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Whole-Body Compliant Dynamical Contacts in Cognitive Humanoids

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Review of human postural control and whole body motion in contact with environment

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Abstract	The aim of this deliverable is to provide a solid multidisciplinary base for future research work within CoDyCo. It provides a thorough review and summary of the recent relevant literature on human postural control and whole body motion in contact with environment. It includes relevant publications up to date. To provide a bridge in methodologies and terminologies used by the project partners from multidisciplinary backgrounds, the deliverable also reviews the methods for evaluation of postural stability of bipedal systems.
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Abstract

The bipedal stance and walking are one of the distinctive features of humans as well as human-inspired humanoid robots. Relatively unstable nature of bipedal systems poses a challenge to its postural control. Many researchers were intrigued by the functioning of central nervous system during the control the human posture in presence of various perturbations. The aim of these studies was mainly to improve our understanding of human postural control, which can be beneficial in fields such as rehabilitation and injury prevention, and could even be applied in control of humanoid robots. This report consists of an review of human postural control studies and methods for evaluation of postural stability of bipedal systems. The review should provide a solid base for future studies of both human and humanoid robot postural control.

1 Introduction

Humans evolved the ability of bipedal terrestrial locomotion which brought some important benefits. When the legs alone became the primary way of moving in the environment, the arms could be devoted to other purposes such as manipulation of objects in the environment and tools use. However, the transition from quadrupedalism to bipedalism came at a cost of decreased postural stability. The unpredictable and unstructured nature of the human environment presents many instances that can destabilise the human body balance. The reduced support polygon requires the central nervous system to develop adequate control mechanisms and strategies to adapt to the new condition and maintain the balance.

This interested many researchers and there have been numerous studies in the past decades that aimed to decipher the functioning and behaviour of the human central nervous system regarding to postural control. The studies of postural control have been performed both in the case of walking and stance. This review mainly focuses on postural control studies of bipedal stance. These were predominantly conducted by observing the human motor behaviour as a result of unpredictable external postural perturbations. The observed connection between motor reactions to the given perturbation and the nature of perturbation itself was then used to identify certain patterns of central nervous system (CNS) functioning.

The results of such studies can be applied to improve human rehabilitation techniques, treatment of various postural control disorders or to produce more efficient support aids such as crutches and handrails. On the other hand, the same studies can potentially provide solutions to robot control as well. The emergence of service robotics was aimed to build robots to assist humans in various tasks in human environment. In attempt for the robots to best fit into such environment, researchers emulated human body structure to build humanoid robots. The similar structure of humanoid robots offers both practical and social benefits. Yet the bipedal nature brings the same drawbacks as with humans. The intrinsically unstable balance of such robots require proficient control mechanisms and strategies dedicated to postural control. Findings from human postural control studies could provide a short-cut for achieving adequate humanoid robot control algorithms.

In this review we first examine the types of postural perturbations that were employed in the

studies of bipedal stance. We continue with a scan of the previous studies on human postural control strategies. These studies include postural control in standing, necessity of stepping reaction for larger perturbations, use of firm hand contacts and use of additional sensory information in a form of light touch to improve the stability. We then examine most notable methods utilised for evaluation of the stability of bipedal systems such as Centre of Pressure, Zero Moment Point and Capture Point, and indicate potential problems with the use of these methods when additional hand contacts are established. In the last section we conclude with an overview of the stability methods that go beyond contacts on a flat surface and without additional hand contacts. We review methods that generalise planar metrics to non-planar, stability metrics in wrench space and finally stability metrics that are based on energy.

2 Types of postural perturbations

2.1 Support surface perturbations

A common technique used to induce postural perturbations was by moving the platform on which the human subjects were standing. These platform motions can be divided into translational and rotational motions. In both cases, the researchers usually specify the motion of the platform by the displacement from the original position/orientation, maximum velocity and maximum acceleration and deceleration. The displacement can also be defined by a fixed duration of the predefined motion of the platform.

