

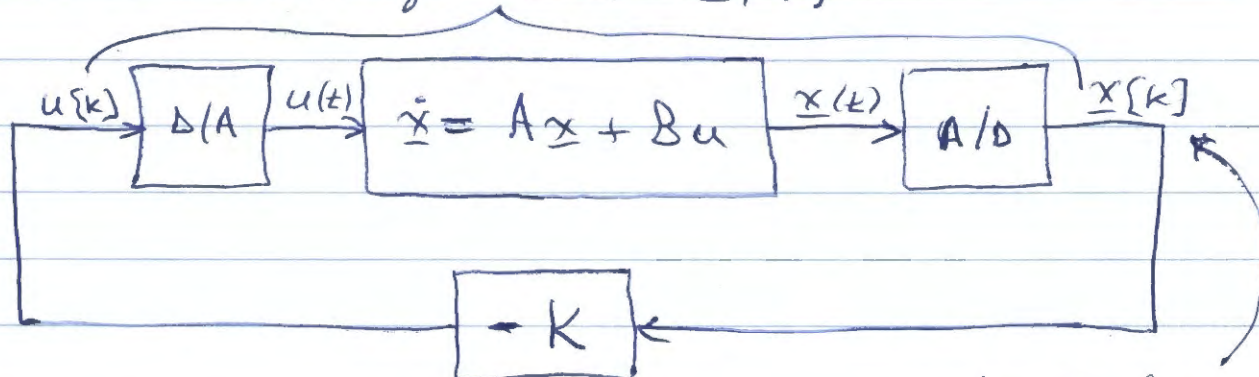
How about the phase margin estimate?

$$\hat{\phi}_{\max} = 2 \sin^{-1} \left( \frac{.5}{2} \right) = 29^\circ$$

Very close to the classical guideline and it is valid for all plant inputs simultaneously.

## Observers (Chapter 7)

Motivation: if we want to control a plant by state feedback, we need to measure all of the state variables. For example, a digital state-feedback regulator: ZOH equivalent ( $\Phi, \Gamma$ )



have to measure all the state variables

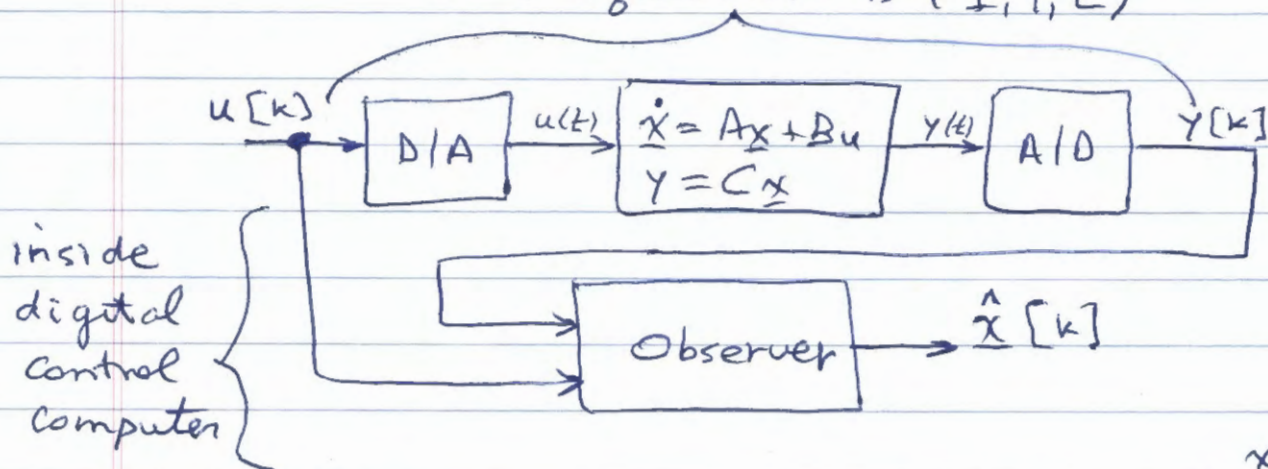
Recall, for the cart-pendulum system the state variables are:

- $x_1$  - pendulum angular position - measured w/ encoder
- $x_2$  - " " velocity - not measured!
- $x_3$  - motor angular position - measured w/ encoder
- $x_4$  - " " velocity - not measured!

Suppose only the plant output  $y = C\underline{x}$  is measured? (Assume  $y$  is one signal for now.)

