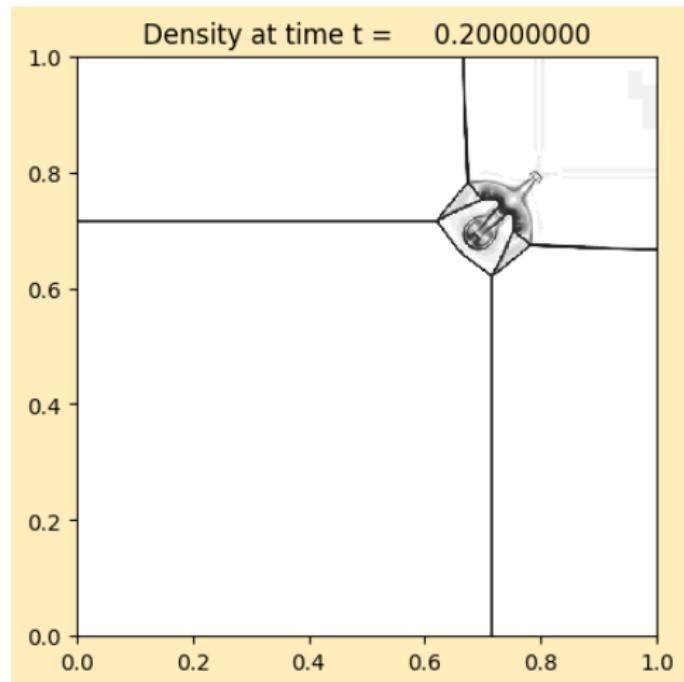
Values in 4 quadrants chosen to give single shock between each



