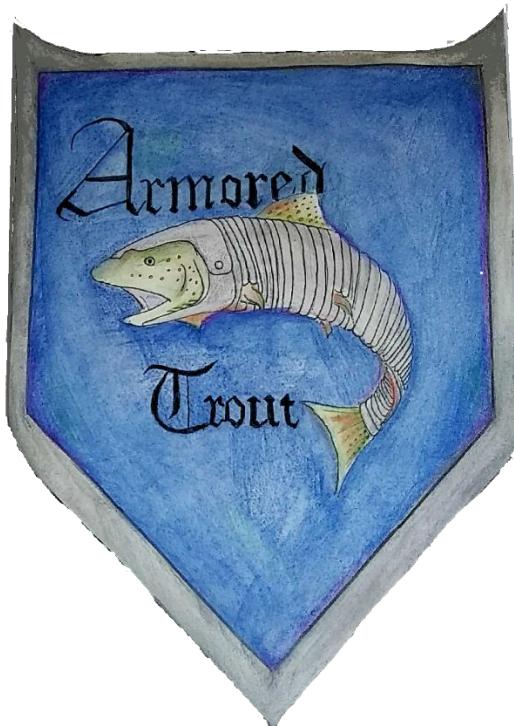


MAE 311 Term Project



Group 1: Flex Sensor

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November 28, 2017

1. Approval of Submission

I, Austin Click, approve this project report for submission. Information contained within is, to the best of my knowledge, complete and true, and in accordance with the process used throughout the completion of this project.

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I, Darnisha Crane, approve this project report for submission. Information contained within is, to the best of my knowledge, complete and true, and in accordance with the process used throughout the completion of this project.

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I, Walter Dietzler, approve this project report for submission. Information contained within is, to the best of my knowledge, complete and true, and in accordance with the process used throughout the completion of this project.

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I, Jacqueline Pepper, approve this project report for submission. Information contained within is, to the best of my knowledge, complete and true, and in accordance with the process used throughout the completion of this project.

Jacqueline Pepper _____

I, Hunter Phillips, approve this project report for submission. Information contained within is, to the best of my knowledge, complete and true, and in accordance with the process used throughout the completion of this project.

Hunter Phillips _____

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2. Abstract

To test the accuracy and implementation of flex sensor technology for robotic industry, this project focuses on measurement of angle of a robotic arm using a FlexPoint sensor. The sensor is an inexpensive solution to measuring a robotic arm angle, which previously was a difficult and expensive process. This device allows the students to measure an angle accurate to $\pm 6.36\%$. Angle measurement of a robotic arm has previously been acquired in research using a potentiometer. This method requires multiple mechanical connections that have potential to fail, as well providing a force against the stepper motor. In contrast, the Flex sensor is a single device that does not impede the movement of the robotic arm. The Flex sensor works by reading a voltage that changes with the bend of the sensor. The voltage is converted to resistance and finally to angle in Matlab. The angle is then displayed live time in Matlab on a compass plot and the data is output to excel to allow easy visibility of the data for users.

3. Device Production

3.1. Concept Development

The project was originally conceptualized as a proof of concept for a new robotic joint measurement mechanism. The objective was to measure the angle of the rotational axis with a new, supposedly higher accuracy, bend sensor. This approach would hopefully lower costs for robotic design, thus enabling quicker turnarounds for cutting edge designs. It was decided that the goal was to provide these measurements in real-time with a controllable test situation to simulate realistic environments.

To ensure reliability and repeatability it was decided that the robotic joint needed to be locked down on a test bed with high precision components to move the assembly. A realistic looking robotic joint with proper extending lever arms was decided against since this was not the point of the project. Being that the purpose was purely for an angle measurement, the superficial accuracy of replicating the extensions would prove no additional value to this particular project. This resulted in a pointer arm being decided on due to its ability to provide higher accuracy references against the mounting plate.

3.2. Electrical Schematic

The electrical design was created in Eagle to ensure proper connections were made. An Electrical Rule Check (ERC) was then applied to the circuit to ensure no faults and missing connections. The resulting schematic, **Figure 1**, was created with the important circuit divisions highlighted for further explanation of testing below.

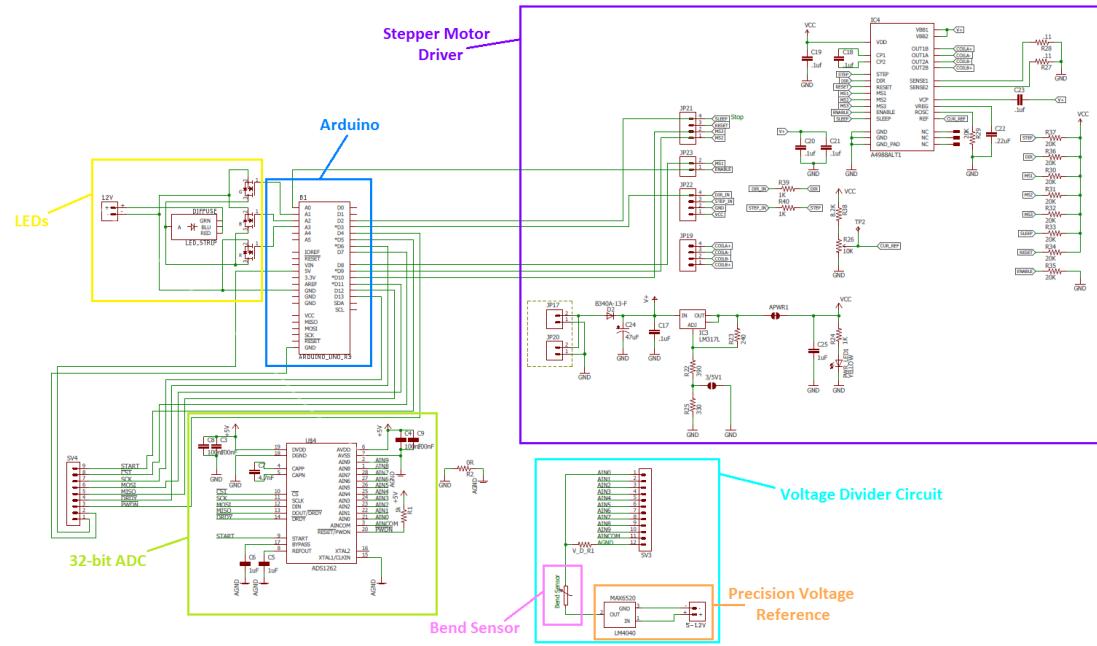


Figure 1: Circuit Schematic

The Arduino, stepper motor driver, and 32-bit ADC were already pre-fabricated boards, thus they did not need further electrical testing. The voltage divider circuit that contains the bend sensor and precision voltage reference needed validation through circuit simulation. The circuit was loaded into LTspice with the bend sensor being simulated with a variable potentiometer. The varying voltage that was to be fed into the 32-bit ADC was verified in simulation. The LEDs circuit was then tested to verify the MOSFETs provided proper switching for real time measurements. It was noted that the typical larger TO-220 MOSFET packages extra power dissipation was not needed for the amperage draw of the 12 V LEDs. These were exchanged for the smaller form factor SOT-23 package which enables a cleaner physical circuit design.

3.3. Programming Overview

The coding flow was that the Arduino would feed data into Matlab that would visually display the information and output the appropriate values to Excel. This logical design can be seen below in **Figure 2**.

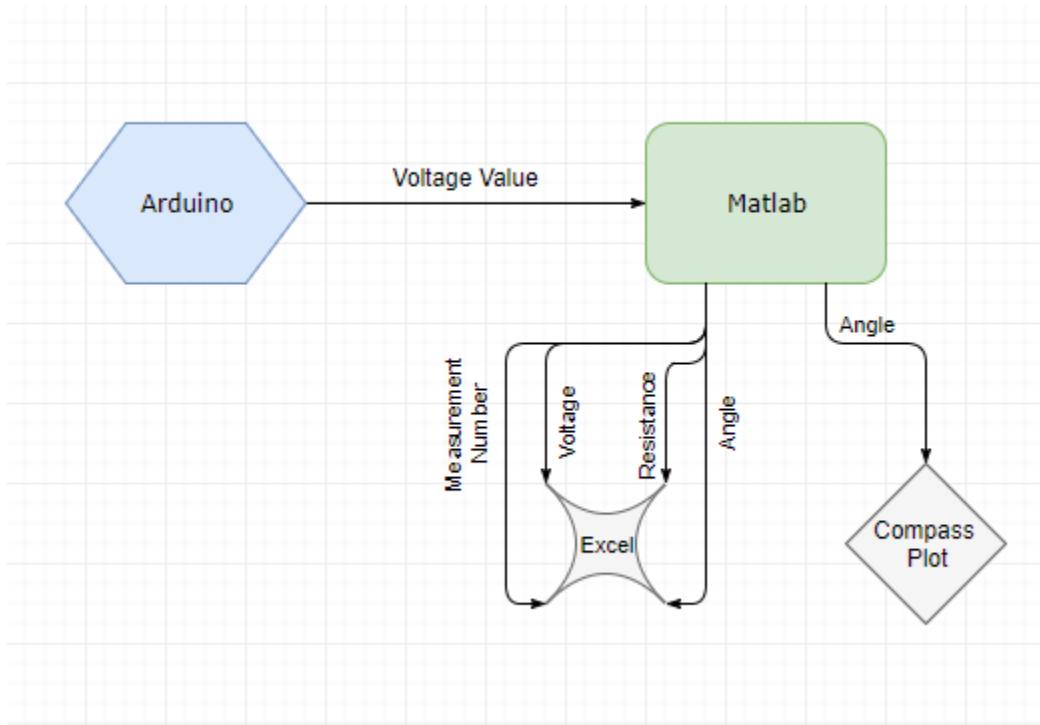


Figure 2: Basic Programming Schematic

3.4. Arduino Programming Analysis

The Arduino code consists mainly of the necessary functions to process the incoming 32-bit ADC byte chain. The code uses a custom ads1262.cpp and ads1262.h library to parse the appropriate ADC count [1]. SPI and SoftwareSerial were also needed for the Arduino to receive the output of the 32-bit ADC. Once the libraries were chosen the code seen below in **Figure 3**.

```
#include <SPI.h>
#include <SoftwareSerial.h>
#include <math.h>
#include <ads1262.h>

#define PGA_1          // Programmable Gain = 1
#define VREF 5.00       // Internal reference of 2.048V
#define VFSR VREF/PGA
#define FSR ((long int)1<<23)-1
ADS1262 PC_ADS1262;           // class
float volt_V=0;
float volt_mV=0;
volatile int i;
volatile char SPI_RX_Buff[10];
volatile long ads1262_rx_Data[10];
volatile static int SPI_RX_Buff_Count = 0;
volatile char *SPI_RX_Buff_Ptr;
volatile int Responsebyte = false;
volatile signed long sads1262Count = 0;
volatile signed long uads1262Count = 0;
double resolution;
bool direct_step = HIGH;

void setup()
{
    // initialize the data ready and chip select pins:
    pinMode(ADS1262_DRDY_PIN, INPUT);           // data ready input line
    pinMode(ADS1262_CS_PIN, OUTPUT);             // chip enable output line
    pinMode(ADS1262_START_PIN, OUTPUT);           // start
    pinMode(ADS1262_PWDN_PIN, OUTPUT);            // Power down output

    Serial.begin(1200);
    // initialize ADS1262 slave
    PC_ADS1262.ads1262_Init();                  // initialise ads1262
}

void loop()
{
    volatile int i,data; // init data for 32-bit adc
    if(digitalRead(ADS1262_DRDY_PIN) == LOW)        // monitor Data ready(DRDY pin)
    {
        SPI_RX_Buff_Ptr = PC_ADS1262.ads1262_Read_Data(); // read 6 bytes conversion register
        Responsebyte = true ;
    }
    if(Responsebyte == true)
    {
        for(i = 0; i <5; i++)
        {
            SPI_RX_Buff[SPI_RX_Buff_Count++] = *(SPI_RX_Buff_Ptr + i);
        }
        Responsebyte = false;
    }

    if(SPI_RX_Buff_Count >= 5)
    {
        ads1262_rx_Data[0]=(unsigned char)SPI_RX_Buff[1]; // read 4 bytes adc count
        ads1262_rx_Data[1]=(unsigned char)SPI_RX_Buff[2];
        ads1262_rx_Data[2]=(unsigned char)SPI_RX_Buff[3];
        ads1262_rx_Data[3]=(unsigned char)SPI_RX_Buff[4];

        uads1262Count = (signed long) (((unsigned long)ads1262_rx_Data[0]<<24)|((unsigned long)ads1262_rx_Data[1]<<16)|(ads1262_rx_Data[2]<<8)|ads1262_rx_Data[3]);
        sads1262Count = (signed long) (uads1262Count); // get signed value
        resolution = (double)(VREF/pow(2,31)); // resolution= Vref/(2^n-1) , Vref=2.5, n=no of bits
        volt_V = (resolution)*(float)sads1262Count; // voltage = (resolution)(adc count)

        serialFloatPrint(volt_V); // call function to print ADC reading as a parsed float
        Serial.println();
    }
    SPI_RX_Buff_Count = 0;
}
```

Figure 3: Arduino Code

Since the device communicates over the SPI interface the first section of variable initialization requires a lot of parsing and timing setup. The void setup() enables the starting sequence for the 32-bit ADC over SPI and creates the Serial connection with the computer. It was discovered that the Matlab portion of the code was unable to process data coming in faster than a 1200 baud rate, thus the typical baud rate of 9600 was not used to enable real-time graphing. The void loop() initially checks if new data is available on the SPI line and if it is, it immediately starts consuming the bytes into an array. Once the byte count has been concatenated into an array they are shifted into a long data type. The resolution of the ADC is then calculated with respect to our VREF coming from the Arduino of 5.00 V. The corresponding voltage is then calculated using the determined resolution and prepared for Serial output to Matlab.

```

void serialFloatPrint(float f) {
    byte * b = (byte *) &f;
    Serial.print("f:");
    // print delimiter
    for(int i=0; i<4; i++) {

        byte b1 = (b[i] >> 4) & 0x0f;
        byte b2 = (b[i] & 0x0f);
        // split the float chain into a 4 byte partitioned chain
        // prepends the upper nibble of a byte

        char c1 = (b1 < 10) ? ('0' + b1) : 'A' + b1 - 10;
        char c2 = (b2 < 10) ? ('0' + b2) : 'A' + b2 - 10;
        // encode the byte process in a standard IEEE HEX Representation
        // prevents incorrect matlab readings due to delimiter tainting

        Serial.print(c1);
        Serial.print(c2);
    }
}

```

Figure 4: Serial Print Float

This is where a roadblock was encountered when outputting a high precision float measurement. Arduino only supports integer Serial output and this was an unacceptable form of data writing. To solve this issue a serial float printing function was written using the IEEE standard as seen in **Figure 4**. Using a standard delimited 4-byte partitioned chain with the top byte being shifted to the upper nibble an array was formed of a separated float chain. These array elements were then encoded using the standard IEEE HEX representation with proper protection against delimiter tainting across the serial output chain. These converted hex value char chains are then outputted across the serial line to be read in by Matlab.

3.5. Matlab Programming Analysis

The Matlab program starts off with setting up the Excel variable workspace as seen in **Figure 5**.

```
8      % Setup Excel X Server
9      Excel = actxserver ('Excel.Application');
10     File='C:\Users\robolux\Desktop\311robot\demo\test1.xls';
11     if ~exist(File,'file')
12     ExcelWorkbook = Excel.workbooks.Add;
13     ExcelWorkbook.SaveAs(File,1);
14     ExcelWorkbook.Close(false);
15   end
16   invoke(Excel.Workbooks,'Open',File); % open the invoked Excel workbook
```

Figure 5: Setting up Excel X Server

The problem with the `xlswrite` function built into Matlab is that it starts a new writing session every time it is called. This causes a ~700 millisecond delay in the main loop which critically delays the real-time aspect of the sensor measurements. By setting up the X server of Excel the function does not have to continually invoke the session as it stays permanently open until the end of the program.

The initialization section of the script seen below in **Figure 6** showcases the variable declarations and purging sequences.

```
18 - mean_angle=[]; % init mean_angle
19 - trip = 2;        % dummy var
20 - w=0;            % need w for assigning positions in arrays during while loop
21 - data2 = [];      % init data 2 to null matrix
22 - value = [];      % initi value to null matrix
23 - figure('units','normalized','outerposition',[0 0 1 1]); % setup the figure
24 - comp = compass(1,1);          % compass graph
25 - arduino=serial('COM4','BaudRate',1200); % open up the com port for the arduino
26 - fopen(arduino);             % at a baud rate of 1200
27
28 - while(trip~=102)           % the first bytes before 102 of information need
29 -   trip=fread(arduino,1);    % to be read and assigned to a dummy variable
30 -   end                      % they contain unreadable characters / symbols
31
32 - data = 102;                % Read one more byte chain
33 - data = [data; fread(arduino,11,'char')]; % and dump the data into a dummy var
34 -                                     % it should be valid, however ensures that proper flushing occurs
35
36 - mapc = @(x) 4.2619958863*(10^(-10))*x^3 - 2.1440571377*(10^(-5))*x^2 + 3.3771916419*(10^(-1))*x - 1.5811722057*(10^(3));
```

Figure 6: Matlab Initialization

The main declarations serve the purpose of setting the variables and figure states before the loop. The serial line is opened with a baud rate of 1200 to correspond to the Arduino script. The following while loop is used to send all data on the serial line before 102 to a dummy variable. This ensures that the byte reading sequence is correct and starting from the 0 position, the delimiter (102), since Matlab can subscribe at any part of the byte chain. An initial set of 11 chars is read in to ensure that readable data is being

read in. If this passes the test the looping sequence begins, as seen in **Figure 7**, and the initialization is over.

```

38 - while(1)          % infinite loop
39 -     delete(comp)    % every iteration need to delete the old arrow from compass plot -> for speed
40 -     www1;           % iterate for array assignment advancement
41 -     data2 = fread(arduino,12,'char');    % get data from serial com
42 -     data_char = char(data2);            % ASCII is converted from raw data chain
43 -     data_converted = [data_char(9) data_char(10) data_char(7) data_char(8) data_char(6) data_char(5) data_char(3) data_char(4)];
44 -     value = hexsingle2num(data_converted); % data comes in backwards and needs to be rearranged and converted
45 -     % from single precision IEEE hexadecimal string to number
46 -     flexR = v2r(value);                % value is in form of voltage, need to convert it to a resistance
47 -     map_value = mapc(flexR);           % map the 0 - 90 degree angles to the straight and bent corresponding resistance values using cal curve
48 -
49 -     data_point = sprintf('A%u',num2str(w));
50 -     v_col = sprintf('B%u',num2str(w));
51 -     r_col = sprintf('C%u',num2str(w));
52 -     a_col = sprintf('D%u',num2str(w));
53 -     xlswrite1('test1.xls',w,1,data_point)      % record data point number
54 -     xlswrite1('test1.xls',value,1,v_col)        % record voltage
55 -     xlswrite1('test1.xls',flexR,1,r_col)        % record resistance
56 -     xlswrite1('test1.xls',map_value,1,a_col)      % record angle
57 -
58 -     mean_angle = [mean_angle, map_value];
59 -     [x_c,y_c] = pol2cart(map_value*(pi/180),1);
60 -     comp = compass(x_c,y_c);
61 -     ylim([0 1])
62 -     if mod(w,250)==0
63 -         fprintf('Mean Angle Measurement : %.2f\n',mean(mean_angle))
64 -         mean_angle = [];
65 -         user_dec=input('\n\nEnter 1 to increment the position of the stepper motor\nEnter 2 to take data points at position\nEnter 3 to end testing : ');
66 -         % Show user the mean of the ~250 measurements
67 -         % ask user to enter value for choice
68 -         if user_dec == 3 % if they pick 3
69 -             break           % exit loop and shutdown processes
70 -         end
71 -         if user_dec == 1
72 -             fprintf(arduino,'%s',char(user_dec));
73 -             pause(0.5)
74 -             fprintf(arduino,'%s',char(user_dec));
75 -         end
76 -         fclose(arduino);
77 -         fopen(arduino);
78 -     end
79 -     drawnow update % force the figure to update even if OPENGL denies it due to timing

```

Figure 7: Main Matlab Loop

The testing loop begins with a few housekeeping items to ensure each looping iteration starts with a proper clean process. Then the 12-byte data chain is read into Matlab with fread. The ASCII sequence is then converted from the data chain. For some undetermined reason the data does not come in linearly and needs to be rearranged into a custom sequence. This array is then converted from the single precision IEEE hexadecimal string to the final voltage value that was sent from the Arduino. This voltage value is then converted into a resistance value using custom values in the v2r function as seen below in **Figure 8**.

```

1  function flexR = v2r(volt_V)
2
3 -     R_DIV = 46880.0;      % Measured resistance of 47k resistor
4 -     VCC = 4.096;          % Measured voltage of precision 4.096 voltage reference
5
6 -     flexR = R_DIV * (VCC / volt_V - 1.0);
7
8 - end

```

Figure 8: v2r Function

The resistance value is then used to calculate the resulting angle using the calibration curve equation. The data values: data number, voltage, resistance, and angle are then

formatted and recorded into the Excel file using `xlswrite1` (a modified version of `xlswrite`). Since there appears to be noise in the value measurements a mean angle is then calculated to display in the command prompt once the set number of data points has been taken. The angle value is then converted to Cartesian coordinates which the compass graphing function takes in as its arguments. The function `ylim` is used to limit the viewing frame to the upper half of a circle since the measurements taken only range from ~0 to ~90 degrees. The following if statement determines when to stop taking measurements using the modulus of the iteration variable, `w`. It was set to 250 measurements as this was determined to be a good data set for each angle being measured. If it was triggered it displays the mean angle measurement of the 250 points and asks the user what they would like to do: take more data points at the angle position, advance the stepper motor, or end testing. The last thing in the while loop, `drawnow update`, forces the figure to update even if Matlab thinks it is a waste of computing time.

Once the loop has been ended by the user, the Arduino serial line is closed, and the Excel X Session is closed and saved as shown in **Figure 9**.

```
81 -      fclose(arduino); % close arduino
82
83      % close Excel and save work
84 -      invoke(Excel.ActiveWorkbook, 'Save');
85 -      Excel.Quit
86 -      Excel.delete
87 -      clear Excel
```

Figure 9: Closing Arguments

3.6. Code Testing

The code was tested extensively using a compile and debug approach typical in software / hardware implementation design. This was a relatively fluid process and enabled improvement iterations to be fast. All code was stored in a GitHub repository so that it could be worked on even when not in physical contact of the testing apparatus. This also made it easier to work on the project as a group since all the files were stored in the cloud and synced locally. The code was tested for varying periods of time to ensure that it could handle extremely long testing periods without slowing down or breaking. During the calibration process the code experienced over a 700 user inputs and 70000+ measurements thus validating its robustness to real world use.

3.7. CAD Modeling and Machining

a. *Machining Metal Protractor Plate*

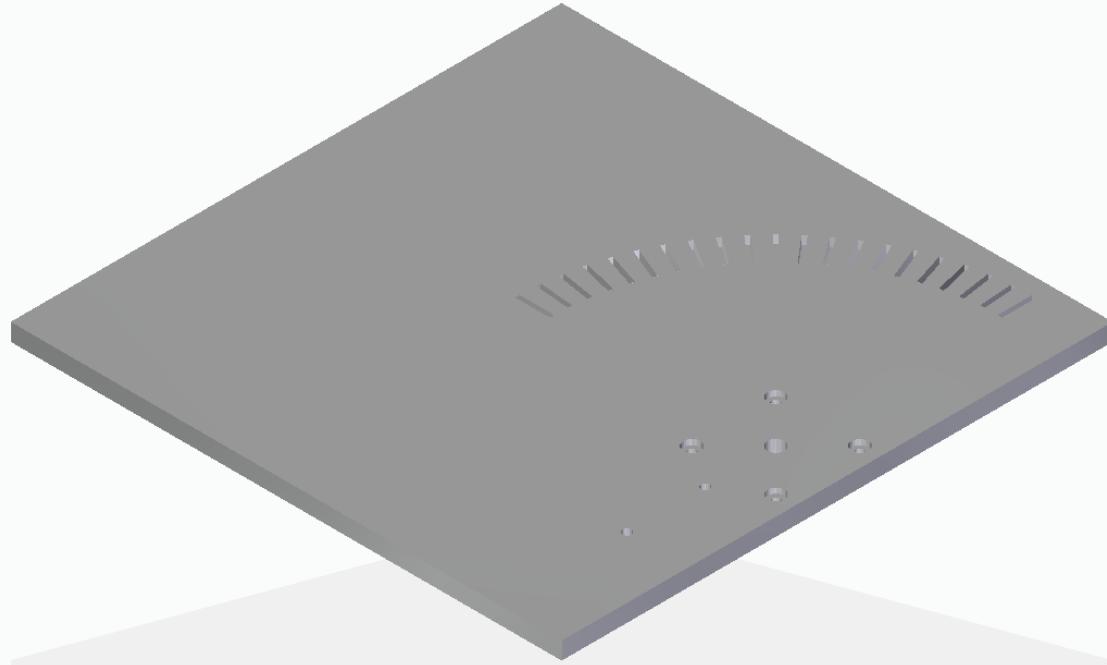


Figure 10: CAD of fully machined plate

The protractor plate shown in **Figure 10** was machined out of MIC6 aluminum, due to its machinable properties. The material was chosen due to its high dimensional stability. There were a total of 5 different processes used in the machining of the plate. The processes implemented were:

Process 1:

The first process was a hole process used to create center-drilled holes. The tool used was a #3 center drill, as it would provide a hole small enough to center both a 1/8" and a 1/4" drill bit so that they would not walk.

