



# Mobile Robots Lab

## Localization using magnets

### Presentation

# The robot and the magnet sensor



# The reed switch



A normally open reed switch.

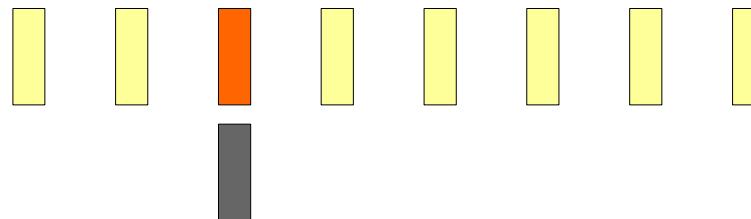
In a sufficiently intense magnetic field, the switch closes.

# The magnet sensor



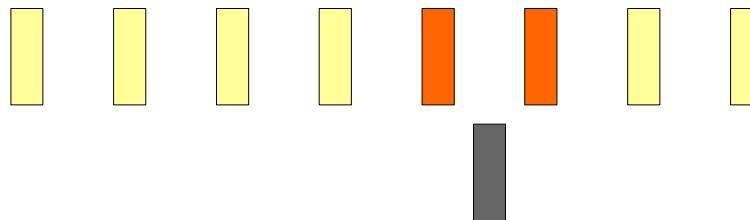
No magnet in the vicinity of the reed switches: all are open

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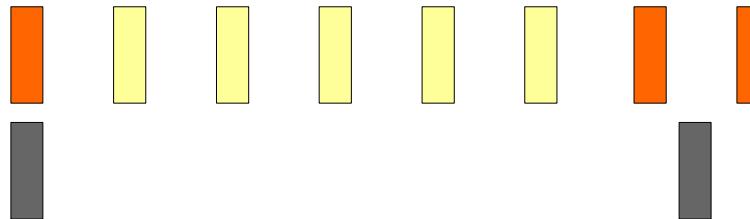
A magnet is right under reed switch 3, which is closed.

# The magnet sensor



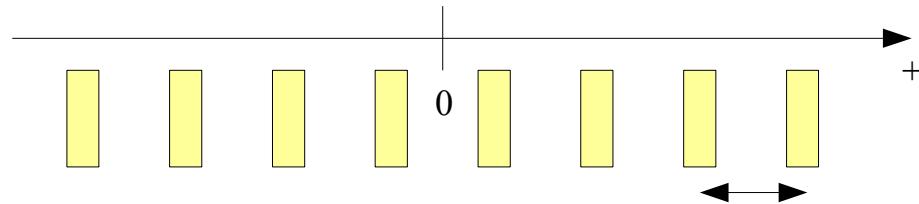
A magnet is right under switches 5 and 6, which are closed.

The measurement vector is a 2 vector

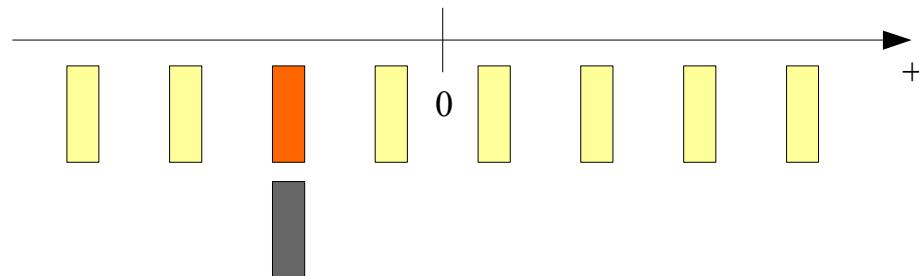


A magnet is right under switch 1, another under 7 and 8

# The magnet sensor measurements

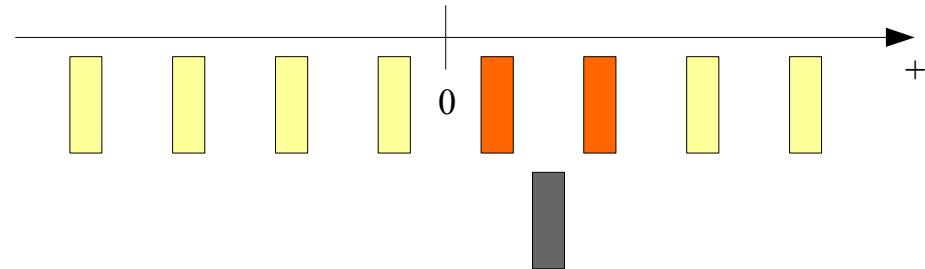


No measurement  
This 8 binary states becomes a measurement when we define  
a zero position in the center and then we multiply by a  
constant  $\Delta$

