# Wavefront reconstruction for adaptive optics

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W.M. Keck Observatory

## Friendly people

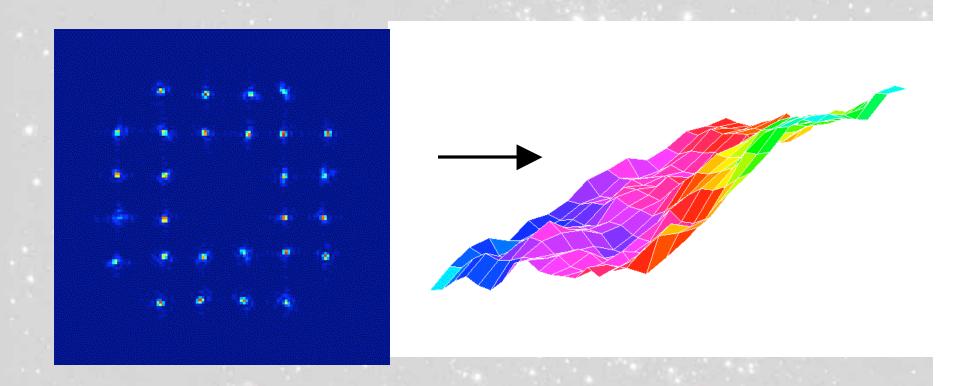
- We borrowed slides from the following people:
  - Lisa Poyneer
  - Luc Gilles
  - Curt Vogel
  - Corinne Boyer
- Mahalo!

Imke de Pater et al

#### **Outline**



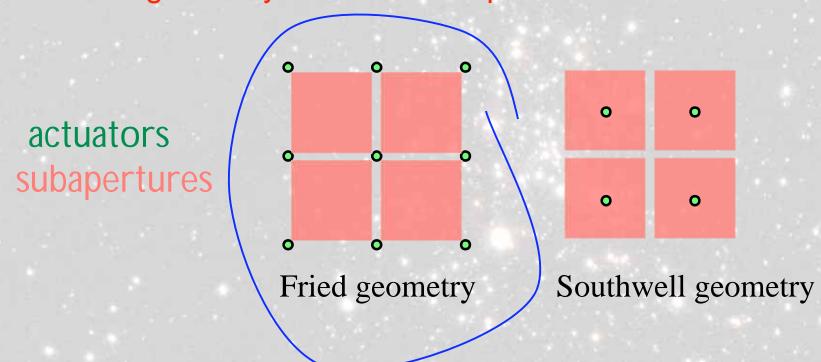
- System matrix, H: from actuators to centroids s = Ha
- Reconstructor, R: from centroids to actuators a = Rs
- Fast algorithms and hardware



### Case Study



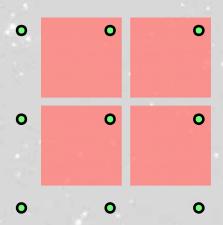
- Consider a Shack-Hartmann wavefront sensor
- Actuators in a square array with a separation equal to the lenslet size
- Fried geometry between subapertures and actuators



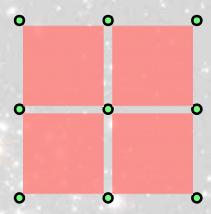
## DM to lenslet registration



How do we ensure that we have the right registration?



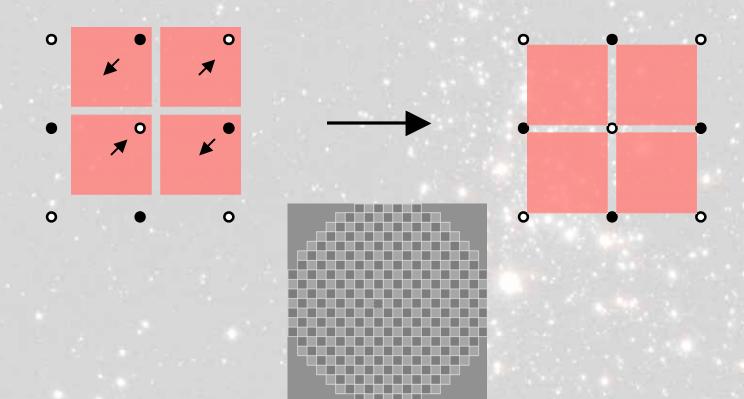




### DM to lenslet registration



Add waffle to the DM and adjust lenslet array or the beam until no centroids are measured