Feeds and Speeds:

- Spindle Speed: 6000 RPM
- Plunge Rate: 15 IPM

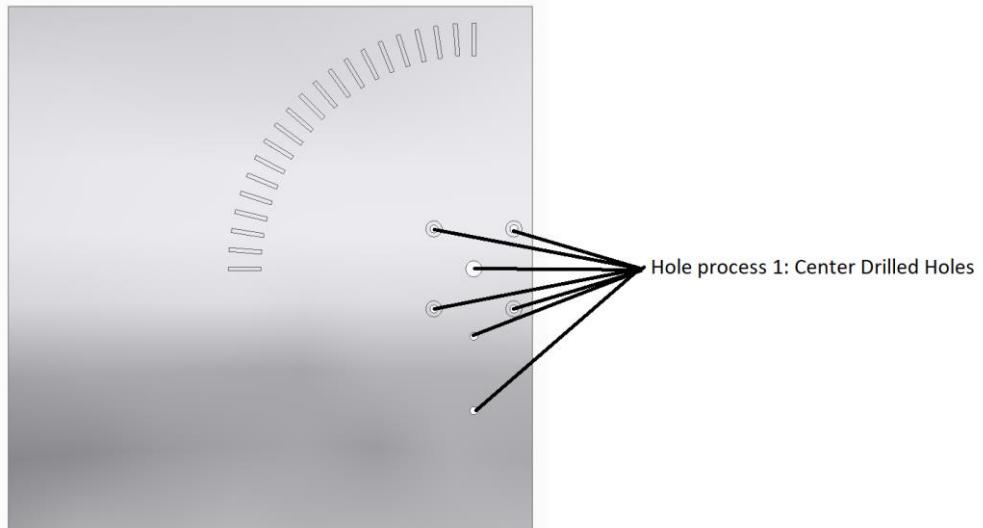


Figure 11: Center Drilled Holes

Process 2

The second process was a hole process to drill the six 1/8" holes for the screws. Every screw being used on the project (M3s and #4) had a shank size slightly less than 1/8", so all the holes where screws would be mounted were drilled to be 1/8". The 4 holes in a square pattern Marked in black, **Figure 11** were to fit the M3 screws being used to mount the stepper motor. The two holes in a line Marked in blue, **Figure 12** were used for the #4 screws that were used to mount the backplate which held the sensor.

Feeds and Speeds:

- Spindle Speed: 3000 RPM
- Plunge Rate: 15 IPM

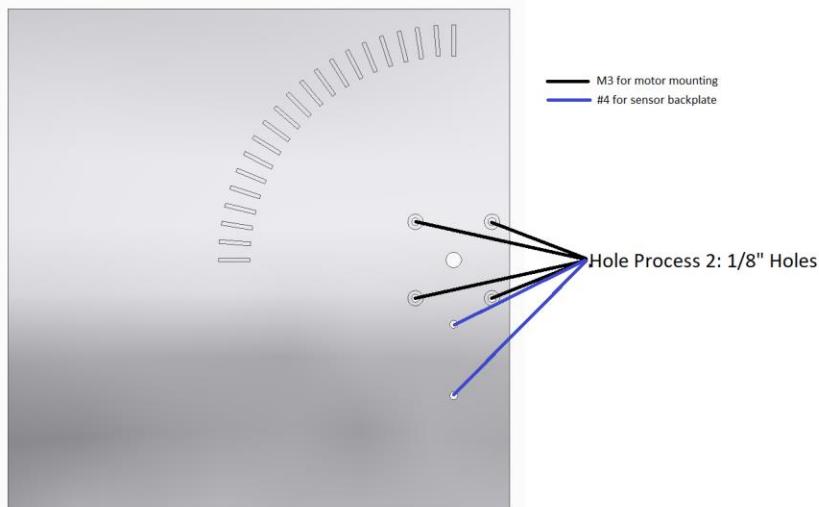


Figure 12: 1/8" Screw Mounting Holes

Process 3

The third process included drilling a 1/4" hole to make room for the shaft of the stepper motor – shown in **Figure 13**. The stepper motor shaft was 5mm, or ~0.197in, in diameter. The 1/4" hole gave enough room to guarantee the motor rotated cleanly.

Feeds and Speeds

- Spindle Speed: 3000 RPM
- Plunge Rate: 15 IPM

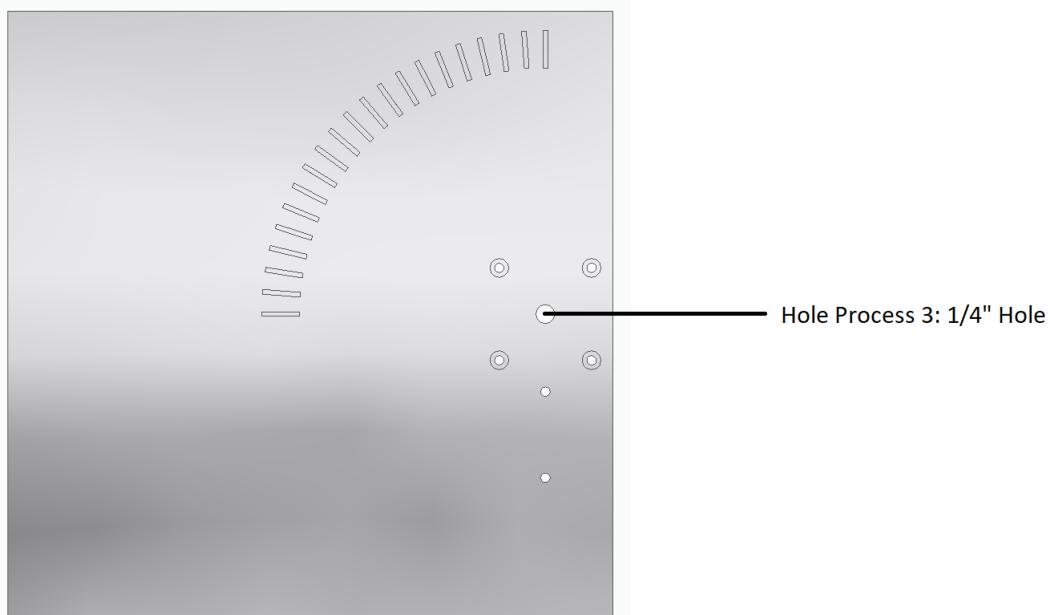


Figure 13: 1/4" Hole

Process 4

The fourth process was a pocketing process used to pocket out the spots in the metal where the screw heads used for mounting the motor would be recessed. A 3/16" end mill was used for this bit, as it was slightly smaller than the pocket size, so it made the machine circle and create a clean cut. The bolt heads were recessed to allow rotation of the protractor pointer. The pocket is 1/8" deep, to accommodate the 2.5mm (~0.098in) screw head. **Figure 14** shows the locations of the holes on the plate in relation to the other geometric entities.

Feeds and Speeds

- Spindle Speed: 6500 RPM
- Feed Rate: 30 IPM

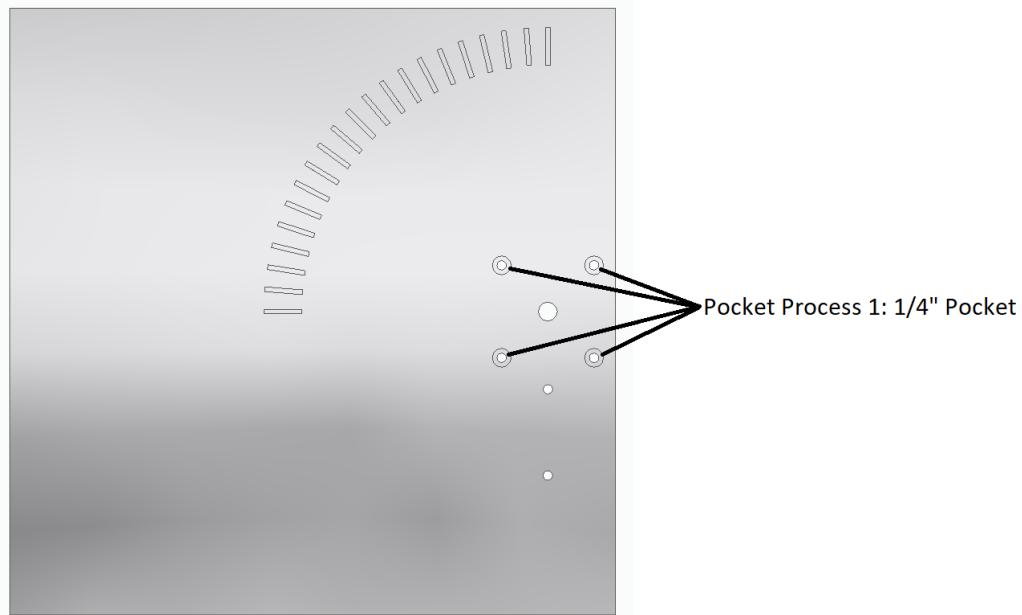


Figure 14: Pocketed Screw Head Recess

Process 5:

The final process was to create the grooves that indicate angle. This was done using a surfacing process using an engraving bit. The grooves had to be shallow, approximately 0.01" deep, to not break the bit during machining, due to the strength of the material. The grooves are highlighted in **Figure 15**.

Feeds and Speeds:

- Spindle Speed: 6500 RPM
- 30 IPM

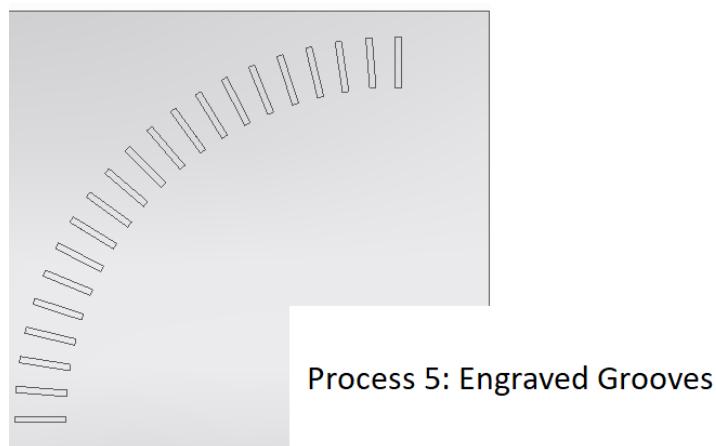


Figure 15: Engraved Grooves

b. Pointer and Sensor Mount

The pointer and mount for the sensor had to be made by additive manufacturing, as traditional manufacturing methods would have been ineffective. Both the pointer and the sensor mount were printed out of PLA. ABS was another potential material, but printing ABS is more expensive and time consuming.

For the pointer **Figure 16**, the printer did a 10% fill grid. This means that of all the volume being used by the pointer, 10% of it was PLA, the rest was air. 10% is a relatively low fill, so the piece was lighter and able to be printed much faster than if a higher fill was used. Because there was no load of any significance being exhibited on any part of the pointer, it made sense for it to be a low fill, so that it could be printed faster.

For the Sensor Mount **Figure 17**, the fill had to be slightly higher, due to the fact that there was a point of worry **Figure 18**. This point was very thin, $< 1/16"$, and it was also the point at which the sensor bent around. The worry was that the bending sensor may flex the thin piece point out of being straight, thus throwing off measurements. Using a 25% fill, the point was much sturdier and resistant to flexing. It took a little longer to print, but it helped prevent erroneous data at large bends.

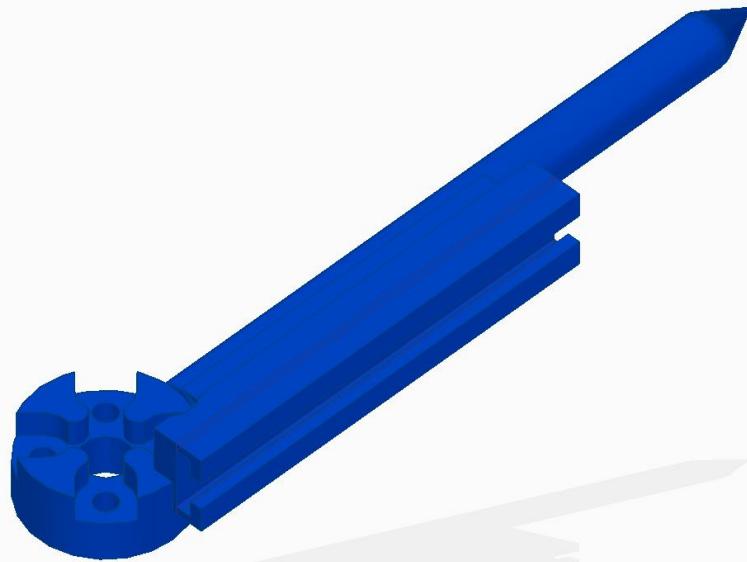


Figure 16: Pointer

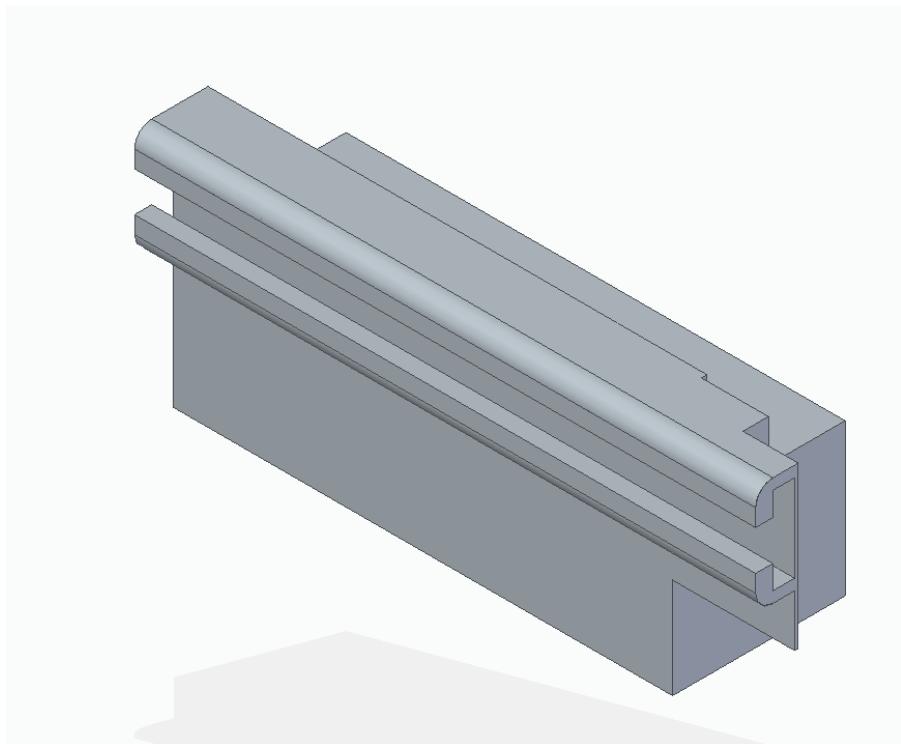


Figure 17: Sensor Mount

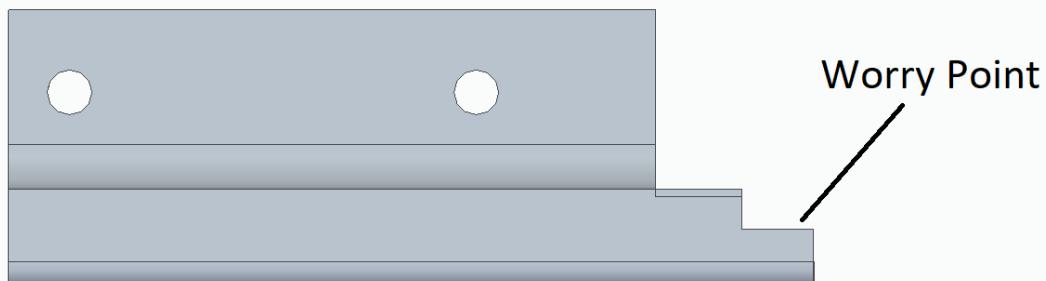


Figure 18: Top view of Sensor Mount with Worry Point

c. Polycarbonate sides

The polycarbonate sides were cut to size on a vertical bandsaw. The polycarbonate sides were attached with double sided tape. This was acceptable since the sides were not under any load. Without a load, the tape was strong enough to hold it together.

3.8. Assembly and Wiring

The assembly process started with connecting the aluminum top plate to the four plexiglass sides. After test drilling holes into the corner of the plexiglass it was determined that cracking would most likely occur. This led to the use of 3M double sided clear adhesive tape that is typically used to hold windows in their frame. This provided over 100 theoretical pounds of adhesion between the aluminum and plexiglass providing a robust structural enclosure to contain the testing equipment. The resulting completed enclosure can be seen below in **Figure 19**.

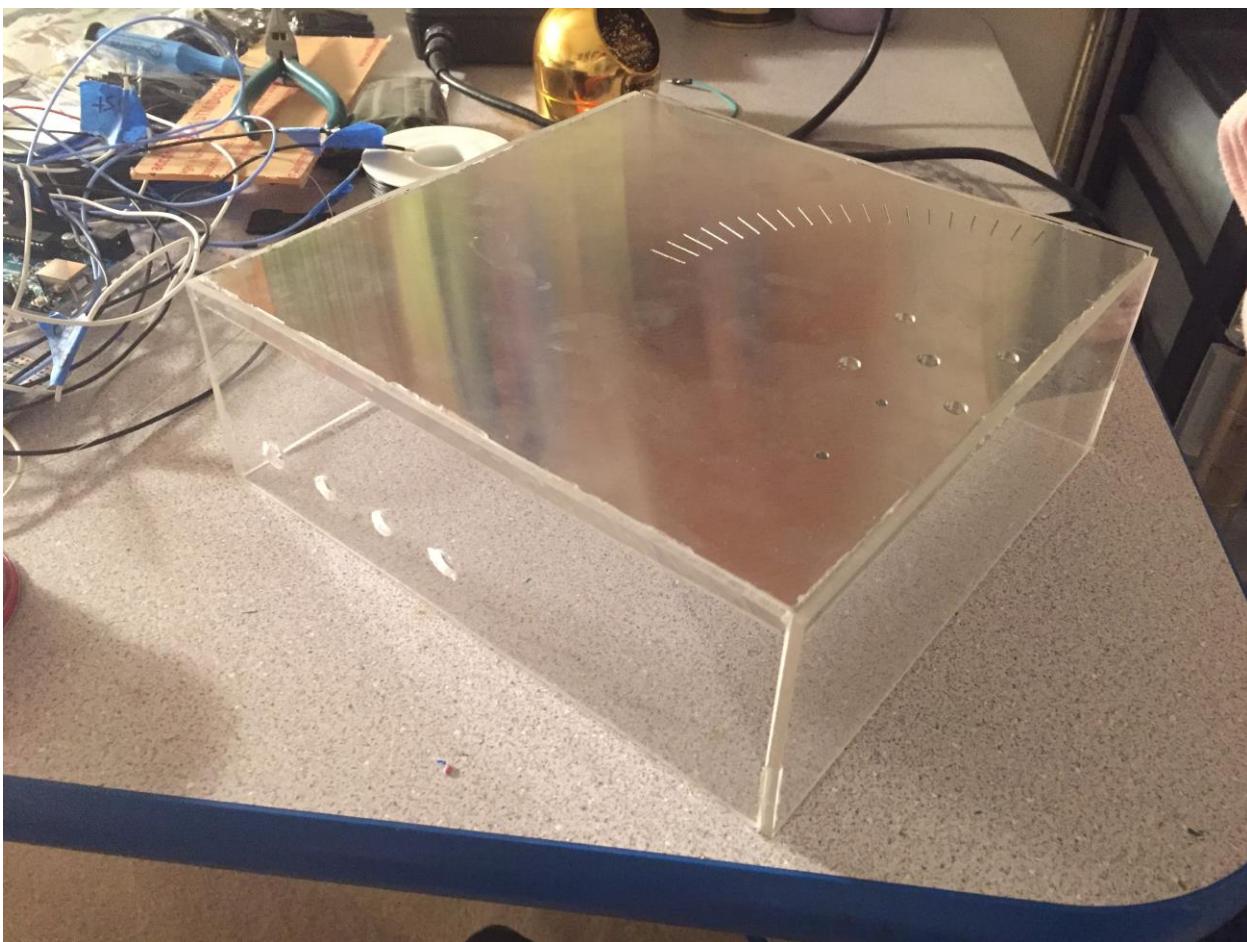


Figure 19: Assembled Enclosure

The wiring had been utilized on a breadboard during initial testing as seen in **Figure 20**.

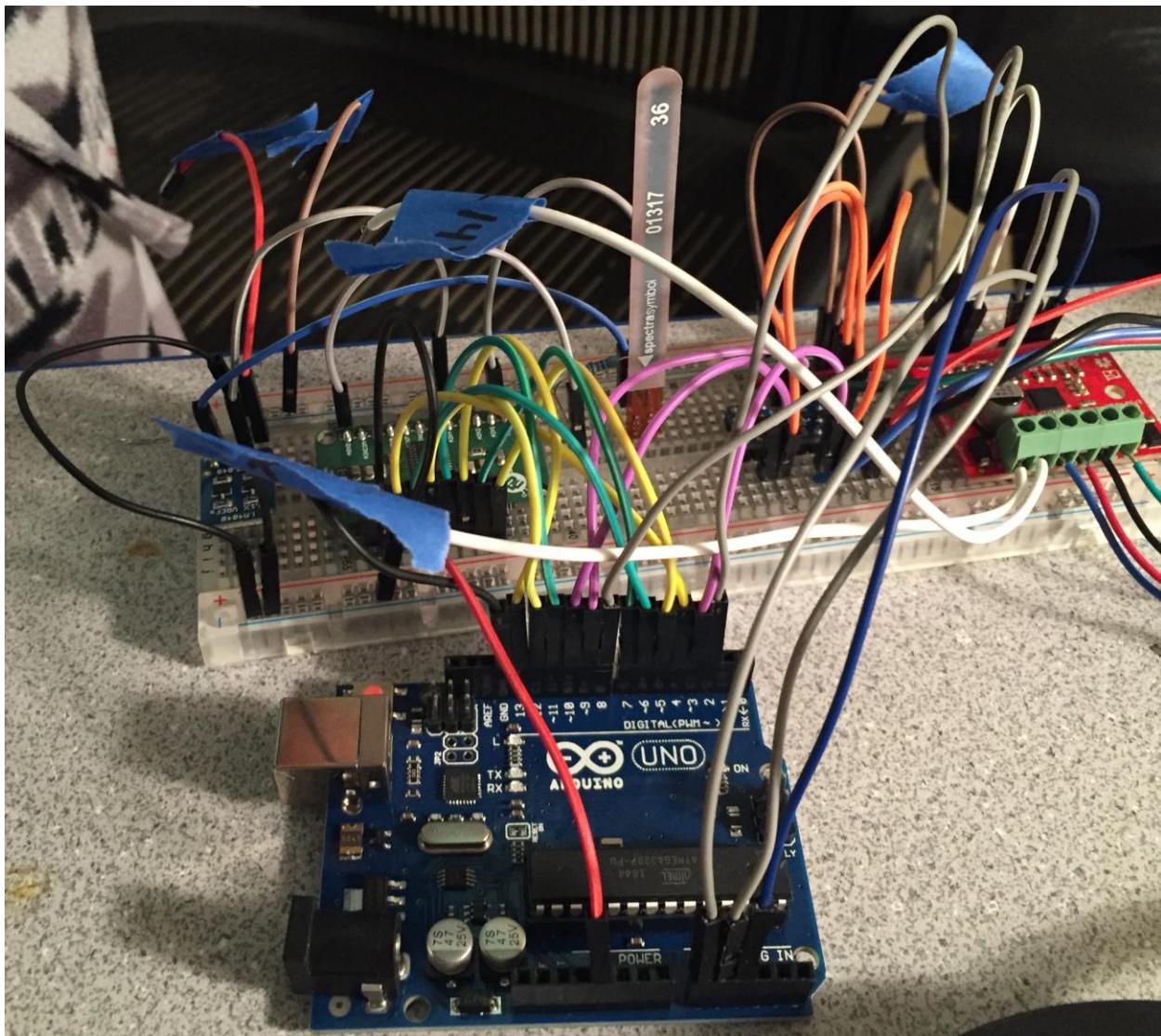


Figure 20: Prototype Breadboard Wiring

This needed to be converted to a more permanent solution once it had been verified that it worked. This came through the use of a solderless breadboard, which all the components were transferred to, populating it as seen in **Figure 21**.