A digital observer is a system that takes  $u[k]$  and  $y[k]$  as inputs and produces an estimate  $\hat{\underline{x}}[k]$  of the plant state vector  $\underline{x}(t)|_{t=k.T}$

ZOH Equivalent is  $(\Phi, \Gamma, C)$

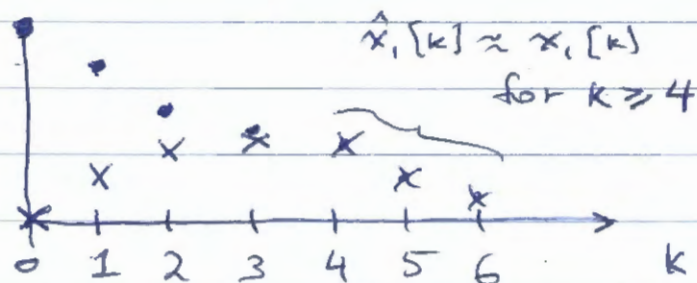


The desired behavior is  $\hat{\underline{x}}[k] \rightarrow \underline{x}(kT) = \underline{x}[k]$  as  $k$  increases

Look at one state variable, say  $x_1[k]$

$$\bullet = x_1[k]$$

$$\times = \hat{x}_1[k]$$



In this example, the observer settling time is

$$T_{so} = 4.T \text{ seconds}$$

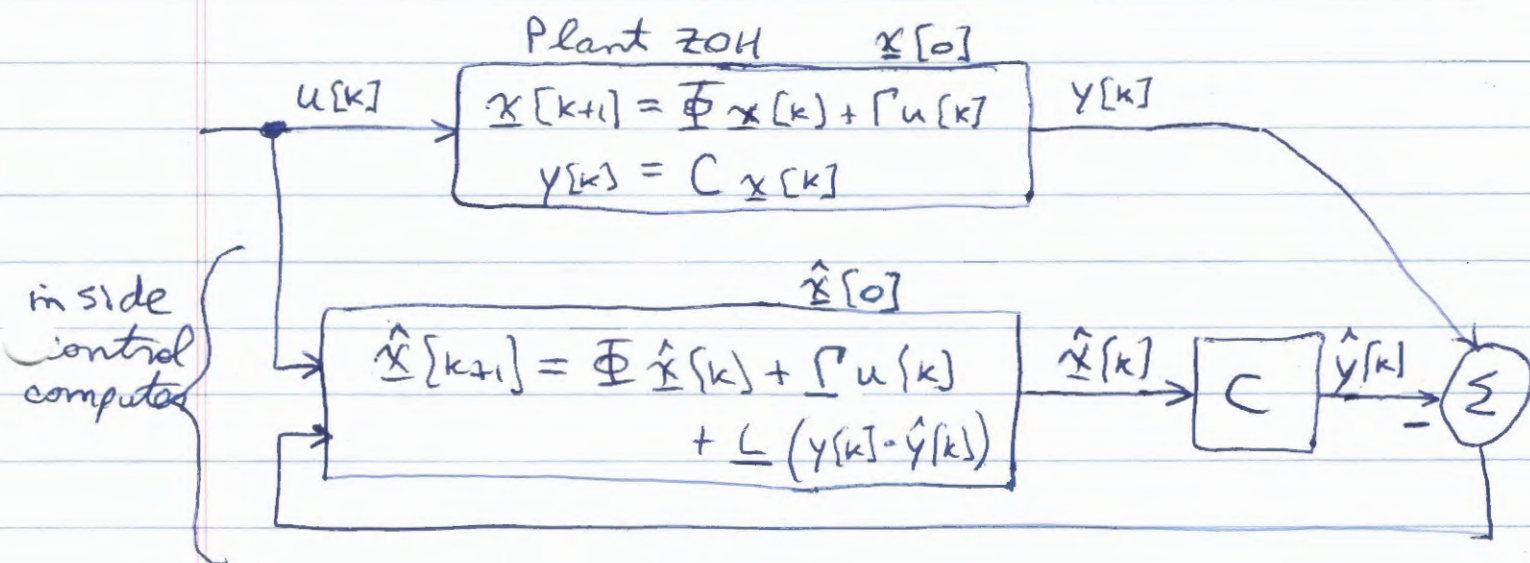
$T_{so}$  is the amount of time it takes for  $\hat{\underline{x}}$  to converge to  $\underline{x}$ .



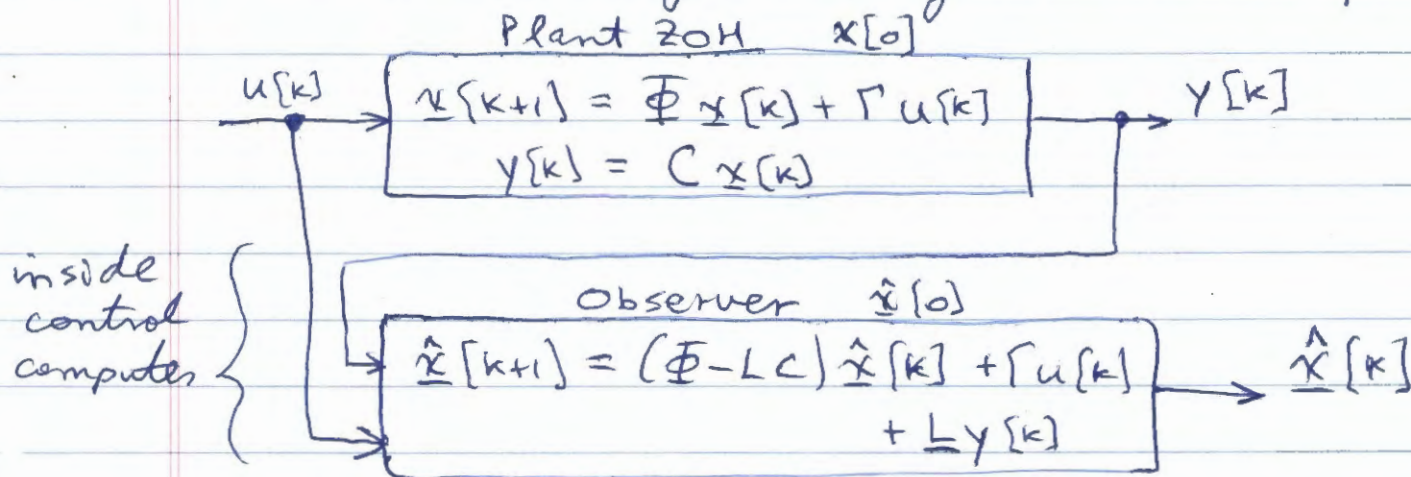
Note that observer has to "hit"  $n$  moving targets (each of the  $n$  plant state variables).