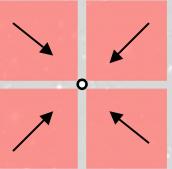


## System matrix generation



System matrix describes how a signal applied to the actuators, *a*, affects the centroids, *s*.

$$s = Ha$$

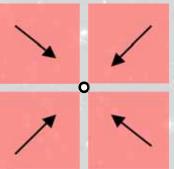


Can be calculated theoretically or, preferably, experimentally

## Theoretical system matrix



For an actuator at (n+1/2,n+1/2),



$$s_x = 1$$

$$s_x = -1$$

$$s_y = -1$$

$$s_y = -1$$

$$s_x = 1$$

$$s_x = -1$$

$$s_y = 1$$

$$s_{v} = 1$$

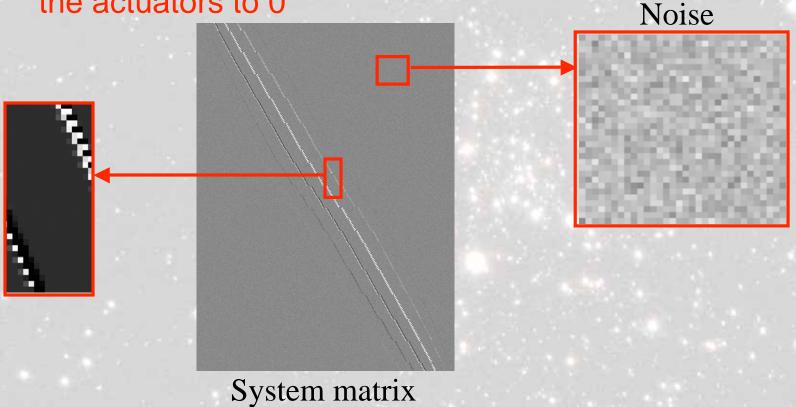
#### Experimental system matrix



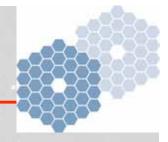
Poke one actuator at a time in the positive and negative directions and record the centroids

Set centroid values from subapertures far away from

the actuators to 0



## Inverting the system matrix



- We have the system matrix s = Ha
- We need a reconstructor matrix to convert from centroids to actuator voltages a = Rs

$$Ha = S$$

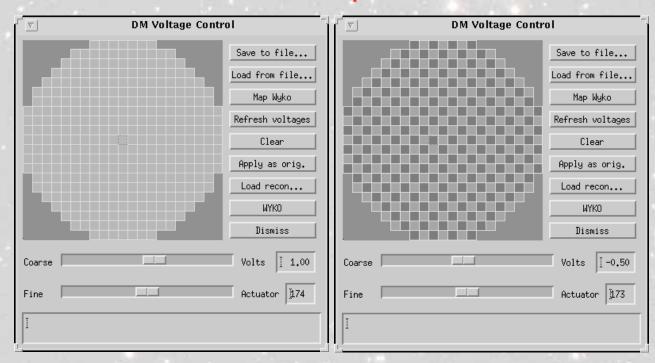
$$H^{T}Ha = H^{T}S$$

$$a = (H^{T}H)^{-1}H^{T}S$$

Least-squares reconstructor R



- Least squares reconstructor is  $(H^T H)^{-1} H^T$
- Minimizes  $(s Ha)^2$
- But  $H^TH$  is not invertible because some modes are invisible!
- Two invisible modes are piston and waffle



## Singular value decomposition



- The SVD reconstructor is found by rejecting small singular values of H.

$$\Lambda = \begin{bmatrix} \lambda_1 & & & \\ & \lambda_2 & & \\ & & \lambda_3 & \\ & & & O \end{bmatrix} \quad \lambda_i \text{ are the eigenvalues of } H^T H$$