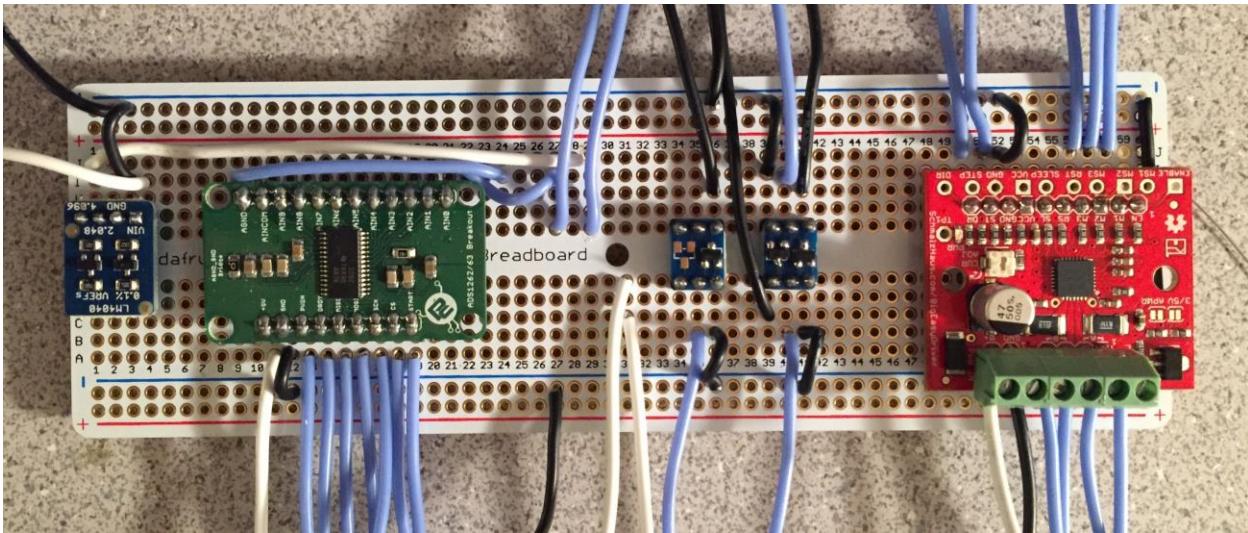


Figure 21: Solderless Breadboard Wiring

The power jacks were then attached to the side of the enclosure and the remaining power connections were soldered together. Once all of the connections were completed, the solderless breadboard and Arduino were stuck to the bottom side of the machined plate with 3M double sided pads. They were used to ensure that no shorts occurred between the pins on the lower side of the electronics, thus providing an electrically nonconductive insulating layer. The stepper motor was then mounted in place and the wires were screwed into the terminal connectors on the stepper motor driver. This completed the inside of the enclosure that can be seen below in **Figure 22**, on the next page.

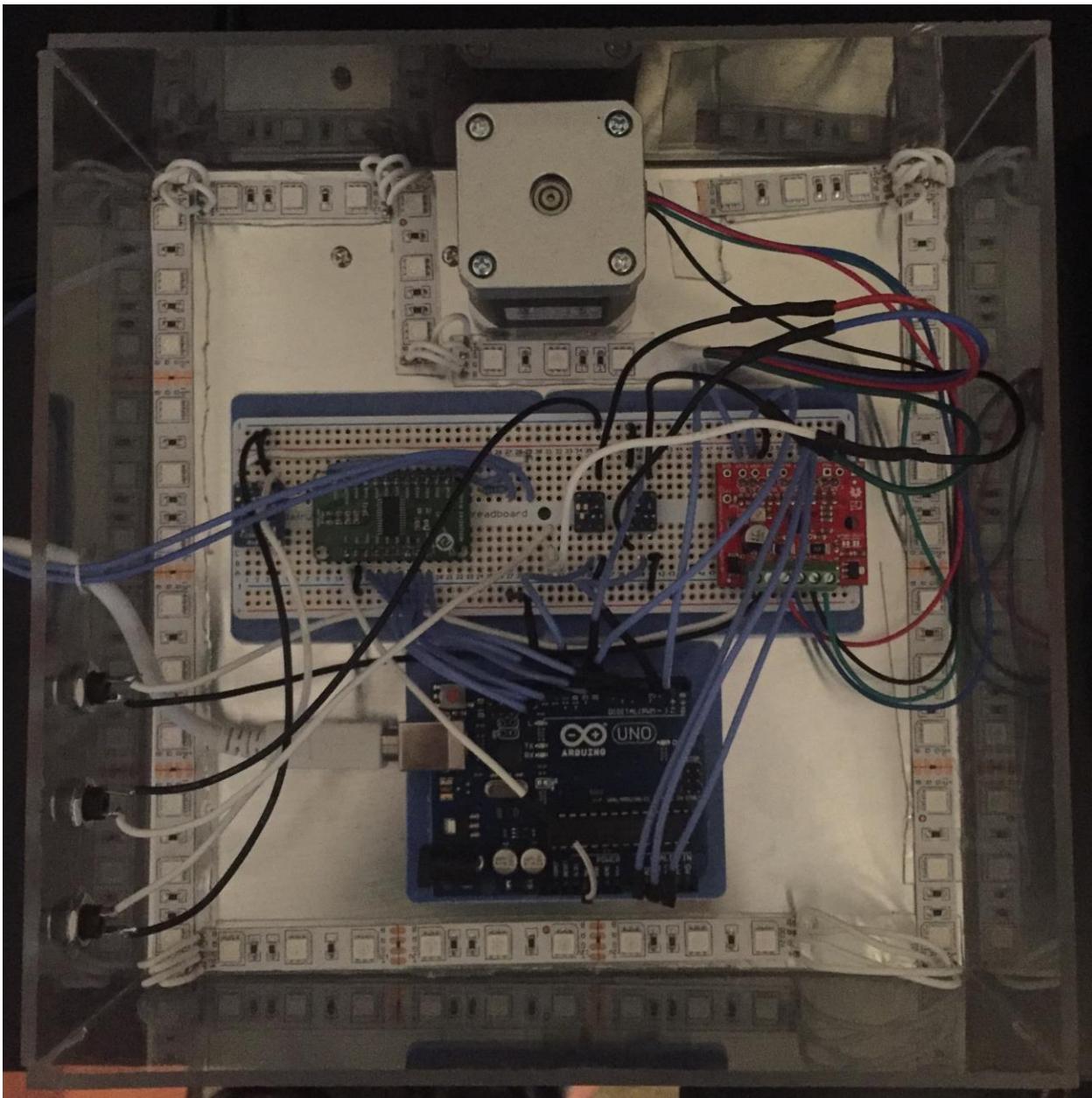


Figure 22: Inside the finished Enclosure

The upper side of the aluminum plate was then populated with the 3D printed components. An aluminum hub was screwed into the 3D printed part and mounted on the stepper motor shaft by turning the set screw. The other half of the 3D printed assembly that holds the flex sensor was secured using screws to the aluminum plate. An attempt was then made to slide the flex sensor and it was discovered the plastic had slightly expanded. An old rusted throttle cable was used as an abrasive surface inside the channel to widen it slightly. After this the flex sensor was successfully slid into the 3D printed assembly and locked into place perfectly. The completed upper portion of the assembly can be seen on the next page in **Figure 23**.

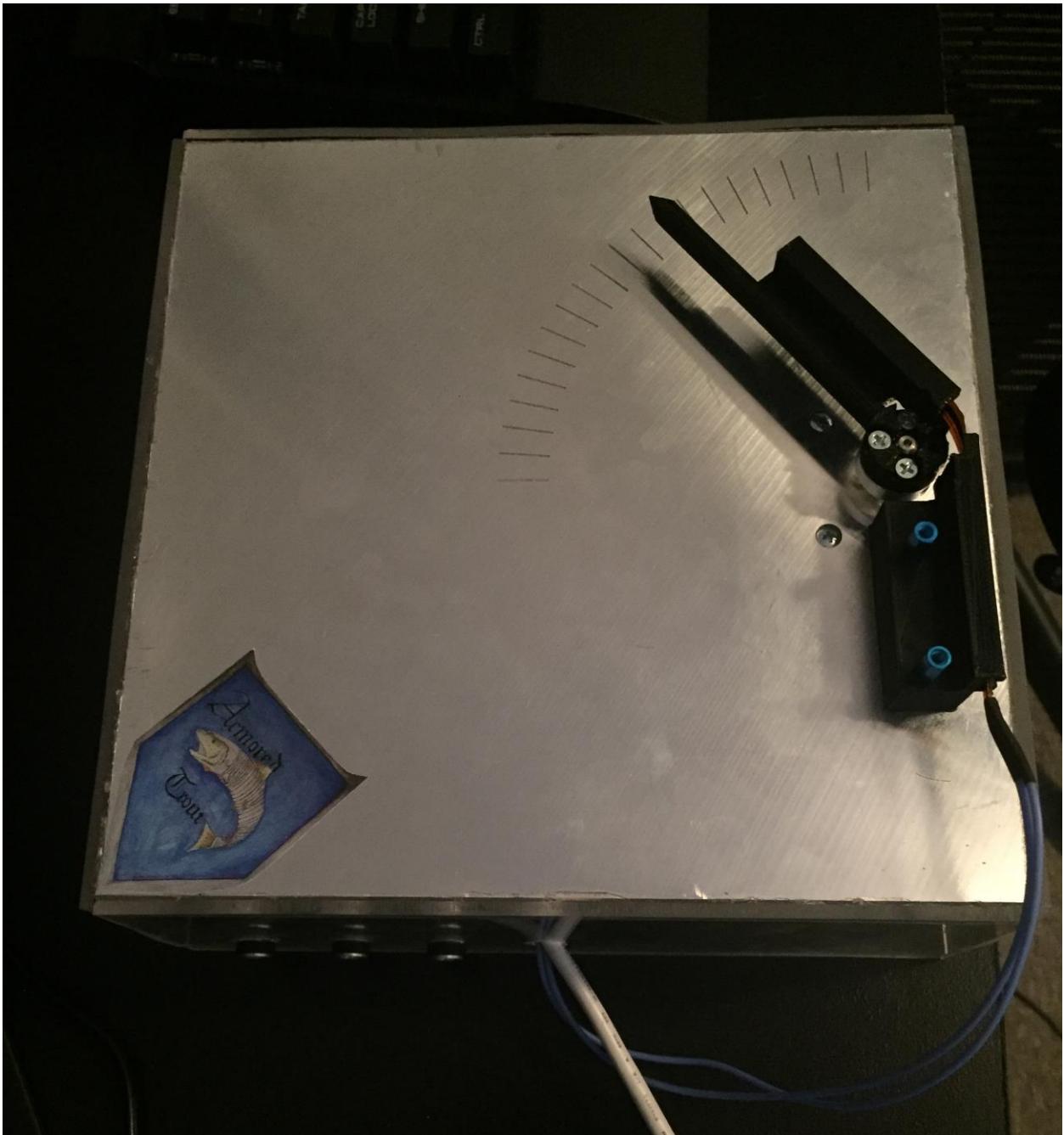


Figure 23: Finished Enclosure

3.9. Testing Setup

Once assembly was completed, tests were completed to ensure the device functioned as expected. A large offset was initially observed with the measurements; however this was later fixed with the calibration. Wide sweep testing of the stepper motor showed that it needed fine tuning to work properly with the stepper driver being loaded at a perpendicular angle. During testing three different power supplies had to be plugged in: 5V for the voltage reference, 12 V for the LED strip, and 14 V for the stepper motor. This was in addition to the USB cable providing data communication to the computer. Although, once the enclosure was powered and the Matlab script was run, data would consistently flow into the script and its logic flow. Once testing was completed and all necessary scripts were terminated, the enclosure could be disconnected and stored until further testing was desired.

4. Theory of Operation

4.1. Flex Sensor

a. Background

The device reads measurements through the Flexpoint bend sensor. The Flexpoint bend sensor we are using is a single layer one-directional bend sensor. This means that the sensor can only take data when bent in one direction. This sensor is a coated substrate that changes electrical conductivity as it is bent. The single layer design reduces risk of sensor damage and interference due to dirt, heat, liquid, and pressure effects [2]. These sensors are durable and used in variety of applications such as the measurement of mechanical movement, air and water flow, vibration and can be used as a durable switch in harsh environments [3]. Flexpoint makes a bi-directional sensor which is being applied to technology in gloves and the bio-medical field due to its durability and ease of bending [4].

b. Mounting

Mounting the digital sensor in a perfect fit was essential in ensuring slippage did not occur. Pressure mounts through the use of screws were considered but there was concern for unreliable resistance measurements [5]. It was decided the channel would be made slightly too small and softly ground out afterwards until the sensor fit perfectly. This worked quite well and the sensor slid as expected on the arm portion and was locked in by friction on the secured end of the mechanism.

c. Measurement Type

The measurement of angles tends to have a myriad of options available to the user for sensors. Instead of using a linear movement with a rotational potentiometer which is typically used on robotic joints a change in voltage is much easier to parse with one application mounting [6]. The change in resistance of the sensor has just recently been brought to such fine detail. This translates to a more accurate and precise angle being obtained by the sensor. The angle is critical for fast moving control of the robotic leg. This high accuracy angle measurement translates to multiple engineering fields if properly sampled at a 32-bit rate.

d. Resolution and Sensitivity

It was expected that minuscule twitching from the stepper motor would provide a slight vibration thus skewing the measurements in either direction [7]. It was also discovered that since the tiny surface mount die resistors on the polyimide base layer were being constantly moved ever so slightly that the resulting change was quite large. Combined with the 4294967296 theoretical levels translating to voltage increments of $9.5367432e-10$ Volts it can be seen the high sample rate with floating point precision translated to a wide swing of measurements. Although when the average of the measurements was taken it could be seen that they tend to center their origin around the desired angle, thus with DSP could be filtered properly.

4.2. Voltage Divider

A voltage divider circuit was used in order to reduce the output voltage and have an accurate reference voltage to use for the conversion calculations. The varying resistance of the flex sensor can be described by the voltage divider equation as seen below in **Equation 1**.

$$V_{out} = V_{in} \left(\frac{R_2}{R_1 + R_2} \right) \quad (1)$$

Where V_{in} is input voltage, V_{out} is output voltage, and R_1 and R_2 are the resistance values of the acting resistors in the circuit. The typical wiring schematic for a voltage divider circuit can be seen below in **Figure 24**.

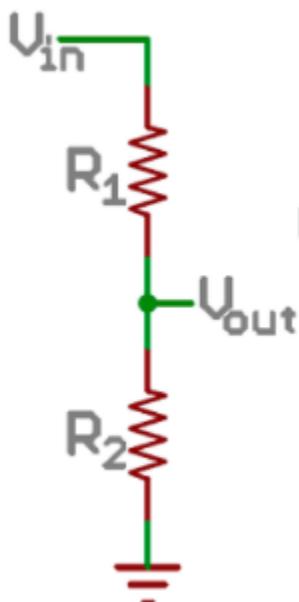


Figure 24: Voltage Divider

In the case of this project, R_1 is a varying resistance due to the fact it is represented by the flex sensor. R_2 and V_{in} are known pre-measured values that do not change, thus enabling the equation to be solved for R_1 to know how much the flex sensor has changed position.

4.3. Stepper Motor Driver

The stepper motor has input pins that receive current from a supply. Stepper motors are driven by energizing the phases in a patterned sequence to make a step occur between coils. Using the generated waveform to command a sequence of steps enables precise control over the test bed environment. By varying the phase angle between coils the stepper motor driver is able to enable microstepping mode [8]. Microstepping provides the ability to move the stepper motor at finer steps than listed by the manufacturer through the use of phase current angles. Through the myriad of features available, the stepper motor driver is able to effectively provide reliable control over the reference for the system under test.

4.4. ADC Sampling

An ADC converts the analog signal to digital periodically. Thus, “sampling” the input at a specified period and rate. This allows an output of discrete time and discrete amplitude signal, rather than continuous time and continuous output signal. For the circuit in this project, a 32-bit ADC was used to sample the varying voltage of the voltage divider circuit [9]. This analog voltage signal is then converted to a digital signal and fed to the host microcontroller over SPI.

5. Tasks and Costs

The original Gantt chart, detailed in **Figure 25**, outlines which team member is responsible specific aspects of the project. Hunter Phillips was the team member responsible for the bend sensor wiring and programming. The wiring was done on a bread-board until everything was finalized and was then transferred onto a solder board. Hunter wrote the Arduino and Matlab scripts that took data from the Arduino and transferred the data into readable output in Matlab that could be written to Excel. This included a live time graph of the angle being read and an output to excel after a set number of data points.

In the original plan, Jacqueline's main duty was a kinematic analysis and animation of the arm. After discussion with the team this was later deemed unnecessary because the arm was not a four-bar linkage as usually is analyzed in kinematics and a simple protractor could be an accurate method of testing our accuracy, as well as comparing to the known stepper motor value. Because of this change, Jacqueline took more of a role in uncertainty, sensor research, and testing. For uncertainty this included planning out methods that could be used ahead of time, assisting with the code for the live time uncertainty, doing Chauvenet's method on the data and creating plots and graphs with the uncertainty from the data [10].

Darnisha Crane's role as specified in the proposal was to perform uncertainty and calibration. Since Jacqueline took more of a role in uncertainty, Darnisha focused more on testing and calibration. This included extensive tests of the stepper motor and bend sensor as well as taking data and calibrating the device using the method discussed in the calibration section.

Austin Click was responsible for the CAD design, construction and collaborating with Darnisha on calibration. Austin worked with Walter on CAD design and assembly of the device. Austin and Walter designed the mechanical components of the robotic arm and housing for the electrical components. He wrote the document presented during the project update that detailed the method of calibration that we would use.

Walter Deitzler was the machinist for the team. In addition to working with Austin on the CAD model, Walter 3-D printed the robotic arm as well as machining the aluminum plate with the engraved marks every .9 degrees.

The report was split up similarly to the physical tasks. Hunter and Walter were responsible for the Device Production Section which details the mechanical assembly as well as circuitry and code. Hunter and Jacqueline co-wrote theory of operation. Jacqueline was responsible for the Tasks and Costs section as well as collaborating on the Calibration and Uncertainty section. Darnisha assisted on the Calibration and Uncertainty section with Austin as well as writing the lessons learned section. Austin was the compiler of the report. All team members met together to review and revise the report before submission.

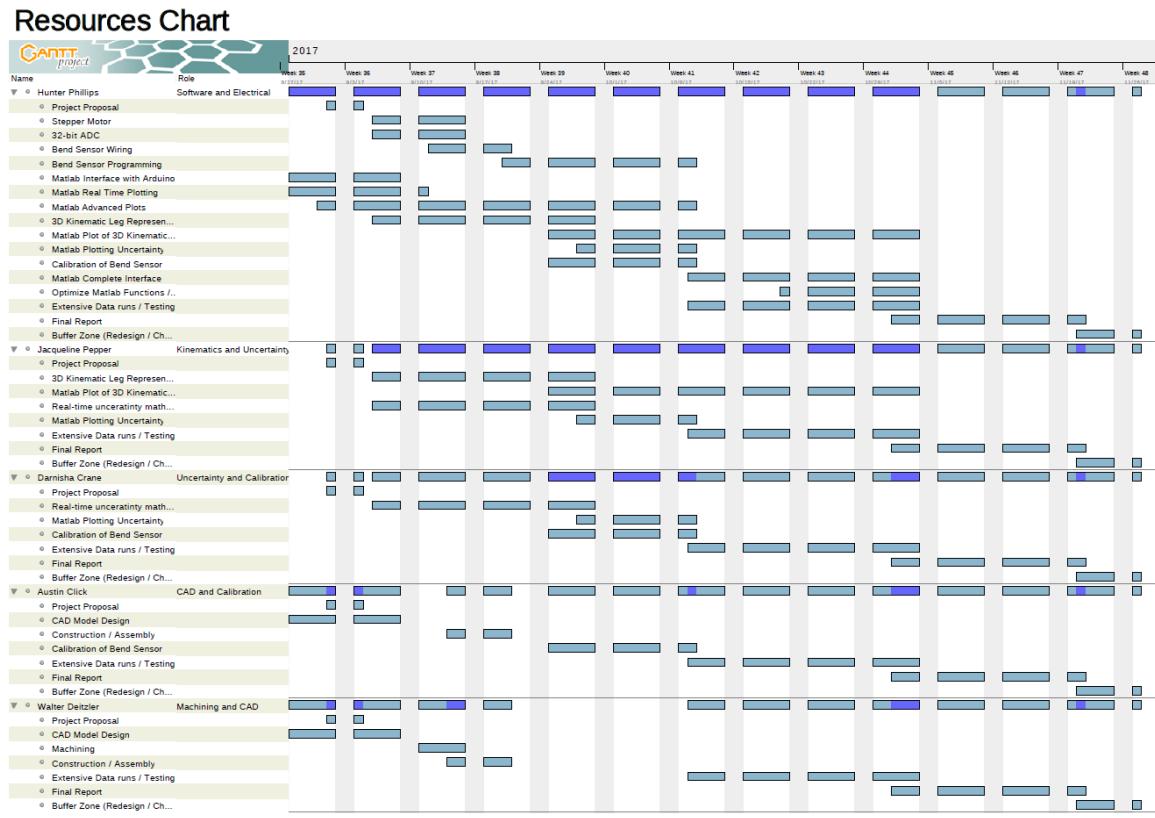


Figure 25: Time Management and Project Schedule Chart

The original Gantt chart timeline was disrupted due to a delay machining the device. The arm needed to be 3-D printed and the aluminum plate needed to be engraved on the CNC machine. Both of these require approval to do in the UAH machine shop. The aluminum ended up being machined in the UAH machine shop, but the arm was 3-D printed in the space hardware lab.

The below bill of materials, **Table 1**, lists all materials used for the project. The “Big Easy Driver” from Sparkfun is the driver motor for the stepper motor purchased. The Arduino Uno was purchased from Sparkfun as well. The 32-bit ADC was purchased from Protocentral. The Precision Voltage Reference, Perma-Proto Half-sized Breadboard, and SOT-23 Breakout Set were all purchased from Adafruit. The plexiglass sheets used belonged to a team member. The aluminum sheets used to create the housing were purchased from McMaster Carr. The bill of materials listed in the proposal did not change throughout the project.

