# Implementation of the SP3 equations in a MOOSE-based application ANS Student Conference 2021 (Paper ID: 34668)

#### Roberto Fairhurst Agosta, Kathryn D. Huff

Advanced Reactors and Fuel Cycles University of Illinois at Urbana-Champaign

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## Outline

- 1 Introduction
  Objectives
  Motivation
- 2 Methodology Equations Implementation Kernels
- Results
  1-G, 2-D
- 4 Final Remarks
  Conclusions
  Acknowledgement



- Implement the  $SP_3$  equations in a MOOSE-based application.
- Verify the implementation by conducting the following exercises:
  - One-group, two-dimensional eigenvalue problem.
  - C5 MOX Benchmark.

#### Motivation

### Why a neutronics solver?

- Neutronics provide information on the power distribution.
- Crucial role in the thermal-fluids behavior of a reactor.
- Multi-physics simulations for safety assessment.

#### Why the $SP_3$ equations?

- Fewer equations than  $P_3$ .
- Reduces the computational expense.
- · Conserves a reasonable accuracy.
- More accurate solution than diffusion approximation.

#### Why MOOSE?

- Partial differential equations describe the reactor physics.
- Computational framework for solving coupled equation systems.
- Open-source.
- Facilitates coupling between various applications targeting different phenomena.

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## $P_3$ equations

- $P_N$  expands the angular dependence in spherical harmonics.
- For N=3, steady-state, and one-dimension [5]:

$$\frac{d}{dx}\phi_{1,g} + \Sigma_{t,g}\phi_{0,g} = \sum_{g'=1}^{G} \Sigma_{s0,g'\to g}\phi_{0,g'} + \frac{\chi_g}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'}\phi_{0,g'} + Q_{0,g}$$
(1)

$$\frac{1}{3}\frac{d}{dx}\phi_{0,g} + \frac{2}{3}\frac{d}{dx}\phi_{2,g} + \Sigma_{t,g}\phi_{1,g} = \sum_{g'=1}^{G} \Sigma_{s1,g'\to g}\phi_{1,g'} + Q_{1,g}$$
 (2)

$$\frac{2}{5}\frac{d}{dx}\phi_{1,g} + \frac{3}{5}\frac{d}{dx}\phi_{3,g} + \Sigma_{t,g}\phi_{2,g} = \sum_{g'=1}^{G} \Sigma_{s2,g'\to g}\phi_{2,g'} + Q_{2,g}$$
(3)

$$\frac{3}{7}\frac{d}{dx}\phi_{2,g} + \Sigma_{t,g}\phi_{3,g} = \sum_{g'=1}^{G} \Sigma_{s3,g'\to g}\phi_{3,g'} + Q_{3,g}. \tag{4}$$

# $P_3$ equations (2)

## Assumptions [2]:

- isotropic external source
- negligible anisotropic group-to-group scattering

$$\frac{d}{dx}\phi_{1,g} + \Sigma_{0,g}\phi_{0,g} = \sum_{g'\neq g}^{G} \Sigma_{s0,g'\to g}\phi_{0,g'} + \frac{\chi_{g}}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'}\phi_{0,g'} + Q_{0,g}$$
 (5)

$$\frac{1}{3}\frac{d}{dx}\phi_{0,g} + \frac{2}{3}\frac{d}{dx}\phi_{2,g} + \Sigma_{1,g}\phi_{1,g} = 0$$
 (6)

$$\frac{2}{5}\frac{d}{dx}\phi_{1,g} + \frac{3}{5}\frac{d}{dx}\phi_{3,g} + \Sigma_{2,g}\phi_{2,g} = 0$$
 (7)

$$\frac{3}{7}\frac{d}{dx}\phi_{2,g} + \Sigma_{3,g}\phi_{3,g} = 0. \tag{8}$$

# $P_3$ equations (3)

With the following definitions:

$$D_{0,g} = \frac{1}{3\Sigma_{1,g}}, \quad D_{2,g} = \frac{9}{35\Sigma_{3,g}}$$

$$\Phi_{0,g} = \phi_{0,g} + 2\phi_{2,g}, \quad \Phi_{2,g} = \phi_{2,g}$$

the equations become:

$$-D_{0,g}\frac{d^2}{dx^2}\Phi_{0,g} + \Sigma_{0,g}\Phi_{0,g} - 2\Sigma_{0,g}\Phi_{2,g} = S_{0,g}$$
(9)

$$-D_{2,g}\frac{d^2}{dx^2}\Phi_{2,g} + \left(\Sigma_{2,g} + \frac{4}{5}\Sigma_{0,g}\right)\Phi_{2,g} - \frac{2}{5}\Sigma_{0,g}\Phi_{0,g} = -\frac{2}{5}S_{0,g}$$
(10)

where

$$S_{0,g} = \sum_{g'\neq g}^G \Sigma_{s0,g'\rightarrow g} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right) + \frac{\chi_g}{k_{eff}} \sum_{g'=1}^G \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right) + \mathcal{Q}_{0,g}.$$