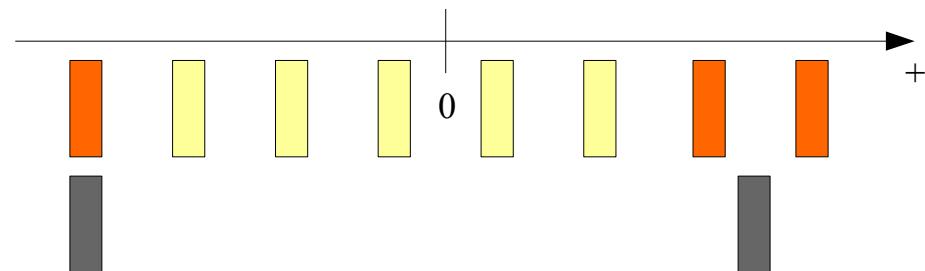


Measurement is  $-1.5 \Delta$

# The magnet sensor measurements



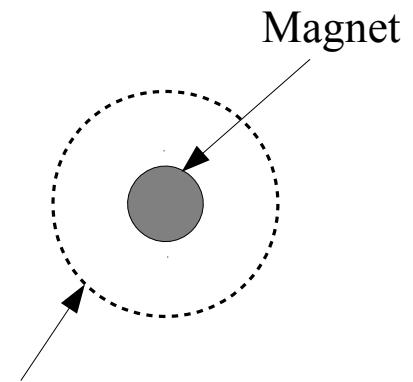
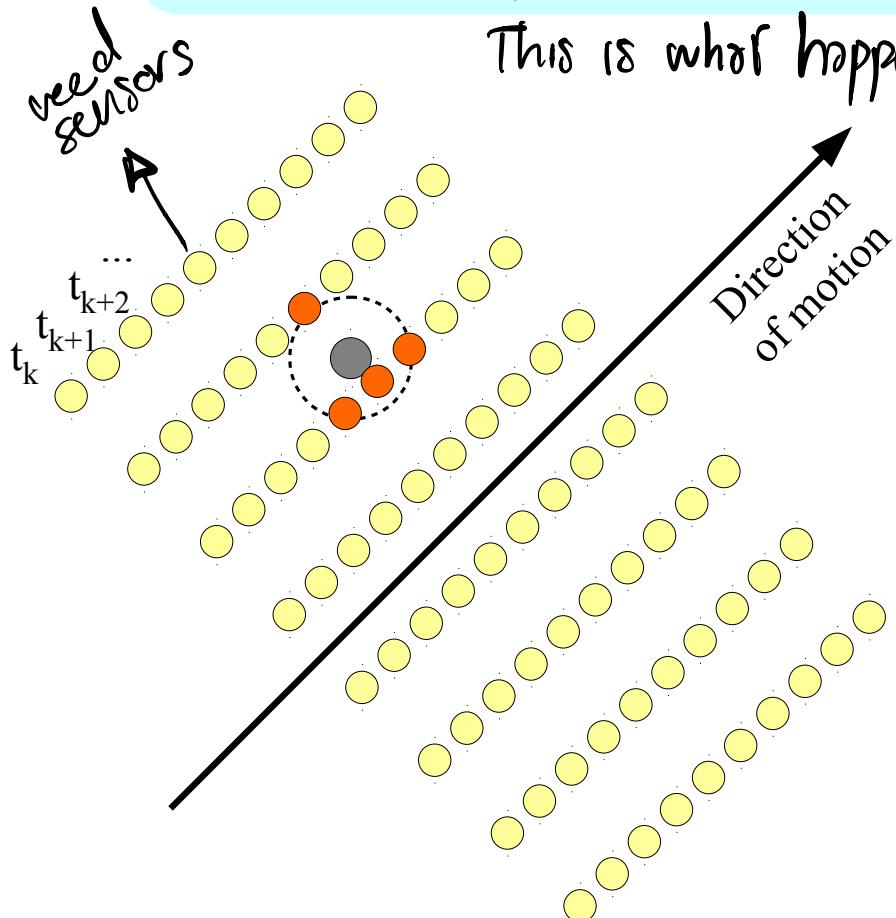
Measurement is  $+\Delta$



Two measurements:  $-3.5\Delta$  and  $+3\Delta$

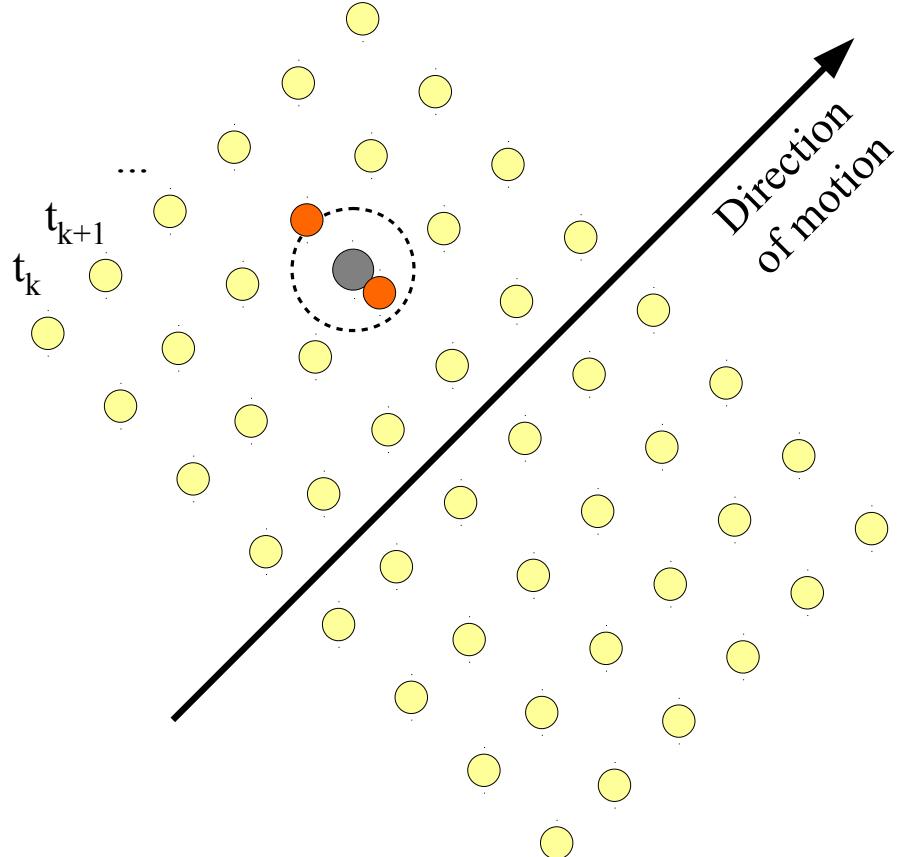
# Sensor passing over a magnet

This is what happens when the robot moves



Area where the magnetic field is intense enough to switch the reed sensor on.

# Sensor passing over a magnet (lower sampling rate)

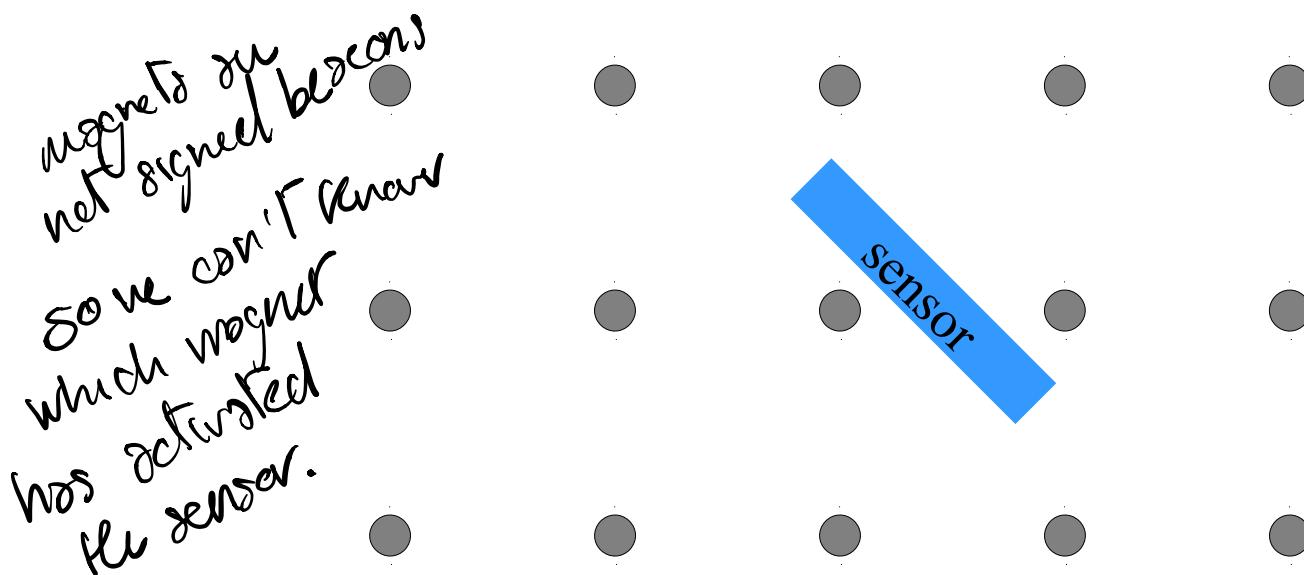


## About the magnet sensor

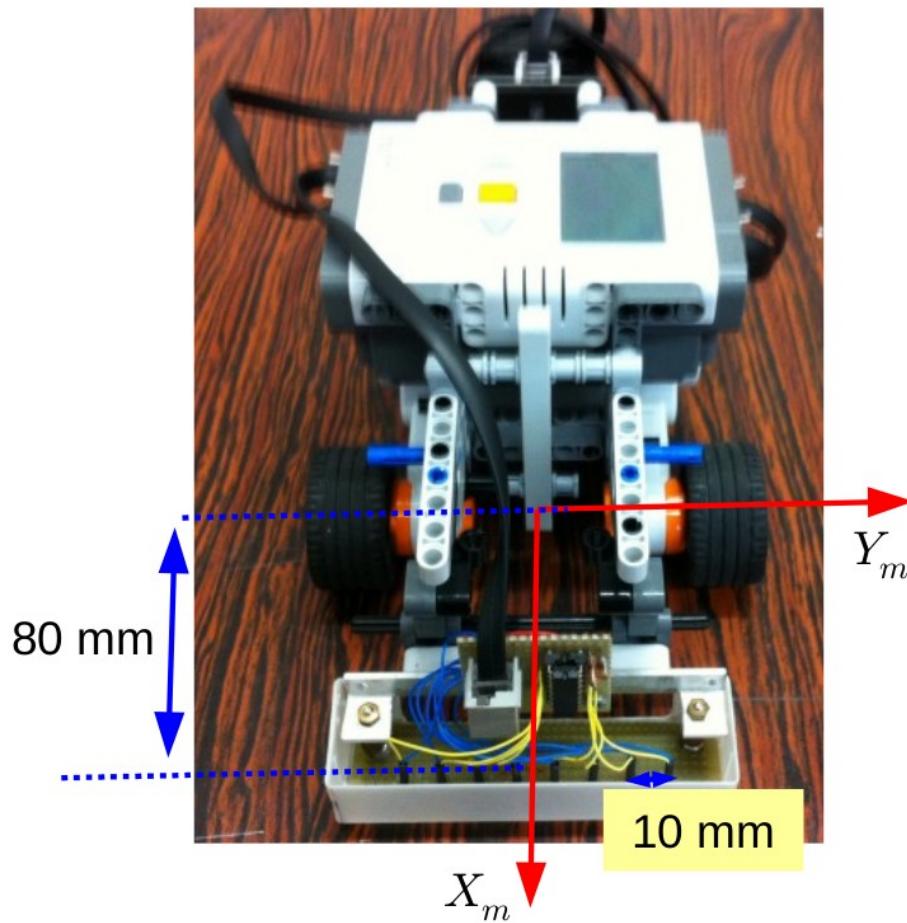
- The system design parameters are:
  - Magnet field intensity.
  - Inter-magnet distance
  - Reed switch sensitivity.
  - Reed switch number/spacing and sensor length.
- The sensor has been designed in such a way that:
  - When passing over a magnet, either one or two reed switches are activated.
  - When the robot moves, the sensor “cannot avoid crossing magnets”

# System characteristics

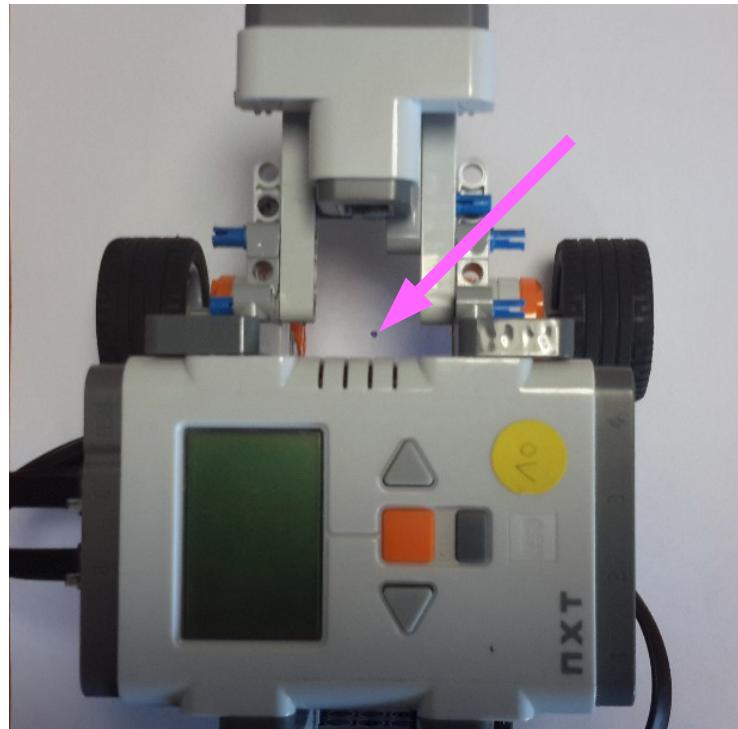
- 8 reed switches.
- 10 mm interval between reed switches
- 55 mm interval between magnets, arranged in a regular square pattern.