Table 1: Bill of Materials

Part Name	Price	Link
Big Easy Driver	\$19.99	https://www.sparkfun.com/products/12859
Stepper Motor (400 steps / rev)	\$16.95	https://www.sparkfun.com/products/10846
Arduino Uno R3	\$24.95	https://www.sparkfun.com/products/11021
ProtoCentral 32-bit ADC	\$50.94	https://www protocentral com/analog-adc-boards/1005-protocentral-ads1262-32-bit-precision-adc-breakout-board-0642078949630.html
Precision LM4040 Voltage Reference	\$7.50	https://www.adafruit.com/product/2200
RGB LED Strip - 1 meter	\$9.95	https://www.sparkfun.com/products/12021
FlexPoint Bend Sensor	\$12.20	http://www.flexpoint.com/product/bend-sensor/
Adafruit Perma-Proto Half-sized Breadboard	\$4.50	https://www.adafruit.com/product/1609
SOT-23 Breakout Set	\$4.95	https://www.adafruit.com/product/1230
1/2" x 12" x 12" Plexiglass Sheet		
1/8" x 12" x 24" Plexiglass Sheet		
1/4" x 8" x 8" Aluminum Sheet - 86825K724	\$22.32	https://www.mcmaster.com/#standard-aluminum-sheets/=195n9so
1" x 1" x 18" Aluminum 6061 - 6546K21		https://www.mcmaster.com/#standard-aluminum-hollow-tubing/=195naau

6. Calibration

The process of calibrating the bend sensor directly impacts the accuracy of the measurements recorded. To generate a curve that the MATLAB script could follow and generate points from, a defined method of calibration had to be set forth. Calibration went as follows.

1. A MATLAB script to increment the stepper motor by a predefined accurate amount had to be written. This was done by Hunter Phillips and Austin Click.
2. The exact steps of the motor were calculated to determine the degree increment per step. The data sheet for the motor states there are 400 steps per revolution. **Equation 2** shows this calculation.

$$increment = \frac{360}{steps} = \frac{360}{400} = .9 \frac{\text{degrees}}{\text{step}} \quad (2)$$

3. When this was done, an exact increment was known. Because the bend sensor changes resistance with each increment, the Arduino reads a different resistance at each increment. This resistance is then associated with a specific degree increment.
4. Resistance values for each increment were recorded from MATLAB directly to a CSV file. For the testing increment of 90 degrees, 100 points were recorded per step. To generate a valid, accurate curve, this was repeated enough times to generate 5 quality data sets.
5. Each CSV was then imported into Microsoft Excel to generate a mean and reject outliers, if there were any. Using Excel's standard deviation function, average function, and Chauvenet's Criterion, data was reduced [10].
6. The mean and standard deviation for each increment are given in the Appendix, and the full calibration document is given in the Online Appendix.
7. The mean after rejecting outliers for each point was used to plot the curve that was necessary for MATLAB functionality. Angles could also be extrapolated through the two nearest points, as the high resolution of the curve gives the highest possible accuracy available through the Arduino.
8. The mode of each data set was also considered as the calibration was done. For example, if a specific value had many points that were the same, but one outlier, the mode was taken instead of the mean, as this was thought to be a more solid comparison (and could even be the mean without outliers). This method was design as a backup plan and was not used.

The calibration curve is shown in **Figure 26**. Also plotted is the line of best fit, and the R^2 value. Individual data sets can be found in the Appendix, Section 10.2., figures

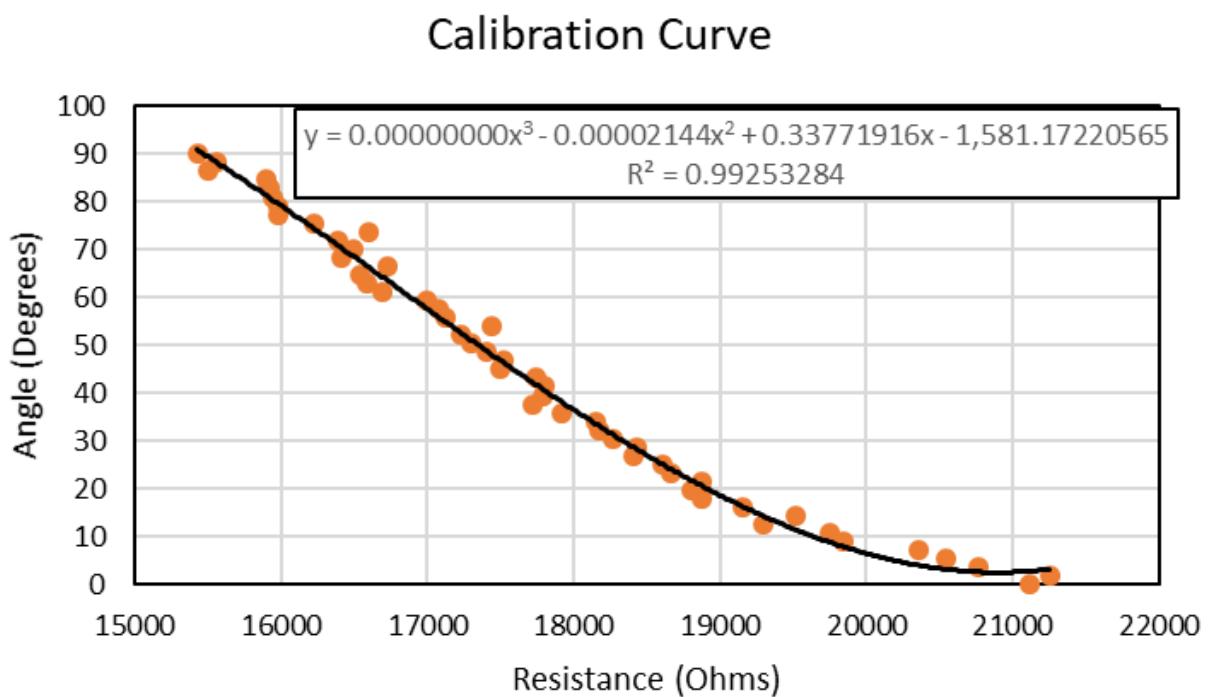


Figure 26: Calibration Curve

7. Uncertainty Analysis

Once the device had been calibrated measurements were taken every 10 degrees and compared to a known stepper motor angle. At each angle, 100 data points were taken. In order to evaluate whether Chauvenet's should be applied, all the data was plotted.

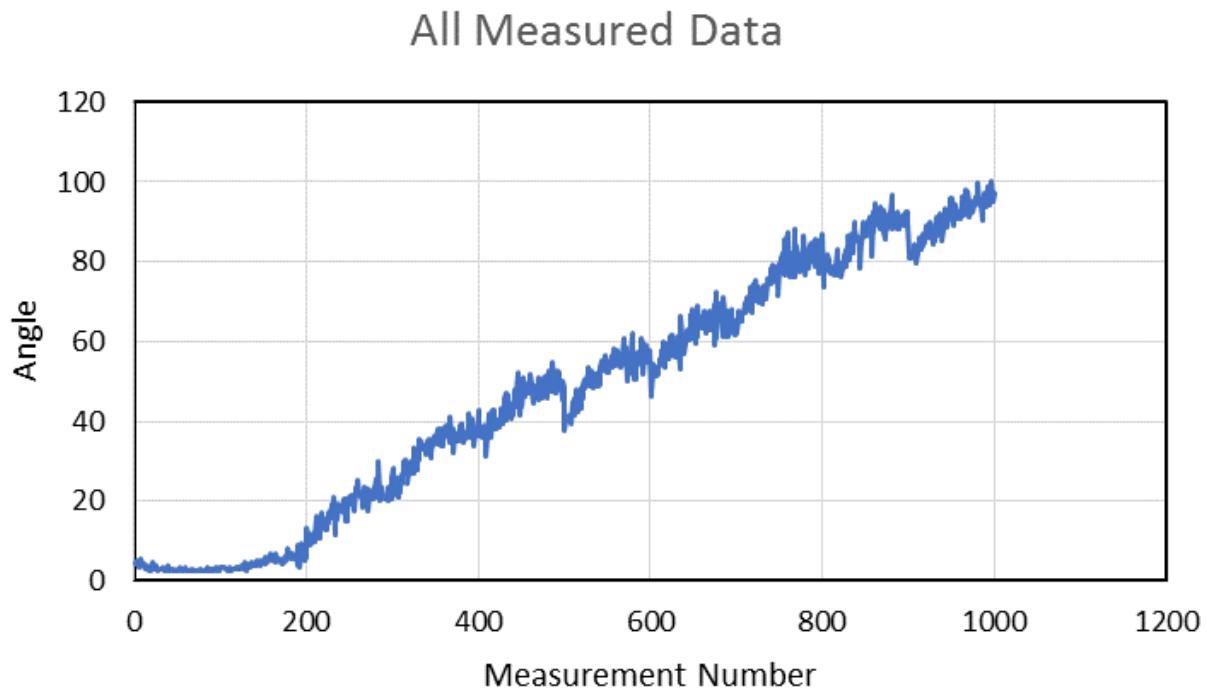


Figure 27: Raw Data

Figure 27 displays the raw data from the first set of data taken after calibration. Having known the device to have random spikes in the past, and seeing that there could be some outlying data points, Chauvenet's criteria was used, but no outliers were found. Raw data can be found in **Appendix section 10.4**.

The mean and standard deviation were taken of each set of 100 measurements corresponding to a specific stepper motor, shown in **Table 2**, on the next page. Raw data that was used to create this table is included in **Appendix section 10.4**.

Table 2: Angle and Error

Reference Angle	Mean Measured Angle	STDEV	Difference	%Error
0	3.066103377	0.615854059	3.066103377	-
10	4.721091445	1.442561212	5.278908555	52.78909
20	18.51655611	4.402685349	1.483443887	7.417219
30	33.29856606	4.988654716	3.298566056	10.99522
40	44.88910136	4.948121998	4.889101359	12.22275
50	51.87002092	5.51185322	1.870020922	3.740042
60	61.26489725	5.316895737	1.264897248	2.108162
70	76.43552672	5.998677265	6.435526724	9.19361
80	85.90880394	5.335016187	5.908803939	7.386005
90	90.69518799	5.061896318	0.695187994	0.772431

This table was used to create several plots to visualize the accuracy of the measurements. **Figure 28**, below, shows the reference angle plot with a trendline, as well as the measured angle.

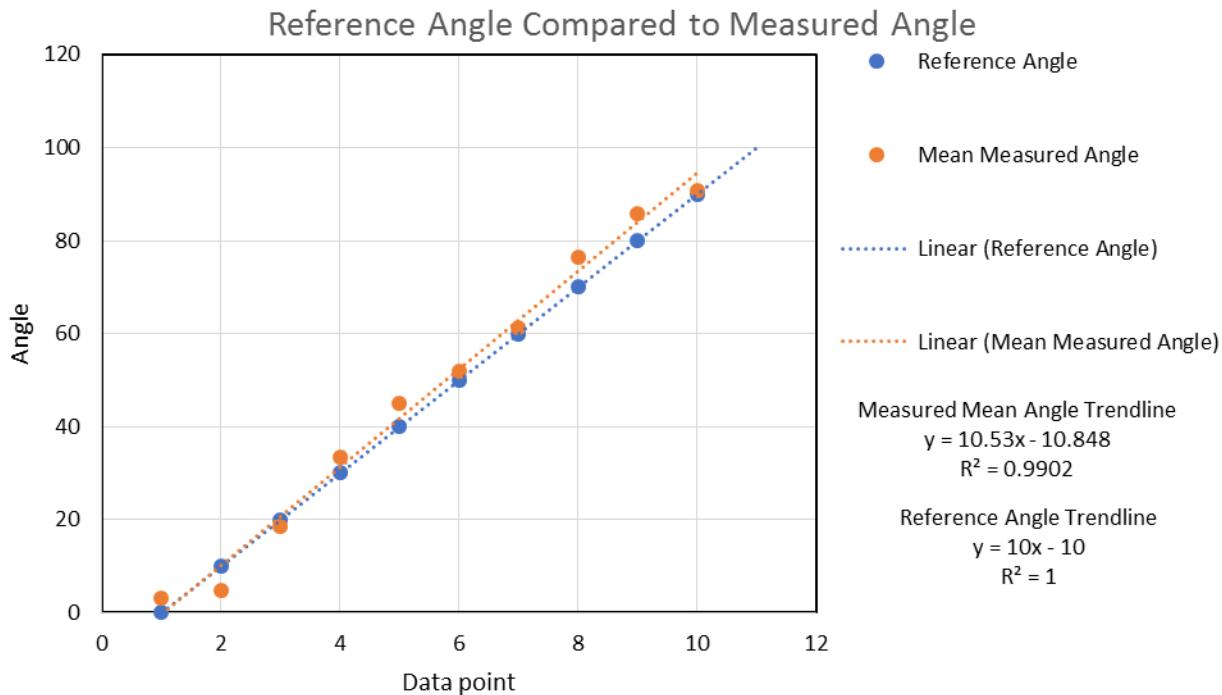


Figure 28: Measured Angle vs Reference Angle

Figure 29 shows the percent error plotted against measurement number.

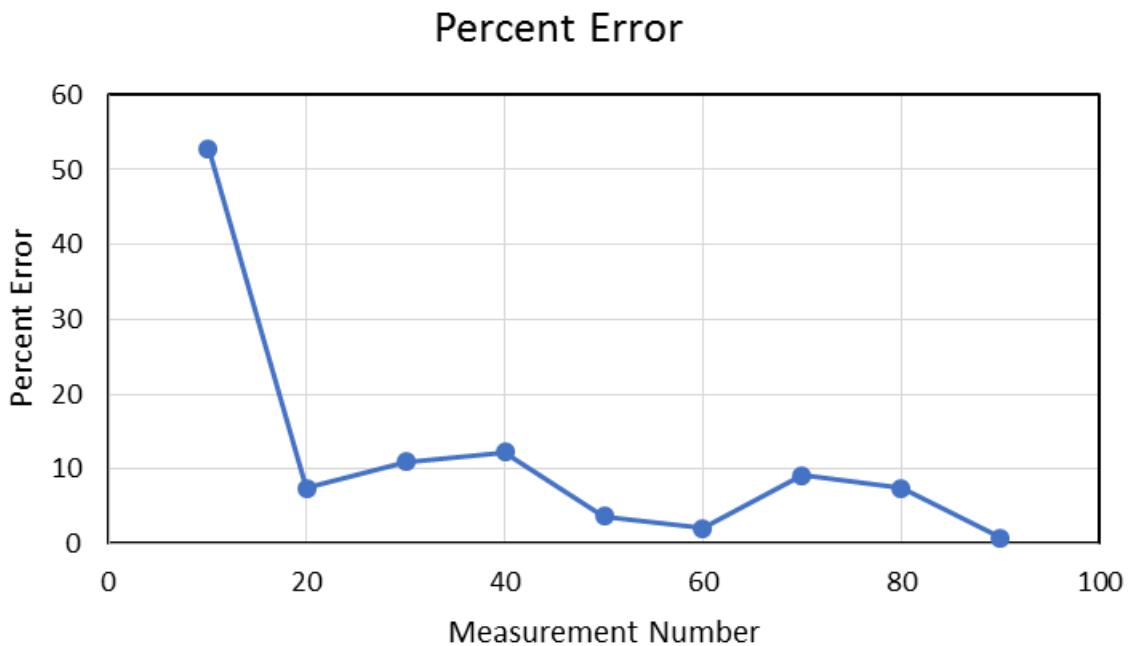


Figure 29: Measurement Number vs Percent Error

Figure 30 similarly shows standard deviation.

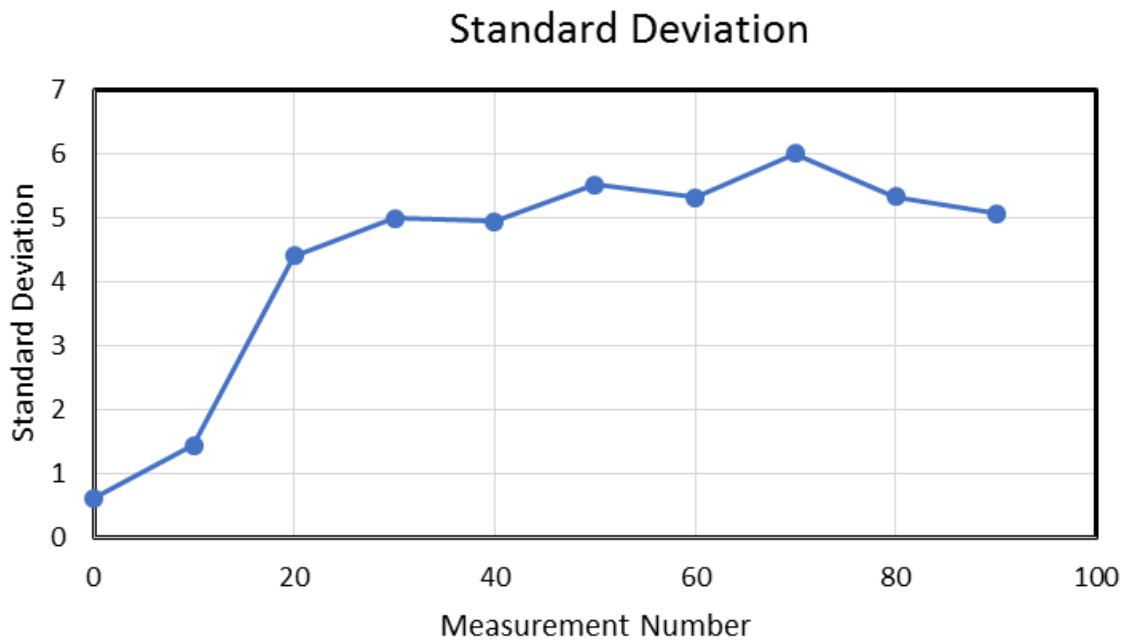


Figure 30: Measurement Number vs Standard Deviation

In order to show the accuracy of the measurements relative to the known stepper motor angle, the measured angle was plotted against the known angle. In an ideal scenario, this would be a linear relationship. It can be noted that compared to the trendline the relationship is almost linear. A perfectly accurate sensor would be perfectly linear with an intercept of zero and a slope of one (1). **Figure 31** shows the measured angle compared with the reference angle, and also includes the slope of reference versus measured angle.

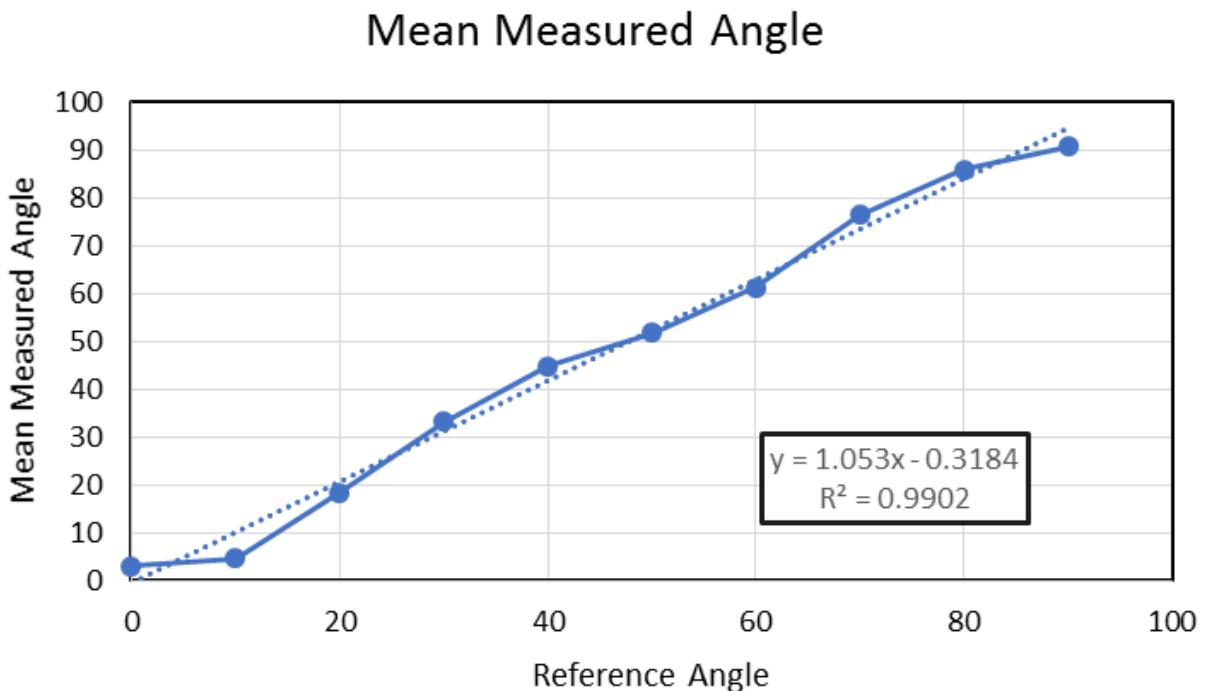


Figure 31: Reference vs Measured Angle

The factors to uncertainty for our device are the stepper motor, sensor, 32-bit ADC, and the voltage reference. The stepper motor has an uncertainty of .05 steps. The largest contributor to the uncertainty is the sensor with an uncertainty of 25%. The ADC has an uncertainty of 78 mV and the voltage reference has uncertainty of .1V. In order to find the total uncertainty, the square root of uncertainty of each component is divided by the value for that component squared as shown in **Equation 3**.

$$u = \sqrt{\left(\frac{u_{stepper}}{stepper}\right)^2 + \left(\frac{u_{sensor}}{sensor}\right)^2 + \left(\frac{u_{ADC}}{ADC}\right)^2 + \left(\frac{u_{volt}}{volt}\right)^2} \quad (3)$$

$u_{stepper}$ = uncertainty of stepper motor

$stepper$ = reference value for stepper motor

u_{sensor} = uncertainty of flex sensor

$sensor$ = reference value for flex sensor

u_{ADC} = uncertainty of 32-bit ADC

ADC = reference value for 32-bit ADC

u_{volt} = uncertainty of voltage reference

$volt$ = reference value for voltage reference

$$u = \sqrt{\left(\frac{.05}{.9}\right)^2 + \left(\frac{.25}{140000}\right)^2 + \left(\frac{.078}{4.096}\right)^2 + \left(\frac{.1}{4.096}\right)^2}$$

$$u = .063601$$

$$u = 6.36\%$$

After inputting the numbers, the total uncertainty comes to 6.36%, which is comparable 5% error in the data taken for uncertainty analysis.

8. Lessons Learned

8.1. Stepper Motor Inconsistent Step Advances

When the stepper motor was being tested, it appeared that it would not turn reliably unless a small amount of pressure was applied to the pointer arm. All the different micro-stepping modes were tried on the stepper motor driver board to alleviate the issue, although none worked. The possibility of not enough current being applied to the coils in the stepper motor was taken into consideration although was quickly passed on since the power supply is 3A which is almost double what the stepper motor requires for full output operation. A final solution was tried through loading more weight on the lever arm and it worked. After further research, it was discovered that sometimes not enough weight on a stepper motor cannot provide enough inertial energy with the coil being electrified and thus won't advance a position. Although this proved to be a disadvantage as it made the pointer arm slight bend downwards ever so slightly. This could cause a variance in the measurement readings from cross-directional bending occurs spiking the resistance. It was decided to just apply the small amount of pressure manually during the calibration and uncertainty analysis to ensure that all data taken as accurate. If the pointer arm was built in the future it would be equipped with more mass so that the stepper motor could function to its full potential.

8.2. Op-Amp Circuit Redesign

The use of a simple voltage divider circuit was the best way the project team knew how to measure a varying resistance into an ADC at the beginning of the semester. Throughout the labs it was hypothesized that if an op-amp was used to amplify the voltage signal a wider range of measurements could be obtained. This would be incredibly helpful as the ADC could have a wider range of voltages to sample. The Flexpoint Electrical Datasheet, found in the **Appendix**, actually lists an op-amp circuit as the recommended design, however at the beginning of the semester, the students were unable to fully understand how the circuit worked and thus avoided it by completing a simpler design.

8.3. ADS1262 32-Bit ADC

The high accuracy and precision provided through the use of a 32-bit ADC seemed promising at the time the project started. After programming with the included libraries, it was quickly realized that the company Protocentral, an Indian company, had minimal tech support and resources available for the user. It was a steep learning curve to fully understand the scope of their libraries and example test script. If the team could go back, they most likely would have chosen a much easier to use 16-bit ADC from a company with great resources such as Adafruit. Although the challenges associated with understanding the vaguely written C++ header files enabled the students to learn a lot about underlying code design. Once implemented and the correct values were being read across SPI by the Arduino, it made for a satisfying experience with the countless hours of work being spent on deciphering the code.

8.4. Linear Interpolation versus a Proper Calibration Curve

It was originally noted that in the datasheet, Flexpoint provides a curve of expected output across a certain bending radius, and it appeared to be a cubic curve across initial inspection. It was assumed that for initial testing a simple linear interpretation between a single obtained data point at 0 and 90 degrees would provide a measurement to a pretty fair degree of accuracy. The students assumed that although they needed to calibrate the device, it wouldn't provide a significant advantage over a simple solution. This assumption was wrong, and the calibrated cubic curve was significantly better across the broad spectrum. It is noted that around the weak point of the linear interpolation, 40 to 60 degrees, the curve exceeded. This is a great example of a big lesson learned with a future impact in the student's careers.