## $SP_3$ approximation

- $P_N$ : yields the exact transport solution as  $N \to \infty$ .
- 3D:  $(N+1)^2$  equations.
- 1D: (N+1) equations yield (N+1)/2.
- $SP_N$  approximation replaces  $\frac{d^2}{dx^2}$  by  $\Delta$ .

## $SP_3$ equations

$$-D_{0,g}\Delta\Phi_{0,g} + \Sigma_{0,g}\Phi_{0,g} - 2\Sigma_{0,g}\Phi_{2,g} = S_{0,g}$$
(11)

$$-D_{2,g}\Delta\Phi_{2,g} + \left(\Sigma_{2,g} + \frac{4}{5}\Sigma_{0,g}\right)\Phi_{2,g} - \frac{2}{5}\Sigma_{0,g}\Phi_{0,g} = -\frac{2}{5}S_{0,g}.$$
 (12)

With the Marshak vacuum BCs [1]

$$\frac{1}{4}\Phi_{0,g} \pm \frac{1}{2}\hat{n} \cdot J_{0,g} - \frac{3}{16}\Phi_{2,g} = 0 \tag{13}$$

$$-\frac{3}{80}\Phi_{0,g} \pm \frac{1}{2}\hat{n} \cdot J_{2,g} + \frac{21}{80}\Phi_{2,g} = 0 \tag{14}$$

where

$$J_{n,g} = -D_{n,g} \nabla \Phi_{n,g}.$$

#### **MOOSE**

- Computational framework for solving coupled equation systems.
- Input are the equation weak forms.
- MOOSE and LibMesh translate them into residual and Jacobian functions
- PetSc solution routines solve the equations.

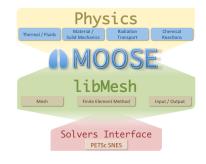
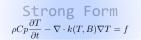


Figure: MOOSE framework. Image reproduced from [6].

# Example Code



$$\int\limits_{\Omega} \rho C p \frac{\partial T}{\partial t} \psi_i + \int\limits_{\Omega} k \nabla T \cdot \nabla \psi_i - \int\limits_{\partial \Omega} k \nabla T \cdot \mathbf{n} \psi_i - \int\limits_{\Omega} f \psi_i = \mathbf{0}$$
 Kernel BoundaryCondition Kernel

```
Actual Code return _k[_qp]*_grad_u[_qp]*_grad_test[_i][_qp];
```

Figure: Translation into MOOSE kernels procedure [6].

## Weak form: Equation 1

$$\langle D_{0,g} \nabla \Phi_{0,g}, \nabla \Psi \rangle - \langle D_{0,g} \nabla \Phi_{0,g}, \Psi \rangle_{BC} + \langle \Sigma_{0,g} \Phi_{0,g}, \Psi \rangle + \langle -2\Sigma_{0,g} \Phi_{2,g}, \Psi \rangle$$

$$+ \left\langle -\sum_{g' \neq g}^{G} \Sigma_{s0,g' \to g} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle$$

$$+ \left\langle -\frac{\chi_g}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle + \langle -Q_{0,g}, \Psi \rangle = 0$$
(15)

with the boundary condition

$$\langle D_{0,g} \nabla \Phi_{0,g}, \Psi \rangle_{BC} = \left\langle \frac{1}{2} \Phi_{0,g} - \frac{3}{4} \Phi_{2,g}, \Psi \right\rangle_{BC}. \tag{16}$$

