

Experimental Design

Note 7

2^k Factorial Design

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2^k Factorial Design

- Involving k factors to detect the important factors in the process with a minimum of experimental units.
- Each factor has two levels (often labeled + and -)
- Factor screening experiment (preliminary study) often used to at the early stage of experimentation to detect potential candidate factors for more detailed investigation.
- Identify important factors and their interactions
- Interaction (of any order) has **ONE** degree of freedom
- Factors need not be on numeric scale
- Ordinary regression model can be employed

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \epsilon$$

where β_1 , β_2 , and β_{12} are related to main effects, interaction effects defined later.

Chemical Processes Example

Factor		Treatment	Replicate			
A	B	Combination	I	II	III	Total
-	-	A low, B low	28	25	27	80
+	-	A high, B low	36	32	32	100
-	+	A low, B high	18	19	23	60
+	+	A high, B high	31	30	29	90

A=reactant concentration, B=catalyst amount, y=recovery

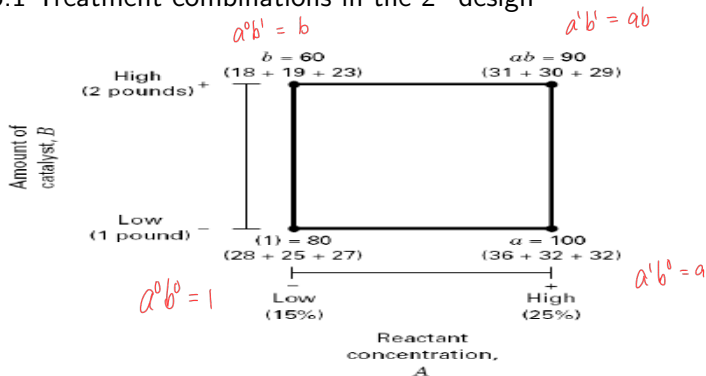
		B	
		-	+
A	-	1, 2, 3	7, 8, 9
	+	4, 5, 6	10, 11, 12

Analysis Procedure for a Factorial Design

- Estimate factor effects
- Formulate model
 - With replication, use full model
 - With an unreplicated design, use normal probability plots
- Statistical testing (ANOVA)
- Refine the model
- Analyze residuals (graphical)
- Interpret results

The Simplest Case: 2^2

Figure 6.1 Treatment combinations in the 2^2 design



- “-” and “+” denote the low and high levels of a factor, respectively.

Estimation of Factor Effects I

$$\begin{aligned}A &= \bar{y}_{A+} - \bar{y}_{A-} = \frac{ab + a}{2n} - \frac{b + (1)}{2n} = \frac{1}{2n} [ab + a - b - (1)] \\B &= \bar{y}_{B+} - \bar{y}_{B-} = \frac{ab + b}{2n} - \frac{a + (1)}{2n} = \frac{1}{2n} [ab + b - a - (1)] \\AB &= \frac{ab + (1)}{2n} - \frac{a + b}{2n} = \frac{1}{2n} [ab + (1) - a - b]\end{aligned}$$

The effect estimates are:

$$A = 8.33, B = -5.00, AB = 1.67$$

The quantities in brackets are **contrasts** in the treatment combinations.

Estimation of Factor Effects II

Effects and Contrasts

factor				effect (contrast)			
A	B	total	mean	1	A	B	AB
-	-	80	$80/3$	1	-1	-1	1
+	-	100	$100/3$	1	1	-1	-1
-	+	60	$60/3$	1	-1	1	-1
+	+	90	$90/3$	1	1	1	1

- There is a one-to-one correspondence between effects and contrasts, and contrasts can be directly used to estimate the effects.

