

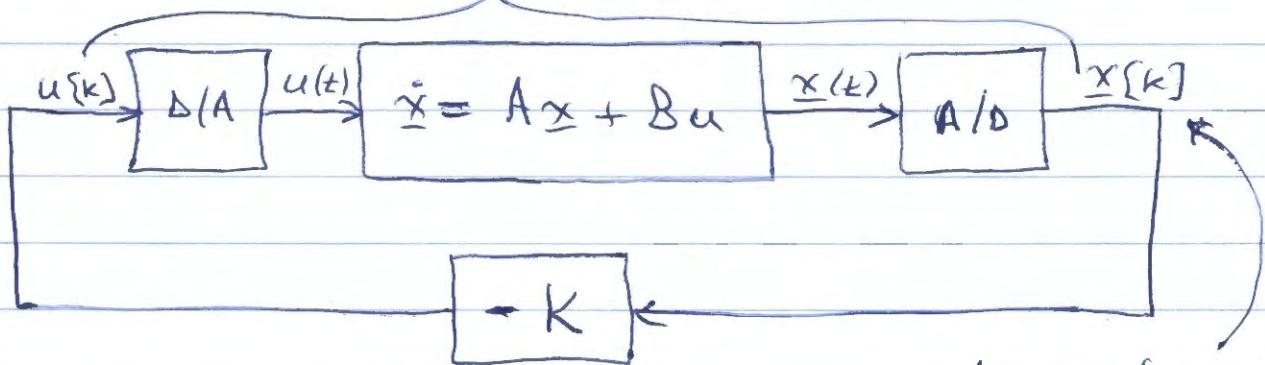
How about the phase margin estimate?

$$\hat{\phi}_{\max} = 2 \sin^{-1} \left(\frac{.5}{2} \right) = 29^\circ$$

Very close to the classical guideline and it is valid for all plant inputs simultaneously.

Observers (Chapter 7)

Motivation: if we want to control a plant by state feedback, we need to measure all of the state variables. For example, a digital state-feedback regulator: zOH equivalent (Φ , Γ)



have to measure all the state variables

Recall, for the cart-pendulum system the state variables are:

x_1 - pendulum angular position - measured w/ encoder

x_2 - " " velocity - not measured!

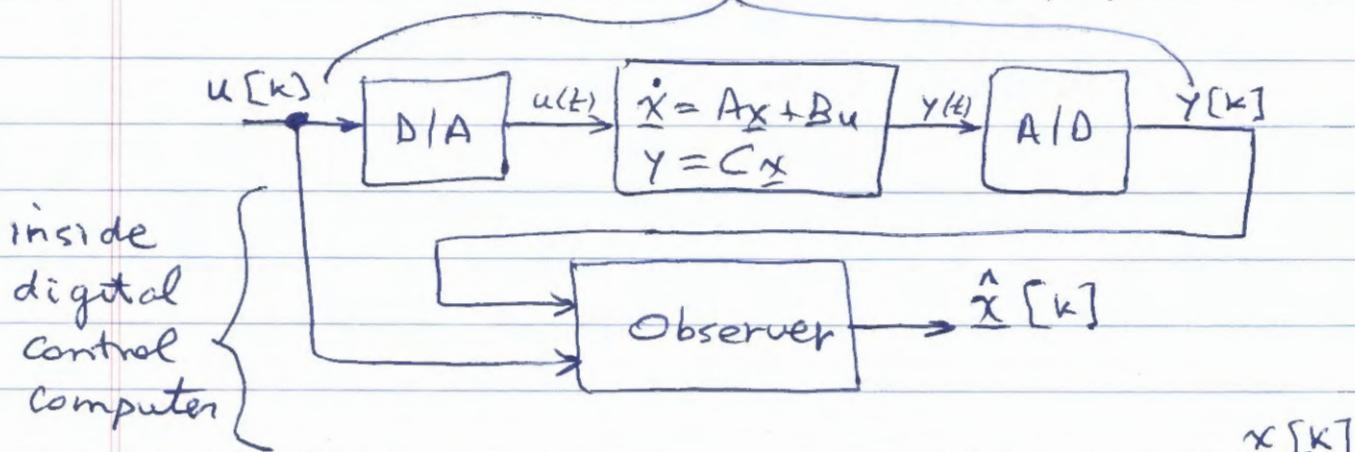
x_3 - motor angular position - measured w/ encoder

x_4 - " " velocity - not measured!

Suppose only the plant output $y = C\hat{x}$ is measured? (Assume y is one signal for now.)