**Clawpack Gallery: euler\_2d\_quadrants**

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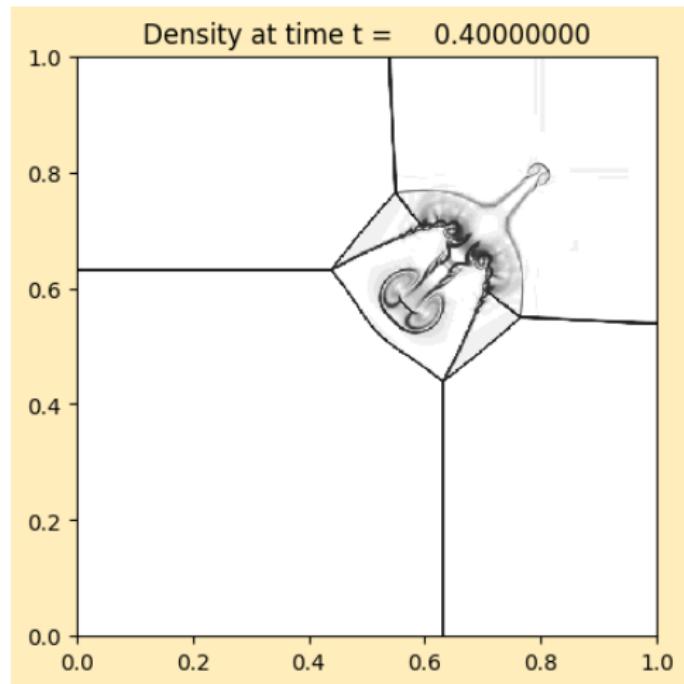
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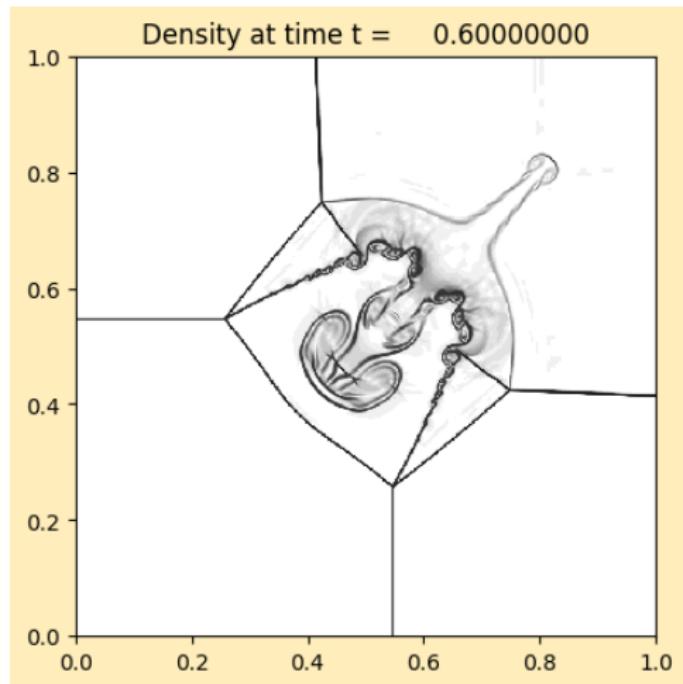
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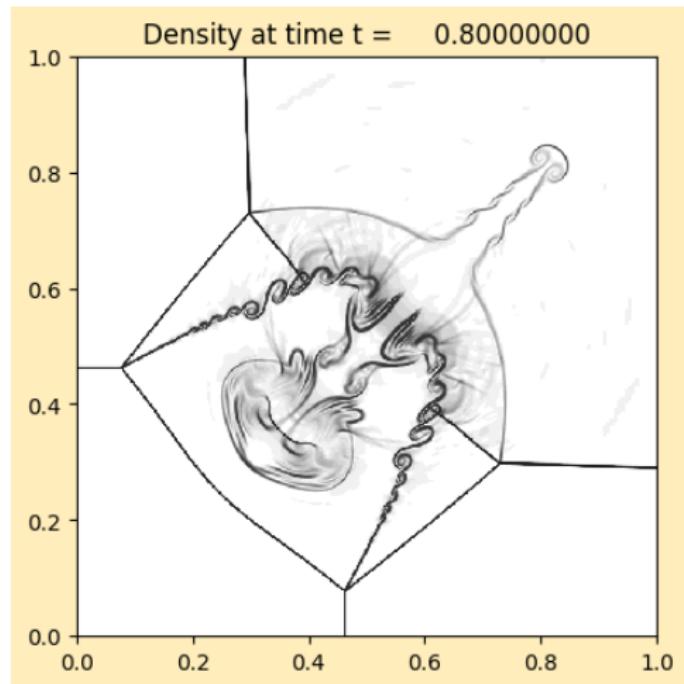
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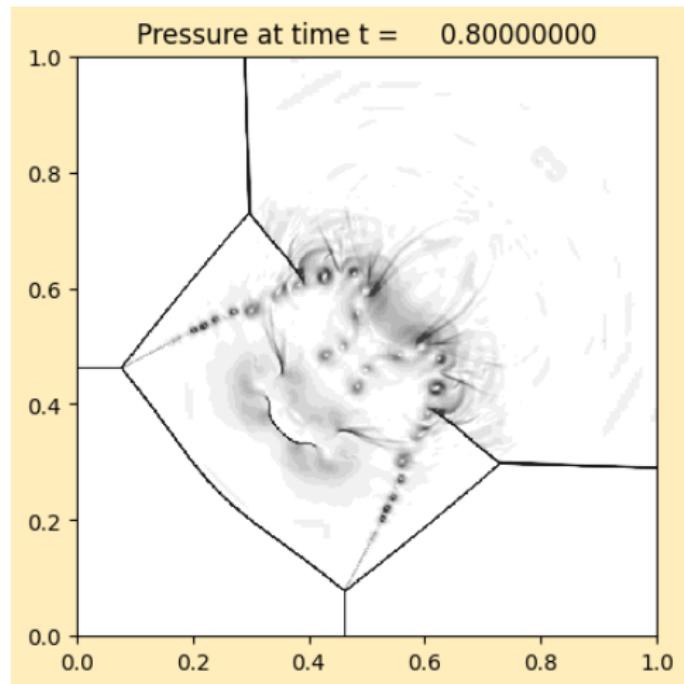
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# Wave propagation algorithms in 2D

Clawpack requires:

Normal Riemann solver `rpn2.f`

Solves 1d Riemann problem  $q_t + Aq_x = 0$

Decomposes  $\Delta Q = Q_{ij} - Q_{i-1,j}$  into  $\mathcal{A}^+ \Delta Q$  and  $\mathcal{A}^- \Delta Q$ .

For  $q_t + Aq_x + Bq_y = 0$ , split using eigenvalues, vectors:

$$A = R\Lambda R^{-1} \implies A^- = R\Lambda^- R^{-1}, A^+ = R\Lambda^+ R^{-1}$$

Input parameter `ixy` determines if it's in  $x$  or  $y$  direction.

In latter case splitting is done using  $B$  instead of  $A$ .

This is all that's required for dimensional splitting.

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Transverse Riemann solver `rpt2.f`

Decomposes  $\mathcal{A}^+ \Delta Q$  into  $\mathcal{B}^- \mathcal{A}^+ \Delta Q$  and  $\mathcal{B}^+ \mathcal{A}^+ \Delta Q$  by splitting this vector into eigenvectors of  $B$ .

(Or splits vector into eigenvectors of  $A$  if `ixy=2`.)

# Transverse Riemann solver in Clawpack

`rpt2` takes vector `asdq` and returns `bmasdq` and `bpasdq`  
where

`asdq` =  $\mathcal{A}^* \Delta Q$  represents either

$\mathcal{A}^- \Delta Q$  if `imp = 1`, or  
 $\mathcal{A}^+ \Delta Q$  if `imp = 2`.

Returns  $\mathcal{B}^- \mathcal{A}^* \Delta Q$  and  $\mathcal{B}^+ \mathcal{A}^* \Delta Q$ .

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Returns  $\mathcal{B}^- \mathcal{A}^* \Delta Q$  and  $\mathcal{B}^+ \mathcal{A}^* \Delta Q$ .

Note: there is also a parameter `ixy`:

`ixy = 1` means normal solve was in  $x$ -direction,

`ixy = 2` means normal solve was in  $y$ -direction,

In this case `asdq` represents  $\mathcal{B}^- \Delta Q$  or  $\mathcal{B}^+ \Delta Q$  and the routine must return  $\mathcal{A}^- \mathcal{B}^* \Delta Q$  and  $\mathcal{A}^+ \mathcal{B}^* \Delta Q$ .

# Gas dynamics in 2D

$\rho(x, y, t)$  = mass density

$\rho(x, y, t)u(x, y, t)$  =  $x$ -momentum density

$\rho(x, y, t)v(x, y, t)$  =  $y$ -momentum density

If pressure =  $P(\rho)$ , e.g. isothermal or isentropic:

$$\rho_t + (\rho u)_x + (\rho v)_y = 0$$

$$(\rho u)_t + (\rho u^2 + p)_x + (\rho uv)_y = 0$$

$$(\rho v)_t + (\rho uv)_x + (\rho v^2 + p)_y = 0$$

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1D equation in  $x$ :  $q_t + f(q)_x = 0$  is:

$$\rho_t + (\rho u)_x = 0$$

$$(\rho u)_t + (\rho u^2 + p)_x = 0$$

$$(\rho v)_t + (\rho u v)_x = 0 \implies v_t + u v_x = 0$$

These are just 1D equations for  $(\rho, \rho u)$   
along with an advected quantity  $v$

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$\rho(x, y, t)v(x, y, t)$  =  $y$ -momentum density

