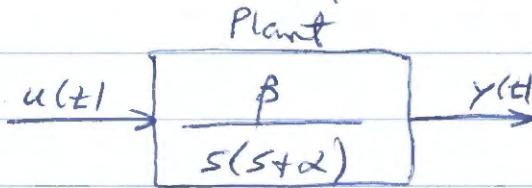


Read sections 4.6, 4.7, 4.8
in book

Consider a typical positioning system
(e.g. a motor-driven system):

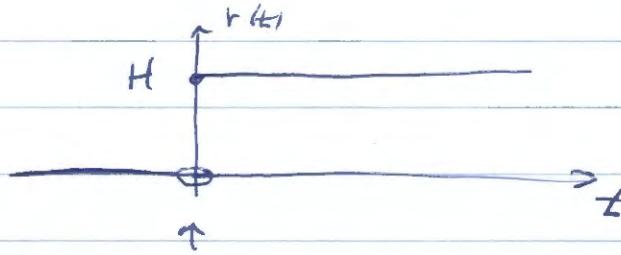


$$\alpha, \beta > 0$$

The system we want to control is called the "plant"

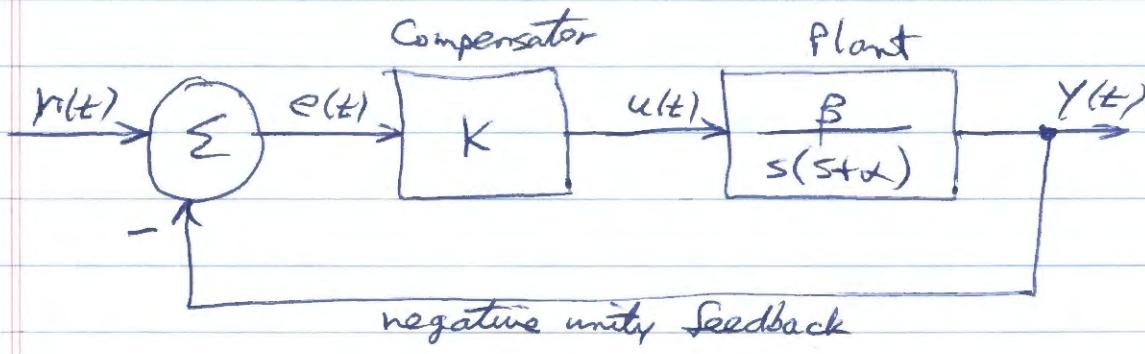
$u(t)$ = voltage applied to motor power amplifier (volts)
 $y(t)$ = sensor signal measuring motor position (radians)

Suppose the motor is at initial position $y(0) = 0$ and we want to command it to go to H radians. We can use the reference command signal $r(t)$:



The step command is given at time zero.

The simplest type of analog (continuous-time) control system is a negative unity feedback system with proportional control:

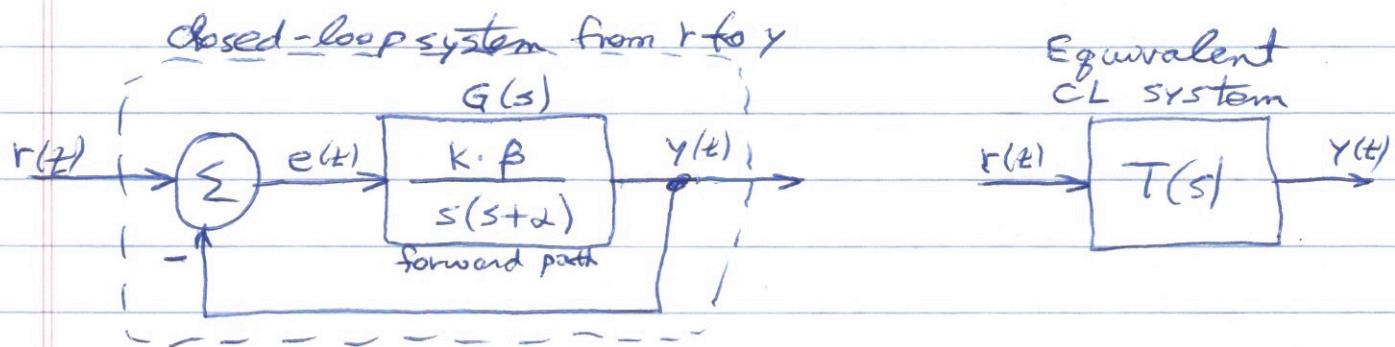


K is a gain (called the proportional gain) ②
 Note that $u(t) = k \cdot e(t)$. The plant input is proportional to the error signal $e(t)$.

How does this type of control system behave for different values of K ?

Can we calculate a "good" value of K ?

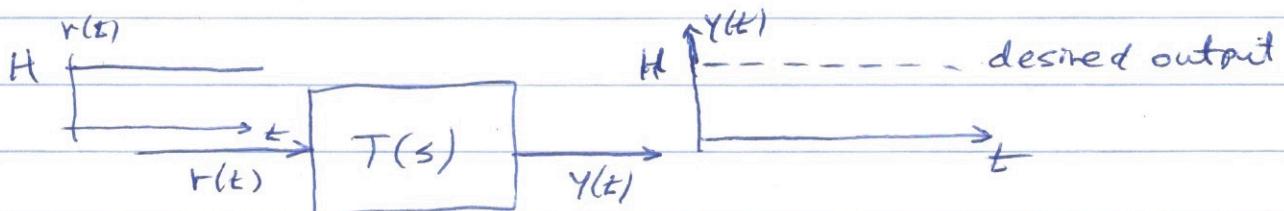
The previous block diagram may be re-drawn as follows:



Using the "feedback formula" the system from $r(t)$ to $y(t)$ is

$$T(s) = \frac{G(s)}{1 + G(s)}$$

$$T(s) = \frac{\frac{K\beta}{s(s+\alpha)}}{1 + \frac{K\beta}{s(s+\alpha)}} \times \frac{s(s+\alpha)}{s(s+\alpha)} = \frac{K\beta}{s(s+\alpha) + K\beta} = \frac{K\beta}{s^2 + s\alpha + K\beta}$$



Does $y(t) \rightarrow H$?

Recall that $T(s)$ (Laplace transform of output) equals transfer function times $R(s)$, or

(3)

$$Y(s) = T(s) R(s)$$

$$R(s) = \frac{H}{s} \quad (\text{see Table 3.2 p. 84})$$

Also, the Final Value Theorem (Table 3.1 p. 83)
says

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s Y(s)$$

we want to know calculate this for
 if this equals H our problem

$$= \lim_{s \rightarrow 0} s \cdot T(s) \cdot \frac{H}{s}$$

$$= T(0) \cdot H$$

$$= \frac{K \cdot B \cdot H}{K \cdot B} = H$$

So $y(t) \rightarrow H$ as t gets large.

What about the transient response when $y(t)$ is moving from 0 to H?

- How long does it take to get to H?
- Is there overshoot and/or oscillation?

Recall that $y(t)$ is the step response of

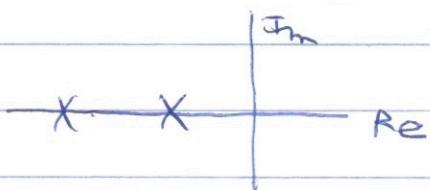
$$T(s) = \frac{KB}{s^2 + \alpha s + KB}$$

The poles of this system are the roots of $s^2 + \alpha s + KB$.

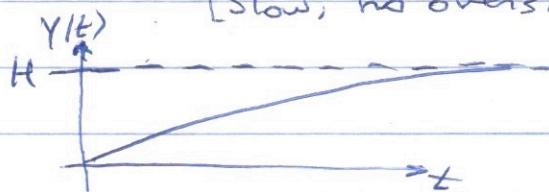
For fixed values of α and B (i.e., a given plant model) the pole locations change as a function of K

There are three possibilities (for fixed α, β):

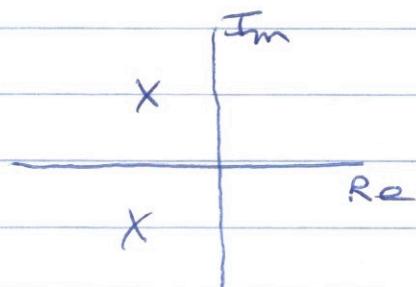
- (a) The poles could be real and unequal



Response is overdamped
[slow, no overshoot]



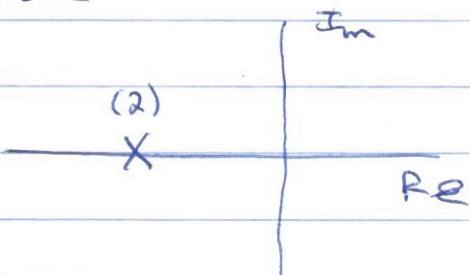
- (b) The poles could be a complex-conjugate pair