2.1.1 Translational perturbations

It was observed that the intensity of motor responses to the postural perturbation are scaled with the amount of displacement of the platform [Horak et al., 1989]. The important phases of translational perturbations are the acceleration and deceleration, which yield motor responses to compensate the inertial forces. MacIroy and Maki [McIlroy and Maki, 1994] studied the effects of platform acceleration and deceleration on human postural control. They were particularly interested in the effects of the deceleration phase and investigated the predictability of the deceleration by replacing the deceleration phase with re-acceleration. Studies performed by Runge et al. [Runge et al., 1999] provided the evidence that deceleration phase actually assists in the recovery of balance. The acceleration in the initial phase produces destabilising forces on the human body that consequently move the centre of mass (COM). Yet the deceleration that stops the platform produces forces in the opposite direction which help the human in balancing the body posture by reversing the motion of COM back towards the equilibrium position. Bothner et al. [Bothner and Jensen, 2001] showed that the velocity of platform has an important stabilisation effect of deceleration. Their studies indicated that the stabilisation is increased with the increased platform velocity.

Brown et al. [Brown et al., 2001] tested the postural control responses for different platform motion profiles. They showed that different acceleration/deceleration profiles produce different reactions even if the peak velocity and displacement are the same. On this basis they stressed

the importance of providing a detailed description of the perturbation for the purpose of comparison between the studies. Carpetner et al. [Carpenter et al., 2005] used different intervals between the acceleration and deceleration phase to further study the stabilisation effects of deceleration phase. They showed that the stabilisation effect as a result of reversed trunk movement is smaller for shorter intervals between the two phases. In addition they provided evidence of CNS being able to adapt the motor response to acceleration phase based on the expected deceleration phase. Van Asseldonk et al. [van Asseldonk et al., 2007] upgraded these studies by investigating the causes of body motion in response to acceleration/deceleration of the platform.

2.1.2 Rotational perturbations

Some studies of postural control used support surface rotation rather than translation to induce perturbation. It has been shown that the responses to the rotational perturbations are different to translational perturbations in the equivalent directions [Nardone et al., 1990]. Therefore the two types of perturbations provide different insights into CNS functioning during postural control. Carpenter et al. [Carpenter et al., 1999] compared the reactions between pitch and roll perturbation. The results suggested that the lateral perturbations induced by pitch movement of support surface may be more destabilising compared to antero-posterior perturbations because they required more complex muscle coordination. In a study conducted by Allum et al. [Allum et al., 2002], the researchers were interested in reaction differences between young and elderly subjects to platform pitch and roll change. The results suggested different trunk roll movement and different arm roll movement between the two groups. In addition, balance-control muscle responses of elderly group were changed in respect to time, amplitude and coordination.

2.2 Waist-pull perturbations

Another type of postural perturbation used in several postural control studies is waist-pull perturbation. In this case the researchers used different mechanisms to pull the human waist from different directions [Luchies et al., 1994, Pidcoe and Rogers, 1998]. For example Mansfield et al. [Mansfield and Maki, 2009] compared support surface translation perturbation and weight-drop waist-pull perturbation in a study of age related balance reaction impairments. They used cables to pull human at the waist in anterior, posterior and both lateral directions. Their findings showed that the surface translation is more destabilising than waist-pull and could potentially be more effective in revealing age-related deficiencies of postural control. Recently, Mille et al. [Mille et al., 2013] used a motor-driven waist-pull mechanism with 6 cables attached to human waist; 3 located at on side and 3 on the other side in respect to medial plane. With the different orientation of the belt the subjects could be perturbed either in antero-posterior or lateral directions. In the study they investigated stepping response to external postural perturbation for two different age groups. The results showed that the younger subjects were mostly able to recover their balance with a single step, while older subjects required multi-step recovery (particularly in case lateral direction of perturbation). A similar

motor-driven pulling mechanism [Peternel and Babič, 2013] was employed in a study of how to transfer human postural control skill to the humanoid robot [Peternel and Babic, 2013]. The mechanism was used to allow the human to perceive the postural perturbation experienced by robot and extract the appropriate reactions.