8.5. Accuracy and Precision of Components

The team originally planned to go with the highest precision components available to ensure the best measurement was obtained. After the project update it was brought to the project team's attention that it is not all about precision since you are only referencing the accuracy of the components. This enabled the avoidance of purchasing unneeded components such as a high precision resistor for the voltage divider circuit. A few high precision components were still purchased such as the voltage reference, since it was incredibly reliable and consistent. Since the accuracy is less important as long as it is consistently at that value. To ensure the values were accurate, they were measured with a high quality Keysight Technologies U1241B. This showed that it is not always the most expensive or cutting-edge components that enable a successful project, it is how the team uses the components at their disposal to the highest potential.

8.6. Ground Loop Issues

When the circuit was first wired each component worked when plugged in individually through its voltage rail, although when the 12V and 14V sources were both plugged in an unexpected issue occurred. When the stepper motor was commanded to do a step the LEDs would get slightly brighter. This consistently happened and sometimes they would even cycle different colors depending on the stepping mode chosen for the stepper motor driver. After a lot of trial and frustrating error it was discovered that a small portion of the LED strip was touching the aluminum plate. A small bit of adhesive had contracted and allowed the contact of one of the strips ground pads to the surface. A multimeter was then used to figure out how the short was being tied to the stepper motor. It was discovered that the casing of the stepper motor was somehow internally connected to one of the coils in the stepper motor. Since the metal stepper motor housing was bolted with stainless steel bolts to the aluminum top plate it caused a connection between the LEDs and stepper motor. It is hypothesized that when the coil was electrified in the stepper motor that the short caused a small amount to travel to the LEDs and potential electrical energy was carried across the connection. Resulting in each and every time the stepper motor

was activated causing the potential electrical energy to increase, causing the brightness and colors to vary according to how the coils were being energized. It can sometimes be the smallest of errors in assembling that prove to provide countless hours of frustration, thus showing the team that attention to detail in assembly is critical to successful testing.

8.7. Digital Signal Processing (DSP)

It was noted that the measurements appeared to have a large bound around the origin when testing. This was not seen during initial research and the measurements in commercial products appeared to be fairly stable. After further investigation, it was assumed that the commercial products use some form of DSP to smooth out the oscillating measurements. This is something the team did not have the necessary amount of time to properly implement, however would greatly improve the measurement precision and accuracy. Although with more time a live time DSP algorithm could be used to filter out the wide bounding measurements and obtain the mean origin point. If this could be successfully completed the live-time readings could be significantly more impactful in robotic applications. This taught the students the importance of filtering data and understanding the nuances of your measurement and how to improve the reading with filtering techniques.

8.8. Graphing Real-Time Updating in Matlab

When measurement data is being fed into Matlab it is critical that the graph visually shows the result as fast as possible. When the functionality was first being explored, the team could not figure out why the graph in Matlab would not update. Delays were added in the loop until a 1 second delay was the only way to get Matlab to plot the measurement. To bypass this issue the animatedline functionality was discovered to use different graphics libraries, however ended up being unusable since the team desired a compass type graph. After many attempts, it was discovered that OpenGL can force Matlab to update graphics using the *drawnow update* command. This was not very well document, however made it possible for the team to real-time plot data in a visually appealing compass plot.

8.9. 3D Kinematic Arm

In the original proposal, a 3D kinematic arm rendering in Matlab was explored. Initial testing was completed on the feasibility and it was determined an unnecessary portion of the experiment and that the team's efforts would be better utilized in other areas. This was due to the fact that Matlab does not have a simple interface to render an optimized 3D design. Especially with the conditions the team was placing the graphics processing unit (GPU) under already with the live-time plotting. It was noted that in the future the use of Python and libraries such as matplotlib and numpy combined with Blender would provide beautiful graphics for this kind of design. Preliminary testing also showed that one of the team member's computers, Hunter Phillips, would be able to handle the graphics load with its Nvidia Quadro M4000 graphics card. Although this was not enough to

necessitate the hours being put into it, since the desktop tower could not be transported to UAH for the demo.

8.10. Live-Time Uncertainty

The original proposal also projected the idea of a live-time uncertainty system to show the user the confidence in their measurements being obtained. This would be implemented in a two-prong approach. The user would be able to see a live-time graph with an uncertainty estimation, approximate error, and theoretical error plot. The functionality was actually built in as seen below in **Figure 32**.

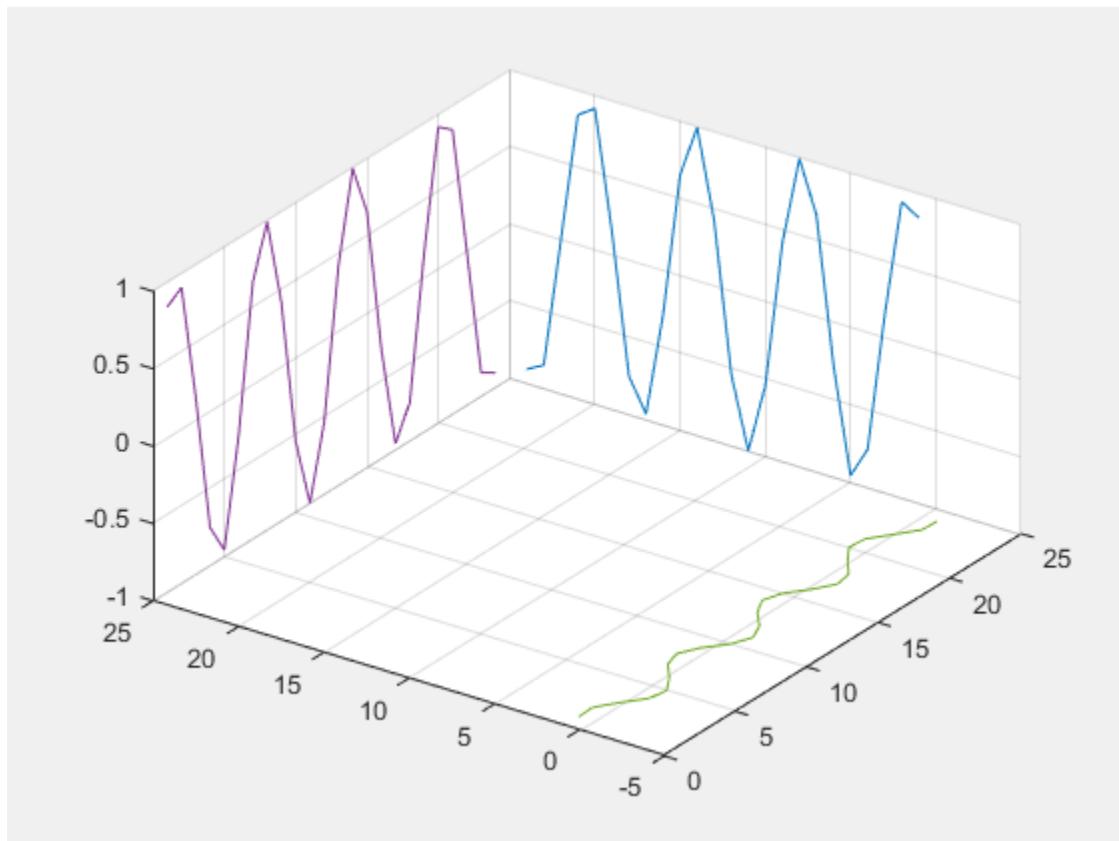


Figure 32: Live Time Uncertainty Plot

The code was never implemented due to the live-time uncertainty code never being reached due to timeline restrictions. Although it required a significant amount of time due to the fact that all 3-axis of the 3D plot had to be filled in real-time ensuring that they were all updated at the same time. This was obtained through the use of axis shifting techniques and array indexing of graphical elements. Purging of old elements in the array was also necessary to ensure that lag wasn't introduced due to the sheer number of points needing to be plotted in the 3D graph.

The LED portion of the uncertainty analysis also suffered the same fate of not having an uncertainty measurements to display in real-time due to time constraints preventing

the code from being written. Although the gradient fading function from green to red was written and can be seen in action below in **Figure 33**.

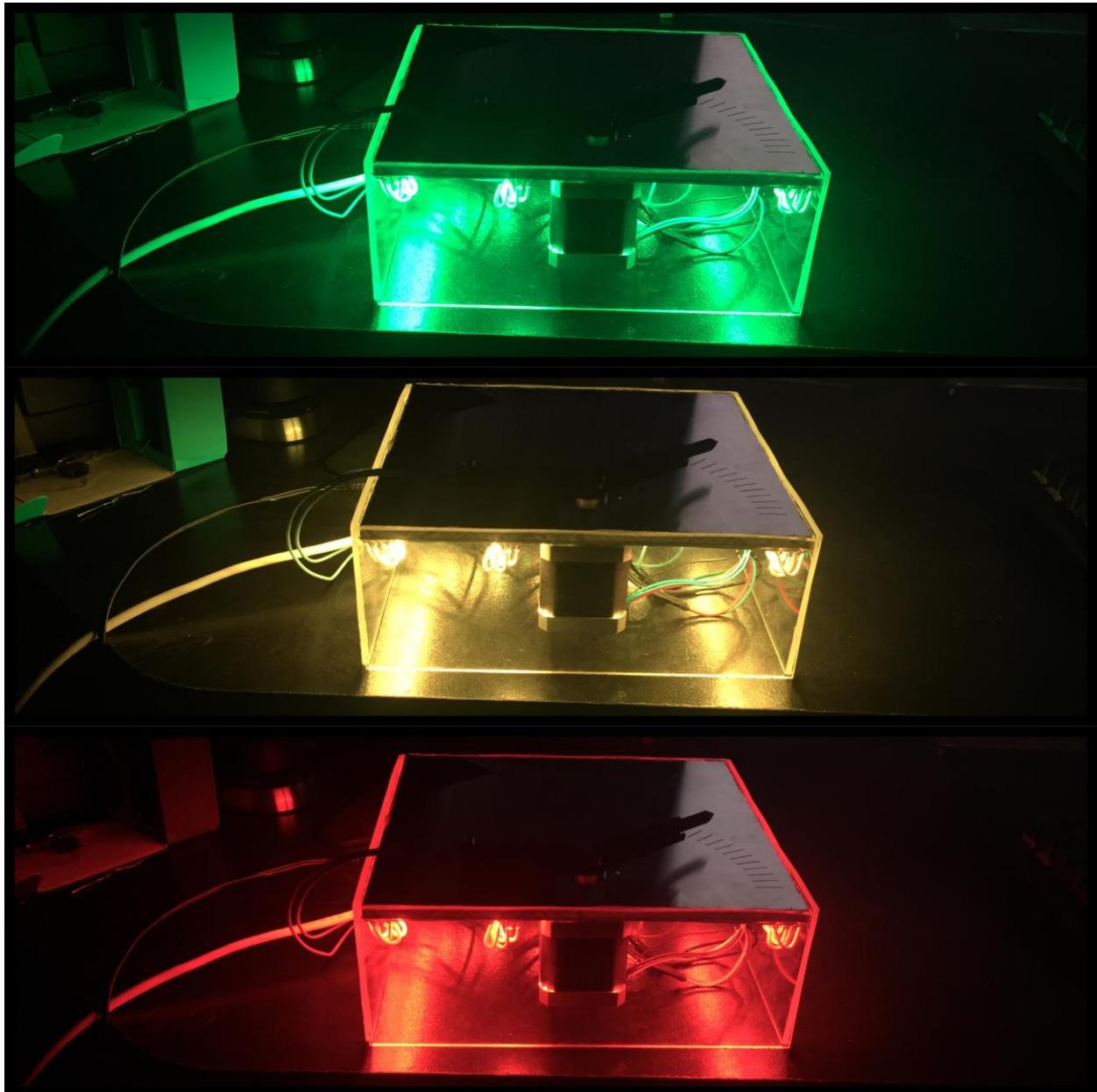


Figure 33: Uncertainty LEDs for Visual Assistance

The original intention of giving the user subliminal visual feedback through the use of LEDs gives the user the ability to notice changes without having to look at the graphs. Understanding the significance of the uncertainty values in the graphs could be hard to visualize, but the use of LEDS provides a simpler approach, since the transition from green to red signifies the measurement is losing confidence in the uncertainty and something might be going wrong with the system.

8.11. Demo Computer Validation

All of the testing on the robotic joint system was completed at Hunter Phillips house on his desktop computer with Windows 10. It was assumed that some initial debugging and testing would have to occur for the demo so the team arrived early on demo day to ensure it would work on another computer. This proved to be a smart decision as the rest of the day was spent debugging tons of issues. Trying to use the 311 labs computers proved to be near impossible since they would not compile the Arduino libraries due to permission errors. Along with a lot of other admin issues on the computers it was decided to move to a couple of team members laptops. Both laptops were missing necessary coding background packages and directory functionality. It also appeared that certain COM functionality was broken with the Arduino as every time the Arduino was unplugged and replugged in, it would no longer transmit data across the TX line. This was later discovered to be issues with the Windows binaries with Hunter's desktop computer having serial libraries already pre-installed from other projects and Arduino automatically detecting them and working. After all these issues were faced it was decided to attempt a rewrite of the code to work on an Apple Macintosh (Mac) computer. It was known that the Excel writing functions would not work on a Mac computer, so this issue was tackled first. With comprehensive research, it was determined that a new xlswrite function needed to be used and the following java libraries added as seen in **Figure 34**.

```
% Setup Excel X Server Apache Libraries
delete(instrfind)
javaaddpath('poi_library/poi-3.8-20120326.jar');
javaaddpath('poi_library/poi-ooxml-3.8-20120326.jar');
javaaddpath('poi_library/poi-ooxml-schemas-3.8-20120326.jar');
javaaddpath('poi_library/xmlbeans-2.3.0.jar');
javaaddpath('poi_library/dom4j-1.6.1.jar');
javaaddpath('poi_library/stax-api-1.0.1.jar');
```

Figure 34: Modifications for Excel Code

After the programming rewrite had been completed the only downside that was noted was the lack of a dedicated graphics unit in the Mac causing 100-200 millisecond delays in the graphing. This huge challenge reminded the team that testing across a large system of computers before demo day is important as different hardware can cause anomalies to appear hindering a smooth testing day.

8.12. Transmitting Floats Across Serial

When the 32-bit ADC was purchased the thought of getting the high precision float measurements to Matlab did not seem to cross the minds of the team. It was quickly realized that the test was not trivial since Arduino did not support this Serial writing functionality. The thought to parse the float into its representative 4-byte chain came after remembering that the IEEE standard can send these shifted bytes as chars across the line encoded. It took forever to realize that a delimiter was needed to prepend the chain for Matlab to understand the following data being parsed. On the Matlab side of code a variety of functions were called to decode the chain and concatenate it back into the original float value. An unusual issue arose, that the byte chain appeared backwards and shifted 2 bits over. To figure out this issue, a known float value was sent across, its hex value being known was then used to figure out where the char values were and how to rearrange them properly. Once it had been completed for one value, the decoding process worked for all incoming encoded float values. This was a huge roadblock in the project progress as it had not been expected initially. Although it taught the team a lot about bit and byte level programming and how to secure data across serial lines between different electronic systems.

9. References

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10. Appendix

10.1. Bend Sensor Mechanical Data Sheets



Bend Sensor® Technology Mechanical Application Design Guide





Bend Sensor® Mechanical Application Guide

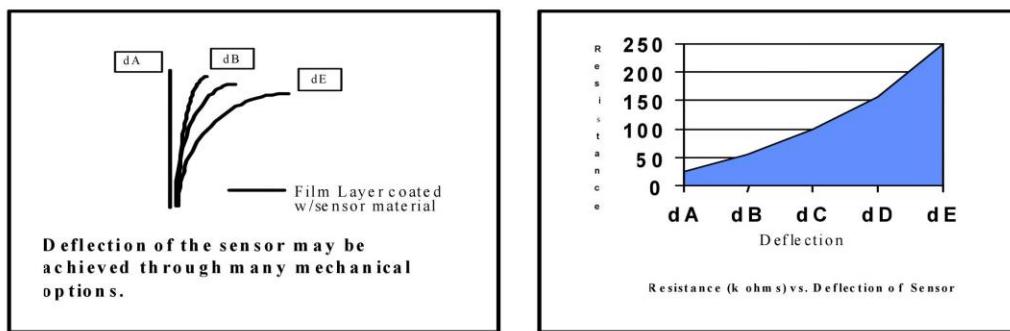
Introduction

This Application Guide is designed to help mechanical designers build interfaces that result in the successful integration of Bend Sensor® components into products. Flexpoint Sensor Systems (Flexpoint) has successfully developed and marketed products incorporating Bend Sensor® technology. As described below the Bend Sensor® device is typically a film – the Bend Sensor® film is put into a system and essentially “goes along for the ride”. The film is attached to a system and measures the movement of the system. Although the sensor itself is capable of being cycled millions of times, the system it is applied to must also be robust. Below is a description of the sensor, and many of the considerations that should be understood in the design of the system.

Description of the Bend Sensor® Device

The Bend Sensor® potentiometer is a product consisting of a plastic substrate coated with a resistive material that changes in electrical conductivity as it is bent. Electronic systems can connect to the sensor and measure with fine detail the amount of bending or movement that occurs. Depending on the configuration and integration of the sensor resistance changes of greater than 10 times can be realized. Refer to the Bend Sensor® Electronic Design Guide (<http://www.flexpoint.com/wp-content/uploads/2015/05/electronicDesignGuide.pdf>) for a description of electronic interfaces.

An example application is one where a sensor is attached to a hinge. As the door is opened, among other things one can measure how far the door is opened and how fast it is moving. The sensor is lightweight, small, easily packaged and very reliable. The breadth of the application for the Bend Sensor® device is limited only by the customer's imagination.



The rate of change as displayed in the graph is dependent on two factors. The first is the bend radius, the smaller the radius the greater the change. Secondly is the angular deflection. For a given radius the more the sensor is bent around it the greater the change.





How the Bend Sensor® Potentiometer Works

Flexpoint's patented Bend Sensor® device consists of a single layer, thin, (0.005" typ.) flexible piece of material that is coated with a proprietary carbon/polymer based ink. This type of resistive element is commonly used to make thick film resistors, resistor networks, slide potentiometers and transducers. Flexpoint's proprietary inks are primarily printed on thin plastic films.

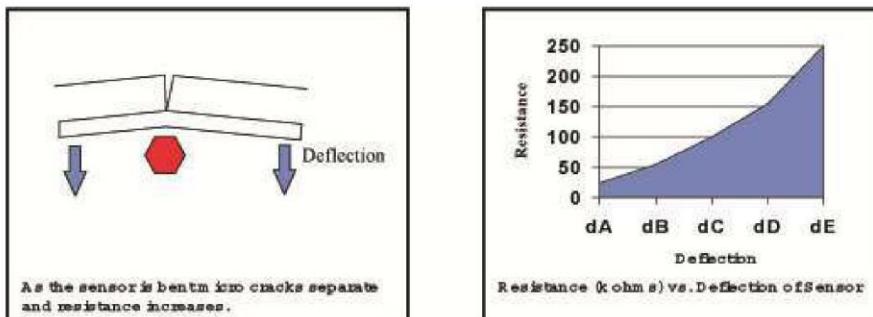
Flexpoint uses a coating that when printed on a plastic film such as polyimide forms a bond that is very strong. The ink is very hard and brittle. During processing micro cracks are introduced into the carbon/polymer coating, when the coated film is bent, the ink's many micro cracks, which upon movement open and close to the specific bending of the material. The ink maintains its integrity in shape and continues to have a very strong bond to the substrate. One of the most unusual characteristics of this ink occurs when the material is bent over a given radius repeatedly. It returns to its original value within the same slope or curve of resistance proportional to displacement.

The sensors are easily customized as the coatings can be applied in many patterns to adjust the resistance and can be screen printed as required by the application. The tremendous reliability, consistency and repeatability of the Bend Sensor® device make it highly desirable to many industries. Other technologies such as force sensors do not display and deliver the reliability and versatility of the Bend Sensor® potentiometer.

As mentioned the Bend Sensor® is a single layer construction. As such dirt, dust and other particulates that cause issue with multiple layer sensors do not affect the Bend Sensor®. The same is true for many liquids including gasoline, diesel fuel, motor oil, antifreeze, alcohol and water to name a few.

Since the coating can be placed on several types of substrates, the sensor may be designed to act as its own spring allowing the sensor to return to its original position.

The proprietary inks are custom manufactured by Flexpoint and can be easily adjusted to the specific resistance requirements of the customer. Flexpoint can design the method of actuation or bending to fit the measurement needs. New inks and products are constantly being developed.



10.2. Bend Sensor Electrical Data Sheets



Bend Sensor® Technology Electronic Interface Design Guide



Introduction

This Design Guide is designed to help electrical designers build interfaces that result in the successful integration of Bend Sensor® components into products. Flexpoint Inc. has successfully developed and marketed products incorporating Bend Sensor® products. Most successful Bend Sensor® interfaces start with the same building blocks. This Design Guide comprises a collection of circuits that effectively empower the designer to modify and build customized circuits that complement their product.

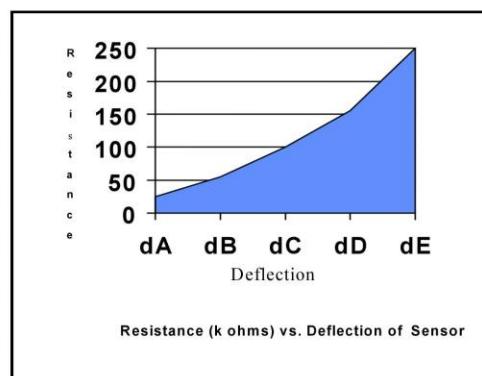
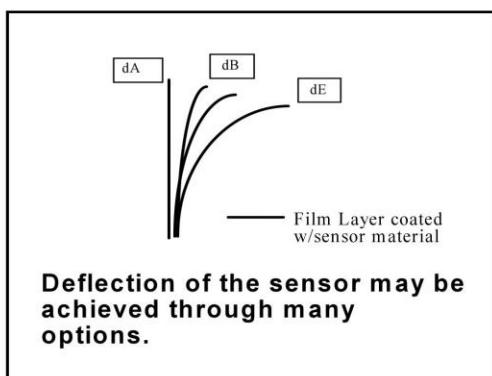
Bend Sensor® Potentiometer

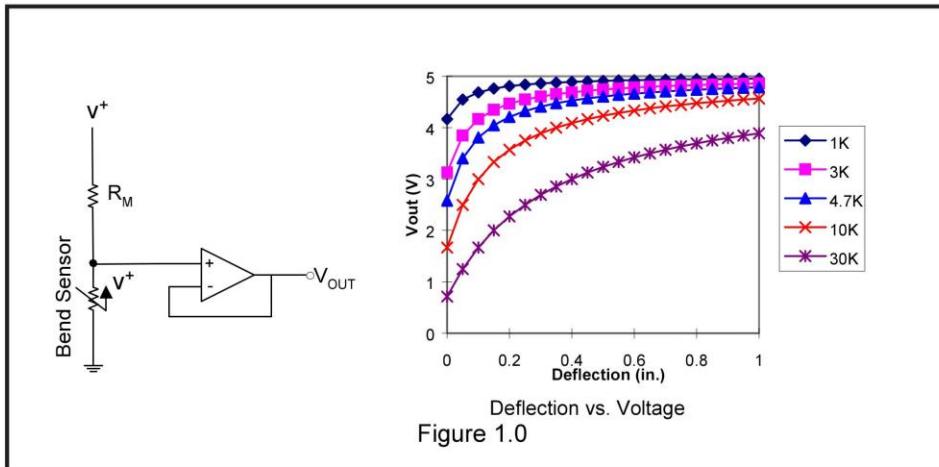
In the late 1980's, a new product was being developed to be a thin (< 0.005" typ.) light weight potentiometer which, when integrated into a glove could provide analog feedback showing finger movement. After substantial development efforts a new product utilizing a bend sensitive ink was created. This new product known as the Bend Sensor® potentiometer was integrated for use in a consumer product known as the Nintendo Power Glove. Many companies have since recognized the simplicity and reliability of the sensor making it an ideal solution which very effectively addresses many issues and challenges associated with standard potentiometers.