Response is underdamped
[fast, overshoot, oscillatory]

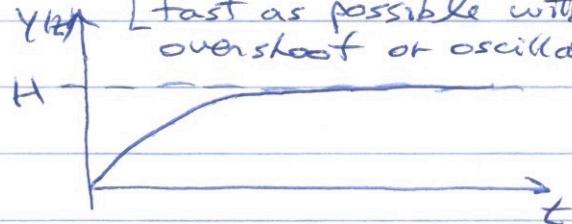


- (c) Could have a double pole



Response is critically damped

[fast as possible with no overshoot or oscillation.]



By selecting a value for the proportional gain, K , we can create a control system with any of these responses.

General principle: write down what you have and set it equal to what you want!

(5)

We have the denominator of $T(s) : s^2 + \alpha s + K\beta$

We want $(s+p)^2$, which has a double pole
 $(s+p)(s+p) = s^2 + 2ps + p^2$ at $-p$. (The number p is unknown)

Set

$$s^2 + \alpha s + K\beta = s^2 + 2ps + p^2$$

Equate corresponding powers of s :

$$s^2 : 1 = 1$$

$$s : \alpha = 2p \Rightarrow p = \frac{\alpha}{2} \quad \begin{array}{l} \text{(the repeated pole)} \\ \text{will occur at} \\ s = -\frac{\alpha}{2} \end{array}$$

$$\text{constant: } K\beta = p^2$$

$$K = \frac{p^2}{\beta} = \boxed{\frac{\alpha^2}{4\beta}}$$

this gain value gives critical damping

end/1/23

Look at the roots of the denominator polynomial
 $s^2 + \alpha s + K\beta$ (use quadratic formula) (CL poles).

$$\text{poles} = -\frac{\alpha}{2} \pm \frac{\sqrt{\alpha^2 - 4K\beta}}{2}$$

$$-\frac{b}{2} \pm \frac{\sqrt{b^2 - 4ac}}{2}$$

$K=0 \Rightarrow$ poles are $-\alpha, 0$

$0 < K < \frac{\alpha^2}{4\beta} \Rightarrow$ poles are real and unequal (overdamped)

$K = \frac{\alpha^2}{4\beta} \Rightarrow$ repeated real poles (critically damped)
at $-\frac{\alpha}{2}$

$K > \frac{\alpha^2}{4\beta} \Rightarrow$ complex conjugate poles (underdamped)
with real part $-\frac{\alpha}{2}$

(6)

Plant used in HW 1: $\beta = 2,400$
 $\alpha = 22$ so plant

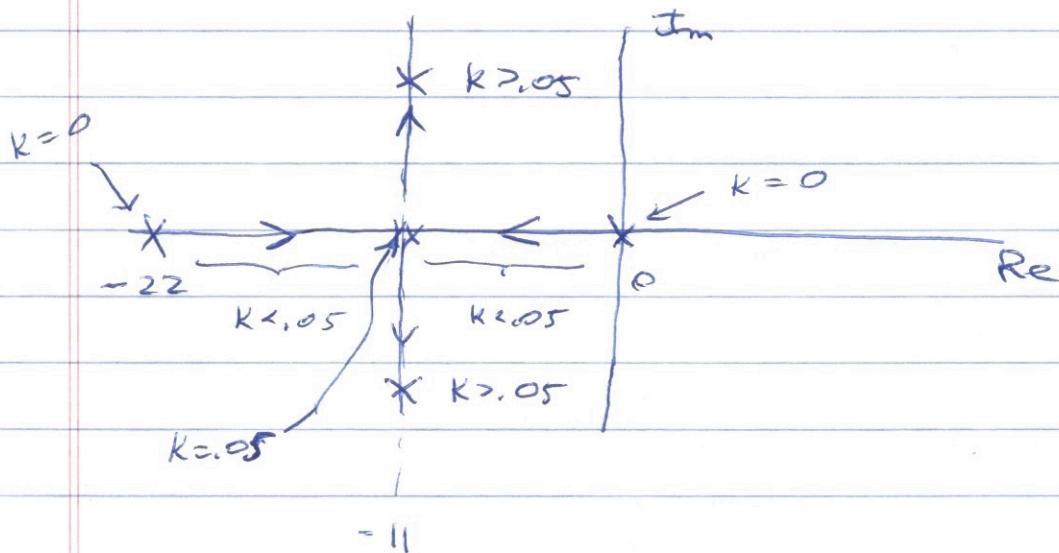
is $\frac{2,400}{s(s+22)}$

With $K = \frac{\alpha^2}{4\beta} = \frac{(22)^2}{4 \cdot 2,400}$

$K = 0.05 \Rightarrow$ CL system has double pole at -11 .