Estimation of Factor Effects III

- For a effect corresponding to contrast $c = (c_1, c_2, \dots)$ in 2^2 design

$$\text{effect} = \frac{1}{2} \sum_i c_i \bar{y}_i$$

where i is an index for treatments and the summation is over all treatments.
For example,

$$\begin{aligned} \text{effect}(A) &= \frac{1}{2n} \{ (y_{++\cdot} + y_{+-\cdot}) - (y_{-+\cdot} + y_{--\cdot}) \} \\ &= \frac{1}{2} \{ \bar{y}_{++} + \bar{y}_{+-} - \bar{y}_{-+} - \bar{y}_{--} \}, \\ \text{effect}(B) &= \frac{1}{2} \{ \bar{y}_{++} + \bar{y}_{-+} - \bar{y}_{+-} - \bar{y}_{--} \}, \\ \text{effect}(AB) &= \frac{1}{2} \{ \bar{y}_{++} + \bar{y}_{--} - \bar{y}_{+-} - \bar{y}_{-+} \}, \end{aligned}$$

Estimation of Factor Effects IV

Sum of Squares due to Effect

- Because effects are defined using contrasts, their sum of squares can also be calculated through contrasts.
- Recall for contrast $c = (c_1, c_2, \dots)$, its sum of squares is

$$SS_{\text{Contrast}} = \frac{(\sum_i c_i \bar{y}_i)^2}{\sum_i c_i^2 / n}$$

So

$$SS_A = \frac{(-\bar{y}(A_-B_-) + \bar{y}(A_+B_-) - \bar{y}(A_-B_+) + \bar{y}(A_+B_+))^2}{4/n} = 208.33$$

$$SS_B = \frac{(-\bar{y}(A_-B_-) - \bar{y}(A_+B_-) + \bar{y}(A_-B_+) + \bar{y}(A_+B_+))^2}{4/n} = 75.00$$

$$SS_{AB} = \frac{(\bar{y}(A_-B_-) - \bar{y}(A_+B_-) - \bar{y}(A_-B_+) + \bar{y}(A_+B_+))^2}{4/n} = 8.33$$

Estimation of Factor Effects V

Sum of Squares and ANOVA

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F
A	SS_A	1	MS_A	
B	SS_B	1	MS_B	
AB	SS_{AB}	1	MS_{AB}	
Error	SSE	$N - 4$	MSE	
Total	SS_T	$N - 1$		

where $SS_T = \sum_{i,j,k} y_{ijk}^2 - y_{...}^2/N$, $SSE = SS_T - SS_A - SS_B - SS_{AB}$.

Revisit Chemical Process Example I

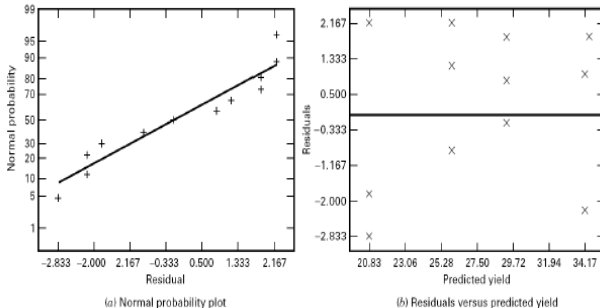
ANOVA Table

See Chemical-Process.SAS.

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F	<i>P</i> -value
A	208.33	1	208.33	53.15	0.0001
B	75.00	1	75.00	19.13	0.0024
AB	8.33	1	8.33	2.13	0.1826
Error	31.34	8	3.92		
Total	323.00	11			

Revisit Chemical Process Example II

Residuals and Diagnostic Checking



■ FIGURE 6.2 Residual plots for the chemical process experiment

Analyzing 2^2 Experiment using Regression Model I

Because every effect in 2^2 design, or its sum of squares, has one degree of freedom, it can be equivalently represented by a numerical variable, and regression analysis can be directly used to analyze the data. The original factors are not necessarily continuous.

Code the levels of factor A and B as follow

A	X_1	B	X_2
-	-1	-	-1
+	1	+	1

$y_{ijk} = \mu + \tau_i + \beta_j + (\tau\beta)_{ij} + \epsilon_{ijk}$
 $\sum \tau_i = 0, \sum \beta_j = 0$

Fit regression model

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \epsilon$$

Analyzing 2² Experiment using Regression Model II

The fitted model should be

$$y = \hat{\beta}_0 \bar{y}_{..} + \frac{\hat{\beta}_1 A}{2} x_1 + \frac{\hat{\beta}_2 B}{2} x_2 + \frac{\hat{\beta}_3 AB}{2} x_1 x_2$$

i.e., the estimated coefficients are half of the effects, respectively.
See Chemical-Process.SAS.

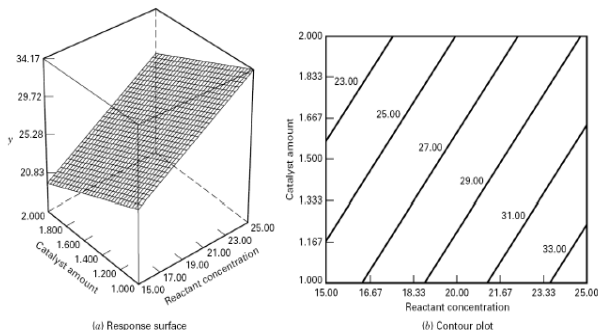
$$y_{ijk} = \beta_0 + \beta_1 x_{i1} + \beta_2 x_{i2} + \beta_3 x_{i1} x_{i2} + \epsilon$$

$$\begin{bmatrix} y_{111} \\ y_{112} \\ y_{121} \\ y_{122} \\ y_{211} \\ y_{212} \\ y_{221} \\ y_{222} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & -1 & -1 \end{bmatrix} \begin{bmatrix} \beta_0 \\ \beta_1 \\ \beta_2 \\ \beta_3 \end{bmatrix} + \begin{bmatrix} \epsilon_{111} \\ \epsilon_{112} \\ \epsilon_{121} \\ \epsilon_{122} \\ \epsilon_{211} \\ \epsilon_{212} \\ \epsilon_{221} \\ \epsilon_{222} \end{bmatrix}$$

$$\hat{\beta} = (X^T X)^{-1} X^T y$$

Analyzing 2^2 Experiment using Regression Model III

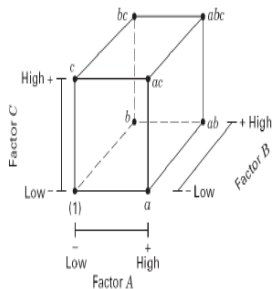
Response Surface



■ FIGURE 6.3 Response surface plot and contour plot of yield from the chemical process experiment

The 2^3 Factorial Design I

■ FIGURE 6.4
The 2^3 factorial
design



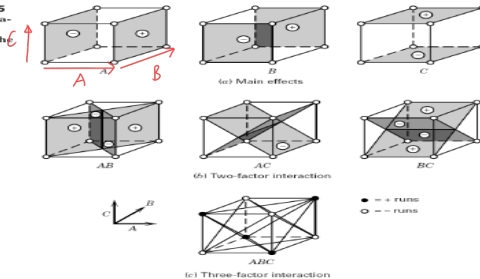
(a) Geometric view

Run	Factor		
	A	B	C
1	-	-	-
2	+	-	-
3	-	+	-
4	+	+	-
5	-	-	+
6	+	-	+
7	-	+	+
8	+	+	+

(b) Design matrix

The 2³ Factorial Design II

■ FIGURE 6.5
Geometric presentation
of contrasts
corresponding to the
main effects and
interactions in the
2³ design



$$A = \bar{y}_{A+} - \bar{y}_{A-}, \quad B = \bar{y}_{B+} - \bar{y}_{B-},$$

$$C = \bar{y}_{C+} - \bar{y}_{C-}, \quad \text{etc...}$$

Analysis is done via computer.