Description of the Bend Sensor® Potentiometer

The Bend Sensor® potentiometer is a product consisting of a coated substrate such as plastic that changes in electrical conductivity as it is bent. Electronic systems can connect to the sensor and measure with fine detail the amount of bending or movement that occurs. A movement of only one inch can yield over 200,000 data points.

An example application is one where a sensor is attached to a door. As the door is opened one can measure how far the door has opened and how fast it is moving. The sensor is light weight, small, easily packaged and very reliable. The breadth of the applications for the Bend Sensor® is limited only by the customer's imagination.





Bend Sensor® Voltage Divider:

For a simple deflection-to-voltage conversion, the Bend Sensor® device is tied to a resistor R_M in a voltage divider configuration. The output is described by the equation:

$$V_{OUT} = (V+) / [1 + R_M / R_{Bend\ Sensor^{\circledR}}]$$

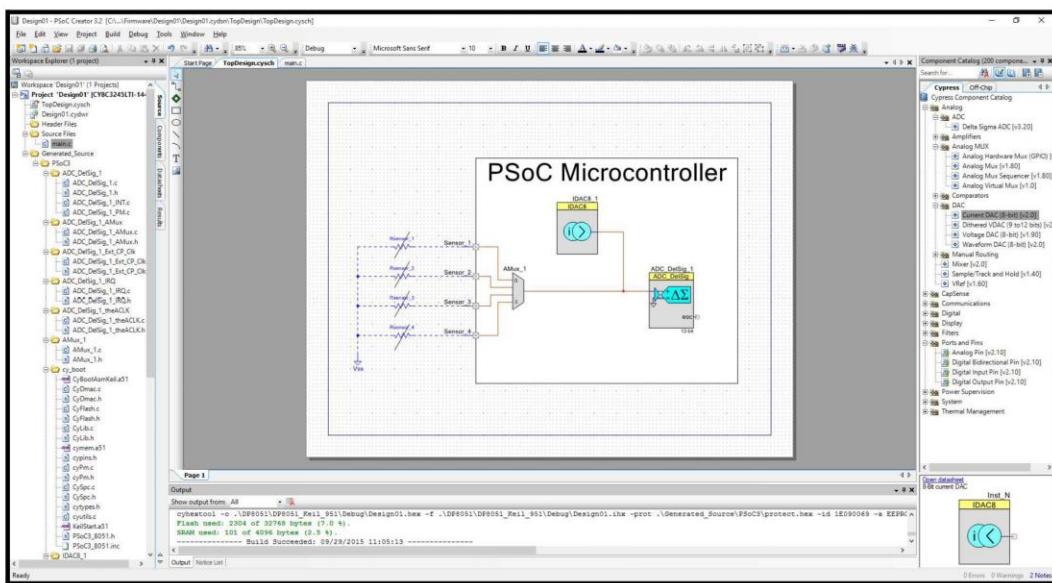
In the shown configuration, the output voltage increases with increasing deflection. If $R_{Bend\ Sensor^{\circledR}}$ and R_M are swapped, the output swing will decrease with increasing deflection. These two output forms are mirror images about the line $V_{OUT} = (V+) / 2$.

The measuring resistor, R_M , is chosen to maximize the desired deflection sensitivity range and to limit current. Suggested op-amps for single sided supply designs are LM358 and LM324. FET input devices such as LF355 and TL082 are also good. The low bias currents of these op-amps reduce the error due to the source impedance of the voltage divider.

A family of DEFLECTION vs. Vout curves is shown in Figure 1.0 for a standard Bend Sensor® device in a voltage divider configuration with various R_M resistors. A (V+) of +5V was used for these examples.



Bend Sensor® Measurement using a Cypress PSoC Microcontroller:

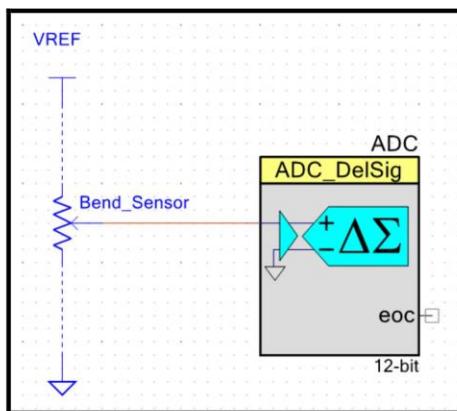


Cypress Semiconductor has a unique microcontroller that has a current DAC. When used in the circuit above the current source sinks current through the Bend Sensor® and generates a voltage across it which can be measured by the ADC. The current DAC also acts like a variable gain amplifier in the circuit which can be adjusted to make sure that the voltage across the Bend Sensor® is always within the range of the ADC. The Mux allows each Bend Sensor® to be measured separately. The PSoC can eliminate the need for any external components to measure the Bend Sensor®.

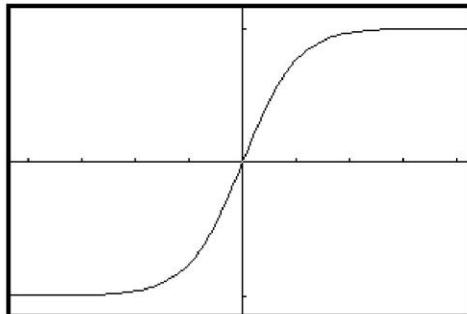


Bi-directional Bend Sensors®:

Flexpoint also makes Bi-directional Bend Sensors®. When bent in one direction one sensor increases in resistance while the other decreases in resistance. This allows for deflection to be measured in either direction. Bi-directional Bend Sensors® share one common pin. Therefore they can be measured individually using many of the above methods as long as the common pin can be tied to VREF or ground. The Bi-directional Bend Sensor® can also be used in a voltage divider circuit using each side as the top and bottom resistor. This looks similar to a potentiometer schematic:



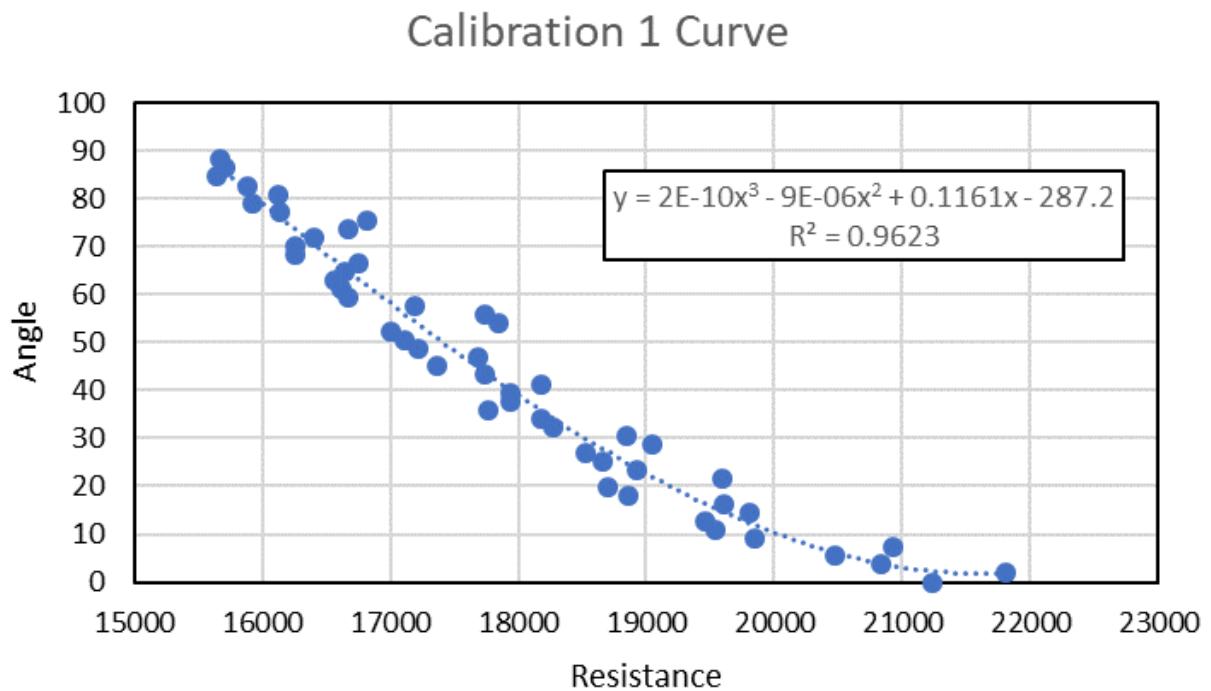
In this configuration the voltage that the ADC will measure will increase or decrease depending on the direction the Bend Sensor® is bent. Because each individual Bend Sensor® cannot go to zero ohms of resistance the response curve looks similar to a hyperbolic tangent function:



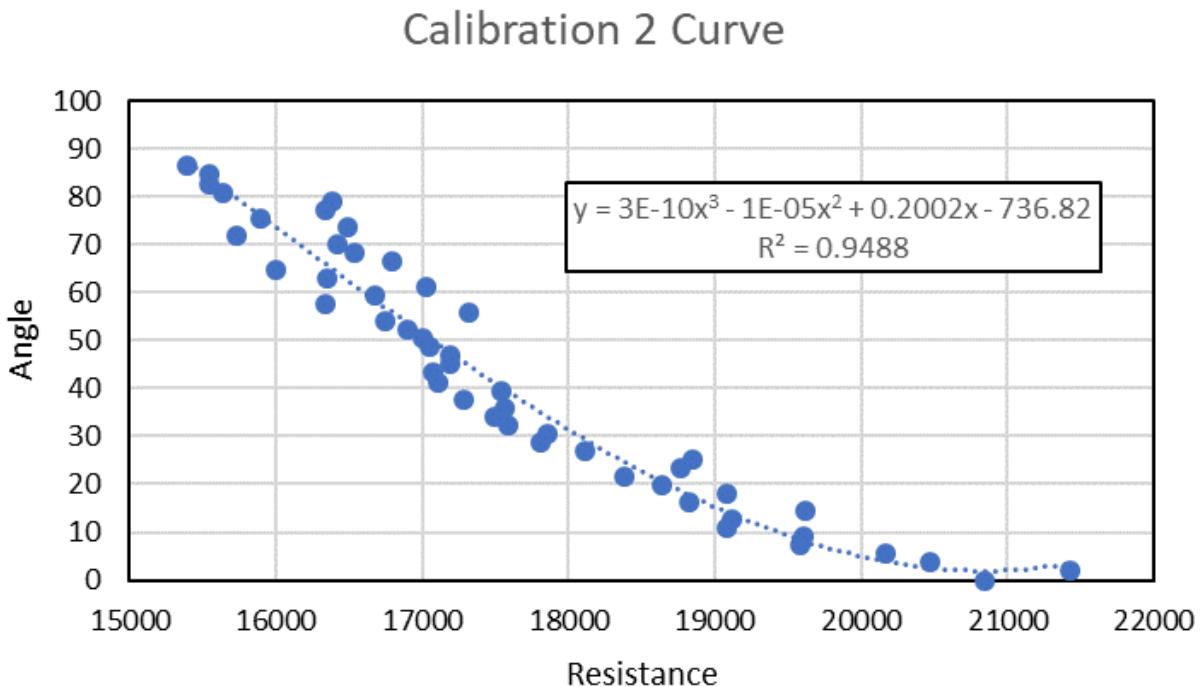
There is however a linear region near the center of the curve ($VREF / 2$).

10.3. Calibration Data Sets 1-5 and Mean Values for Each Reading

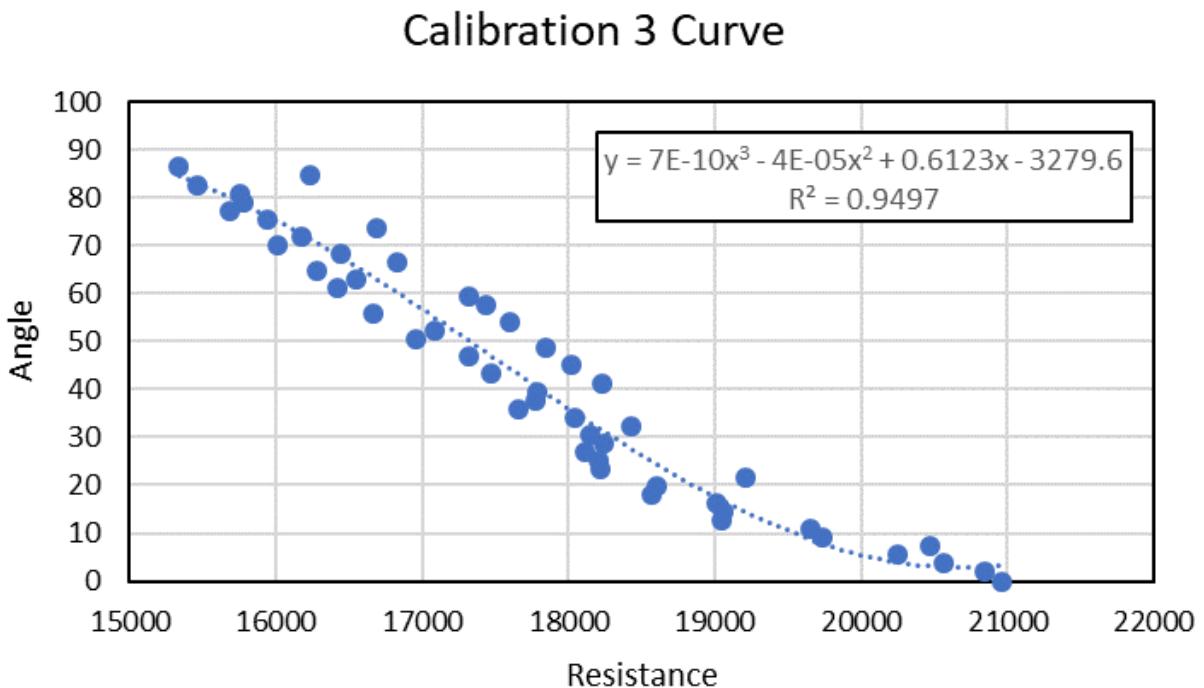
a. Data Set 1



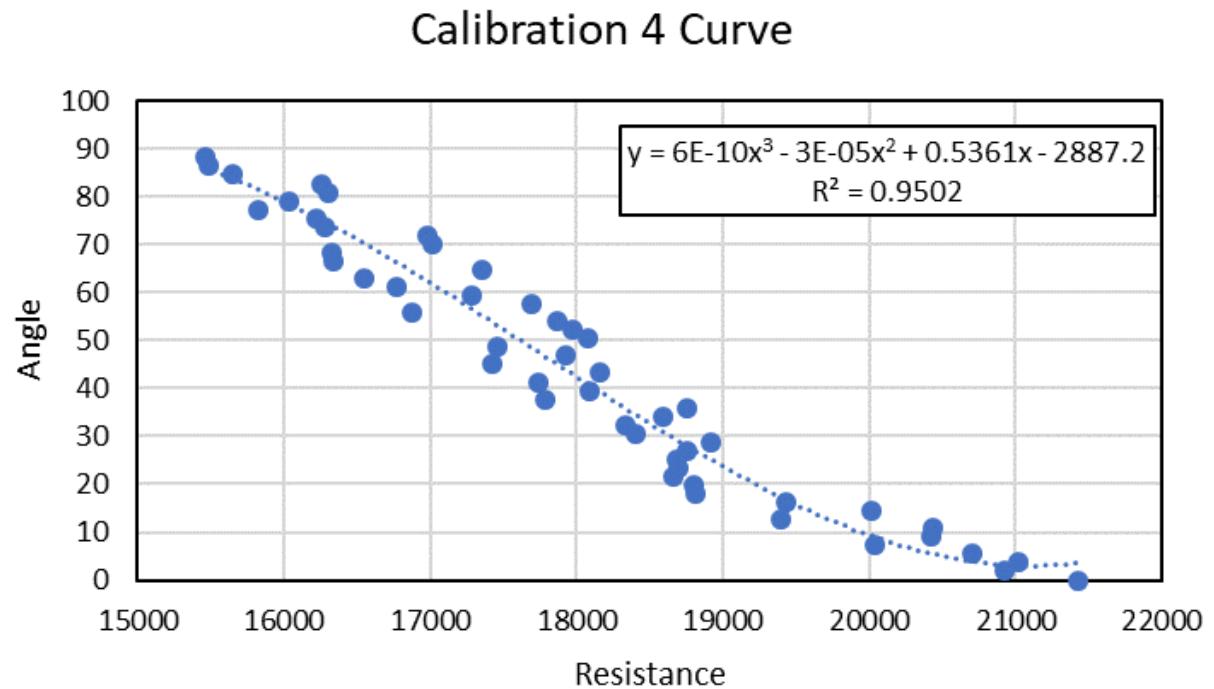
b. Data Set 2



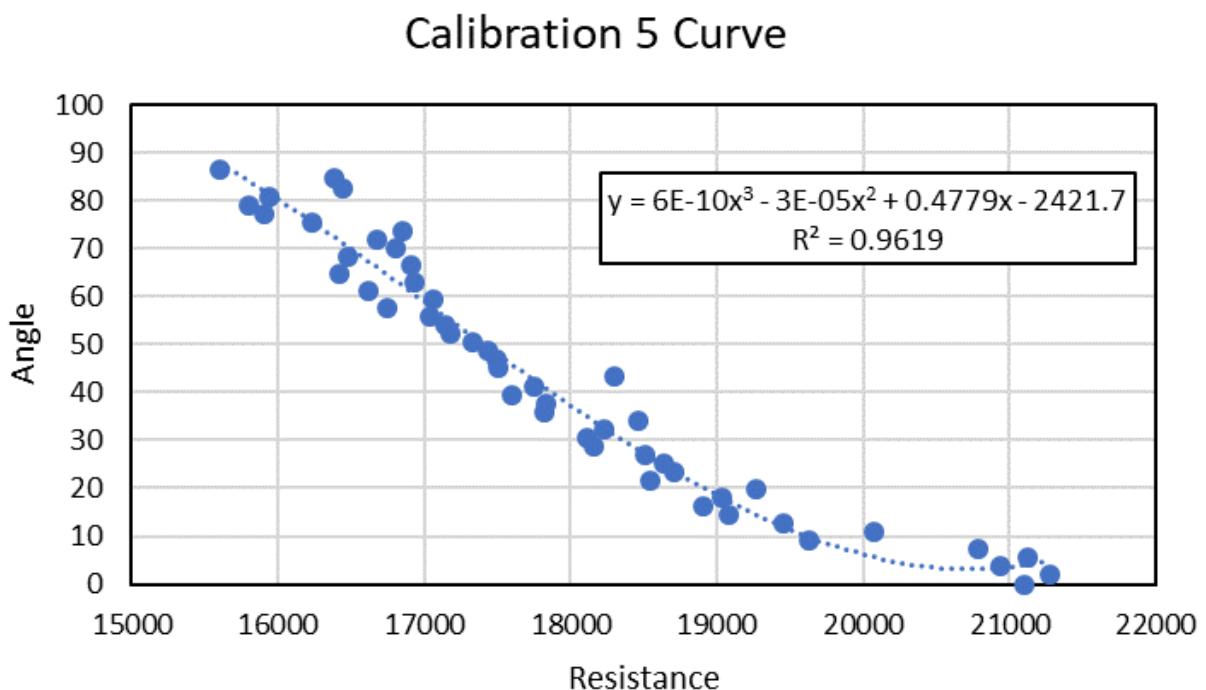
c. Data Set 3



d. Data Set 4



e. Data Set 5



10.4. Raw Uncertainty Data

Measurement Number	Voltage	Resistance	Angle	Z
1	2.808063	21501.8269	4.6295	0.555298
2	2.810202	21449.7871	4.2904	0.562502
3	2.807467	21516.3449	4.7299	0.553165
4	2.806065	21550.5213	4.9764	0.547927
5	2.813244	21375.9015	3.8647	0.571548
6	2.818159	21256.8485	3.3135	0.58326
7	2.802963	21626.2481	5.5737	0.535238
8	2.811714	21413.0299	4.0705	0.567175
9	2.811731	21412.6129	4.0681	0.567226
10	2.808046	21502.2391	4.6323	0.555239
11	2.809336	21470.8429	4.4237	0.559671
12	2.817666	21268.7657	3.3612	0.582244
13	2.818811	21241.0922	3.2528	0.584549
14	2.820031	21211.6163	3.1469	0.586798
15	2.819204	21231.5982	3.2176	0.585296
16	2.814527	21344.7888	3.7047	0.574948
17	2.818515	21248.2433	3.28	0.583971
18	2.828068	21018.1066	2.6939	0.596422
19	2.829589	20981.6064	2.6547	0.597257
20	2.820939	21189.7015	3.0746	0.588334
21	2.818588	21246.4857	3.2732	0.584114
22	2.808859	21482.4405	4.4994	0.558063
23	2.81993	21214.0515	3.1553	0.58662
24	2.815188	21328.7492	3.6266	0.576606
25	2.813983	21357.9566	3.771	0.573538
26	2.820078	21210.4879	3.1431	0.58688
27	2.822526	21151.442	2.9613	0.590741
28	2.826477	21056.3308	2.7506	0.595219
29	2.821425	21177.973	3.0381	0.589109
30	2.823148	21136.4524	2.9215	0.591588
31	2.822899	21142.4498	2.9371	0.591256
32	2.821547	21175.0343	3.0292	0.589298
33	2.821923	21165.9783	3.0024	0.589868
34	2.817446	21274.0886	3.3831	0.58178
35	2.829592	20981.5321	2.6546	0.597258

36	2.822832	21144.0584	2.9414	0.591165
37	2.829082	20993.7764	2.6662	0.597012
38	2.824342	21107.6867	2.8519	0.593066
39	2.812375	21396.9929	3.9796	0.569106
40	2.821209	21183.1781	3.0541	0.58877
41	2.83198	20924.3266	2.6219	0.597952
42	2.825285	21084.99	2.8035	0.594093
43	2.82564	21076.4453	2.7868	0.594449
44	2.825286	21084.967	2.8035	0.594094
45	2.835056	20850.7465	2.631	0.59776
46	2.822955	21141.0939	2.9335	0.591332
47	2.832023	20923.2877	2.6217	0.597958
48	2.832427	20913.6138	2.6197	0.598
49	2.826377	21058.732	2.7547	0.595132
50	2.83778	20785.7444	2.686	0.596591
51	2.824819	21096.216	2.8268	0.5936
52	2.827619	21028.8926	2.7083	0.596117
53	2.819852	21215.9341	3.1618	0.586482
54	2.818537	21247.7189	3.278	0.584014
55	2.836157	20824.453	2.648	0.597399
56	2.831086	20945.7395	2.6301	0.597779
57	2.838921	20758.5356	2.722	0.595827
58	2.828239	21014.0084	2.6888	0.596531
59	2.821748	21170.1811	3.0148	0.589606
60	2.815276	21326.635	3.6166	0.57682
61	2.832926	20901.6836	2.6186	0.598022
62	2.833835	20879.9393	2.6206	0.597981
63	2.837021	20803.8446	2.6663	0.59701
64	2.83867	20764.5176	2.7134	0.596008
65	2.827302	21036.4974	2.7192	0.595886
66	2.82778	21025.0163	2.703	0.59623
67	2.825671	21075.6999	2.7854	0.594479
68	2.837478	20792.9481	2.6778	0.596766
69	2.838683	20764.2222	2.7138	0.596
70	2.833112	20897.2344	2.6186	0.598022
71	2.832921	20901.8034	2.6186	0.598022
72	2.834088	20873.897	2.622	0.597951
73	2.832247	20917.9225	2.6204	0.597984
74	2.834482	20864.4765	2.625	0.597888
75	2.829361	20987.079	2.6596	0.597151