Denominator of $T(s)$ is $s^2 + \alpha \cdot s + K \cdot \beta$

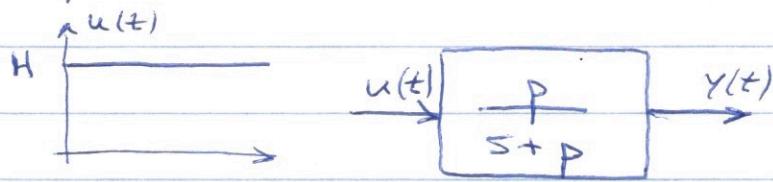
CL Poles as a function of gain:



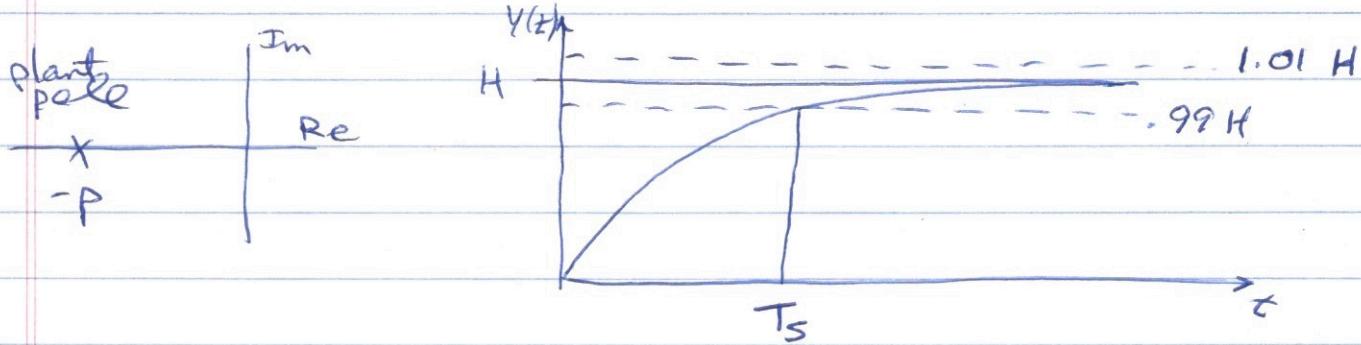
Relationship Between Pole Locations and settling Time

Def The 1% settling time T_S is the time at which the step response enters and stays within $\pm 1\%$ of its desired value, H .

Consider a first-order system with a step input:



$$y(t) = H(1 - e^{-Pt}) \quad (\text{see Table 3.2})$$



The settling time is found as follows:

$$y(t) \Big|_{t=T_s} = .99H$$

or

$$H(1 - e^{-P \cdot T_s}) = .99H$$

$$0.01 = e^{-P \cdot T_s}$$

$$\ln(0.01) = -P \cdot T_s$$

$$T_s = \frac{-\ln(0.01)}{P} = \boxed{\frac{4.62}{P}}$$

settling time for
first-order system
with pole at $-P$.

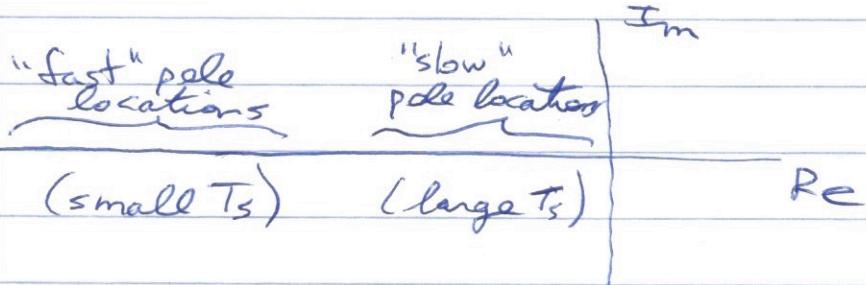
Note: I have rounded

$$-\ln(0.01) = 4.6052$$

up to a nice number 4.62

When p is a large number T_s is small ("fast" system).