3 Human postural control strategies

3.1 Stance

Nasher and McCollum [Nashner and McCollum, 1985] hypothesised that CNS uses distinctive postural control strategies for counteracting antero-posterior support surface translations during standing. Horak and Nashner [Horak and Nashner, 1986] later described the ankle strategy and hip strategy, where the ankle strategy primarily uses ankle torque to position body COM and the hip strategy uses a combination of ankle and hip torques. It has been suggested that CNS employs ankle strategy if the perturbation can be compensated solely by the ankle torque. In case of bigger perturbations hip strategy is required. However a study by Scholtz et al. [Scholz et al., 2007] suggested that CNS makes use of multi-joint redundancy and performs postural control by a single strategy that considers all degrees of freedom.

3.2 Stepping and contact with environments

If the intensity of the perturbation exceeds the limits when they can be compensated by either or the stance strategies, a stepping strategy may be required [Lee et al., 2014, Horak and Nashner, 1986, Mcllroy and Maki, 1995]. During the step human moves the leg to shift the support polygon¹ under the COM gravity vector and prevents the fall [Maki and Mcllroy, 1997]. In addition to using the legs, human can also employ arms to help stabilising the body. Several studies suggested that arm movement can provide inertial or gravitational balancing aid [Romick-Allen and Schultz, 1988, Allum et al., 2002]. Alternatively, human can use arms to make a hand contact with the environment to help retaining the balance [Mcllroy and Maki, 1995, Maki and Mcllroy, 1997, Jeka, 1997]. Compared to using the inertia of arms for counter-balancing reactions, contact with the surrounding objects offers better stabilising potential [Maki et al., 2003]. Several studies showed that even a light contact with environment can improve postural control by providing CNS with additional sensory information [Jeka, 1997, Riley et al., 1997, Clapp and Wing, 1999]. However a more reliable strategy to counteract the external perturbation is a reach-to-grasp action [Mcllroy and Maki, 1995, Maki and Mcllroy, 1997]. In this case the human makes a firm hand contact with the environment that increases the support polygon.

In their study, Mcllroy and Maki et al. [Mcllroy and Maki, 1995] were interested in initial muscle activation patterns of human arm reaching as a reaction to translational perturbations

¹Support polygon is an area that includes the contact surfaces of feet and a convex hull in-between them. COM must be located above the support polygon for body to be statically stable.

of support surface. They observed that the shoulder muscles activated even when the arm reaction provided no immediate stabilisation effect. However they concluded that this action is not merely a startle reaction since it scaled with the magnitude of perturbation. A study from Maki and McIlroy [Maki and McIlroy, 1997] suggested that stepping and grasping strategies are not used just in last resort, but are commonly employed by CNS even when perturbations are relatively small. Their results showed that both strategies can be initiated well before the COM gravity vector reaches the limit of the support polygon. Cheng et al. [Cheng et al., 2012] investigated the importance of visiospatial information (VSI) in reach-to-grasp reactions. They found that subjects were able to successfully grasp the handrail using either online or stored VSI. They simulated both VSI conditions by blocking the subject's eyes either before or after the onset of the perturbation. The results however suggested that stored VSI has predominant effect on initial reaching reactions, while online VSI affects the final stages of reaching.

Recently, some studies investigated the effects of handle locations on the postural control. Sarraf et al. [Sarraf et al., 2014] replicated the accelerating/decelerating conditions experienced by humans on public transports. They compared responses to 4 different surface translations (antero-posterior and lateral) at 2 different position of hand contact (shoulder height and overhead height). Based on the results they concluded that grasping the handrail at shoulder height yield smaller centre-of-pressure (COP) excursion, while grasping at overhead produces smaller forces between hand and handrail. Moreover Babič et al. [Babic et al., 2014] studied postural control responses to translational perturbations in antero-posterior directions for 4 different locations of hand contact. Contrary to Sarraf et al. [Sarraf et al., 2014], the handle was not fixed to the platform and did not move together with the perturbation. Their experimental setup emulated situations when balance of an individual is challenged either due to intrinsic or extrinsic causes. They found that an additional supportive hand contact significantly reduced the COP displacement regardless of the position of the handle, direction of the perturbation and its intensity. Interestingly, they showed that the position of the handle had no effects on the maximal COP displacement which supports the idea that maintaining postural stability is the task of the highest priority and that the CNS does whatever necessary to keep the body balanced. However, they found significant effects of perturbation direction, intensity and handle position on the maximal force in the handle. An interesting practical implication of their work is that the handles should be positioned to approximately shoulder height to efficiently provide balance support.

4 Stability evaluation methods for bipedal systems

In this section we review the methods for evaluation of postural stability of general bipedal systems for flat-surface contacts. We first describe the most commonly used measures such as Centre of Pressure (COP) and Zero Moment Point (ZMP) and then focus on other, less known, measures, namely Foot Rotation Indicator (FRI), Centroidal Moment Pivot (CMP) and Capture Point (CP). Identical definitions with focus on humanoid balance control and its application to the CoDyCo first year validation scenario can be found in Deliverable 5.1.

Stability evaluation methods for the bipedal systems were mainly investigated by researches

from the two different fields, namely biomechanics and robotics. In human postural control studies, some researchers used centre of mass (COM) position as a measure of postural stability [Maki et al., 2003]. Its gravity vector must be pointing within the support polygon for a stable pose. However just observing COM position only gives information about body stability in static conditions. In case of dynamic stability one must also consider inertial forces and moments acting on the body. Centre of pressure (COP), on the other hand, includes also inertial factors and can provide a suitable measure for dynamical stability of the human body. Other measures for assessing the stability in the field of biomechanics are Equilibrium Score (ES) and Posture Stability Index (PSI), which were discussed in details along with their pros and cons in [Chaudhry et al., 2011].

In robotics the researchers were mainly interested in developing algorithms for preserving stability of humanoid robots. The most commonly used approach for more than four decades was the use of Zero Moment Point (ZMP) [Vukobratovic and Juricic, 1969, Kemp et al., 2008, Kajita and Espiau, 2008, Hirai et al., 1998, Huang et al., 2001]. ZMP is the point at the contact of the foot with the ground, where the total vertical inertia and gravity forces equals to zero. This methodology was used for maintaining stability of humanoids while performing tasks like walking [Li et al., 1993, Arakawa and Fukuda, 1997, Harada et al., 2003], suffering external perturbations [Hyon et al., 2007] or even skiing [Petrič et al., 2013]. The other stability evaluation methods used in robotics were also Centre of Pressure (COP), which is closely related to the ZMP and it is widely used in the field of physiology, Foot Rotation Indicator (FRI) [Goswami, 1999], which is an extension of the ZMP, Centroidal Moment Pivot (CMP) [Popovic et al., 2004], which determines the rotational balance of the body, and Capture Point (CP) [Pratt et al., 2006], which determines the point on the ground where the supportive contact would stabilise the biped without requiring another step. The main advantage of this approach compared to the others, is the knowledge where the supportive contact should be made in order to preserve the postural stability.

4.1 Centre of Pressure (COP)

The location of the COP is determined on the base of support by the resulting vertical ground reaction vector that would act if it could be considered to have a single point of application. Because this can be easily measured by the force plate or with force sensors on the feet of humanoids [Winter, 1995, Goswami, 1999, Popovic and Herr, 2005], it is the most commonly used stability measure in biomechanics for studying human walking and stability [Winter, 1995].

On the flat surface when all horizontal forces are compensated by the friction force the COP point is calculated as

$$\mathbf{p}_{COP} = \frac{\int_A \mathbf{p} \rho dA}{\int_A \rho dA} \quad (1)$$

where A is the surface area of the contact (support polygon), \mathbf{p} is the location and ρ is the pressure of the infinitesimal calculus of the supportive surface area dA .

