Accuracy of original MPM

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Outline

- "Original" MPM
- Numerical accuracy
- Benchmarks
 - Vibrating bar
 - Oedometer
- Sources of spatial errors
 - Analogy with FEM
 - Grid crossing
- Outlook





"Original" MPM

- Modified Lagrangian algorithm
- Euler-Cromer time integration
- Piecewise linear basis functions
- No additional interventions



"Original" MPM

- Modified Lagrangian algorithm
- Euler-Cromer time integration
- Piecewise linear basis functions
- No additional interventions
- Own MATLAB implementation
- 1D (UL)FEM/MPM
- Simplified version of Deltares' code





Numerical Approximation

$$u_{ex} = u_{num} + O(\Delta x^n) + O(\Delta t^m)$$

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Example

$$n$$
 Grid size Error Δx E 1 $\Delta x/2$ $E/2$



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$$n$$
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Numerical Approximation

$$u_{ex} = u_{num} + O(\Delta x^n) + O(\Delta t^m)$$

Example

n Grid size Error Δx E

 $2 \Delta x/2 E/4$

RMS Error

$$Error_{RMS} = \sqrt{\frac{1}{n_p} \sum_{p=1}^{n_p} \left(u_{num}(x_p, t) - u_{ex}(x_p, t) \right)^2}$$





Temporal accuracy

MPM is first order accurate in time, i.e. m = 1.

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Spatial accuracy

Order of spatial accuracy Source

2 Gong (2015); Steffen (2008)

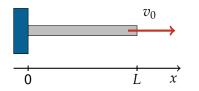
0.5 - 1 Tran (2010)

lack of spatial convergence Gong (2015); Steffen (2008)





Vibrating bar



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial x^2}$$

Boundary conditions:

$$u(0,t)=0$$

$$\frac{\partial u}{\partial x}(L,t) = 0$$

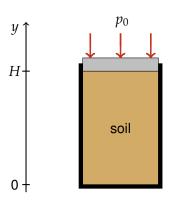
Initial conditions:

$$u(x,0)=0$$

$$\frac{\partial u}{\partial t}(x,0) = v_0 \sin\left(\frac{\pi x}{2L}\right)$$



Oedometer



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial^2 y} - g$$

Boundary conditions:

$$u(0,t)=0$$

$$\frac{\partial u}{\partial y}(H,t) = \frac{p_0}{E}$$

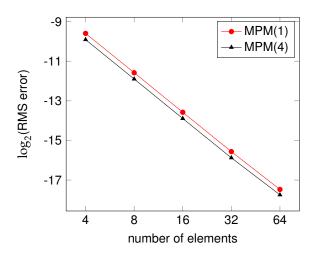
Initial conditions:

$$u(y,0)=0$$

$$\frac{\partial u}{\partial t}(y,0) = 0$$

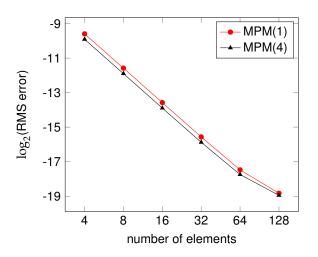


Accuracy: vibrating bar





Accuracy: vibrating bar



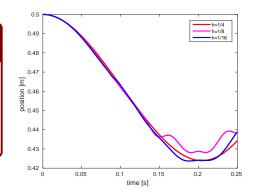


Accuracy: oedometer

Richardson's extrapolation

The order of accuracy *n* is obtained from

$$\frac{u_{num}(2h) - u_{num}(4h)}{u_{num}(h) - u_{num}(2h)} = 2^{n}.$$



Accuracy: oedometer

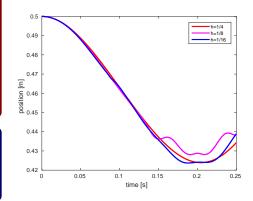
Richardson's extrapolation

The order of accuracy n is obtained from

$$\frac{u_{num}(2h) - u_{num}(4h)}{u_{num}(h) - u_{num}(2h)} = 2^{n}.$$

Conclusion

Lack of spatial convergence.



FEM: oedometer

Theoretical order of accuracy

k+1, where k is the order of the interpolating polynomials¹.

¹Van Kan (2008)



FEM: oedometer

Theoretical order of accuracy

k + 1, where k is the order of the interpolating polynomials¹.

Observations

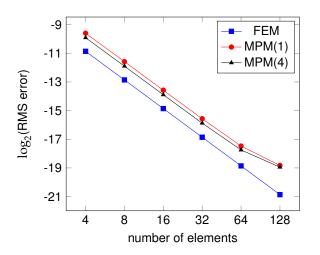
- Lack of spatial convergence
- Problems arise due to external forces

$$\mathbf{M} \frac{d\mathbf{v}}{dt} = \mathbf{F}_{ext} - \mathbf{F}_{int},$$
where $\mathbf{F}_{ext} = \mathbf{N}(H)^T p_0 - \int_0^H \mathbf{N}^T \rho g dy$

¹Van Kan (2008)

