# Quadrilateral Quality

C.B. Hovey

July 5, 2022

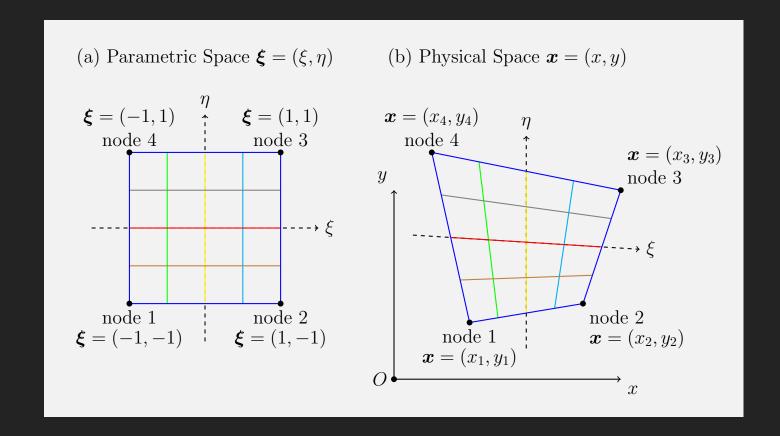


Figure 1: Parametric mapping  $\boldsymbol{x} = f(\boldsymbol{\xi})$  from parametric space to physical space.

#### Isoparametric Mapping 0.1

Let the parametric mapping  $f: \boldsymbol{\xi} \mapsto \boldsymbol{x}$  be defined as

$$x(\xi, \eta) = \sum_{a=1}^{4} N_a(\xi, \eta) \ x_a,$$

$$y(\xi, \eta) = \sum_{a=1}^{4} N_a(\xi, \eta) \ y_a,$$
(2)

$$y(\xi, \eta) = \sum_{a=1}^{4} N_a(\xi, \eta) y_a,$$
 (2)

where a nodal **shape function** is defined for each of the four nodes

$$N_1(\xi, \eta) \stackrel{\Delta}{=} \frac{1}{4} (1 - \xi)(1 - \eta),$$
 (3)

$$N_2(\xi, \eta) \stackrel{\Delta}{=} \frac{1}{4} (1 + \xi)(1 - \eta),$$
 (4)

$$N_3(\xi, \eta) \stackrel{\Delta}{=} \frac{1}{4} (1 + \xi)(1 + \eta),$$
 (5)

$$N_4(\xi, \eta) \stackrel{\Delta}{=} \frac{1}{4} (1 - \xi)(1 + \eta).$$
 (6)

## 0.2 Jacobian

For the quadrilateral element, the Jacobian J is calculated as the partial matrix of derivatives of  $\mathbf{x} = (x, y)$  with respect to  $\boldsymbol{\xi} = (\xi, \eta)$ ,

$$\boldsymbol{J}(\xi,\eta) \stackrel{\Delta}{=} \begin{bmatrix} \frac{\partial \boldsymbol{x}}{\partial \boldsymbol{\xi}} \end{bmatrix} = \begin{bmatrix} x,\xi & x,\eta \\ y,\xi & y,\eta \end{bmatrix}. \tag{7}$$

Substituting  $x(\xi, \eta)$  and  $y(\xi, \eta)$  with shape function equations (1)-(2) and expanding terms, the Jacobian takes the form

$$\boldsymbol{J}(\xi,\eta) = \frac{1}{4} \begin{bmatrix} -1+\eta & 1-\eta & 1+\eta & -1-\eta \\ -1+\xi & -1-\xi & 1+\xi & 1-\xi \end{bmatrix} \begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ x_3 & y_3 \\ x_4 & y_4 \end{bmatrix}.$$
(8)

The determinant of the Jacobian,  $det(\mathbf{J})$ , can be found to be

$$\det(\boldsymbol{J}(\xi,\eta)) = c_0 + c_1 \xi + c_2 \eta, \tag{9}$$

where

$$c_0 = \frac{1}{8} \left[ (x_1 - x_3)(y_2 - y_4) - (x_2 - x_4)(y_1 - y_3) \right], \tag{10}$$

$$c_1 = \frac{1}{8} \left[ (x_3 - x_4)(y_1 - y_2) - (x_1 - x_2)(y_3 - y_4) \right], \tag{11}$$

$$c_2 = \frac{1}{8} \left[ (x_2 - x_3)(y_1 - y_4) - (x_1 - x_4)(y_2 - y_3) \right]. \tag{12}$$

## 0.3 Quality

We follow *The Verdict Geometry Quality Library* documentation<sup>1</sup> and implementation<sup>2</sup> for the definitions of quality metrics. The SNL Cubit help manual is also helpful.<sup>3</sup>