4.2 Zero Moment Point (ZMP)

ZMP is defined as a point on the surface, where the sum of the horizontal torques due to the angular momentum and gravity equals zero [Vukobratovic and Borovac, 2004, Huang et al., 2001]. A dynamical model of a biped is required for calculation, therefore this measure is mainly used in robotics community. Note that unless a correct and exhaustive dynamic model is available, the error in the ZMP calculation may be substantial.

For the i -th link we denote the mass m_i , the mass centre point $\mathbf{r}_i = [x_i, y_i, z_i]^T$ relative to the inertial frame, the inertial tensor \mathbf{I}_i , and the angular velocity $\boldsymbol{\omega}_i$. The external torques and forces are denoted as $\mathbf{M}_{i,j}$ and $\mathbf{F}_{i,k}$, where index j tracks all torques and index k tracks all forces acting on the i -th link. The overall equation of the system at an arbitrary point $\mathbf{p} = [x_p, y_p, 0]^T$ on the plane $z = 0$ (on flat ground this equals the ground) is

$$\sum_i \{m_i (\mathbf{r}_i - \mathbf{p}) \times (\ddot{\mathbf{r}}_i + \mathbf{g}) + \boldsymbol{\iota}_i\} + \boldsymbol{\xi} = \mathbf{M}_p, \quad (2)$$

where

$$\boldsymbol{\iota}_i = \mathbf{I}_i \dot{\boldsymbol{\omega}}_i + \boldsymbol{\omega}_i \times \mathbf{I}_i \boldsymbol{\omega}_i, \quad (3)$$

$$\boldsymbol{\xi} = - \sum_j \mathbf{M}_j - \sum_k (\mathbf{s}_k - \mathbf{p}) \times \mathbf{F}_k. \quad (4)$$

Here \mathbf{s}_k is the vector that points towards the position, where the external force \mathbf{F}_k is acting on the robot, \mathbf{g} is the gravity acceleration vector and \mathbf{M}_p is the resulting torque at the observed point \mathbf{p} .

In accordance to the ZMP definition, only the moment $\mathbf{M}_p = [0, 0, M_z]^T$ acts at the point $\mathbf{p}_{ZMP} = [x_{ZMP}, y_{ZMP}, 0]^T$. When no external forces are acting on the robot, the components of \mathbf{p}_{ZMP} are

$$x_{ZMP} = \frac{\sum_i m_i \{x_i (\ddot{z}_i + g_z) - z_i (\ddot{x}_i + g_x) - I_{yi} \dot{\omega}_{yi}\}}{\sum_i m_i (\ddot{z}_i + g_z)}, \quad (5)$$

and

$$y_{ZMP} = \frac{\sum_i m_i \{y_i (\ddot{z}_i + g_z) - z_i (\ddot{y}_i + g_y) - I_{xi} \dot{\omega}_{xi}\}}{\sum_i m_i (\ddot{z}_i + g_z)}. \quad (6)$$

If a biped is standing on a flat surface, then the horizontal torque components of the ZMP point are zero $\mathbf{M}(\mathbf{r}_{ZMP}) = [0, 0, M_z]^T$. In this case, if all horizontal forces are compensated by the friction force, the resultant reaction force F_z acts perpendicularly to the supportive surface at the COP point. Consequently the horizontal torque lever-arm is zero

$$\mathbf{M}(\mathbf{p}_{COP}) = \frac{\int_A (\mathbf{p} - \mathbf{p}_{COP}) \rho dA}{\int_A \rho dA} \times \int_A d\mathbf{F}_z = [0 \quad 0 \quad M_z]^T \quad (7)$$

In this case the COP and ZMP are equal [Goswami, 1999, Popovic and Herr, 2005]. If the ZMP or COP are inside the support polygon or at the edge and if the external forces are zero the biped is dynamically stable [Vukobratovic and Juricic, 1969, Huang et al., 2001, Arakawa and Fukuda, 1997].