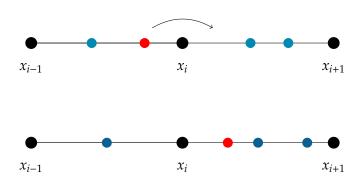


FEM: vibrating bar



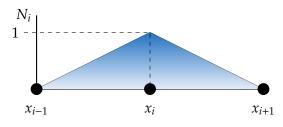


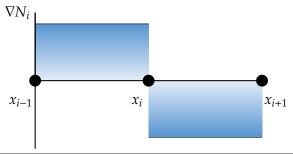
Grid-crossing





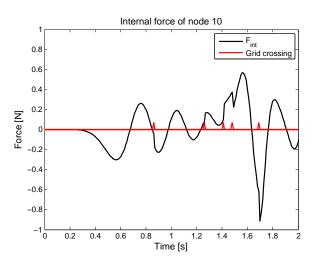
Grid-crossing: properties of shape functions







Grid crossing: internal force







Grid crossing: vibrating bar

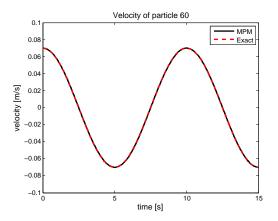


Figure: No grid crossing (30 elements).





Grid crossing: vibrating bar

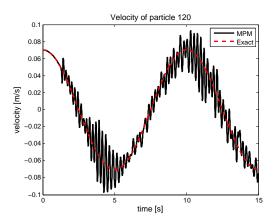
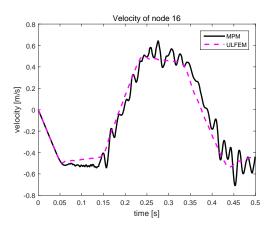


Figure: Grid crossing (60 elements).





Grid crossing: oedometer







Main sources of spatial errors

Presented today

- Errors arising due to external forces
- Grid crossing errors

Other sources

- Mass mapping error
- Momentum mapping error
- Force mapping error





Conclusions

Vibrating bar

Without grid crossing 2nd order accuracy.

Oedometer

Lack of convergence due to grid crossing and external forces.





• External forces: further analysis



- External forces: further analysis
- Higher order interpolation functions





- External forces: further analysis
- Higher order interpolation functions
- 2D MPM code in MATLAB





- External forces: further analysis
- Higher order interpolation functions
- 2D MPM code in MATLAB
- Deltares' implementation: analysis and recommendations





References

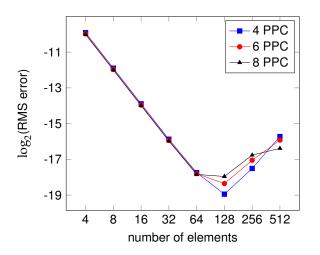
- Gong M. *Improving the Material Point Method.* The University of New Mexico, July, 2015.
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- Steffen M., Kirby R. M., Berzins M. *Analysis and reduction of quadrature errors in the material point method (MPM).* International Journal for Numerical Methods in Engineering 76, pp. 922-946, 2008.
- Tran L.T., Kim J., Berzins M. Solving time-dependent PDEs using the material point method, a case study from gas dynamics.
 International Journal for Numerical Methods in Fluids 62, pp. 709-732, 2010.



Grid crossing: internal force

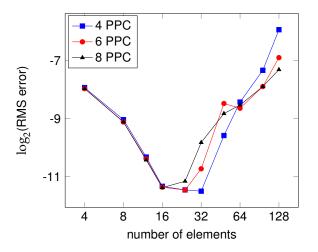
$$\begin{split} F_{i+1}^{int} &\approx \sum_{p=1}^{n_i} \nabla N_i(\xi_p) \sigma_p \Omega_p + \sum_{p=1}^{n_{i+1}} \nabla N_i(\xi_p) \sigma_p \Omega_p \\ F_{i+1}^{int} &\approx \sigma \Omega(n_i - n_{i+1}) \\ \begin{cases} F_{i+1}^{int} &= 0, & \text{if } n_i = n_{i+1} \\ F_{i+1}^{int} &\neq 0, & \text{otherwise} \end{cases} \end{split}$$

Depenence on PPC: vibrating string





Depenence on PPC: oedometer





Settings: vibrating bar

	Symbol	Value	Unit
Length	L	25	m
Tension	Ε	100	Pa
Density	ρ	1	kg/m ³
Maximum velocity	v_0	0.1	m/s
Time step	Δt	$1 \cdot 10^{-3}$	S
Measurement time ¹	t	0.5	S
PPC^2		4	



Settings: oedometer

	Symbol	Value	Unit
Height	L	1	m
Young's modulus	Ε	$1\cdot 10^5$	Pa
Density	ρ	$1 \cdot 10^3$	kg/m ³
Load	p_0	0	Pa
Gravitational acceleration	g	9.81	m/s^2
Time step	Δt	$1 \cdot 10^{-3}$	s
Measurement time ¹	t	0.5	S
Position particle ¹	x_p	≈ 0.5	m
Number of elements ²	,	30	
PPC^2		10	



Settings: Steffen

	Symbol	Value	Unit
Length	L	1	m
Tension	Ε	100	Pa
Density	ρ	100	kg/m ³
Load	p_0	0.7	Pa
Gravitational acceleration	8	0	m/s^2
Time step	Δt	$1 \cdot 10^{-2}$	S
Domain		1.15	m
Number of elements		20	
PPC		10	