If pressure =  $P(\rho)$ , e.g. isothermal or isentropic:

$$\rho_t + (\rho u)_x + (\rho v)_y = 0$$

$$(\rho u)_t + (\rho u^2 + p)_x + (\rho u v)_y = 0$$

$$(\rho v)_t + (\rho u v)_x + (\rho v^2 + p)_y = 0$$

1D equation in  $y$ :  $q_t + g(q)_y = 0$  is:

$$\rho_t + (\rho v)_y = 0$$

$$(\rho u)_t + (\rho u v)_y = 0 \implies u_t + v u_y = 0$$

$$(\rho v)_t + (\rho v^2 + p)_y = 0$$

These are just 1D equations for  $(\rho, \rho v)$   
along with an advected quantity  $u$

## Gas dynamics in 2D – transverse solver

If Roe solver is used for normal Riemann problems:

Eigenvectors of  $\hat{A} \approx f'(q)$  are used for splitting in  $x$ ,

$$\hat{\rho} = \frac{1}{2}(\rho_{i-1,j} + \rho_{i,j}), \quad \hat{u} = \frac{\sqrt{\rho_{i-1,j}}u_{i-1,j} + \sqrt{\rho_{i,j}}u_{i,j}}{\sqrt{\rho_{i-1,j}} + \sqrt{\rho_{i,j}}}$$

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Use the same Roe averages for this interface to also define  
 $\hat{B} \approx g'(q)$  near this interface.

Split  $\mathcal{A}^* \Delta Q$  into eigenvectors of  $\hat{B}$  to define

$\mathcal{B}^- \mathcal{A}^* \Delta Q$  and  $\mathcal{B}^+ \mathcal{A}^* \Delta Q$

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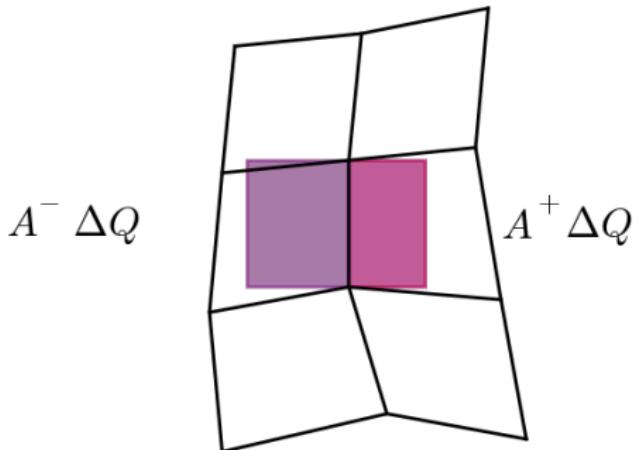
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Many normal and transverse solvers available in

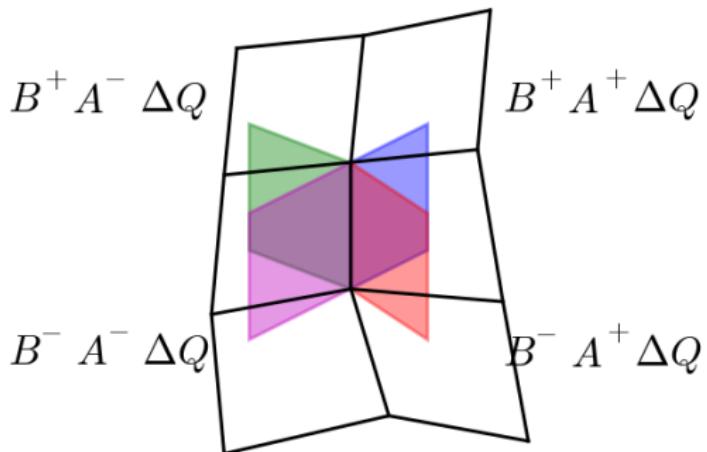
**\$CLAW/riemann/src**

# Wave propagation algorithm on a quadrilateral grid



Example: [\*\*\\$CLAW/amrclaw/examples/advection\\_2d\\_annulus\*\*](#)

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Example: [\*\*\\$CLAW/amrclaw/examples/advection\\_2d\\_annulus\*\*](#)