4.3 Foot Rotation Indicator (FRI)

If the ZMP or COP is at the very edge of the support polygon and additional rotational acceleration is acting on the biped, then neither ZMP nor COP are not applicable as a stability measure. ZMP and COP are only defined under the supportive polygon, since reaction force can only act on the foot. Even though the COP is at the very edge of the supportive polygon the horizontal components are not equal to zero because of the additional rotational acceleration of the foot. To describe this dynamics a Foot Rotation Indicator (FRI) or also known as Fictitious Zero Moment Point (FZMP) was defined [Vukobratovic and Borovac, 2004]. It is defined as a point on a flat surface, where the resultant force should act such that the horizontal torque components are zero. Unlike the ZMP and COP, the FRI is defined also outside the supportive polygon. The FRI is equal to the ZMP and COP when the foot is stationary. It is calculated by

$$x_{FRI} = \frac{x_s \dot{G}_{sz} - z_s \dot{G}_{sx} - x_{ZMP} F_{Rz} - \dot{\Gamma}_{sy}^{(s)}}{\dot{G}_{sz} - F_{Rz}} \quad (8)$$

$$y_{FRI} = \frac{y_s \dot{G}_{sz} - z_s \dot{G}_{sy} - y_{ZMP} F_{Rz} + \dot{\Gamma}_{sx}^{(s)}}{\dot{G}_{sz} - F_{Rz}} \quad (9)$$

where x_s , y_s in z_s are positions of mass centre of gravity, G_s is foot momentum, and $\Gamma_s^{(s)}$ the angular momentum of the foot in the foot coordinate system.

4.4 Centroidal Moment Pivot (CMP)

CMP comes from the biomechanics and it is used to determine the rotational stability of the bipedal systems. It is defined as a point on the surface through which a straight line goes, which is parallel to the ground reaction forces and intersects the body COM point [Goswami, 2004, Popovic and Herr, 2005]. It is defined with

$$(\mathbf{p}_{CMP} - \mathbf{p}_{COM}) \times \mathbf{F}_R = 0 \quad (10)$$

where \mathbf{p}_{CMP} is the vector from the base coordinate system that points towards the CMP.

If CMP is equal to ZMP, then the torque around COM is zero. If CMP is outside the supportive polygon, then the body loses the rotational stability. This does not necessary mean losing also the postural stability.

4.5 Capture Point (CP)

CP defines a point where the biped should step in order to keep or to re-establish its postural stability [Pratt et al., 2006, Koolen et al., 2012]. Unlike the stability measures like ZMP or COP, which may lead to a situation in which there is no longer possible to maintain stability, the CP stability measure includes dynamic predictions. Lets assume that we have a simple 2D cart-table model with constant height h of the COM. For such case ZMP derives into

$$x_{ZMP} = x - \frac{h}{g_y} \ddot{x}, \quad (11)$$

where g_y is the gravity acceleration and x is the position of the cart, which is equal to the position of the COM ($x \equiv x_{COM}$). The error between the desired ZMP trajectory $x_{ZMP,d}$ and the actual ZMP x_{ZMP} is given by

$$\tilde{x}_{ZMP} = x_{ZMP,d} - x_{ZMP}, \quad (12)$$

and the error dynamics can be written as

$$\ddot{x} = -\frac{g_y}{h}(x_{ZMP,d} - x). \quad (13)$$

By assuming that $x_{ZMP,d} < x$, then $x_{ZMP,d} - x < 0$ and according to Eq. 13 the acceleration $\ddot{x} > 0$. This further means that $x_{ZMP,d} < x(t) < x(t+1)$, where $t+1$ denotes the next time step. This implies that $\ddot{x}(t) < \ddot{x}(t+1) < \ddot{x}(t+\infty)$, which shows that a direct control of x_{ZMP} over time is only possible if the x is diverging from the desired ZMP position $x_{ZMP,d}$ (note that this also implies that the accelerations go towards the infinity).