## Weak form: Equation 2

$$\langle D_{2,g} \nabla \Phi_{2,g}, \nabla \Psi \rangle - \langle D_{2,g} \nabla \Phi_{2,g}, \Psi \rangle_{BC} + \left\langle \left( \Sigma_{2,g} + \frac{4}{5} \Sigma_{0,g} \right) \Phi_{2,g}, \Psi \right\rangle$$

$$+ \left\langle -\frac{2}{5} \Sigma_{0,g} \Phi_{0,g}, \Psi \right\rangle + \left\langle \frac{2}{5} \sum_{g' \neq g}^{G} \Sigma_{s0,g' \to g} \left( \Phi_{0,g'} - 2 \Phi_{2,g'} \right), \Psi \right\rangle$$

$$+ \left\langle \frac{2}{5} \frac{\chi_g}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2 \Phi_{2,g'} \right), \Psi \right\rangle + \left\langle \frac{2}{5} Q_{0,g}, \Psi \right\rangle = 0.$$
 (17)

with the boundary condition

$$\left\langle D_{2,g} \nabla \Phi_{2,g}, \Psi \right\rangle_{BC} = \left\langle -\frac{3}{40} \Phi_{0,g} + \frac{21}{40} \Phi_{2,g}, \Psi \right\rangle_{BC}. \tag{18}$$

## SP3 Kernels: Equation 1

Table:  $SP_3$  kernels.

Kernel name	Equation 1		
SP3Diffusion	$\langle D_{0,g} abla\Phi_{0,g}, abla\Psi angle$		
SP3SigmaR	$\langle \Sigma_{0,g} \Phi_{0,g}, \Psi  angle$		
SP3SigmaCoupled	$\langle -2\Sigma_{0,g}\Phi_{2,g},\Psi angle$		
SP3InScatter	$ \left\langle -\sum_{g'\neq g}^{G} \sum_{s0,g'\rightarrow g} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle $ $\left\langle -\frac{\chi_g}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle $		
SP3FissionEigenKernel	$\left\langle -\frac{\chi_g}{k_{aff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2 \Phi_{2,g'} \right), \Psi \right\rangle$		
BodyForce (MOOSE)	$\langle -Q_{0,g},\Psi angle$		
BC Kernel name			
SP3Vacuum	$\left\langle rac{1}{2}\Phi_{0, extit{g}} - rac{3}{4}\Phi_{2, extit{g}}, \Psi  ight angle_{ extit{BC}}$		

## SP3 Kernels: Equation 2

Table:  $SP_3$  kernels.

Kernel name	Equation 2		
SP3Diffusion SP3SigmaR SP3SigmaCoupled SP3InScatter	$\begin{array}{c} \langle D_{2,g} \nabla \Phi_{2,g}, \nabla \Psi \rangle \\ \langle \left( \Sigma_{2,g} + \frac{4}{5} \Sigma_{0,g} \right) \Phi_{2,g}, \Psi \rangle \\ \langle -\frac{2}{5} \Sigma_{0,g} \Phi_{0,g}, \Psi \rangle \\ \langle \frac{2}{5} \sum_{\sigma' \neq \sigma}^{G} \Sigma_{50,g' \to g} \left( \Phi_{0,g'} - 2 \Phi_{2,g'} \right), \Psi \rangle \end{array}$		
SP3FissionEigenKernel BodyForce (MOOSE)	$ \left\langle \frac{2}{5} \sum_{g'\neq g}^{G} \Sigma_{s0,g'\to g} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle $ $\left\langle \frac{2}{5} \frac{\chi_g}{k_{eff}} \sum_{g'=1}^{G} \nu \Sigma_{f,g'} \left( \Phi_{0,g'} - 2\Phi_{2,g'} \right), \Psi \right\rangle $ $\left\langle \frac{2}{5} Q_{0,g}, \Psi \right\rangle $		
BC Kernel name			
SP3Vacuum	$\left\langle -rac{3}{40}\Phi_{0,g}+rac{21}{40}\Phi_{2,g},\Psi ight angle_{BC}$		

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## One-group, two-dimensional eigenvalue problem

- Problem presented in Brantley and Larsen, 2000 [2].
- One-energy group.
- Two-dimensional problem.
- Two materials: fuel and moderator.

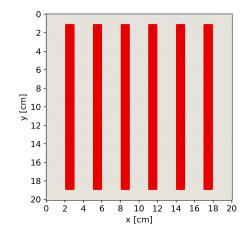


Figure: Problem's geometry.

# One-group, two-dimensional eigenvalue problem (2)

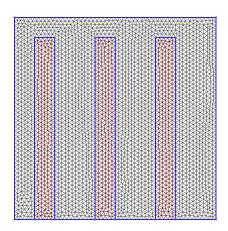


Figure: Gmsh 2D mesh.

# One-group, two-dimensional eigenvalue problem (3)

Table: Eigenvalue comparison.

k <sub>Ref</sub>	k <sub>SP3</sub>	$\Delta_{ ho}$
0.79862	0.79854	12

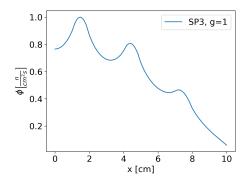


Figure: Scalar flux over line at y=4.5 cm.