#### 0.3.1 Preliminaries

Let the four edge vectors and their respective lengths be defined as

$$e_1 \stackrel{\Delta}{=} \boldsymbol{x}_2 - \boldsymbol{x}_1, \qquad \qquad \ell_1 \stackrel{\Delta}{=} \parallel \ \boldsymbol{e}_1 \parallel,$$
 (13)

$$\boldsymbol{e}_2 \stackrel{\Delta}{=} \boldsymbol{x}_3 - \boldsymbol{x}_2, \qquad \qquad \ell_2 \stackrel{\Delta}{=} \parallel \boldsymbol{e}_2 \parallel, \qquad (14)$$

$$e_3 \stackrel{\Delta}{=} x_4 - x_3, \qquad \qquad \ell_3 \stackrel{\Delta}{=} \parallel e_3 \parallel, \qquad \qquad (15)$$

$$\boldsymbol{e}_4 \stackrel{\Delta}{=} \boldsymbol{x}_1 - \boldsymbol{x}_4, \qquad \qquad \ell_4 \stackrel{\Delta}{=} \parallel \boldsymbol{e}_4 \parallel . \tag{16}$$

The two (non-normalized) principal axes are the defined though vector addition of the two opposing side lengths

$$\boldsymbol{X} \stackrel{\Delta}{=} \boldsymbol{e}_1 - \boldsymbol{e}_3 = (\boldsymbol{x}_2 - \boldsymbol{x}_1) - (\boldsymbol{x}_4 - \boldsymbol{x}_3), \tag{17}$$

$$Y \stackrel{\Delta}{=} e_2 - e_4 = (x_3 - x_2) - (x_1 - x_4).$$
 (18)

<sup>&</sup>lt;sup>1</sup>Knupp PM, Ernst CD, Thompson DC, Stimpson CJ, Pebay PP. The verdict geometric quality library. Sandia National Laboratories (SNL), Albuquerque, NM, and Livermore, CA (United States); 2006 Mar 1. OSTI <a href="https://www.osti.gov/servlets/purl/901967">https://www.osti.gov/servlets/purl/901967</a>.

<sup>&</sup>lt;sup>2</sup>See https://github.com/Kitware/VTK/blob/master/ThirdParty/verdict/vtkverdict/ and in particular, the quad\_scaled\_jacobian function in the V\_QuadMetric.cpp implementation.

 $<sup>{\</sup>rm ^3See\ https://cubit.sandia.gov/files/cubit/16.04/help\_manual/WebHelp/cubithelp.htm}$ 

At each vertex, there is a normal vector and its respective normalized unit vector

$$\mathbf{N}_1 \stackrel{\Delta}{=} \mathbf{e}_4 \times \mathbf{e}_1, \qquad \hat{\mathbf{n}}_1 \stackrel{\Delta}{=} \mathbf{N}_1 / \parallel \mathbf{N}_1 \parallel,$$
 (19)

$$\mathbf{N}_2 \stackrel{\Delta}{=} \mathbf{e}_1 \times \mathbf{e}_2, \qquad \hat{\mathbf{n}}_2 \stackrel{\Delta}{=} \mathbf{N}_2 / \parallel \mathbf{N}_2 \parallel,$$
 (20)

$$\mathbf{N}_3 \stackrel{\Delta}{=} \mathbf{e}_2 \times \mathbf{e}_3, \qquad \hat{\mathbf{n}}_3 \stackrel{\Delta}{=} \mathbf{N}_3 / \parallel \mathbf{N}_3 \parallel,$$
 (21)

$$\mathbf{N}_4 \stackrel{\Delta}{=} \mathbf{e}_3 \times \mathbf{e}_4, \qquad \hat{\mathbf{n}}_4 \stackrel{\Delta}{=} \mathbf{N}_4 / \parallel \mathbf{N}_4 \parallel .$$
 (22)

At the center of the element, there is principal axis normal as well

$$\mathbf{N}_c \stackrel{\Delta}{=} \mathbf{X} \times \mathbf{Y}, \qquad \hat{\mathbf{n}}_c \stackrel{\Delta}{=} \mathbf{N}_c / \parallel \mathbf{N}_c \parallel .$$
 (23)

There are four contributions to the quadrilateral area from each of the four nodal areas

$$\alpha_1 \stackrel{\Delta}{=} \mathbf{N}_1 \cdot \hat{\mathbf{n}}_c, \tag{24}$$

$$\alpha_2 \stackrel{\Delta}{=} \mathbf{N}_2 \cdot \hat{\mathbf{n}}_c, \tag{25}$$

$$\alpha_3 \stackrel{\Delta}{=} N_3 \cdot \hat{n}_c,$$
 (26)

$$\alpha_4 \stackrel{\Delta}{=} \mathbf{N}_4 \cdot \hat{\mathbf{n}}_c.$$
 (27)