The pseudo inverse is  $H^+ = V \Lambda^{-1} U^T$ 

## Singular value decomposition

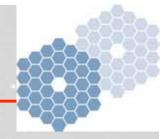


The pseudo inverse is  $H^+ = V\Lambda^{-1}U^T$ 

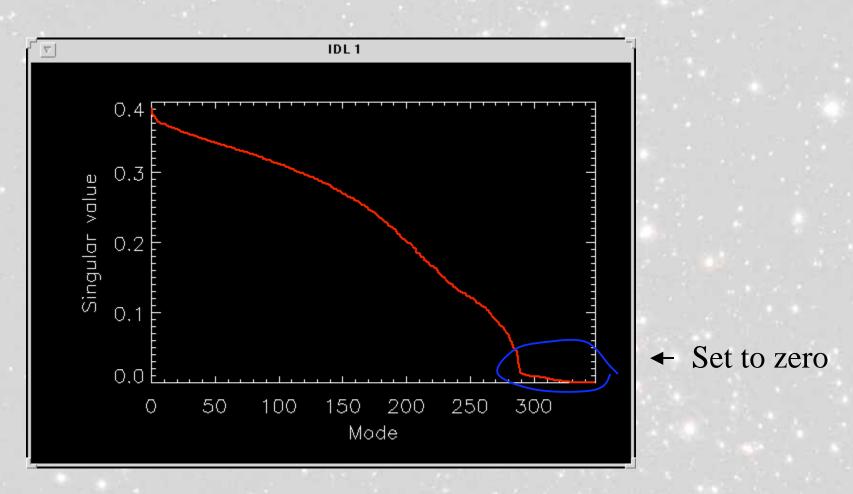
$$\Lambda^{-1} = \begin{bmatrix} \lambda_1^{-1} & & & \\ & \lambda_2^{-1} & & \\ & & \lambda_3^{-1} & \\ & & & O \end{bmatrix}$$

Replace all the  $\lambda_i^{-1}$  with 0 for small values of  $\lambda_i$ 

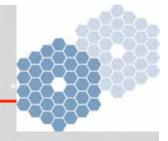
## Singular value decomposition







#### Noise propagation



- Suppose we only have centroid noise in the system with variance  $\sigma^2$
- Variance of actuator commands is:

$$Var(a) = Var(Rs)$$

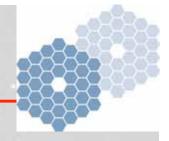
$$= E[(Rs)^{2}] - (E[(Rs)])^{2}$$

$$= E[(Rs)^{2}]$$

$$= |R|^{2}E[s^{2}]$$

$$= |R|^{2}\sigma^{2}$$

### Noise propagation



- Recall  $Var(a) = |R|^2 \sigma^2$
- The total noise for all actuators is  $|R|^2 = \sum R_{i,j}^2$
- For the SVD, this is equal to the sum of the singular modes of the reconstructor  $|R|^2 = \sum \lambda_i^{-2}$

Throw away the noisiest modes!

The average noise propagation is  $|R|^2 = \sum R_{i,j}^2 / N$  where N is the number of actuators.



For well-conditioned *H* matrices, we can penalize piston, *p*, and waffle, *w*:

$$p = [1,1,1,1,1,1,...]^T$$
 Invertible
$$w = [1,-1,1,-1,1,...]^T$$

$$R = (H^T H + pp^T + ww^T)^{-1} H^T$$

Minimizes  $(s - Ha)^2 + (p^T a)^2 + (w^T a)^2$ 

Choose the actuator voltages that best cancel the measured centroids



For well-conditioned H matrices, just heavily penalize piston, *p*, and waffle, *w*:

$$p = [1,1,1,1,1,1,...]^{T}$$

$$w = [1,-1,1,-1,1,...]^{T}$$

$$R = (H^{T}H + pp^{T} + ww^{T})^{-1}H^{T}$$

Minimizes 
$$(s - Ha)^2 + (p^T a)^2 + (w^T a)^2$$

Choose the actuator voltages such that there is no piston

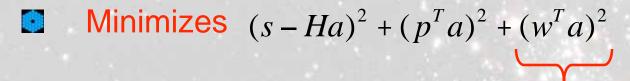


For well-conditioned H matrices, just heavily penalize piston, *p*, and waffle, *w*:

$$p = [1,1,1,1,1,1,...]^{T}$$

$$w = [1,-1,1,-1,1,...]^{T}$$

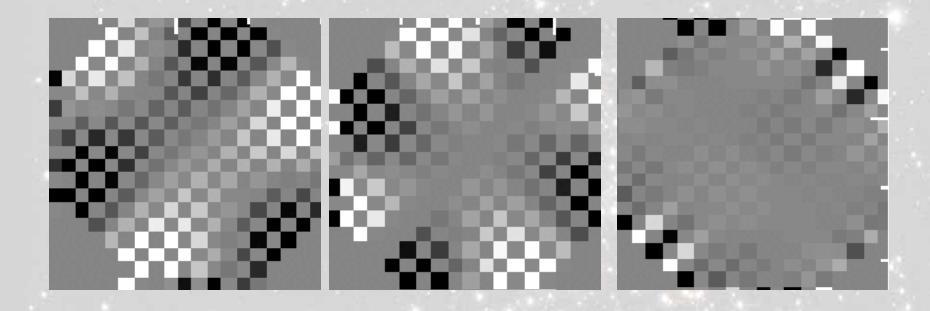
$$R = (H^{T}H + pp^{T} + ww^{T})^{-1}H^{T}$$



Choose the actuator voltages such that there is no waffle

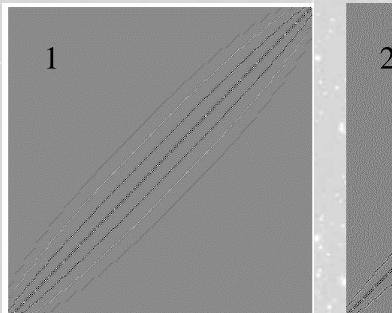


- Most modes have local waffle but no global waffle
- Must regularize before inverting





- Penalize waffle in the inversion:
  - 1. Inverse covariance matrix of Kolmogorov turbulence or
  - 2. Waffle penalization matrix



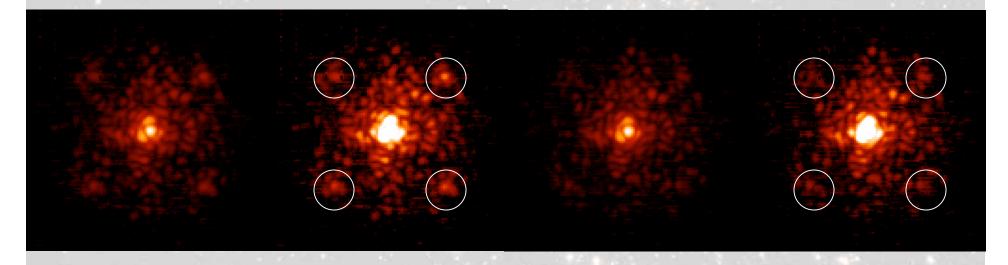
2



$$R = (H^T H + \alpha C_{\phi}^{-1})^{-1} H^T$$

Inverse covariance matrix for Kolmogorov turbulence





**SVD** 

Bayesian



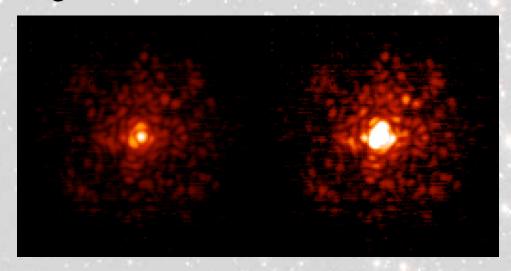
$$R = (H^T H + \alpha C_{\phi}^{-1})^{-1} H^T$$

Noise-to-signal parameter

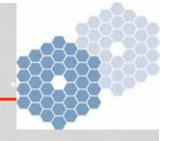
Minimizes  $(s - Ha)^2 + \alpha a^T C_{\phi}^{-1} a$ 