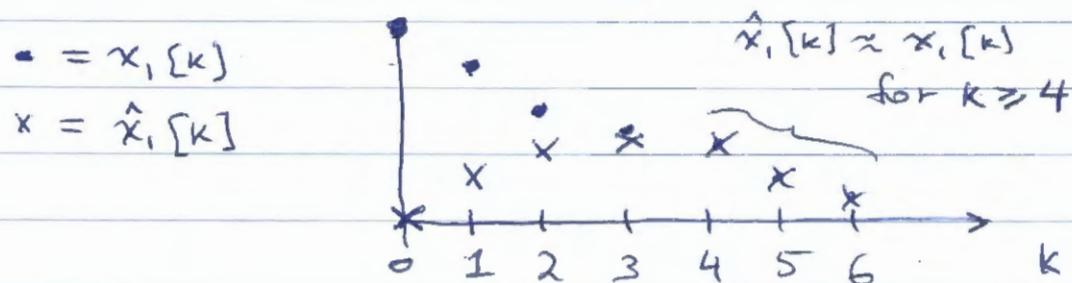
A digital observer is a system that takes $u[k]$ and $y[k]$ as inputs and produces an estimate $\hat{x}[k]$ of the plant state vector $\underline{x}(t)|_{t=kT}$

ZOH Equivalent is (Φ, Γ, C)



The desired behavior is $\hat{x}[k] \rightarrow \underline{x}(kT) = \underline{x}[k]$ as k increases

Look at one state variable, say $x_1[k]$



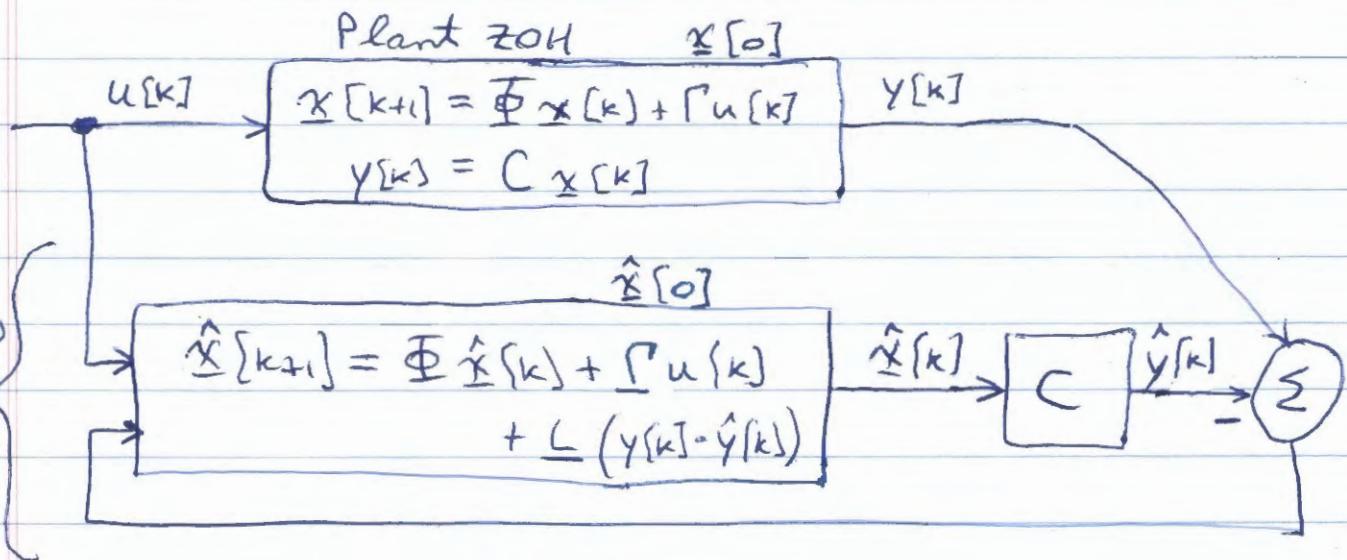
In this example, the observer settling time is $T_{so} = 4T$ seconds

T_{so} is the amount of time it takes for \hat{x} to converge to x .