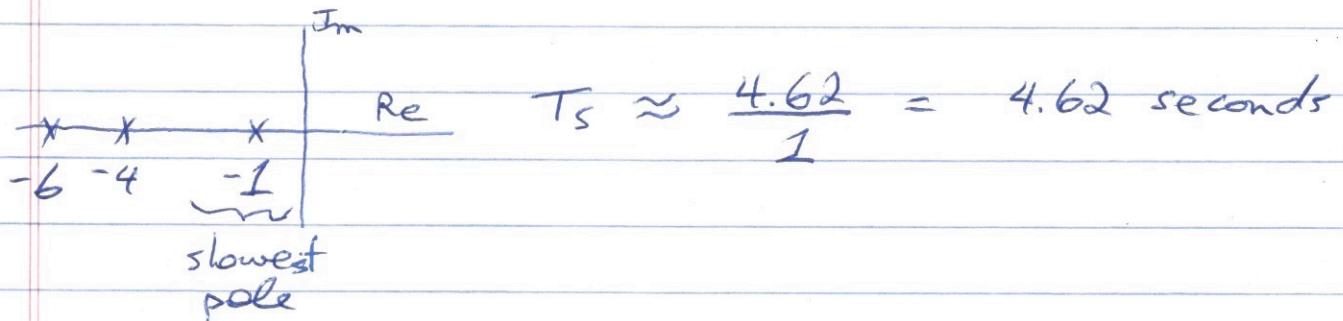
When p is a small number T_s is large ("slow" system).



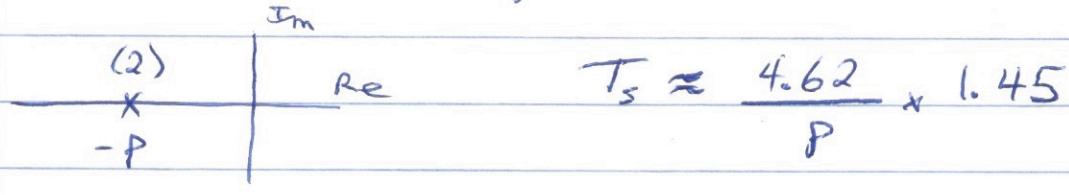
How about higher-order systems?

For systems with more than one pole, the settling time is approximately equal to the settling time of the slowest pole.

Example : 3rd-order system



For a double pole at $-p$ there is a 45% increase in settling time:

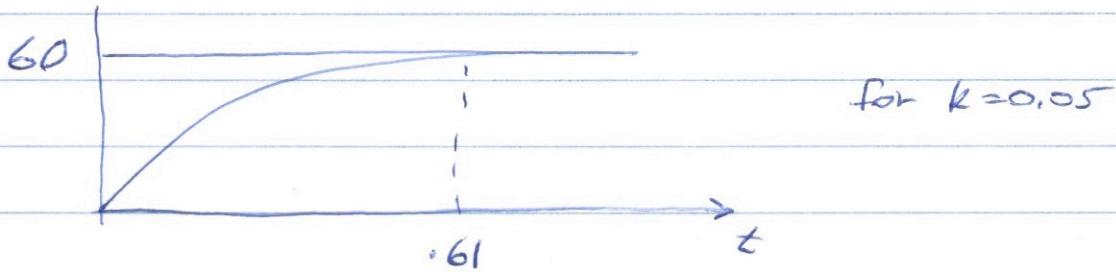


9

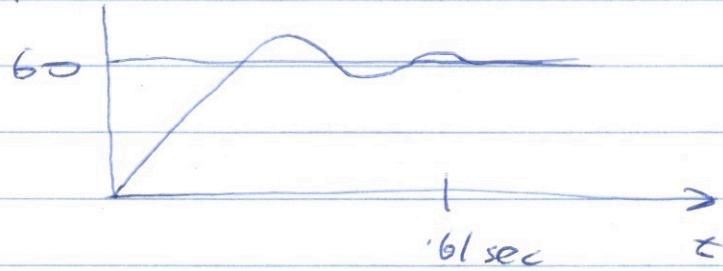
For the HW 1 proportional control system the closed-loop system has a double pole at -11 . Therefore the settling time is

$$T_s = \frac{4.62}{11} \times 1.45 = .61 \text{ sec}$$

We expect the following step response:



If we make the proportional gain $K > 0.05$ the system will be "faster" but will have overshoot and oscillation



Can we get a faster system without overshoot?

Also, the hardware plant has the constraint that

$$|u(t)| \leq 5 \quad (\text{plant input signal must be less than } 5 \text{ volts})$$