To efficiently control the stability of such system, we have to consider also the CP. For a simple card-table model the CP is given by

$$x_{CP} = x + \dot{x} \sqrt{\frac{h}{g_y}}. \quad (14)$$

If both ZMP and CP are inside the supportive polygon, the system will remain postural stability. The detailed description of the CP is in [Pratt et al., 2006, Koolen et al., 2012].

5 Stability metrics with non-planar contacts

Up to now, methods for the stability measure have considered contact only on a flat surface and without any hand contacts. However, most everyday tasks that humans do, and which humanoid robots are to perform as well, must include non-planar contacts over multiple parts of the body. Understanding stability in such a situation becomes less intuitive, as simple geometric concepts like zero moment point are no longer valid. Thus these issues are still an open topic of research in both the robotic and biomechanical communities.

5.1 Generalizing planar metrics to non-planar

Earliest works in this domain have attempted to extend the traditional concepts of COP and ZMP to handle non-planar contact. In the case that the two feet do not coincide on the same plane, the ZMP (or COP) of each foot can be linearly combined into a single virtual ZMP [Takenaka, 1999]:

$$\mathbf{p}_{VZMP} = (1 - h)\mathbf{p}_{ZMP1} + h\mathbf{p}_{ZMP2}, \quad (15)$$

with the weighting factor chosen, for example, to aid transition from a double support to single support phase: $h = (t - t_{\text{start}})/(t_{\text{end}} - t_{\text{start}})$. The virtual ZMP will exist on a virtual surface

defined by the surface normal that results from the linear combination of the two real surface normals:

$$\mathbf{n} = (1 - h)\mathbf{n}_1 + h\mathbf{n}_2. \quad (16)$$

While this blending of ZMPs may serve as an adequate heuristic for the control of bipedal locomotion, it turns out that the sum moment of all contact forces may not be directed purely along this virtual surface normal. Thus the so-called virtual zero moment point may not have an actual “zero moment” (in direction perpendicular to the surface normal). Instead, [Sardain and Bessonnet, 2004] create a different virtual surface such that the sum moment of contact forces will be perpendicular to it. This virtual surface passes through the intersection line of the two real surfaces, with normal defined as:

$$\mathbf{n} = \frac{R_1^p \mathbf{n}_1 + R_2^p \mathbf{n}_2}{\|R_1^p \mathbf{n}_1 + R_2^p \mathbf{n}_2\|}, \quad (17)$$

where R_1^p and R_2^p are the local pressure contact forces at the feet. Then the authors define the pseudo COP-ZMP point C to be the point on the virtual surface where the contact moment is parallel to the surface normal (and thus remains consistent with the definition of ZMP):

$$C = \frac{\mathbf{n} \times \mathbf{M}^C}{\mathbf{R}^C \cdot \mathbf{n}}, \quad (18)$$

where \mathbf{R}^C and \mathbf{M}^C are the resultant contact force and moment, combining the local contact forces and moments at each foot. While the authors succeed at generalising the concept of ZMP to non-planar contacts, they admit that their method is not able to define a pseudo-support-polygon, i.e. the set of all possible pseudo-ZMP points that define the region of dynamic stability. In order to define such a support polygon, the work of [Harada et al., 2003] defines a *generalised ZMP* which takes into account the forces and moments created by hand contact. However, this ZMP is still projected onto the floor where the feet stand. The edges of the convex hull of the contact points are projected onto the floor as well, creating an expanded region of dynamic stability that considers hand contacts.