76	2.834058	20874.6152	2.6218	0.597955
77	2.824048	21114.7754	2.8682	0.59272
78	2.831193	20943.1578	2.6288	0.597806
79	2.831335	20939.7654	2.6273	0.597838
80	2.835833	20832.2057	2.6422	0.597521
81	2.83132	20940.1366	2.6275	0.597835
82	2.839885	20735.5888	2.7582	0.595057
83	2.836943	20805.7047	2.6645	0.597049
84	2.83725	20798.3732	2.6719	0.596891
85	2.83292	20901.8148	2.6186	0.598022
86	2.819096	21234.2076	3.2272	0.585093
87	2.838561	20767.1141	2.7098	0.596085
88	2.830723	20954.4227	2.6348	0.59768
89	2.829396	20986.2555	2.6589	0.597167
90	2.842621	20670.5071	2.8898	0.592261
91	2.840764	20714.6714	2.7958	0.594257
92	2.831514	20935.4768	2.6256	0.597875
93	2.829363	20987.0275	2.6596	0.597152
94	2.836874	20807.3486	2.6629	0.597082
95	2.850202	20490.83	3.4705	0.579924
96	2.840989	20709.3051	2.8062	0.594037
97	2.84006	20731.4111	2.7653	0.594905
98	2.833941	20877.4026	2.6211	0.597969
99	2.85129	20465.1135	3.5791	0.577617
100	2.835441	20841.5659	2.6361	0.597651
101	2.851444	20461.4759	3.5949	0.577279
102	2.850675	20479.6622	3.5169	0.578938
103	2.851561	20458.717	3.607	0.577022
104	2.850497	20483.8595	3.4993	0.579312
105	2.847792	20547.8536	3.2522	0.584561
106	2.84721	20561.6248	3.2042	0.585581
107	2.844058	20636.3662	2.9758	0.590434
108	2.839511	20744.4965	2.7435	0.59537
109	2.835226	20846.7027	2.6331	0.597714
110	2.849609	20504.8429	3.4139	0.581125
111	2.839393	20747.2902	2.739	0.595464
112	2.841901	20687.6104	2.8511	0.593083
113	2.838897	20759.1264	2.7211	0.595845
114	2.846464	20579.3002	3.1452	0.586834
115	2.842818	20665.8106	2.901	0.592024

116	2.845423	20603.973	3.0681	0.588473
117	2.846337	20582.3176	3.1355	0.587041
118	2.851156	20468.2953	3.5653	0.577909
119	2.849974	20496.2293	3.4485	0.580391
120	2.849509	20507.2222	3.4045	0.581325
121	2.842456	20674.4223	2.8807	0.592454
122	2.8441	20635.3701	2.9785	0.590377
123	2.844534	20625.0652	3.0068	0.589775
124	2.850967	20472.7447	3.5462	0.578315
125	2.853181	20420.4873	3.7823	0.573298
126	2.854237	20395.6	3.9038	0.570718
127	2.842636	20670.1559	2.8906	0.592243
128	2.845483	20602.5651	3.0723	0.588383
129	2.859686	20267.4081	4.6194	0.555513
130	2.839938	20734.3286	2.7603	0.595012
131	2.848939	20520.7004	3.3522	0.582436
132	2.847521	20554.2614	3.2296	0.585041
133	2.857158	20326.8131	4.2692	0.562954
134	2.851961	20449.2765	3.649	0.57613
135	2.848346	20534.72	3.2997	0.583552
136	2.857685	20314.4214	4.3396	0.561458
137	2.86088	20239.3671	4.7958	0.551766
138	2.858422	20297.0919	4.4404	0.559316
139	2.853801	20405.8574	3.853	0.571796
140	2.857046	20329.4378	4.2544	0.563267
141	2.85464	20386.0817	3.9517	0.569699
142	2.85414	20397.8873	3.8924	0.57096
143	2.862504	20201.2965	5.0463	0.546443
144	2.85607	20352.424	4.128	0.565953
145	2.861064	20235.0603	4.8235	0.551178
146	2.862812	20194.0898	5.0952	0.545404
147	2.852912	20426.8372	3.7523	0.573937
148	2.862095	20210.8911	4.982	0.54781
149	2.861654	20221.2265	4.9135	0.549263
150	2.861715	20219.8009	4.9229	0.549064
151	2.86052	20247.8312	4.7418	0.552913
152	2.85743	20320.4204	4.3053	0.562186
153	2.86901	20049.1783	6.173	0.522504
154	2.866007	20119.2983	5.629	0.534063
155	2.860662	20244.48	4.7631	0.55246

156	2.865451	20132.3151	5.5326	0.53611
157	2.864957	20143.87	5.4483	0.537902
158	2.872719	19962.7746	6.9	0.507058
159	2.866816	20100.3926	5.7716	0.531034
160	2.863663	20174.1536	5.2327	0.542482
161	2.864142	20162.9399	5.3116	0.540806
162	2.869697	20033.1639	6.3031	0.51974
163	2.865801	20124.1254	5.5931	0.534826
164	2.861357	20228.193	4.868	0.550232
165	2.873183	19951.9586	6.9954	0.505032
166	2.86204	20212.171	4.9734	0.547991
167	2.863997	20166.3165	5.2877	0.541313
168	2.863174	20185.589	5.1534	0.544167
169	2.865921	20121.3105	5.614	0.534381
170	2.862273	20206.7054	5.0099	0.547216
171	2.859296	20276.5625	4.5634	0.556703
172	2.858484	20295.6351	4.449	0.559133
173	2.866254	20113.5246	5.6722	0.533144
174	2.860166	20256.1295	4.6895	0.554024
175	2.86057	20246.6507	4.7493	0.552754
176	2.869249	20043.6113	6.218	0.521548
177	2.863033	20188.912	5.1306	0.544653
178	2.870608	20011.9232	6.4789	0.516005
179	2.879036	19816.1036	8.2728	0.47789
180	2.866872	20099.1003	5.7814	0.530824
181	2.875453	19899.1991	7.474	0.494863
182	2.871818	19983.7287	6.7181	0.510924
183	2.866337	20111.5854	5.6868	0.532835
184	2.871613	19988.5085	6.677	0.511795
185	2.869037	20048.5554	6.178	0.522397
186	2.868889	20052.0095	6.1503	0.522988
187	2.865178	20138.6888	5.486	0.537102
188	2.870088	20024.0368	6.3782	0.518145
189	2.872099	19977.1958	6.7744	0.509727
190	2.855347	20369.4283	4.0377	0.567873
191	2.881467	19759.8252	8.8445	0.465744
192	2.860364	20251.4849	4.7187	0.553403
193	2.84914	20515.9344	3.3705	0.582047
194	2.88307	19722.7868	9.234	0.457468
195	2.871679	19986.9707	6.6902	0.511515

196	2.869447	20038.9793	6.2556	0.520749
197	2.869979	20026.5768	6.3572	0.518591
198	2.870292	20019.2798	6.4176	0.517308
199	2.864321	20158.7378	5.3415	0.540172
200	2.867282	20089.5153	5.855	0.529261
201	2.897402	19393.3238	13.14	0.374487
202	2.892897	19496.5433	11.833	0.402241
203	2.890705	19546.8766	11.223	0.415206
204	2.885697	19662.1572	9.8939	0.443448
205	2.881861	19750.7174	8.9393	0.463729
206	2.883738	19707.352	9.3994	0.453955
207	2.888342	19601.2043	10.585	0.428771
208	2.894114	19468.634	12.179	0.39489
209	2.893644	19479.4034	12.045	0.39774
210	2.885718	19661.6624	9.8994	0.443331
211	2.89129	19533.4236	11.385	0.411778
212	2.906759	19179.9927	16.063	0.312378
213	2.888641	19594.3344	10.664	0.42708
214	2.897438	19392.5058	13.15	0.374261
215	2.905959	19198.1818	15.802	0.317913
216	2.888294	19602.3238	10.572	0.429045
217	2.896141	19422.1905	12.767	0.382404
218	2.90987	19109.3747	17.094	0.290479
219	2.901951	19289.4409	14.527	0.345021
220	2.906167	19193.4602	15.87	0.316481
221	2.897871	19382.5932	13.28	0.371513
222	2.904618	19228.6965	15.37	0.327102
223	2.897009	19402.3232	13.023	0.376968
224	2.897092	19400.425	13.047	0.376446
225	2.905104	19217.6177	15.526	0.32378
226	2.901473	19300.3425	14.378	0.348183
227	2.909827	19110.3479	17.079	0.290785
228	2.911162	19080.072	17.53	0.281205
229	2.90687	19177.4625	16.099	0.311604
230	2.916298	18963.9124	19.31	0.243393
231	2.905524	19208.0827	15.661	0.320908
232	2.919905	18882.5683	20.601	0.215951
233	2.920895	18860.2863	20.962	0.208301
234	2.891437	19530.0502	11.425	0.410914
235	2.910453	19096.1523	17.29	0.286308

236	2.915744	18976.4195	19.114	0.247543
237	2.904797	19224.6161	15.427	0.32588
238	2.91623	18965.4574	19.286	0.243907
239	2.911822	19065.1389	17.755	0.276437
240	2.914834	18996.986	18.795	0.254327
241	2.913411	19029.1597	18.301	0.264836
242	2.911177	19079.7371	17.535	0.281098
243	2.909585	19115.8202	16.998	0.292504
244	2.920178	18876.4313	20.7	0.21385
245	2.920142	18877.2474	20.687	0.21413
246	2.903644	19250.8653	15.059	0.333699
247	2.9031	19263.2643	14.887	0.33736
248	2.911028	19083.1243	17.484	0.282176
249	2.920505	18869.0663	20.819	0.211322
250	2.918039	18924.6239	19.929	0.230236
251	2.916122	18967.8961	19.248	0.244717
252	2.92202	18834.9789	21.374	0.199543
253	2.922357	18827.3927	21.498	0.196903
254	2.918029	18924.8604	19.925	0.230315
255	2.91397	19016.5193	18.494	0.260722
256	2.911153	19080.2881	17.527	0.281274
257	2.928051	18699.6229	23.635	0.151502
258	2.926937	18724.5749	23.211	0.160506
259	2.927505	18711.8588	23.427	0.155926
260	2.932564	18598.7001	25.38	0.114424
261	2.922029	18834.7698	21.377	0.19947
262	2.922311	18828.4434	21.481	0.197269
263	2.921416	18848.5742	21.152	0.204256
264	2.924724	18774.2201	22.377	0.178224
265	2.921538	18845.8118	21.197	0.2033
266	2.913705	19022.5045	18.402	0.262672
267	2.92167	18842.8512	21.245	0.202275
268	2.927327	18715.8387	23.359	0.157361
269	2.920518	18868.7765	20.824	0.211222
270	2.92236	18827.3391	21.499	0.196885
271	2.927031	18722.4694	23.247	0.159749
272	2.911458	19073.385	17.63	0.279073
273	2.922945	18814.1919	21.715	0.192295
274	2.92589	18748.0592	22.815	0.168921
275	2.92265	18820.8211	21.606	0.194612

276	2.921067	18856.4229	21.024	0.206968
277	2.92003	18879.7708	20.646	0.214994
278	2.924465	18780.0329	22.28	0.180282
279	2.927702	18707.4467	23.502	0.154332
280	2.927691	18707.6924	23.497	0.154421
281	2.933422	18579.5413	25.717	0.107269
282	2.920885	18860.5116	20.958	0.208378
283	2.931331	18626.2392	24.899	0.124645
284	2.944015	18344.0096	29.99	0.016478
285	2.923076	18811.2449	21.763	0.191264
286	2.918997	18903.0333	20.273	0.222928
287	2.92566	18753.2095	22.728	0.170758
288	2.928227	18695.6823	23.702	0.150074
289	2.920465	18869.9627	20.805	0.21163
290	2.920902	18860.1253	20.964	0.208245
291	2.91962	18889.0072	20.498	0.218152
292	2.920066	18878.944	20.66	0.214711
293	2.921562	18845.2755	21.206	0.203115
294	2.91962	18889.0072	20.498	0.218152
295	2.918266	18919.5111	20.01	0.22851
296	2.928055	18699.5374	23.636	0.151471
297	2.921479	18847.1528	21.175	0.203765
298	2.91942	18893.5082	20.426	0.219687
299	2.920208	18875.7549	20.711	0.213618
300	2.934273	18560.5532	26.052	0.100143
301	2.940038	18432.2344	28.361	0.051081
302	2.934158	18563.1322	26.006	0.101113
303	2.928631	18686.6336	23.857	0.146789
304	2.934125	18563.8714	25.993	0.101391
305	2.927057	18721.887	23.257	0.15954
306	2.922	18835.4186	21.367	0.199695
307	2.92128	18851.6319	21.102	0.205314
308	2.929902	18658.185	24.345	0.136404
309	2.924302	18783.7053	22.219	0.181579
310	2.93423	18561.5263	26.035	0.100509
311	2.930396	18647.1473	24.536	0.132353
312	2.935727	18528.1501	26.628	0.0879
313	2.938082	18475.7257	27.571	0.067882
314	2.943971	18344.9868	29.972	0.016865
315	2.938133	18474.5855	27.591	0.067444

316	2.944576	18331.5938	30.222	0.011554
317	2.935956	18523.0403	26.72	0.085961
318	2.929505	18667.0712	24.192	0.139657
319	2.938052	18476.3887	27.559	0.068137
320	2.935315	18537.3251	26.465	0.091377
321	2.944209	18339.7261	30.07	0.014781
322	2.937644	18485.459	27.395	0.071618
323	2.943211	18361.8416	29.658	0.023527
324	2.936996	18499.8813	27.135	0.077138
325	2.936723	18505.9695	27.025	0.079462
326	2.952178	18163.6555	33.415	0.056291
327	2.944243	18338.9656	30.084	0.014479
328	2.94017	18429.3162	28.415	0.049947
329	2.938809	18459.5594	27.864	0.061657
330	2.943512	18355.1515	29.782	0.020885
331	2.945037	18321.3889	30.413	0.007497
332	2.957574	18044.9984	35.732	0.105531
333	2.9512	18185.2155	32.999	0.047456
334	2.955643	18087.4145	34.899	0.087813
335	2.952228	18162.5734	33.436	0.056736
336	2.953742	18129.225	34.082	0.070473
337	2.951684	18174.5625	33.204	0.051817
338	2.951221	18184.7529	33.008	0.047645
339	2.952212	18162.9149	33.429	0.056595
340	2.948135	18252.857	31.706	0.019972
341	2.955088	18099.6223	34.66	0.082737
342	2.956297	18073.0322	35.181	0.093806
343	2.957243	18052.2689	35.589	0.102485
344	2.954343	18116.0043	34.34	0.075942
345	2.946355	18292.2174	30.961	0.004148
346	2.949153	18230.3837	32.133	0.029064
347	2.956908	18059.6301	35.444	0.099405
348	2.953146	18142.3461	33.828	0.065058
349	2.959482	18003.1289	36.561	0.123144
350	2.957438	18047.9765	35.674	0.104283
351	2.956225	18074.6142	35.15	0.093146
352	2.957387	18049.1019	35.652	0.103811
353	2.963145	17922.9303	38.165	0.157204
354	2.954328	18116.3347	34.333	0.075805
355	2.961212	17965.2288	37.317	0.139188

356	2.963108	17923.7437	38.148	0.156857
357	2.962725	17932.1189	37.98	0.153281
358	2.952833	18149.2447	33.694	0.062216
359	2.953196	18141.2437	33.849	0.065513
360	2.955904	18081.687	35.011	0.090198
361	2.960623	17978.1428	37.059	0.13371
362	2.964248	17898.8135	38.65	0.167527
363	2.964612	17890.8636	38.811	0.170938
364	2.964108	17901.8773	38.589	0.166214
365	2.959254	18008.1315	36.462	0.121033
366	2.965243	17877.0784	39.09	0.176861
367	2.954654	18109.1547	34.473	0.078781
368	2.970231	17768.3308	41.307	0.223977
369	2.9584	18026.8683	36.091	0.113143
370	2.962226	17943.0422	37.761	0.148624
371	2.962973	17926.6847	38.089	0.155601
372	2.949563	18221.3419	32.306	0.032733
373	2.961261	17964.1638	37.338	0.13964
374	2.956115	18077.0397	35.102	0.092135
375	2.958801	18018.0764	36.265	0.116842
376	2.956125	18076.8249	35.106	0.092224
377	2.957322	18050.5205	35.624	0.103217
378	2.959729	17997.7141	36.669	0.12543
379	2.964715	17888.603	38.857	0.171908
380	2.96588	17863.1794	39.371	0.182845
381	2.956807	18061.8294	35.401	0.098485
382	2.955405	18092.6503	34.796	0.085634
383	2.957186	18053.5253	35.564	0.101959
384	2.956764	18062.7719	35.382	0.098091
385	2.961078	17968.1736	37.258	0.137938
386	2.958294	18029.1857	36.045	0.112169
387	2.959431	18004.2632	36.539	0.122665
388	2.965682	17867.5046	39.284	0.180981
389	2.971531	17740.0409	41.889	0.236342
390	2.958791	18018.2856	36.261	0.116754
391	2.958603	18022.4119	36.179	0.115017
392	2.968965	17795.8977	40.742	0.21197
393	2.968033	17816.2114	40.327	0.203149
394	2.952783	18150.3368	33.673	0.061767
395	2.954463	18113.3608	34.391	0.077037

396	2.961433	17960.3946	37.413	0.141241
397	2.962177	17944.1066	37.739	0.14817
398	2.9592	18009.3183	36.439	0.120533
399	2.961395	17961.2298	37.397	0.140886
400	2.973343	17700.6712	42.703	0.25362
401	2.95903	18013.0513	36.364	0.118959
402	2.963246	17920.7144	38.209	0.158151
403	2.962773	17931.0653	38.001	0.153731
404	2.958117	18033.078	35.968	0.110533
405	2.964086	17902.3566	38.579	0.166008
406	2.96092	17971.6251	37.189	0.136474
407	2.964688	17889.2124	38.844	0.171647
408	2.958398	18026.905	36.09	0.113128
409	2.946758	18283.2955	31.129	0.007724
410	2.958858	18016.8109	36.29	0.117375
411	2.959294	18007.2585	36.479	0.121401
412	2.971833	17733.488	42.024	0.239212
413	2.961762	17953.1916	37.557	0.144303
414	2.965268	17876.5369	39.101	0.177094
415	2.958577	18022.982	36.168	0.114777
416	2.967654	17824.4601	40.159	0.199574
417	2.973433	17698.719	42.743	0.254479
418	2.973786	17691.0563	42.902	0.257852
419	2.965734	17866.3647	39.307	0.181472
420	2.966992	17838.9146	39.864	0.193318
421	2.963409	17917.1483	38.281	0.159676
422	2.966623	17846.9557	39.701	0.189844
423	2.964504	17893.2286	38.763	0.169923
424	2.964375	17896.0313	38.707	0.16872
425	2.968712	17801.4191	40.629	0.20957
426	2.967761	17822.1365	40.206	0.20058
427	2.974882	17667.267	43.395	0.268341
428	2.96581	17864.6991	39.341	0.18219
429	2.968526	17805.4555	40.547	0.207817
430	2.969551	17783.1341	41.004	0.217524
431	2.980592	17543.6042	45.982	0.323299
432	2.982837	17495.1175	47.005	0.345028
433	2.967669	17824.1482	40.165	0.199709
434	2.982132	17510.3313	46.683	0.3382
435	2.974653	17672.2283	43.292	0.266151

436	2.977808	17603.8454	44.718	0.29644
437	2.977091	17619.3586	44.394	0.28955
438	2.969132	17792.2519	40.817	0.213555
439	2.97114	17748.5502	41.714	0.232618
440	2.970659	17759.007	41.499	0.228048
441	2.970616	17759.9461	41.48	0.227637
442	2.985055	17447.2793	48.018	0.366558
443	2.975221	17659.9014	43.549	0.271595
444	2.976856	17624.452	44.287	0.28729
445	2.984173	17466.3001	47.615	0.357987
446	2.994343	17247.7493	52.284	0.457199
447	2.9917	17304.41	51.067	0.431335
448	2.987948	17385.0019	49.343	0.394712
449	2.970725	17757.5753	41.528	0.228673
450	2.985093	17446.4624	48.035	0.366926
451	2.975932	17644.4928	43.869	0.278409
452	2.984005	17469.9144	47.538	0.35636
453	2.991264	17313.7515	50.867	0.42708
454	2.981061	17533.4693	46.195	0.327833
455	2.988259	17378.3209	49.486	0.39774
456	2.984779	17453.2346	47.892	0.363873
457	2.986042	17426.0104	48.47	0.376157
458	2.98346	17481.67	47.289	0.351071
459	2.98389	17472.4081	47.485	0.355238
460	2.983914	17471.8734	47.497	0.355478
461	2.993054	17275.3645	51.69	0.444583
462	2.987282	17399.3274	49.038	0.388223
463	2.984254	17464.542	47.652	0.358779
464	2.977273	17615.4176	44.476	0.291299
465	2.980974	17535.3548	46.156	0.326989
466	2.984354	17462.3881	47.698	0.359749
467	2.98686	17408.4142	48.844	0.384112
468	2.986762	17410.5132	48.8	0.383162
469	2.981678	17520.1499	46.476	0.333798
470	2.991063	17318.0804	50.774	0.425109
471	2.979234	17572.9602	45.365	0.31019
472	2.981399	17526.1651	46.349	0.331103
473	2.981064	17533.4023	46.197	0.327863
474	2.980148	17553.1958	45.78	0.319012
475	2.986363	17419.1053	48.617	0.379278

476	2.991828	17301.6634	51.126	0.432587
477	2.985894	17429.2145	48.402	0.37471
478	2.981834	17516.7668	46.548	0.335314
479	2.992852	17279.6984	51.597	0.442605
480	2.980151	17553.134	45.782	0.319039
481	2.985947	17428.0591	48.426	0.375232
482	2.987373	17397.3625	49.08	0.389113
483	2.994771	17238.5751	52.482	0.461395
484	2.984636	17456.3232	47.826	0.362481
485	2.983712	17476.2442	47.404	0.353512
486	2.983574	17479.2064	47.341	0.352179
487	2.999964	17127.5897	54.878	0.512312
488	2.989591	17349.6899	50.097	0.410734
489	2.984327	17462.9741	47.685	0.359485
490	2.983287	17485.3991	47.21	0.349395
491	2.986059	17425.6612	48.477	0.376315
492	2.990142	17337.8442	50.351	0.416117
493	2.994948	17234.803	52.563	0.463121
494	2.994317	17248.3161	52.272	0.45694
495	2.991072	17317.8809	50.778	0.4252
496	2.98405	17468.9427	47.559	0.356797
497	2.988357	17376.1984	49.531	0.398702
498	2.979535	17566.4619	45.502	0.313089
499	2.989632	17348.8037	50.116	0.411136
500	2.985801	17431.2223	48.359	0.373804
501	2.961863	17950.9788	37.602	0.145245
502	2.968664	17802.4632	40.608	0.209116
503	2.969613	17781.7791	41.031	0.218114
504	2.968247	17811.5501	40.422	0.205171
505	2.970163	17769.8046	41.277	0.223334
506	2.97092	17753.3425	41.615	0.230523
507	2.967595	17825.7597	40.132	0.199011
508	2.965831	17864.2463	39.35	0.182385
509	2.978796	17582.4523	45.166	0.30596
510	2.975359	17656.9121	43.611	0.272916
511	2.970729	17757.5026	41.53	0.228705
512	2.979881	17558.98	45.659	0.316428
513	2.973618	17694.7062	42.826	0.256245
514	2.984965	17449.2317	47.977	0.365677
515	2.972362	17721.9771	42.262	0.24426

516	2.981888	17515.6083	46.572	0.335833
517	2.981458	17524.8981	46.376	0.33167
518	2.976276	17637.029	44.025	0.281714
519	2.974791	17669.2276	43.355	0.267476
520	2.986134	17424.0388	48.512	0.377048
521	2.98016	17552.9484	45.785	0.319122
522	2.987866	17386.7608	49.306	0.393915
523	2.990425	17331.772	50.481	0.418879
524	2.985948	17428.0386	48.427	0.375241
525	2.990366	17333.0365	50.454	0.418303
526	2.989412	17353.537	50.015	0.408986
527	2.993787	17259.6537	52.028	0.451758
528	2.996972	17191.5046	53.497	0.482955
529	2.994643	17241.3215	52.423	0.460139
530	2.986879	17407.9934	48.853	0.384302
531	2.994716	17239.7696	52.456	0.460848
532	2.988052	17382.7559	49.391	0.395729
533	2.985406	17439.7223	48.179	0.369967
534	2.993691	17261.7174	51.984	0.450815
535	2.99324	17271.3837	51.776	0.4464
536	2.986792	17409.8717	48.813	0.383452
537	2.990865	17322.3127	50.683	0.423183
538	2.992935	17277.9147	51.636	0.443419
539	2.994094	17253.0907	52.169	0.454757
540	2.986499	17416.1794	48.679	0.3806
541	2.9881	17381.7253	49.413	0.396197
542	2.997353	17183.3452	53.673	0.486698
543	3.000678	17112.3732	55.208	0.519313
544	2.99523	17228.7605	52.693	0.465886
545	2.999597	17135.4296	54.709	0.508706
546	3.000432	17117.6107	55.094	0.516903
547	2.999067	17146.7375	54.464	0.503508
548	3.003515	17051.9197	56.519	0.547169
549	2.994306	17248.5357	52.267	0.45684
550	2.99753	17179.5592	53.754	0.488435
551	2.993898	17257.2735	52.079	0.452846
552	2.997452	17181.2407	53.718	0.487664
553	3.001042	17104.605	55.376	0.522889
554	2.999767	17131.7918	54.787	0.510379
555	3.003857	17044.6431	56.677	0.550526