## Robot and sensor



# Initial positioning of the robot



Initial state on  
the axle of the  
two wheels  
→ not very  
precise.

The center point of the fixed wheel axle  
is put above a dot painted at (0,0).

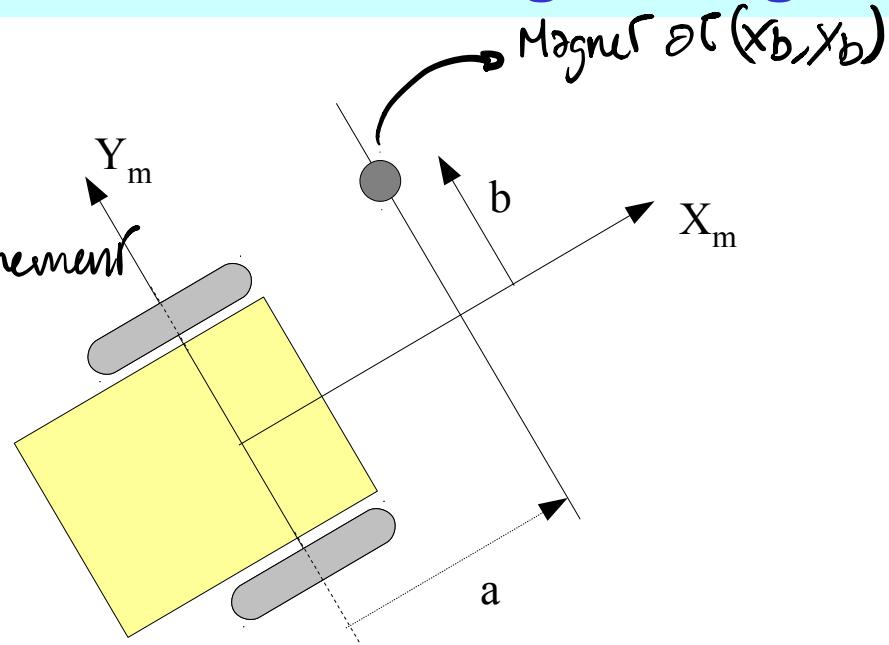
# Robot characteristics

- Encoders:
  - 360 dots per wheel revolution.
  - “Dumbed down” to 45 dots per revolution to make the problem a bit more challenging.
- Recording frequency:
  - 20 Hz.  look at the data at 20Hz when determining the noise variance
  - We will work at 5 Hz.

There is a file which contains the frequency parameter  
change it to 1 → to see at 20Hz  
change it to 4 → to work at 5Hz

# The robot detecting a magnet

It's a big error  
to think that  
the noise measurement  
is determined  
by trial and  
error.



- Express in plain English what the sensor measures.
- Write the measurement equation

- ① The sensor is showing whether the magnetic field surrounding it is over a certain threshold.  
 IT MEASURES the coordinates of the magnetic field w.r.t. the robot frame, which is located at the center of the wheel axle.
- The a coordinate is always 80, because the sensors are always at distance a.

In the equations of the Kalman filter we have  $y \rightarrow$

$$\rightarrow y = 80 \text{ but usually } \overset{2 \times 1}{y} \neq 80$$

$$y = g(x) = \begin{bmatrix} a \\ b \end{bmatrix}$$

- <sup>o</sup>M is known
- <sup>m</sup>M is measured  
 $\rightarrow = g(x)$

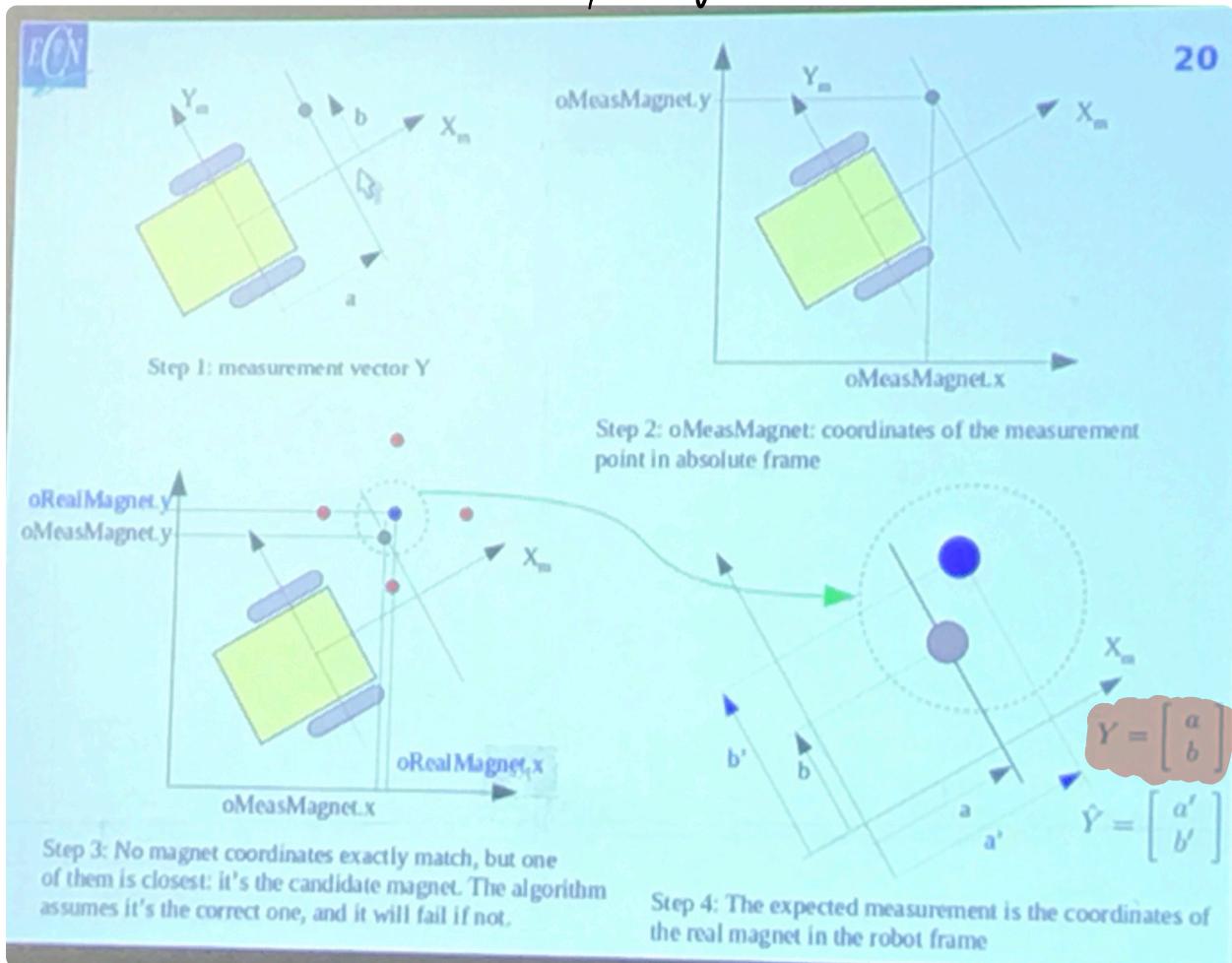
Surely we're not measuring angles. And we're also not measuring distances  
 $\rightarrow$  We're measuring coordinates.

$$\rightarrow {}^oT_m = \begin{bmatrix} \cos\theta & -\sin\theta & x \\ \sin\theta & \cos\theta & y \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} R & P \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

We're actually going to use the inverse  ${}^mT_o = \begin{bmatrix} R^T & -R^T P \\ 0 & 1 \end{bmatrix}$

$$\rightarrow {}^0M = \begin{bmatrix} X_M \\ Y_M \\ 1 \end{bmatrix} \rightarrow {}^mM = {}^mT_0 {}^0M$$

$X_M$  and  $Y_M$  will be multiples of 55.



To take the measurement, express it in absolute coordinates  
determine the candidate magnet and project its coordinates  
onto the robot frame.  $\rightarrow$  this is the expected measurement

Let  $z$  be a gaussian vector  $z^T P^{-1} z$  follows a  $\chi^2$  bw.  
 The shape of the  $\chi^2$  distribution depends on the dimension of  $z$  (number of lines). The threshold is obtained in Matlab with the "chi2inv" function :  $\text{chi2inv}(p, v)$ .

$p = 0,95$  to  $0,99$  typically,  $v = \text{dim}(Y)$

We use  $z = Y - \hat{Y}$ ,  $P = CPC^T + Q_J$

The value of the threshold depends on the dimension of the output vector. NO TRIAL & ERROR

$$[\dot{\omega}] = JTC \begin{bmatrix} \dot{q}_R \\ \dot{q}_L \end{bmatrix}$$

↳ Jacobian to Cartesian

$$\begin{bmatrix} \Delta D \\ \Delta \theta \end{bmatrix} = JTC \begin{bmatrix} \Delta q_R \\ \Delta q_L \end{bmatrix}$$

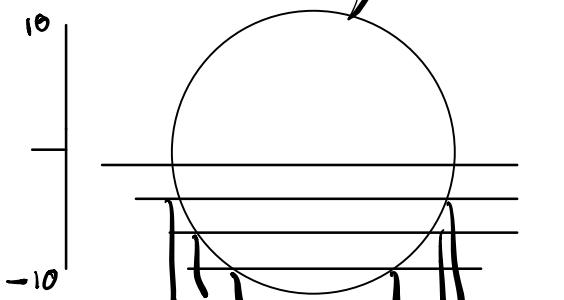
$$X = \text{evolutionModel}(x, u)$$

↳  $x_{k+1} = f(x, u)$

$$\begin{aligned}
 \text{Compute } C = \frac{\partial g_\theta}{\partial x} &= \frac{\partial}{\partial x} \left[ \begin{array}{l} \cos \theta (\hat{x}_m - x) + \sin \theta (\hat{y}_m - y) \\ \cos \theta (\hat{y}_m - y) - \sin \theta (\hat{x}_m - x) \end{array} \right] \\
 &= \begin{bmatrix} -\cos \theta & -\sin \theta & (-\sin \theta (\hat{x}_{mag} - x) + \cos \theta (\hat{y}_{mag} - y)) \\ \sin \theta & -\cos \theta & (-\sin \theta (\hat{y}_{mag} - y) - \cos \theta (\hat{x}_{mag} - x)) \end{bmatrix} -
 \end{aligned}$$

The distance between the revolutions vary because of the frequency

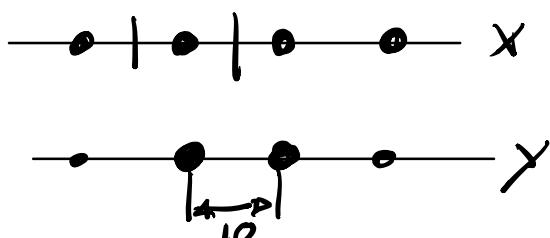
$$\sigma_x^2 = \frac{20^2}{12} \text{ eq.}$$



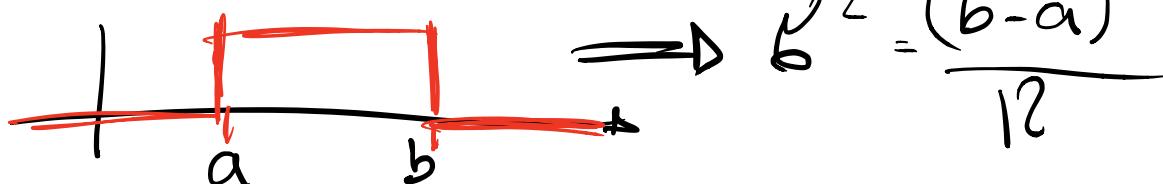
smaller intervals

Along  $y$  is completely different:

$$\sigma_y^2 = \frac{10^2}{12} \quad \text{fig (7)}$$



Uniform Noise Variance:



If we set  $\sigma$  tuning very low,  $P$  increases too slowly

→  $\underbrace{CPC^T}_{\text{variance of } \hat{y}}$  is also too low so you are trusting your  $\hat{y}$  much more than you trust  $y$ , so each  $y$  that has a discrepancy from  $\hat{y}$  gets REJECTED

→  $CPC^T + \underbrace{Q_y}_{\text{variance of } y}$  is also too low, so its inverse is too high → an high gain that goes to multiply the mahalanobis distance. So you accept pretty anything, and that is why all the red dots are below threshold

Mahalanobis distance =

$$\rightarrow \underbrace{(y - \hat{y})^\top}_{\text{innov}} \underbrace{(CPC^T + Q_y)^{-1}}_{\text{variance of } \hat{y}} \underbrace{(y - \hat{y})}_{\text{innov}}$$

⇒ To compute the threshold for the system use  $\chi^2_{\text{inv}}(\% \text{ of acceptable measurements}, \text{dimension of } y)$

## LAB ②

New state:

$$\begin{bmatrix} x \\ y \\ \theta \\ v_c \\ r_m \end{bmatrix}$$

New evolution model:

$$V_{K+1} = V_K + \text{some noise}$$

$$\Delta K$$

$$Q_d = \left[ \begin{array}{c|c} \emptyset_{3 \times 3} & \emptyset_{3 \times 2} \\ \hline \emptyset_{2 \times 3} & \begin{matrix} b^2 & 0 \\ 0 & b^2 \end{matrix} \end{array} \right]$$

→ controls the behaviour  
of the wheel radius

So:

$b^2$  small →  $r$  is low-pass filtered (low noise)  
but the radius will only be able to  
track slow variation.  
(NOT ILLUSTRATED in the lab)

Also  $P_{init}$  is affected:

$$P_{init} = \left\{ \begin{matrix} b_x^2 & b_y^2 & \emptyset \\ b_y^2 & b_z^2 & \emptyset \\ \emptyset & \emptyset & b_{min}^2 \\ \emptyset & \emptyset & b_{max}^2 \end{matrix} \right\}$$

The  $b^2$  must have  
to be of the  
order of magnitude  
of the initial  
error.

When I need to identify a parameter constant or  
slowly evolving, we add it to the state vector and

make it evolving adding some noise.

→(e.g.) Car Tyres which lower their pressure based on velocity, temperature ...

TO-DO-LIST point ⑥

b) Two loops has a sharp correction at (60, 260), why?

Looking at figure 3-4 we can clearly see the sudden variation on x's standard deviation:

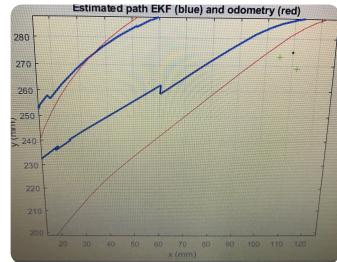
Observation: we also see that from  $t=14s$  to  $t=17s$  there are no measurements available

→ The robot goes blind for 3 seconds and when the measurement comes it suddenly corrects the trajectory.

Figure 3 → Standard deviation in absolute frame

Figure 4 → " " in robot frame

c) In diag 45 degree we have two diverging lines, why?



## Variant of Kalman filter equations

- The program uses a slight variant of the Kalman filter equations, where the input  $u$  is assumed to be disturbed by noise:

$$X_{k+1} = f(X_k, U_k^*) + \alpha_k$$

$U_k^* = U_k + \beta_k$  The measured input is affected by an additive noise

$$P_{k+1} = A_k P_k A_k^T + B_k Q_\beta B_k^T + Q_\alpha$$

The error propagation equation is the only change.

$$A_k = \frac{\partial f}{\partial X} \quad B_k = \frac{\partial f}{\partial U}$$

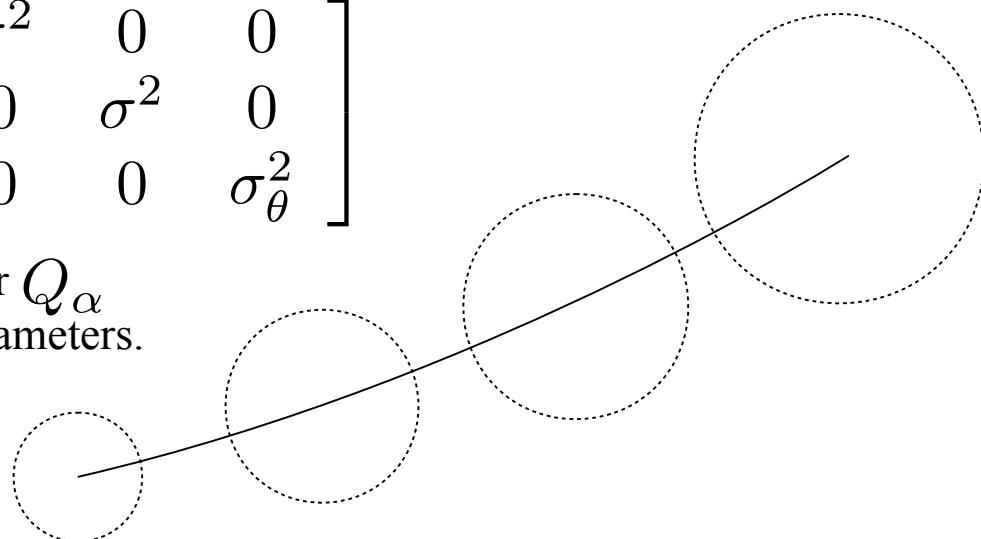
See paragraph 5.2 of the “book” form of the localization class material for the equations.

# Evolution of uncertainty (standard form of the equations)

$$P_{k+1} = A_k P_k A_k^T + Q_\alpha$$

$$Q_\alpha = \begin{bmatrix} \sigma^2 & 0 & 0 \\ 0 & \sigma^2 & 0 \\ 0 & 0 & \sigma_\theta^2 \end{bmatrix}$$

A logical for for  $Q_\alpha$   
Two tuning parameters.



Assuming the initial uncertainty is the same in x and y, the uncertainty ellipse in the x-y plane starts as a circle and remains a circle during successive odometry phases (no update phase).

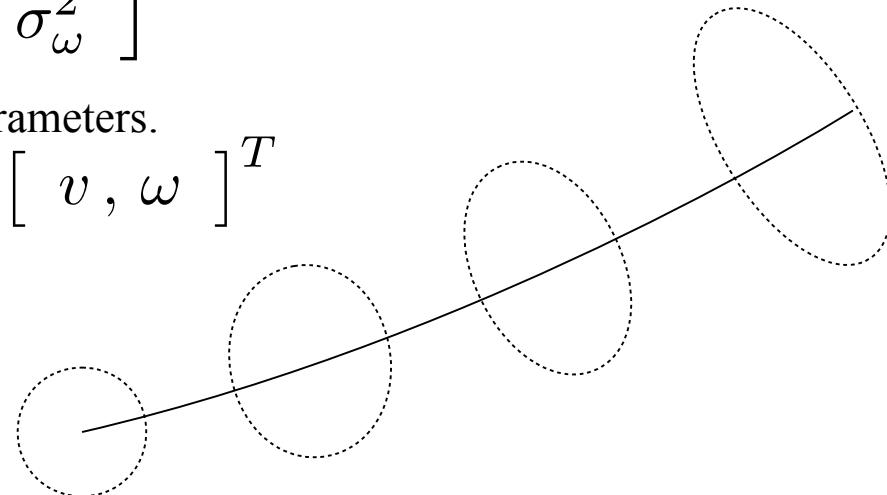
# Evolution of uncertainty (form with noisy input)

$$P_{k+1} = A_k P_k A_k^T + B_k Q_\beta B_k^T \quad (Q_\alpha \text{ has been set to zero})$$

$$Q_\beta = \begin{bmatrix} \sigma_v^2 & 0 \\ 0 & \sigma_\omega^2 \end{bmatrix}$$

Still two tuning parameters.

Remember:  $u = [v, \omega]^T$



Now the uncertainty ellipse orients with the motion of the robot. The result is closer to the way errors actually evolve during odometry.

$$\hat{\mathbf{x}}_{k+1/k} = f(\hat{\mathbf{x}}_{k|k}, u_k) = \begin{bmatrix} x_k + \Delta D_x \cos \theta_k \\ y_k + \Delta D_k \sin \theta_k \\ \theta_k + \Delta \theta_k \end{bmatrix}$$

ODOMETRY

3x1 nx1

Estimate of the state vector 3

$$\begin{matrix} \text{2x1} \\ \text{px1} \end{matrix} \mathbf{U}_K = \begin{bmatrix} \Delta D_K \\ \Delta \theta_K \end{bmatrix} \quad \text{This is the input of the system measured from encoders (sensors)}$$

$$A_X = \frac{\partial f}{\partial X} \quad , \quad B_X = \frac{\partial f}{\partial U} \quad \left. \begin{array}{l} \\ \end{array} \right\} \begin{array}{l} \text{linear approx} \\ \text{of system} \\ \text{equation.} \end{array}$$

2

$$\text{measurements} \quad Y = g_B(x) = \begin{bmatrix} a \\ b \end{bmatrix} \Rightarrow Q_Y = \text{quality of the measurements}$$

2x1

5

2x2

m x m

$$G_K = \frac{\partial g_B}{\partial x}$$

$P_k$  = quality of the state estimate

$3 \times 3$   
 $n \times n$

# STEPS OF THE ALGORITHM

After completing  
the year update  
 and 

## The input noise in the lab

$$\begin{cases} v = (r_r \dot{q}_r + r_l \dot{q}_l) / 2 \\ \omega = (r_r \dot{q}_r - r_l \dot{q}_l) / e \end{cases}$$

There is a linear relation between  $v, \omega$  and the rotation speed of the wheels.

So  $Q_\beta$  can be written as a function of the covariance matrix of errors on  $\dot{q}_r$  and  $\dot{q}_l$ .

$$Q_\beta = K Q_{\dot{q}} K^T \quad \text{with} \quad K = \begin{bmatrix} r_r/2 & r_l/2 \\ r_r/e & -r_l/e \end{bmatrix}$$

A reasonable form for  $Q_{\dot{q}}$ :

$$Q_{\dot{q}} = \begin{bmatrix} \sigma_{\dot{q}}^2 & 0 \\ 0 & \sigma_{\dot{q}}^2 \end{bmatrix}$$

Now the number of tuning parameters for the input noise is 1.

## REPORT QUESTIONS

① If overestimated → initial uncertainty high  
→ P high → great attention on first data in  
order to correct trajectory.

If underestimated → when given wrong <sup>initial</sup> position  
it drift and diverge, because  $\hat{y} - y$  will be  
very big and so won't be under understand  
threshold

②

## OBSERVABILITY

We suppose to make a snapshot of the system w/ only one magnet  $\rightarrow$  the car in  $(0,0)$ .