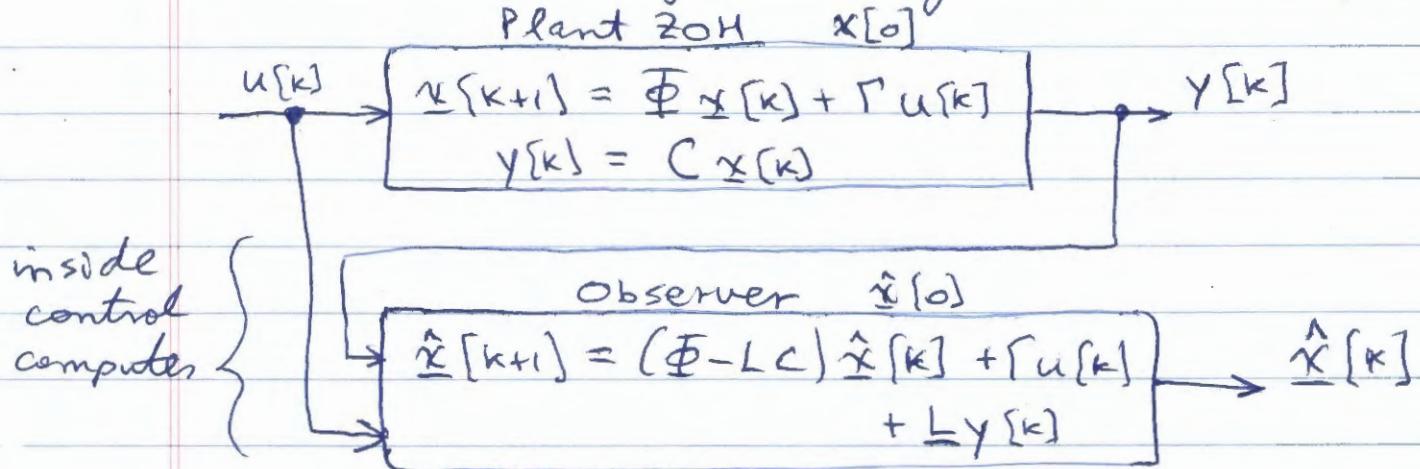
Note that observer has to "hit" n moving targets (each of the n plant state variables).

Derive observer equation as follows:

- (1) Copy the plant ZOH equation
- (2) Add a correction term through an observer gain vector $L = \begin{bmatrix} l_1 \\ l_2 \\ \vdots \\ l_n \end{bmatrix}$ (for a single-output plant).



Re-draw this diagram using the fact that $\hat{y}[k] = C \hat{x}[k]$



Calculate L so that $\hat{x}[k] \rightarrow x[k]$

Analyze observer performance:

Define an error vector: $\underline{e}[k] = \underline{x}[k] - \hat{\underline{x}}[k]$

true
plant
state vector

observer
estimate

Assume $\underline{e}[0] \neq 0$

The goal is $\underline{e}[k] \rightarrow 0$. That is, the observer should drive the error vector to zero.

This is similar to a state-feedback regulator driving the plant state vector to zero, $\underline{x}[k] \rightarrow 0$.

From the block diagram at the bottom of page 52 we can write the following:

$$\begin{aligned} \underline{e}[k+1] &= \underline{x}[k+1] - \hat{\underline{x}}[k+1] \quad (\text{by the definition}) \\ &\quad \text{of } \underline{e}[k] \\ &= \left\{ \Phi \underline{x}[k] + \Gamma \underline{u}[k] \right\} - \left\{ (\Phi - Lc) \hat{\underline{x}}[k] + \Gamma \underline{u}[k] \right. \\ &\quad \left. + Lc \underline{x}[k] \right\} \\ &= \Phi \underline{x}[k] - (\Phi - Lc) \hat{\underline{x}}[k] - Lc \underline{x}[k] \\ &= (\Phi - Lc) \underline{x}[k] - (\Phi - Lc) \hat{\underline{x}}[k] \\ &= (\Phi - Lc) (\underline{x}[k] - \hat{\underline{x}}[k]) \end{aligned}$$

$$\underline{e}[k+1] = (\Phi - Lc) \underline{e}[k], \underline{e}[0] \neq 0$$

We have seen an equation of this form twice before, in Chap. 3 and in Chap. 6.

Chapter 3

$$\text{solution} \rightarrow \underline{x}[k+1] = A \underline{x}[k]$$

$$\underline{x}[k] = A^k \underline{x}_0$$

$\underline{x}[k] \rightarrow 0$ if all eigenvalues of A are inside the unit circle

Chapter 6

State feedback regulator:

$$\underline{x}[k+1] = (\Phi - \Gamma K) \underline{x}[k]$$

$\underline{x}[k] \rightarrow 0$ if all eigenvalues of $\Phi - \Gamma K$ are inside the unit circle.

Calculate K to make this happen. (Choose poles, map to z -polar = $\exp(T * s$ -poles).

Chapter 7 Observer Design (see bottom of pg 53)

$$\underline{e}[k+1] = (\Phi - LC) \underline{e}[k]$$

$\underline{e}[k] \rightarrow 0$ if all eigenvalues of $\Phi - LC$ are inside the unit circle.

Look more carefully at the two problems:

