

# Accuracy of original MPM

Lisa Wobbes, Roel Tielen

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# Outline

- Numerical accuracy
- Benchmarks
  - Vibrating bar
  - Oedometer
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# Numerical accuracy

## Numerical Approximation

$$u_{ex} = u_{num} + O(\Delta x^n) + O(\Delta t)$$

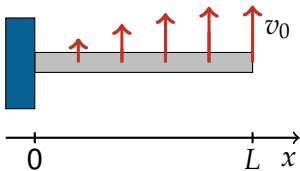
## RMS Error

$$Error_{RMS} = \sqrt{\frac{1}{n_p} \left( \sum_{p=1}^{n_p} u_{num}(x_p, t) - u_{ex}(x_p, t) \right)^2}$$

## Accuracy in displacement

For  $\Delta t \rightarrow 0$ , the order of accuracy is equal to  $n$ , i.e. the reduction of  $\Delta x$  by a factor of 2 decreases the RMS error by  $2^n$ .

# Vibrating bar



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial x^2}$$

Boundary conditions:

$$u(0, t) = 0$$

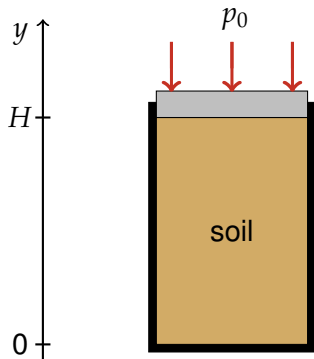
$$\frac{\partial u}{\partial x}(L, t) = 0$$

Initial conditions:

$$u(x, 0) = 0$$

$$\frac{\partial u}{\partial t}(x, 0) = v_0 \sin\left(\frac{\pi x}{2L}\right)$$

# Oedometer



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial x^2} - g$$

Boundary conditions:

$$u(0, t) = 0,$$

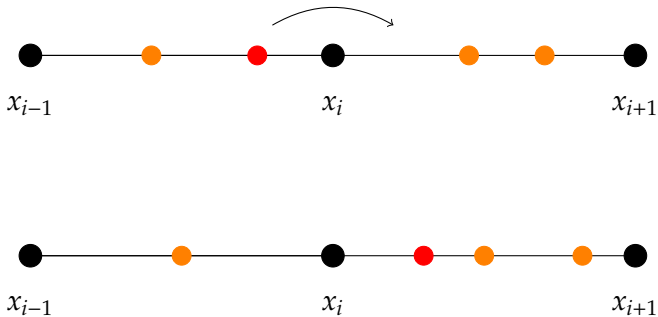
$$\frac{\partial u}{\partial x}(L, t) = \frac{p_0}{E}$$

Initial conditions:

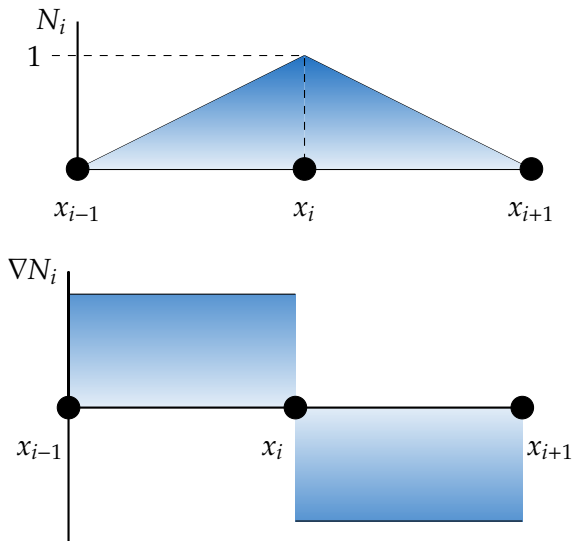
$$u(x, 0) = 0$$

$$\frac{\partial u}{\partial t}(x, 0) = v_0 \sin\left(\frac{\pi x}{2L}\right)$$

# Grid-crossing



# Grid-crossing: properties of shape functions



## Grid crossing: internal force

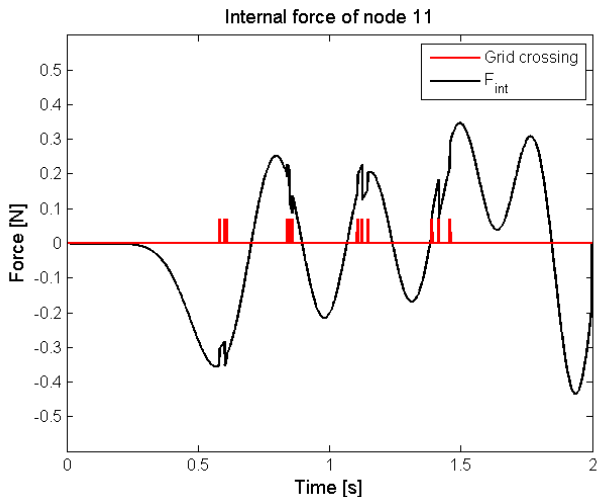
$$F_{i+1}^{int} \approx \sum_{p=1}^{n_i} \nabla N_i(\xi_p) \sigma_p \Omega_p + \sum_{p=1}^{n_{i+1}} \nabla N_i(\xi_p) \sigma_p \Omega_p$$

$$F_{i+1}^{int} \approx \sigma \Omega (n_i - n_{i+1})$$

$$\begin{cases} F_{i+1}^{int} = 0, & \text{if } n_i = n_{i+1} \\ F_{i+1}^{int} \neq 0, & \text{otherwise} \end{cases}$$



# Grid crossing: internal force



# Grid crossing: vibrating bar

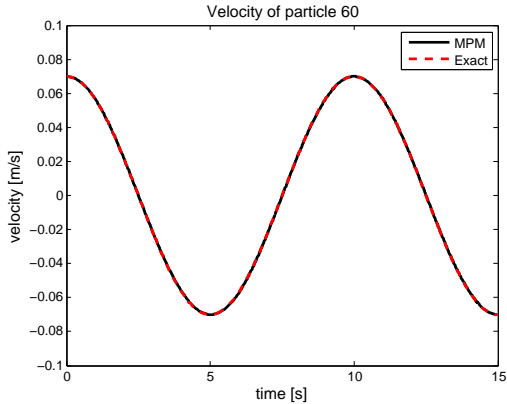


Figure: No grid crossing (30 elements).

# Grid crossing: vibrating bar

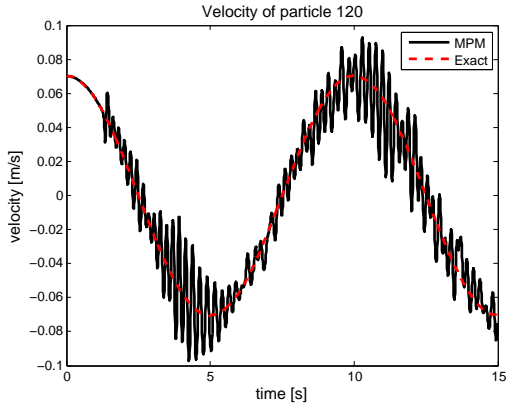


Figure: Grid crossing (60 elements).

## Grid crossing: oedometer