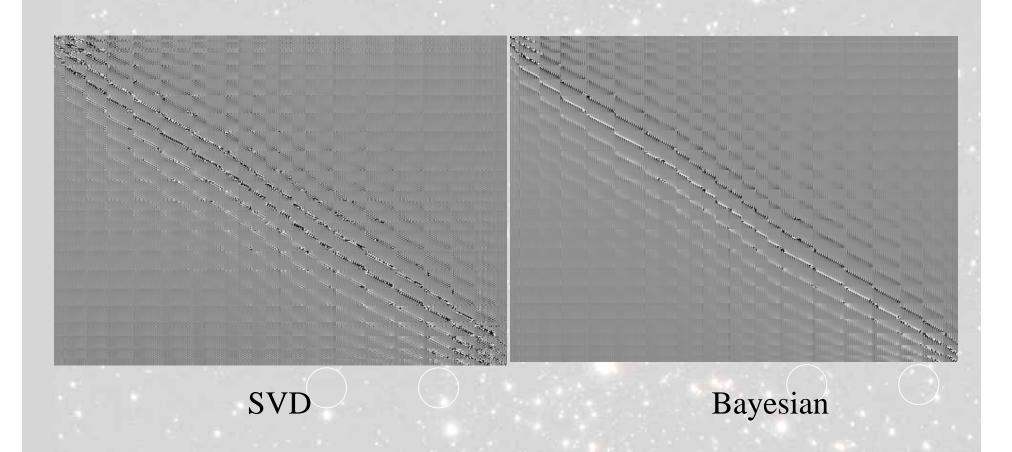
Bright star  $\alpha=1$ 

Faint star  $\alpha$ =30



# SVD vs Bayesian

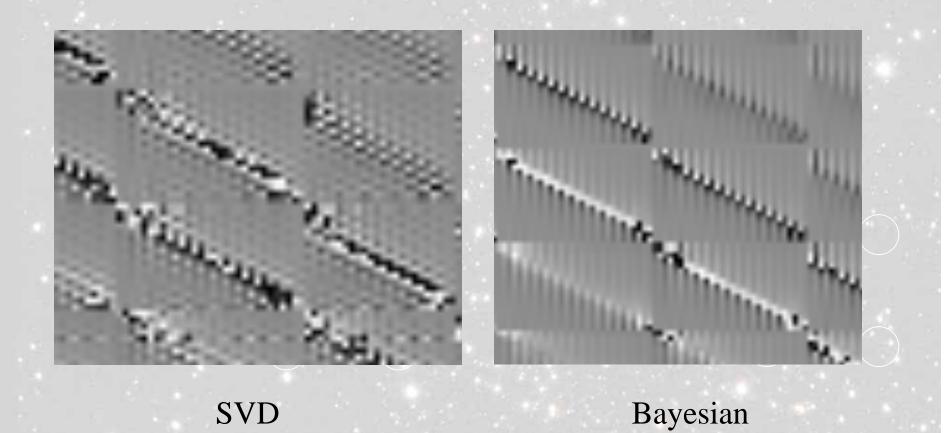




Noise propagation

# SVD vs Bayesian



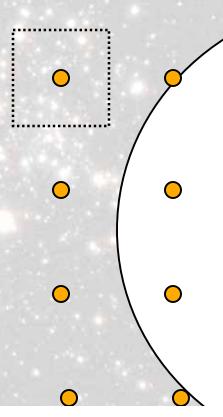


#### Slaved actuators

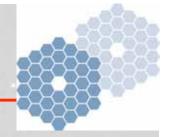


- Some actuators are located outside the pupil and do not directly affect the wavefront
- They are often "slaved" to the average value of its neighbors

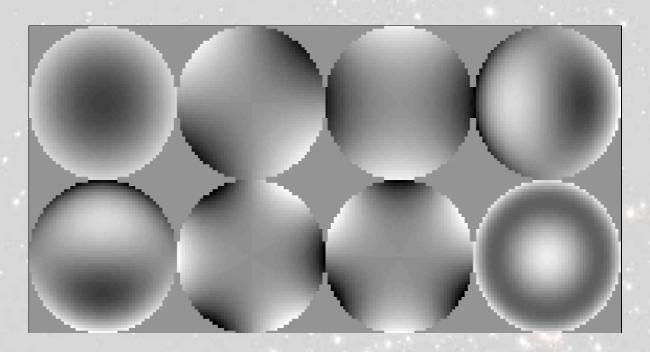
Slaved to average value of its neighbors



#### Modal reconstructors



- Can choose to only reconstruct certain modes
- Avoids reconstructing unwanted modes (e.g., waffle)



Zernike modes

#### Modal reconstructors



$$Z = [z_1, z_2, z_3, \dots]$$
 Zernike modes

HZ Centroids measured by applying Zernike modes to the DM

$$R = Z[(HZ)^{T}(HZ)]^{-1}(HZ)^{T}$$
 Zernike reconstructor



The slope measurements are derivatives of the phase, φ

$$s_x[m,n] = \phi[m+1,n] - \phi[m,n]$$
  $s_y[m,n] = \phi[m,n+1] - \phi[m,n]$ 

We can take the Fourier transform of both equations



$$S_x[m,n] = \phi[m+1,n] - \phi[m,n]$$



Fourier transform

$$S_x[k,l] = \Phi[k,l] \exp[j2\pi k/N] - \Phi[k,l]$$



$$s_y[m,n] = \phi[m,n+1] - \phi[m,n]$$



Fourier transform

$$S_{y}[k,l] = \Phi[k,l] \exp[j2\pi l/N] - \Phi[k,l]$$

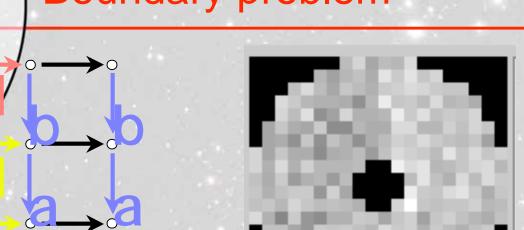


Solve for  $\Phi[k,l]$ 

$$\hat{\Phi} = \frac{(\exp[-j2\pi k/N] - 1)S_x[k,l] + (\exp[-j2\pi l/N] - 1)S_y[k,l]}{4(\sin^2[\pi k/N] + \sin^2[\pi l/N])}$$

- We can now apply any filter in the Fourier domain: e.g., we can low pass filter the signal to remove high spatial frequencies.
- Take the inverse Fourier transform to get the phase

## Boundary problem

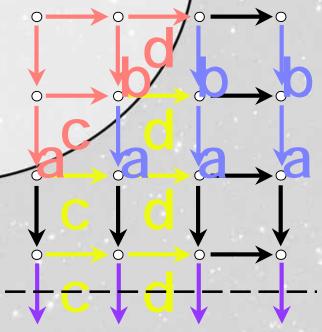


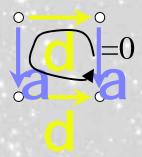


Finite sized aperture creates a boundary problem leading to incorrect wavefront estimation

### Boundary problem





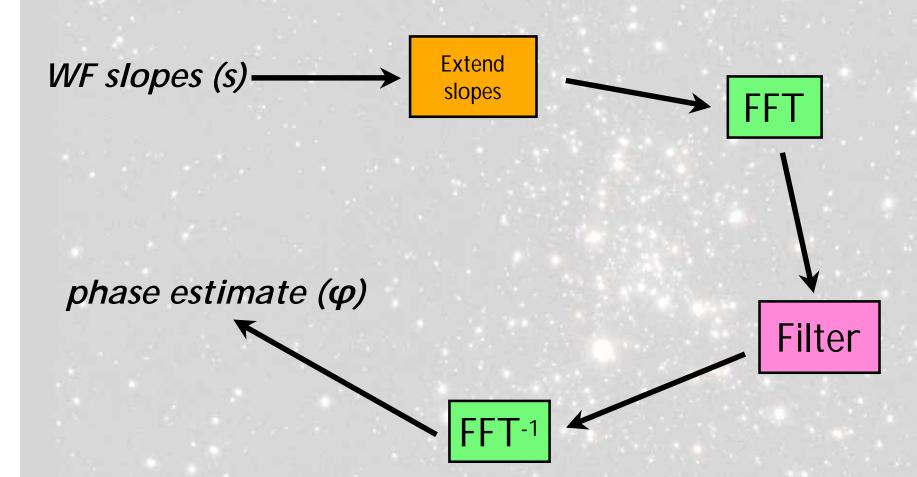


Matrix extent

- Solve by managing slopes outside the aperture
- Extend slopes in orthogonal directions outside the aperture
- Set wrap-around slopes to enforce periodicity

## Summary of FFT Reconstructor





#### **Control laws**



Now that we have the reconstructed wavefront, a, what do we do?

$$u[n] = a$$
 Wavefront error at time  $n$ 

$$y[n]$$
 Mirror position at time  $n$ 

Simplest control law is integrator with variable loop gain, k

$$y[n] = y[n-1] + ku[n]$$

New mirror command Current mirror command Reconstructed wavefront

#### **Control laws**



Need to clip the voltages to the maximum voltage, Vmax

$$y[n] = \min(y[n], V \max)$$

Actuator clipping and DM hysteresis can introduce invisible modes. These can be removed using a "leaky" integrator