Derive observer equation as follows:

- (1) Copy the plant ZOH equation
- (2) Add a correction term through an observer gain vector  $\underline{L} = \begin{bmatrix} l_1 \\ l_2 \\ \vdots \\ l_n \end{bmatrix}$  (for a single-output plant).



Re-draw this diagram using the fact that  $\hat{y}[k] = C \hat{\underline{x}}[k]$



Calculate  $\underline{L}$  so that  $\hat{\underline{x}}[k] \rightarrow \underline{x}[k]$

Analyze observer performance:

Define an error vector:  $\underline{e}[k] = \underline{x}[k] - \hat{\underline{x}}[k]$

true plant state vector
observer estimate

Assume  $\underline{e}[0] \neq 0$

The goal is  $\underline{e}[k] \rightarrow 0$ . That is, the observer should drive the error vector to zero.

This is similar to a state-feedback regulator driving the plant state vector to zero,  $\underline{x}[k] \rightarrow 0$ .

From the block diagram at the bottom of page (52) we can write the following:

$$\begin{aligned}
 \underline{e}[k+1] &= \underline{x}[k+1] - \hat{\underline{x}}[k+1] \quad (\text{by the definition of } \underline{e}[k]) \\
 &= \left\{ \Phi \underline{x}[k] + \Gamma u[k] \right\} - \left\{ (\Phi - LC) \hat{\underline{x}}[k] + \Gamma u[k] + LC \underline{x}[k] \right\} \\
 &= \Phi \underline{x}[k] - (\Phi - LC) \hat{\underline{x}}[k] - LC \underline{x}[k] \\
 &= (\Phi - LC) \underline{x}[k] - (\Phi - LC) \hat{\underline{x}}[k] \\
 &= (\Phi - LC) (\underline{x}[k] - \hat{\underline{x}}[k])
 \end{aligned}$$

$$\underline{e}[k+1] = (\Phi - LC) \underline{e}[k], \quad \underline{e}[0] \neq 0$$

We have seen an equation of this form twice before, in Chap. 3 and in Chap. 6.



Chapter 3

solution  $\begin{cases} x[k+1] = A x[k] \\ x[k] = A^k x_0 \end{cases}$

$x[k] \rightarrow 0$  if all eigenvalues of  $A$  are inside the unit circle

Chapter 6

state feedback regulator:

$$x[k+1] = (\Phi - \Gamma K) x[k]$$

$x[k] \rightarrow 0$  if all eigenvalues of  $\Phi - \Gamma K$  are inside the unit circle.

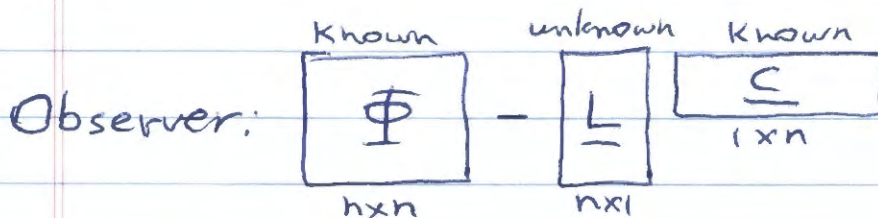
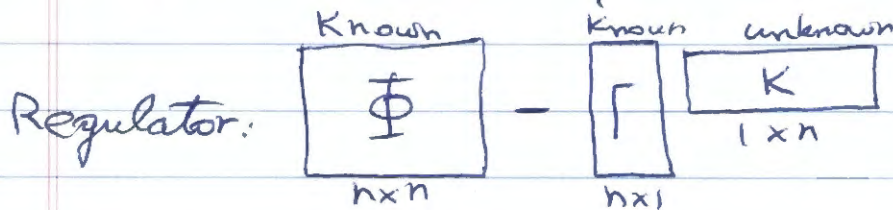
Calculate  $K$  to make this happen. (Choose poles, map to zpoles =  $\exp(T * \text{poles})$ ).

Chapter 7 Observer Design (see bottom of pg 53)

$$e[k+1] = (\Phi - LC) e[k]$$

$e[k] \rightarrow 0$  if all eigenvalues of  $\Phi - LC$  are inside the unit circle.

Look more carefully at the two problems:



not identical problems