<sup>&</sup>lt;sup>4</sup> It may be tempting to (erroneously) write  $\hat{\boldsymbol{n}}_1 \stackrel{\text{2D}}{\longrightarrow} \hat{\boldsymbol{n}}_2 \stackrel{\text{2D}}{\longrightarrow} \hat{\boldsymbol{n}}_3 \stackrel{\text{2D}}{\longrightarrow} \hat{\boldsymbol{n}}_4 \stackrel{\text{2D}}{\longrightarrow} \hat{\boldsymbol{n}}_c$  and  $\alpha_1 \stackrel{\text{2D}}{\longrightarrow} \parallel \boldsymbol{N}_1 \parallel, \alpha_2 \stackrel{\text{2D}}{\longrightarrow} \parallel \boldsymbol{N}_2 \parallel$ ,  $\alpha_3 \stackrel{\text{2D}}{\longrightarrow} \parallel \boldsymbol{N}_3 \parallel, \alpha_4 \stackrel{\text{2D}}{\longrightarrow} \parallel \boldsymbol{N}_4 \parallel$  given that for the 2D quadrilateral case, all unit norms are in the same plane. The problem with such a construction is that it destroys the sign information carried by each normal vector. For the non-degenerate case, the foregoing simplification is true, since all give normals will carry the same sign. However, for degenerate cases, such as when a quadrilateral folds over onto itself, the sign information is no longer homogenous, and the sign information *must* be retained to accurately calculate Jacobian metrics that go negative.

## 0.3.2 Signed Area

The **signed area** SA is defined as the average of all nodal area contributions:

$$SA \stackrel{\Delta}{=} \frac{\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4}{4}.$$
 (28)

The metric dimension is  $L^2$  and the idea (unit square) value is 1.0.

## 0.3.3 Aspect Ratio

The **aspect ratio** AR is defined as the maximum edge length ratios taken at the quadrilateral center. This can be expressed in terms of the norms of the principal axes as

$$AR = \max\left(\frac{\parallel \boldsymbol{X} \parallel}{\parallel \boldsymbol{Y} \parallel}, \frac{\parallel \boldsymbol{Y} \parallel}{\parallel \boldsymbol{X} \parallel},\right)$$
 (29)

Alternatively, the perimeter length multiplied by the maximum side length, divided by four times the area to define a triangle aspect ratio that is meaningful for quadrilaterals, with dimension  $L^0$  and acceptable range [1.0, 1.3].

 $<sup>^5</sup>$ Robinson J. CRE method of element testing and the Jacobian shape parameters. Engineering Computations. 1987 Feb 1.

<sup>&</sup>lt;sup>6</sup>Knupp 2006, op. cit. at 38.

#### 0.3.4 Minimum Jacobian

The Minimum Jacobian  $J_{\min}$  is defined as the minimum pointwise area of local map at the four corners and center of quadrilateral<sup>7</sup>

$$J_{\min} \stackrel{\Delta}{=} \min \left( \alpha_1, \alpha_2, \alpha_3, \alpha_4 \right). \tag{30}$$

### 0.3.5 Minimum Scaled Jacobian

The Minimum Scaled Jacobian  $\hat{J}_{min}$  is the minimum nodal area divided by the lengths of the two edge vector connecting that point<sup>8</sup>

$$\hat{J}_{\min} \stackrel{\Delta}{=} \min \left( \frac{\alpha_1}{\ell_4 \ell_1}, \frac{\alpha_2}{\ell_1 \ell_2}, \frac{\alpha_3}{\ell_2 \ell_3}, \frac{\alpha_4}{\ell_3 \ell_4} \right), \tag{31}$$

We warned previously in Footnote 4 for Jacobians that errors may result if sign information is not properly retained. We note a similar admonishment for Scaled Jacobians, since the latter is a function of the former.

The dimension is  $L^0$ . The full range is [-1.0, 1.0]. The acceptable range is typically taken as [0.3, 1.0] in the generous case and [0.5, 1.0] in the more restricted case.

<sup>&</sup>lt;sup>7</sup>Knupp 2006, op. cit. at 42.

<sup>&</sup>lt;sup>8</sup>Knupp 2006, op. cit. at 51.

<sup>&</sup>lt;sup>9</sup>It may (again) be tempting to (erroneously) write for the 2D case  $\hat{J}_{\min} \xrightarrow{2D} \min(\sin \theta_1, \sin \theta_2, \sin \theta_3, \sin \theta_4)$ , where  $\theta_1$  is the angle between  $e_4$  and  $e_1$ ,  $\theta_2$  with  $e_1$  and  $e_2$ ,  $\theta_3$  with  $e_2$  and  $e_3$ , and  $\theta_4$  with  $e_3$  and  $e_4$ . Such a simplification will only work if  $\theta$  is retained as a vector quantity (thus retaining the sign). If  $\theta$  is considered only as a scalar, errors will result when the Jacobian metric goes negative.