So we need to modify  ${}^m P_{mag}$   $\rightarrow$  matrix of the coordinates of the magnet in robot frame.

$${}^m P_{mag} = \begin{bmatrix} -x \cos \theta - y \sin \theta \\ -y \cos \theta + x \sin \theta \end{bmatrix}$$

We need to compute the new C matrix:  $\frac{\partial \mathbf{s}_B}{\partial \mathbf{x}}$

$$\rightarrow C = \begin{bmatrix} -\cos \theta & -\sin \theta & +x \sin \theta - y \cos \theta \\ \sin \theta & -\cos \theta & y \sin \theta + x \cos \theta \end{bmatrix} \begin{array}{l} dg_1 \\ dg_2 \end{array}$$

$$\begin{cases} \dot{x} = v \cos \theta \\ \dot{y} = v \sin \theta \\ \dot{\theta} = w \end{cases}$$

$$\begin{aligned} \frac{\partial L f g_1}{\partial} &= \frac{\partial}{\partial} (+x \sin \theta \cdot \dot{\theta} - \dot{x} \cos \theta - \\ &\quad \dot{y} \sin \theta - \cos \theta \cdot \dot{y} \dot{\theta}) \\ &= \frac{\partial}{\partial} (x w \sin \theta - v \cos^2 \theta - \\ &\quad v \sin^2 \theta - y w \cos \theta) \end{aligned}$$

WRONG

We need to use two different magnets because otherwise we get  $L f g_1$  depending on  $w$ .

$${}^m P_{mag} = \begin{bmatrix} -x \cos \theta - y \sin \theta \\ -y \cos \theta + x \sin \theta \\ \cos \theta (1-x) - y \sin \theta \\ -y \cos \theta - x \sin \theta (1-x) \end{bmatrix}$$

$$C = \begin{bmatrix} -\cos \theta & -\sin \theta & x \sin \theta - y \cos \theta & dg_1 \\ \sin \theta & -\cos \theta & y \sin \theta + x \cos \theta & dg_2 \\ -\cos \theta & -\sin \theta & -\sin \theta + x \sin \theta - y \cos \theta & dg_3 \\ +\sin \theta & -\cos \theta & y \sin \theta + x \cos \theta - \cos \theta & dg_4 \end{bmatrix}$$

I try to compute the O matrix: if it's full rank the sys is obs and so i'm done.

$$O = \begin{bmatrix} -\cos \theta & ; & \sin \theta & | & -\cos \theta \\ -\sin \theta & ; & -\cos \theta & | & -\sin \theta \\ x \sin \theta - y \cos \theta & ; & y \sin \theta + x \cos \theta & | & -\sin \theta + x \sin \theta - y \cos \theta \end{bmatrix}_{dg_i}$$

The  $\text{rank}(O) = 3$  so the system is observable

Doing the math:

$$\begin{aligned}
 \text{rank}(0) &= - (x \sin \theta - y \cos \theta) \left[ \begin{matrix} -\sin^2 \theta & \cos^2 \theta \end{matrix} \right] - (y \sin \theta + x \cos \theta) \\
 &\quad \left[ \begin{matrix} +\sin \theta \cos \theta & -\sin \theta \cos \theta \end{matrix} \right] + (-\sin \theta + x \sin \theta - y \cos \theta) \\
 &\quad \left[ \begin{matrix} \cos^2 \theta & \sin^2 \theta \end{matrix} \right] = \cancel{y \cos \theta} - \cancel{x \sin \theta} - \cancel{\sin \theta} + \cancel{x \sin \theta} \\
 &\quad - \cancel{y \cos \theta} = \underline{-\sin \theta} \neq 0
 \end{aligned}$$

```

% The variables and the evolution equation
syms x y theta v w
X = [x y theta].'
U = [v w].'
f = [ v*cos(theta) ; v*sin(theta) ; w ]
pause

% The general measurement equation for magnet
(x_mag,y_mag) is:
% 
$$g(X) = \begin{vmatrix} \cos(\theta)(x_{mag}-x) + \sin(\theta)(y_{mag}-y) \\ \cos(\theta)(y_{mag}-y) - \sin(\theta)(x_{mag}-x) \end{vmatrix}$$


% Case when the two coordinates of each magnet in the
robot frame are
% measured. Should of course be observable. Let's practice
by checking it.
% Without loss of generality, the magnet coordinates are :
% M0=(0,0) and M1=(1,0)
% The four components of the measurement equation are
called
% g0x, g0y, g1x, g1y, with the obvious meaning.

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g0x = -x*cos(theta) - y*sin(theta)
g0y = -y*cos(theta) + x*sin(theta)
g1x = cos(theta)*(1-x) - sin(theta)*y
g1y = -y*cos(theta) + (x-1)*sin(theta)
pause

% Gradient vectors of the four measurement components.

dg0x = jacobian(g0x,X).'
dg0y = jacobian(g0y,X).'
dg1x = jacobian(g1x,X).'
dg1y = jacobian(g1y,X).'
pause

```

WITH ONLY 1 MAG

$$C = \begin{bmatrix} -\cos\theta & -\sin\theta & \overbrace{x\sin\theta - y\cos\theta}^{\text{with only 1 mag}} \\ \sin\theta & -\cos\theta & y\sin\theta + x\cos\theta \end{bmatrix} \begin{bmatrix} \delta g_1 \\ \delta g_2 \end{bmatrix}$$

$$\begin{aligned}
\delta L f_{g_1} &= \delta (+x\sin\theta \cdot \dot{\theta} - \dot{x}\cos\theta - \\
&\quad \dot{y}\sin\theta - \dot{c}\cos\theta \cdot \dot{y}) \\
&= \delta (x\omega\sin\theta - v\cos^2\theta - \\
&\quad v\sin^2\theta - y\omega\cos\theta) \\
&= \delta (w x \sin\theta - w y \cos\theta - v)
\end{aligned}$$

$$\delta L f_{g_1} = \begin{bmatrix} w\sin\theta \\ -w\cos\theta \\ -w x \cos\theta + w y \sin\theta \end{bmatrix}$$

w multiplies everything so, when  $\theta=0$  or constant the system is not observable in this case

Now we try with  $dLfg_2$ :  $-y \cos\theta + x \sin\theta$

$$\begin{aligned} dLfg_2 &= J(-\cos\theta \dot{y} + \sin\theta \dot{x} + x \sin\theta + x \cos\theta \dot{\theta}) \\ &= J(-v_{\sin\theta} \cos\theta + w_{\sin\theta} + v_{\cos\theta} \sin\theta + x w_{\cos\theta}) \\ &= \begin{bmatrix} w_{\cos\theta} \\ w_{\sin\theta} \\ w_{\cos\theta} - x w_{\sin\theta} \end{bmatrix} \end{aligned}$$

Same as before.