5.2 Stability metrics in wrench space

Inspired by work in grasping, several have considered stability metrics in the space of forces and moments (or wrench space [Takao et al., 2003]), rather than as positions of a point in Cartesian space. An advantage of these works, are that they can also explicitly consider contact force limitations (e.g. due to friction). If we approximate friction cones as L -sided polyhedrals, then the set of possible contact forces created by K contacts will be given by:

$$\mathbf{f}_C = \sum_{k=1}^K \sum_{l=1}^L \epsilon_k^l (\eta_k + \mu_k \mathbf{t}_k^l), \quad (19)$$

where \mathbf{t}_k^l is the unit tangent along the l th edge of the polyhedron. Likewise, the set of possible moments is:

$$\boldsymbol{\tau}_C = \sum_{k=1}^K \sum_{l=1}^L \epsilon_k^l \mathbf{p}_k \times (\eta_k + \mu_k \mathbf{t}_k^l), \quad (20)$$

where \mathbf{p}_k is the position of the k th contact. The set of $(\mathbf{f}_C, \boldsymbol{\tau}_C)$ form a polyhedral convex cone in the space of contact forces and moments, and is called a *polyhedral convex cone of the contact wrench* [Hirukawa et al., 2006]. When the set of gravity and inertial forces and moments acting on the robot $(\mathbf{f}_G, \boldsymbol{\tau}_G)$ are within this polyhedral convex cone, the robot is said to be dynamical stable. In order to quantify the quality of stability, [Barthélemy and Bidaud, 2008] borrow the concept of *residual radius* from grasping literature [Kirkpatrick et al., 1992]. For a given wrench w the largest hypersphere centred at w and fully contained within the polyhedron defined by $(\mathbf{f}_C, \boldsymbol{\tau}_C)$ is called the *residual ball*. The residual radius is the radius of that ball. Computing the largest hypersphere can be formulated as a linear program.

5.3 Energy Metrics

Works in multi-legged locomotion have considered stability metrics based on energy. A robot with multiple contact points will tumble if the sum of all moments about any edge of the support polygon induces a rotation about that edge. Thus a robot will be dynamically stable only if every moment M_i , about the i th-edge of the support polygon is positive (where positive is defined to be in the stabilising direction):

$$M_i = ((\mathbf{F}_I + \mathbf{F}_g) \times \mathbf{R} + \mathbf{M}_I) \cdot \mathbf{e}_i > 0. \quad (21)$$

Here \mathbf{F}_I and \mathbf{M}_I are the sums of the inertial, manipulation, and perturbation forces and moments (respectively), \mathbf{F}_g is the gravity force, \mathbf{e}_i is the unit vector along the edge of rotation, and \mathbf{R} is the shortest displacement between the edge and the COM. The smallest of all such moments, normalised by total weight, is defined to be the *Dynamic Stability Margin* (DSM) [Lin and Song, 2001]:

$$S_{\text{DSM}} = \min_i \left(\frac{M_i}{W_g} \right). \quad (22)$$

Garcia et al. show that DSM can become discontinuous at the time of instability [Garcia and de Santos, 2005] and thus rather derive the energy required to topple the robot about edge i :

$$E_i = mg\|\mathbf{R}\|(\cos \phi - \cos \varphi) \cos \psi + ((\mathbf{F}_I \cdot \mathbf{t})\|\mathbf{R}\| + \mathbf{M}_I \cdot \mathbf{e}_i) \theta - \frac{1}{2} I_i \omega_i^2. \quad (23)$$

Here \mathbf{t} is the unit vector tangential to the rotation, I_i is the moment of inertia about the rotation edge, ω_i is the angular velocity, and the various angles are defined by geometry. In this energy equation, the first term represents the potential energy required to overcome gravity, the second term is the potential energy required to overcome inertial and perturbation forces, and the last term is kinetic energy. Subsequently the *Normalised Dynamic Energy Stability Margin* (NDESM) [Garcia and Gonzalez de Santos, 2006] is defined as the smallest such energy required to topple the robot, normalised by mass:

$$S_{\text{NDESM}} = \min_i \left(\frac{E_i}{mg} \right) \quad (24)$$

The authors show that NDESM represents the maximal impact energy that the robot can absorb, and compared to other energy stability metrics such as [Messuri and Klein, 1985, Papadopoulos and Rey, 1996, Hirose et al., 2001], NDESM is the only stability margin that takes into account dynamics and perturbations while remaining continuous during the transition to instability.

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