#### C5 MOX Benchmark

- Exercise defined in 1994 by OECD/NEA [4].
- Two-energy groups.
- Two-dimensional problem.
- Two types of fuel: UO<sub>2</sub>, MOX.

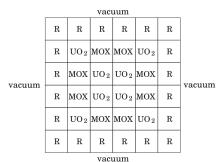


Figure: 2-D C5 MOX benchmark configuration. *R* represents the reflectors. Image reproduced from [3].

# C5 MOX Benchmark (2)

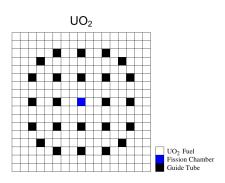


Figure:  $UO_2$  assembly. Image reproduced from [3].

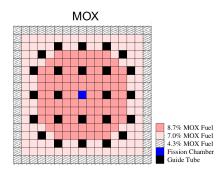


Figure: MOX assembly. Image reproduced from [3].

# C5 MOX Benchmark (3)



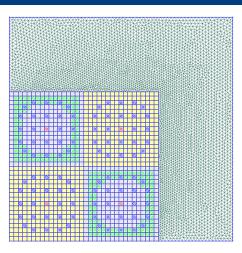


Figure: Gmsh 2D mesh.

## C5 MOX Benchmark (4)

If the higher order information of the scattering cross-section is not available (no correction):

$$D_{0,g} = \frac{1}{3\Sigma_{1,g}} = \frac{1}{3\Sigma_{t,g}} \tag{19}$$

The definition of the benchmark [4] recommends applying the diagonal transport correction:

$$D_{0,g} = \frac{1}{3\Sigma_{tr,g}}$$

$$\Sigma_{tr,g} = \Sigma_{t,g} - \bar{\mu}_g \Sigma_{s0,g}$$
(20)

where

 $\Sigma_{tr,g}=$  group g transport cross-section  $ar{\mu}_g=$  group g average cosine deviation angle.

# C5 MOX Benchmark (5)

	C5G2 Benchmark	SP3	
Case	$k_{Ref}$	$k_{SP_3}$	$\Delta_ ho$ [pcm]
No correction	0.96969	0.97106	145
Transport correction	0.93755	0.93792	43

# C5 MOX Benchmark (6)

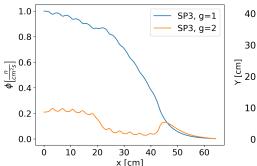


Figure: Scalar flux at y=10.71cm.

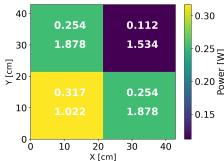


Figure: Assembly power distribution. Top: Assembly power. Bottom: Pin power relative difference expressed in %.

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#### Conclusions'

- Implemented the kernels to solve the steady-state SP<sub>3</sub> equations in a MOOSE-based application.
- Conducted two exercises whose reference results were known.
- Eigenvalue for the first exercise within 12 pcm.
- Eigenvalues for the second exercise within 145 pcm.
- Transport correction is necessary when the scattering higher moments are unknown.
- Calculated pin power values within 2% difference.
- Future work may develop new applications or integrate this application to other physics solvers.

# Acknowledgement

This research was performed using funding received from the DOE Office of Nuclear Energy's University Program (Project 20-19693, DE-NE0008972) 'Evaluation of micro-reactor requirements and performance in an existing well-characterized micro-grid'.

# Thank you. Questions?

#### References I

- [1] C. Beckert and U. Grundmann.
  - Development and verification of a nodal approach for solving the multigroup P3 equations.

Annals of Nuclear Energy, 2007.

- [2] P.S. Brantley and E.W. Larsen.
  - The Simplified P3 Approximation.

Nuclear Science and Engineering, 2000.

- [3] M. Capilla, D. Ginestar, and G. Verdú.
  - Applications of the multidimensional equations to complex fuel assembly problems.

Annals of Nuclear Energy, 36(10):1624-1634, October 2009.

- [4] C. Cavarec, J.F. Perron, D. Verwaerde, and J.P. West.
  - Benchmark Calculations of Power Distributions within Assemblies.

Technical Report HT-12/94006 A, NEA/NSC/DOC (94) 28, Nuclear Energy Agency Committee on Reactor Physics, 1994.

- [5] B. Davidson.
  - Neutron Transport Theory.

Oxford University Press, London, 1957.

### References II

#### [6] INL.

Moose Workshop Slides, December 2020.

https://moose framework.inl.gov/workshop.