$$y[n] = 0.99y[n-1] + ku[n]$$

$$y[n] = \min(y[n], V \max)$$

#### **Control laws**



Controllers can preempt the response

$$y[n] = y[n-1] + ku[n] + c(u[n] - u[n-1])$$

Add a fraction of the way the error is changing

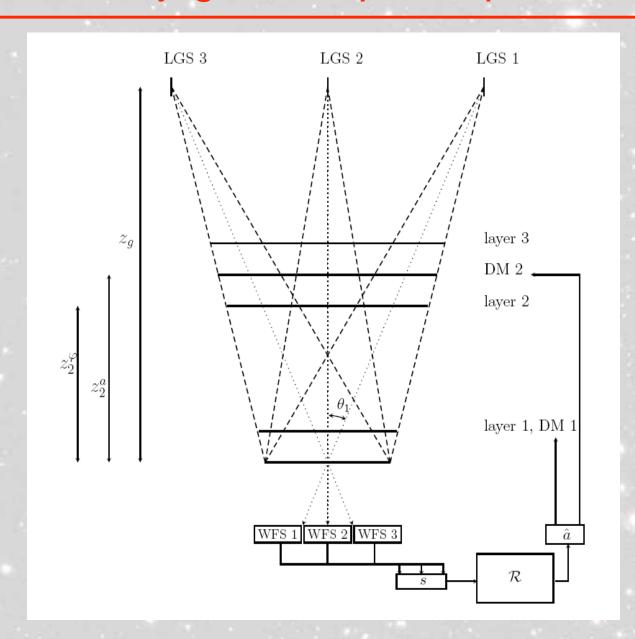
Or to allow for computational delay (Smith compensator)

$$y[n] = y[n-1] - c(y[n-1] - y[n-2]) + ku[n]$$

Remove portion of the way the DM is moving

## Multi-conjugate adaptive optics

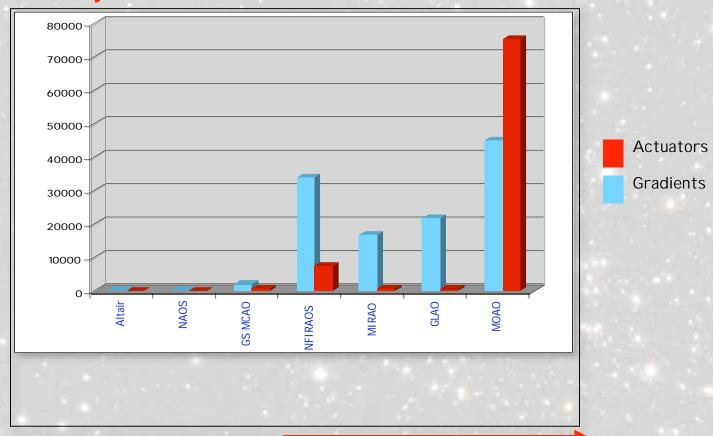




## System complexity increases



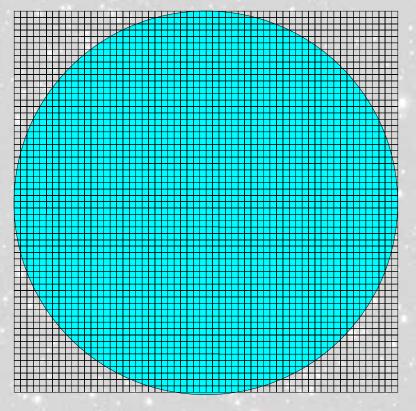
Next generation telescopes and AO systems will have much greater computational demands than current systems



## Computationally efficient reconstructors



- For example, for the Thirty Meter Telescope (TMT) AO system NFIRAOS
  - DM with 60x60 actuators
  - 6 LGS with 60x60 subapertures per WFS
  - 800 Hz sampling rate for LGS



## TMT reconstructor example

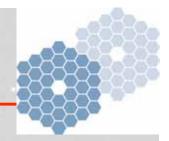


- 3600 actuators and 43200 slope measurements
- H is 43200 x 3600 element matrix
- Offline calculation (not in real time but as pupil rotates, etc):

$$R = (H^T H + \alpha C_{\phi}^{-1})^{-1} H^T$$

- Inverse is  $O(a^3) \approx 5x10^{10}$  floating point operations (flops)
- 1000 times more flops than Keck!

## TMT reconstructor example



Online calculation (at 800 Hz) is

$$a = Rs$$

- 2000 times more than Keck
- Online and offline calculations for TMT are not feasible using current algorithms and hardware

# Now for the good stuff!





#### Fast reconstructors



Bayesian reconstructor:

$$R = (H^T H + \alpha C_{\phi}^{-1})^{-1} H^T$$

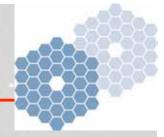
Slopes to actuators:

$$a = (H^T H + \alpha C_{\phi}^{-1})^{-1} H^T s$$

Substitute and rearrange:

$$(H^T H + \alpha C_{\phi}^{-1})a = H^T s$$

#### Problem formulation



Problem formulation:

$$(H^T H + \alpha C_{\phi}^{-1})a = H^T s$$

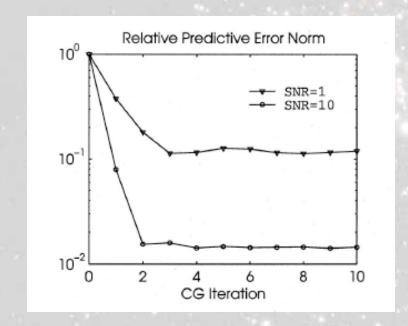
$$P \qquad v$$

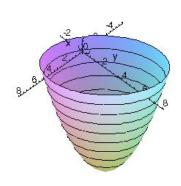
We want to solve the linear system: Pa = y