556	2.996649	17198.4068	53.348	0.479791
557	3.005887	17001.4642	57.615	0.570462
558	3.007385	16969.6548	58.307	0.585164
559	2.999821	17130.642	54.812	0.510908
560	2.998401	17160.957	54.156	0.496975
561	3.006079	16997.3856	57.704	0.572346
562	2.99898	17148.5954	54.424	0.502654
563	3.0016	17092.7022	55.634	0.52837
564	3.004772	17025.1658	57.1	0.559516
565	3.003448	17053.3559	56.488	0.546507
566	2.997301	17184.4713	53.648	0.486181
567	2.999774	17131.6595	54.79	0.51044
568	3.003554	17051.0925	56.537	0.547551
569	3.013221	16845.9857	61.002	0.64241
570	3.005334	17013.2266	57.359	0.565029
571	2.999955	17127.783	54.874	0.512223
572	3.008086	16954.7663	58.631	0.592049
573	2.989719	17346.9393	50.156	0.411983
574	2.993484	17266.1568	51.888	0.448787
575	2.993222	17271.772	51.768	0.446223
576	3.003673	17048.5501	56.592	0.548724
577	2.997541	17179.335	53.759	0.488538
578	3.004333	17034.5023	56.897	0.555206
579	3.015717	16793.2419	62.152	0.666851
580	2.996976	17191.4077	53.499	0.483
581	2.99425	17249.7407	52.241	0.456289
582	2.990933	17320.8643	50.714	0.423842
583	2.990816	17323.3721	50.661	0.4227
584	2.99697	17191.5351	53.496	0.482941
585	2.998977	17148.6667	54.422	0.502622
586	3.00506	17019.0562	57.233	0.562337
587	3.003803	17045.7847	56.652	0.55
588	3.00508	17018.6304	57.242	0.562533
589	3.001957	17085.1014	55.799	0.531872
590	3.012613	16858.841	60.721	0.636455
591	3.010124	16911.5521	59.572	0.612045
592	2.993095	17274.4804	51.709	0.444986
593	3.004382	17033.4676	56.92	0.555684
594	3.006289	16992.9175	57.801	0.574411
595	3.006218	16994.4372	57.768	0.573709

596	3.009397	16926.9614	59.237	0.604913
597	2.999945	17128.0017	54.869	0.512122
598	3.004148	17038.4385	56.812	0.553389
599	3.000057	17125.6211	54.921	0.513217
600	3.006064	16997.7098	57.697	0.572197
601	2.981611	17521.5763	46.446	0.333159
602	2.98436	17462.2596	47.7	0.359807
603	2.994279	17249.1229	52.255	0.456571
604	2.998662	17155.3866	54.277	0.499534
605	2.996774	17195.7252	53.405	0.48102
606	2.994113	17252.6668	52.178	0.454951
607	2.992576	17285.6228	51.47	0.439901
608	2.992276	17292.0442	51.332	0.436972
609	2.993645	17262.6931	51.963	0.450369
610	2.996713	17197.0303	53.377	0.480422
611	2.998379	17161.4407	54.146	0.496753
612	3.00174	17089.7145	55.699	0.529747
613	3.001366	17097.6976	55.526	0.52607
614	3.005914	17000.8916	57.628	0.570727
615	3.0041	17039.4683	56.789	0.552914
616	3.010924	16894.5999	59.942	0.619893
617	2.997306	17184.349	53.651	0.486238
618	3.00468	17027.1333	57.057	0.558607
619	3.001629	17092.0874	55.647	0.528654
620	3.010171	16910.5618	59.594	0.612504
621	3.007937	16957.9388	58.562	0.590582
622	3.001672	17091.1677	55.667	0.529077
623	3.003407	17054.2085	56.469	0.546113
624	3.013468	16840.7573	61.116	0.644833
625	3.014195	16825.3846	61.451	0.651956
626	3.003474	17052.7875	56.5	0.546769
627	3.003172	17059.2284	56.36	0.543798
628	3.008823	16939.1313	58.972	0.599282
629	3.002325	17077.2586	55.969	0.535486
630	3.002681	17069.6665	56.134	0.538985
631	3.013124	16848.0329	60.957	0.641462
632	3.014158	16826.1808	61.433	0.651587
633	3.003649	17049.0728	56.581	0.548483
634	3.005182	17016.4505	57.289	0.56354
635	2.99646	17202.4346	53.261	0.477944

636	3.024888	16600.1992	66.361	0.756276
637	3.013985	16829.8243	61.354	0.649899
638	3.015628	16795.1146	62.111	0.665983
639	3.01096	16893.8374	59.958	0.620247
640	3.004148	17038.4588	56.811	0.55338
641	3.010325	16907.288	59.665	0.614019
642	3.017238	16761.1518	62.852	0.681724
643	3.015623	16795.2203	62.109	0.665934
644	3.013578	16838.4434	61.166	0.645905
645	3.012255	16866.4185	60.556	0.632945
646	3.012545	16860.2837	60.69	0.635787
647	3.025529	16586.7377	66.654	0.762503
648	3.014605	16816.7389	61.639	0.655962
649	3.028919	16515.7085	68.199	0.79533
650	3.021501	16671.3528	64.81	0.723334
651	3.017927	16746.6217	63.169	0.688458
652	3.010037	16913.3863	59.532	0.611196
653	3.021482	16671.764	64.801	0.723143
654	3.0135	16840.0868	61.13	0.645143
655	3.03036	16485.5675	68.854	0.809241
656	3.018692	16730.4956	63.521	0.695931
657	3.022608	16648.0882	65.317	0.734108
658	3.023877	16621.4209	65.899	0.746455
659	3.020501	16692.3963	64.352	0.713585
660	3.024528	16607.7603	66.196	0.752777
661	3.018111	16742.7314	63.254	0.690261
662	3.027491	16545.6235	67.549	0.781512
663	3.024508	16608.1807	66.187	0.752582
664	3.016035	16786.5374	62.298	0.669958
665	3.017548	16754.6049	62.995	0.684758
666	3.017047	16765.1801	62.764	0.679857
667	3.020457	16693.3196	64.331	0.713157
668	3.027813	16538.8712	67.695	0.784632
669	3.017735	16750.6633	63.081	0.686585
670	3.017167	16762.6403	62.819	0.681034
671	3.020057	16701.7311	64.148	0.70926
672	3.025288	16591.7995	66.544	0.760162
673	3.023218	16635.2626	65.597	0.740047
674	3.031449	16462.8024	69.348	0.819738
675	3.008964	16936.1478	59.037	0.600662

676	3.038388	16318.133	72.477	0.886217
677	3.013188	16846.6916	60.986	0.642083
678	3.030329	16486.2106	68.84	0.808944
679	3.02809	16533.064	67.822	0.787315
680	3.023253	16634.5263	65.613	0.740388
681	3.028709	16520.1101	68.103	0.793298
682	3.024804	16601.9654	66.322	0.755458
683	3.032064	16449.9519	69.626	0.825659
684	3.013631	16837.3192	61.191	0.646426
685	3.035166	16385.2361	71.028	0.855435
686	3.026637	16563.5151	67.159	0.773242
687	3.016189	16783.2864	62.369	0.671465
688	3.021535	16670.6307	64.826	0.723668
689	3.013451	16841.1203	61.108	0.644665
690	3.027956	16535.8751	67.761	0.786016
691	3.013847	16832.7525	61.29	0.648542
692	3.024629	16605.6234	66.243	0.753766
693	3.018296	16738.8365	63.339	0.692066
694	3.028884	16516.4371	68.183	0.794994
695	3.023766	16623.7591	65.848	0.745372
696	3.01514	16805.4213	61.886	0.661207
697	3.022952	16640.8431	65.475	0.737463
698	3.017704	16751.3168	63.066	0.686282
699	3.014444	16820.1243	61.566	0.654393
700	3.015834	16790.7754	62.206	0.667994
701	3.016459	16777.5702	62.494	0.674114
702	3.023043	16638.9394	65.517	0.738344
703	3.028039	16534.1474	67.798	0.786814
704	3.025101	16595.7314	66.458	0.758343
705	3.023463	16630.1239	65.709	0.742426
706	3.021892	16663.1398	64.989	0.727138
707	3.027083	16554.1708	67.363	0.777562
708	3.026521	16565.9391	67.107	0.772122
709	3.026688	16562.4406	67.183	0.773739
710	3.032188	16447.3576	69.683	0.826854
711	3.026752	16561.1113	67.212	0.774354
712	3.035754	16372.9784	71.293	0.861066
713	3.028633	16521.7072	68.069	0.79256
714	3.029322	16507.2763	68.382	0.799223
715	3.033659	16416.6497	70.348	0.840992

716	3.027985	16535.2659	67.774	0.786298
717	3.040555	16273.1069	73.446	0.906811
718	3.027006	16555.7747	67.328	0.77682
719	3.039605	16292.8469	73.021	0.897789
720	3.033552	16418.8883	70.3	0.839962
721	3.043362	16214.8557	74.696	0.933372
722	3.039708	16290.6915	73.068	0.898774
723	3.044539	16190.467	75.218	0.944463
724	3.036344	16360.6858	71.559	0.866709
725	3.033487	16420.2564	70.27	0.839332
726	3.032463	16441.6218	69.807	0.829496
727	3.040707	16269.9378	73.514	0.908258
728	3.037454	16337.5786	72.057	0.877307
729	3.037358	16339.5685	72.014	0.876395
730	3.031331	16465.2685	69.294	0.818601
731	3.039572	16293.5208	73.007	0.89748
732	3.035732	16373.4404	71.283	0.860853
733	3.04244	16233.9707	74.286	0.924667
734	3.040774	16268.5613	73.544	0.908887
735	3.034694	16395.0625	70.815	0.850919
736	3.043311	16215.9085	74.674	0.932892
737	3.045712	16166.1811	75.737	0.955488
738	3.04353	16211.3662	74.771	0.93496
739	3.043479	16212.4288	74.748	0.934476
740	3.043319	16215.7454	74.677	0.932967
741	3.052128	16033.6475	78.552	1.015296
742	3.04414	16198.7262	75.041	0.940709
743	3.053387	16007.7046	79.099	1.026925
744	3.047599	16127.1279	76.57	0.973177
745	3.048914	16099.9603	77.147	0.985451
746	3.046062	16158.9271	75.892	0.958778
747	3.052252	16031.0773	78.606	1.016449
748	3.040426	16275.7861	73.388	0.905587
749	3.036531	16356.7928	71.643	0.868495
750	3.051806	16040.2681	78.412	1.012324
751	3.054247	15989.9827	79.473	1.034853
752	3.055296	15968.4011	79.926	1.04449
753	3.0578	15916.9428	81.004	1.067385
754	3.060923	15852.8713	82.337	1.095719
755	3.053429	16006.8305	79.118	1.027317

756	3.04822	16114.3049	76.842	0.978974
757	3.068905	15689.7025	85.688	1.166921
758	3.052999	16015.6802	78.931	1.023353
759	3.067527	15717.8211	85.116	1.154755
760	3.072675	15612.9307	87.241	1.199896
761	3.052366	16028.7285	78.656	1.017503
762	3.046755	16144.582	76.198	0.965278
763	3.051271	16051.3006	78.179	1.007368
764	3.051921	16037.9038	78.462	1.013386
765	3.060358	15864.459	82.097	1.090609
766	3.048926	16099.7141	77.153	0.985562
767	3.047061	16138.2649	76.332	0.968138
768	3.075572	15554.0608	88.419	1.224933
769	3.04653	16149.2479	76.098	0.963164
770	3.064634	15776.9126	83.906	1.129044
771	3.058572	15901.0876	81.335	1.074414
772	3.059925	15873.3273	81.912	1.086694
773	3.052447	16027.0578	78.691	1.018253
774	3.049349	16090.9835	77.338	0.989501
775	3.054081	15993.4085	79.4	1.033322
776	3.059265	15886.8595	81.631	1.080713
777	3.064295	15783.84	83.763	1.126017
778	3.070805	15650.9944	86.473	1.183592
779	3.056061	15952.6719	80.256	1.051501
780	3.048248	16113.7235	76.855	0.979236
781	3.062486	15820.8431	83	1.109807
782	3.053089	16013.8433	78.97	1.024176
783	3.061892	15833.0147	82.749	1.104459
784	3.051887	16038.6116	78.447	1.013068
785	3.066103	15746.8756	84.522	1.142138
786	3.062891	15812.5655	83.171	1.113439
787	3.055984	15954.2651	80.223	1.050791
788	3.066763	15733.4135	84.797	1.14799
789	3.065959	15749.8172	84.462	1.140858
790	3.058005	15912.7224	81.092	1.069257
791	3.052774	16020.3172	78.833	1.021275
792	3.068509	15697.7776	85.524	1.163432
793	3.05798	15913.2511	81.081	1.069022
794	3.064831	15772.8865	83.988	1.130802
795	3.060784	15855.7202	82.278	1.094463

796	3.049191	16094.2283	77.269	0.988037
797	3.068425	15699.4891	85.489	1.162692
798	3.054642	15981.8517	79.644	1.038486
799	3.049353	16090.89	77.34	0.989543
800	3.072039	15625.8754	86.98	1.194361
801	3.040693	16270.2398	73.508	0.90812
802	3.051986	16036.562	78.49	1.013988
803	3.054573	15983.2795	79.613	1.037848
804	3.051042	16056.0412	78.079	1.005236
805	3.056636	15940.8606	80.503	1.056758
806	3.059943	15872.9557	81.92	1.086858
807	3.05642	15945.2856	80.411	1.054789
808	3.049867	16080.2866	77.565	0.994323
809	3.05016	16074.2284	77.693	0.997052
810	3.048316	16112.3095	76.885	0.979875
811	3.052699	16021.8647	78.801	1.020581
812	3.052104	16034.1439	78.542	1.015073
813	3.047656	16125.9548	76.595	0.973707
814	3.052998	16015.7195	78.93	1.023335
815	3.051658	16043.3306	78.347	1.010949
816	3.052938	16016.9425	78.905	1.022787
817	3.062348	15823.6793	82.942	1.108561
818	3.048078	16117.2318	76.78	0.977651
819	3.054417	15986.4837	79.546	1.036417
820	3.050959	16057.7478	78.042	1.004469
821	3.055119	15972.0551	79.849	1.04286
822	3.046903	16141.5342	76.263	0.966658
823	3.052849	16018.7895	78.866	1.02196
824	3.050319	16070.9562	77.763	0.998525
825	3.060003	15871.7334	81.946	1.087398
826	3.05692	15935.0203	80.626	1.059355
827	3.062399	15822.6346	82.963	1.10902
828	3.052307	16029.9569	78.63	1.016952
829	3.066185	15745.2151	84.556	1.14286
830	3.070353	15660.2056	86.287	1.179633
831	3.056704	15939.4543	80.533	1.057383
832	3.064918	15771.1076	84.025	1.131578
833	3.06787	15710.8158	85.259	1.15779
834	3.071679	15633.2062	86.832	1.191222
835	3.067765	15712.961	85.215	1.156861

836	3.060563	15860.2457	82.184	1.092468
837	3.079074	15483.0678	89.826	1.25482
838	3.074476	15576.3178	87.975	1.215493
839	3.070264	15662.0074	86.25	1.178858
840	3.070469	15657.8261	86.335	1.180656
841	3.069506	15677.4504	85.937	1.172207
842	3.068143	15705.2419	85.372	1.160203
843	3.066504	15738.6857	84.69	1.145699
844	3.052009	16036.1	78.5	1.014195
845	3.06884	15691.0247	85.662	1.16635
846	3.066038	15748.2197	84.494	1.141553
847	3.079165	15481.2088	89.862	1.255598
848	3.070011	15667.1558	86.146	1.176642
849	3.072212	15622.3586	87.051	1.195866
850	3.071292	15641.0677	86.674	1.187852
851	3.077628	15512.3543	89.247	1.242532
852	3.070754	15652.0334	86.452	1.183145
853	3.080668	15450.7937	90.46	1.268292
854	3.075195	15561.7282	88.266	1.221685
855	3.074504	15575.7559	87.986	1.215732
856	3.082535	15413.0455	91.197	1.283954
857	3.081653	15430.8774	90.849	1.276568
858	3.058169	15909.3593	81.162	1.070748
859	3.085594	15351.2816	92.392	1.309352
860	3.073015	15606.0264	87.379	1.202844
861	3.091432	15233.7724	94.628	1.356852
862	3.077507	15514.8098	89.199	1.241499
863	3.08851	15292.5339	93.516	1.333238
864	3.079703	15470.3222	90.076	1.260149
865	3.081418	15435.6215	90.757	1.274599
866	3.085222	15358.7885	92.248	1.306281
867	3.074646	15572.8646	88.044	1.21696
868	3.089546	15271.6777	93.912	1.341652
869	3.078141	15501.9545	89.453	1.246902
870	3.081719	15429.5276	90.876	1.277128
871	3.08703	15322.3286	92.948	1.321158
872	3.072518	15616.1215	87.176	1.198533
873	3.069206	15683.5783	85.813	1.169564
874	3.070382	15659.6083	86.299	1.17989
875	3.083114	15401.335	91.425	1.288791

876	3.075204	15561.5442	88.27	1.221763
877	3.085021	15362.8433	92.169	1.30462
878	3.081915	15425.575	90.953	1.278767
879	3.081118	15441.6876	90.638	1.272079
880	3.084573	15371.8784	91.995	1.300914
881	3.097361	15114.8737	96.835	1.403742
882	3.075171	15562.222	88.256	1.221475
883	3.081581	15432.3237	90.821	1.275968
884	3.079339	15477.6937	89.931	1.257068
885	3.078307	15498.5966	89.519	1.248312
886	3.082057	15422.6928	91.009	1.279961
887	3.075458	15556.3841	88.373	1.223949
888	3.085777	15347.6033	92.463	1.310856
889	3.074644	15572.9179	88.043	1.216937
890	3.075687	15551.7378	88.465	1.225916
891	3.080854	15447.0265	90.533	1.269859
892	3.078705	15490.5294	89.679	1.251695
893	3.083454	15394.4678	91.558	1.291623
894	3.078491	15494.8767	89.593	1.249872
895	3.077448	15516.0183	89.175	1.240991
896	3.076932	15526.4663	88.968	1.23659
897	3.077205	15520.9445	89.077	1.238917
898	3.085822	15346.6898	92.481	1.311229
899	3.085518	15352.8251	92.363	1.308721
900	3.077733	15510.2325	89.289	1.243424
901	3.059906	15873.7233	81.904	1.086519
902	3.057278	15927.6675	80.78	1.062623
903	3.060508	15861.3747	82.161	1.09197
904	3.057344	15926.2961	80.808	1.063232
905	3.059236	15887.4661	81.618	1.080444
906	3.060133	15869.0737	82.001	1.088572
907	3.058609	15900.3193	81.351	1.074755
908	3.065766	15753.7623	84.381	1.13914
909	3.054332	15988.2356	79.509	1.035634
910	3.060851	15854.347	82.307	1.095068
911	3.061003	15851.2345	82.371	1.09644
912	3.067693	15714.4204	85.185	1.156229
913	3.070103	15665.2955	86.184	1.177443
914	3.062678	15816.9139	83.081	1.111532
915	3.067245	15723.5773	84.998	1.152259

916	3.064284	15784.0545	83.759	1.125924
917	3.071534	15636.1467	86.773	1.189962
918	3.066681	15735.088	84.763	1.147263
919	3.068729	15693.2998	85.615	1.165367
920	3.077388	15517.2365	89.151	1.240478
921	3.072964	15607.0591	87.359	1.202403
922	3.070835	15650.3779	86.486	1.183856
923	3.069336	15680.9103	85.867	1.170715
924	3.069498	15677.6254	85.934	1.172132
925	3.079093	15482.6864	89.833	1.25498
926	3.073598	15594.1706	87.617	1.207899
927	3.071591	15634.9967	86.796	1.190455
928	3.065571	15757.7567	84.299	1.1374
929	3.07384	15589.257	87.716	1.209991
930	3.067718	15713.9145	85.196	1.156448
931	3.074731	15571.1552	88.078	1.217686
932	3.082556	15412.6071	91.205	1.284135
933	3.071103	15644.9215	86.596	1.186199
934	3.073086	15604.5721	87.408	1.203465
935	3.075618	15553.1461	88.437	1.22532
936	3.083264	15398.3154	91.483	1.290037
937	3.084435	15374.6645	91.941	1.299771
938	3.072338	15619.7928	87.102	1.196963
939	3.067906	15710.0813	85.274	1.158109
940	3.075561	15554.2883	88.414	1.224836
941	3.080492	15454.3636	90.39	1.266805
942	3.078361	15497.5047	89.541	1.24877
943	3.087665	15309.5429	93.192	1.32635
944	3.079424	15475.975	89.965	1.257787
945	3.076041	15544.5567	88.608	1.228954
946	3.083577	15391.9881	91.606	1.292645
947	3.082745	15408.8011	91.279	1.285708
948	3.085854	15346.0407	92.493	1.311494
949	3.095103	15160.1027	96.002	1.38605
950	3.094953	15163.0993	95.947	1.384871
951	3.086173	15339.6087	92.617	1.31412
952	3.077409	15516.8062	89.159	1.240659
953	3.091124	15239.9526	94.512	1.354382
954	3.089965	15263.2567	94.072	1.345039
955	3.08621	15338.8541	92.631	1.314428

956	3.081082	15442.4206	90.624	1.271775
957	3.084441	15374.5442	91.944	1.29982
958	3.085325	15356.7156	92.288	1.307129
959	3.085738	15348.3774	92.448	1.310539
960	3.086481	15333.4039	92.736	1.31665
961	3.081161	15440.8195	90.655	1.27244
962	3.09349	15192.44	95.402	1.373291
963	3.095741	15147.3024	96.239	1.391075
964	3.091916	15224.0447	94.811	1.360734
965	3.084193	15379.5636	91.847	1.297758
966	3.090368	15255.1448	94.225	1.348296
967	3.100346	15055.1758	97.921	1.426811
968	3.090695	15248.5734	94.349	1.350931
969	3.09953	15071.4833	97.626	1.420542
970	3.092193	15218.4854	94.915	1.362949
971	3.082702	15409.6634	91.263	1.285352
972	3.091115	15240.1251	94.508	1.354313
973	3.084309	15377.215	91.892	1.298723
974	3.092304	15216.2542	94.957	1.363837
975	3.086103	15341.0219	92.589	1.313543
976	3.09009	15260.7491	94.119	1.346046
977	3.091227	15237.8924	94.55	1.355206
978	3.096068	15140.7633	96.359	1.393637
979	3.096606	15129.9857	96.558	1.397851
980	3.091253	15237.3606	94.56	1.355419
981	3.105491	14952.5637	99.75	1.465682
982	3.090526	15251.9764	94.285	1.349567
983	3.090765	15247.1788	94.376	1.35149
984	3.09215	15219.3376	94.899	1.36261
985	3.090145	15259.6272	94.141	1.346497
986	3.080671	15450.7359	90.461	1.268316
987	3.094211	15177.9766	95.671	1.379009
988	3.096919	15123.7128	96.673	1.400299
989	3.098556	15090.9655	97.272	1.41302
990	3.088694	15288.8337	93.587	1.334733
991	3.091473	15232.9485	94.643	1.357182
992	3.102622	15009.7429	98.737	1.444146
993	3.100132	15059.4579	97.843	1.425167
994	3.090865	15245.1564	94.414	1.3523
995	3.096111	15139.8989	96.375	1.393975

996	3.093916	15183.8922	95.561	1.376672
997	3.106275	14936.9592	100.02	1.471504
998	3.094034	15181.52	95.605	1.37761
999	3.092164	15219.0647	94.904	1.362718
1000	3.098257	15096.9456	97.163	1.410704