## Conjugate gradient algorithm

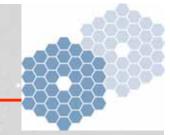


- Solve Pa=y by minimizing  $|Pa-y|^2$ .
- Conjugate gradient is an iterative method
- Get closer to solution with more iterations
- Trade-off speed vs accuracy
- Convergence depends on condition number of P





### Preconditioning



Preconditioning matrix M applied to transform problem to speed up convergence

$$Pa = y$$

$$M^{-1}PM^{-1}Ma = M^{-1}y$$

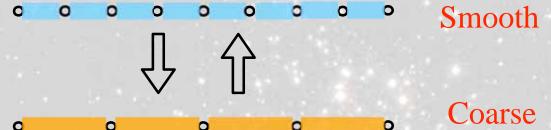
$$P' \quad a' \quad y'$$

- Apply conjugate gradient algorithm to transformed problem
- Choice of preconditioner M is critical to speed and accuracy
- Convergence now dependent on condition number of P' not P

## Multi-grid preconditioned CG



- This a multiple resolution solution
- Example: consider the problem Pa=y in 2 different grid sizes (coarse and smooth)

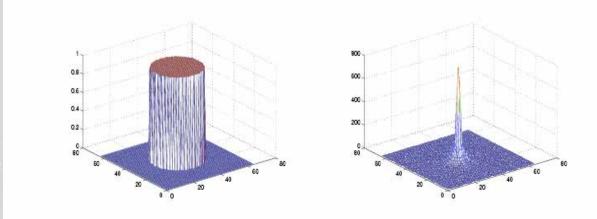


- Perform CG method with fast convergence for high frequencies to the smooth grid
- Project the low frequency error onto the coarser grid
- Perform CG method on the coarse grid
- Project the coarse grid solution back to the smooth grid
- Perform CG method on the smooth grid using high frequencies from the smooth grid solution and low frequencies from the coarse grid solution

### Fourier domain preconditioned CG



Key idea is to transform P to Fourier domain where F is Fourier transform matrix  $P' = F^{-1}PF$ 



Pupil Mask Fourier transform of pupil mask

- In spatial domain, pupil mask matrix is almost full
- In Fourier domain, truncate the FT of the pupil mask to only a few pixels
- This matrix is now sparse so far fewer matrix multiplies

## Complexity of methods

Approximate number of operations to solve: a = Rs where there are n actuators

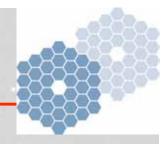
Method	Operations
Direct solve	O(n <sup>3</sup> )
Fourier transform reconstructor	O(n log n)
Multi-grid preconditioned CG	O(n log n)
Fourier domain preconditioned CG	O(n log n)

### Hardware approaches

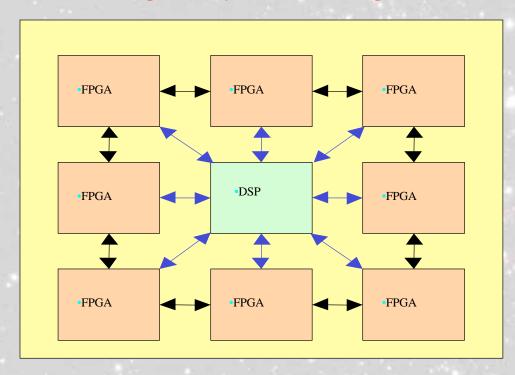


- Lick uses 2 Pentium processors for online and offline computation
- Need to use more processors and be able to split the problem into parallel blocks
- DSP Digital Signal Processor (a fast mathematical processor)
- FPGA Field Programmable Gate Array (lots and lots of logic gates)

## Hardware approach for TMT



- Proposed TMT hardware solution is to use combination of FPGAs and DSPs
- DSP does pixel processing (centroiding etc)
- FPGAs do tomography and fitting steps



# Mahalo!