The 2^3 Factorial Design III

Table of - and + Signs for the 2^3 Factorial Design

■ TABLE 6.3

Algebraic Signs for Calculating Effects in the 2^3 Design

Treatment Combination	Factorial Effect							
	<i>I</i>	<i>A</i>	<i>B</i>	<i>AB</i>	<i>C</i>	<i>AC</i>	<i>BC</i>	<i>ABC</i>
(1)	+	-	-	+	-	+	+	-
<i>a</i>	+	+	-	-	-	-	+	+
<i>b</i>	+	-	+	-	-	+	-	+
<i>ab</i>	+	+	+	+	-	-	-	-
<i>c</i>	+	-	-	+	+	-	-	+
<i>ac</i>	+	+	-	-	+	+	-	-
<i>bc</i>	+	-	+	-	+	-	+	-
<i>abc</i>	+	+	+	+	+	+	+	+

The 2³ Factorial Design IV

Properties of the Table

- Except for column I , every column has an equal number of + and - signs
- The sum of the product of signs in any two columns is zero
- Multiplying any column by I leaves that column unchanged (identity element)
- The product of any two columns yields a column in the table:

$$A \times B = AB, \quad AB \times BC = AB^2C = AC$$

- Orthogonal design
- Orthogonality is an important property shared by all factorial designs

The 2^3 Factorial Design V

Contrasts for Calculating Effects in 2^3 Design

			factorial effects								
A	B	C	treatment	<i>I</i>	<i>A</i>	<i>B</i>	<i>AB</i>	<i>C</i>	<i>AC</i>	<i>BC</i>	<i>ABC</i>
-	-	-	(1)	1	-1	-1	1	-1	1	1	-1
+	-	-	a	1	1	-1	-1	-1	-1	1	1
-	+	-	b	1	-1	1	-1	-1	1	-1	1
+	+	-	ab	1	1	1	1	-1	-1	-1	-1
-	-	+	c	1	-1	-1	1	1	-1	-1	1
+	-	+	ac	1	1	-1	-1	1	1	-1	-1
-	+	+	bc	1	-1	1	-1	1	-1	1	-1
+	+	+	abc	1	1	1	1	1	1	1	1

The 2³ Factorial Design VI

$$\hat{\mu} = \bar{y}_{...} = \frac{1}{8n} (y_{+++} + y_{++-} + y_{+--} + y_{-++} + y_{-+-} + y_{-+ -} + y_{--+} + y_{---}) = \frac{1}{8} (\bar{y}_{+++} + \dots + \bar{y}_{---})$$

Estimates:

$$\text{grand mean: } \frac{\sum_i \bar{y}_{i.}}{2^3}$$

$$\text{effect: } \frac{\sum_i c_i \bar{y}_{i.}}{2^{3-1}}$$

Contrast Sum of Squares:

$$SS_{\text{effect}} = \frac{(\sum_i c_i \bar{y}_{i.})^2}{2^3/n} = 2n(\text{effect})^2$$

Variance of Estimate:

$$\text{var}(\text{effect}) = \frac{\sigma^2}{n2^{3-2}}$$

The 2^3 Factorial Design VII

t -test for effects (confidence interval approach):

$$\text{effect} \pm t_{\alpha/2, 2^k(n-1)} SE(\text{effect})$$

Example I

Model Coefficients-Full Model

■ TABLE 6.4

The Plasma Etch Experiment, Example 6.1

Run	Coded Factors			Etch Rate		Total	Factor Levels		
	A	B	C	Replicate 1	Replicate 2		Low (-1)	High (+1)	
1	-1	-1	-1	550	604	(1) = 1154	A (Gap, cm)	0.80	1.20
2	1	-1	-1	669	650	<i>a</i> = 1319	B (C ₂ F ₆ flow, SCCM)	125	200
3	-1	1	-1	633	601	<i>b</i> = 1234	C (Power, W)	275	325
4	1	1	-1	642	635	<i>ab</i> = 1277			
5	-1	-1	1	1037	1052	<i>c</i> = 2089			
6	1	-1	1	749	868	<i>ac</i> = 1617			
7	-1	1	1	1075	1063	<i>bc</i> = 2138			
8	1	1	1	729	860	<i>abc</i> = 1589			

A=Gap, B=Flow, C=Power, y=Etch Rate

Example II

Full Model

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3 + \beta_{123} x_1 x_2 x_3 + \epsilon$$

Model Coefficients for Full Model

Factor	Coefficient Estimated	DF	Standard Error	95% CI Low	95% CI High
Intercept	776.06	1	11.87	748.70	803.42
A-Gap	-50.81	1	11.87	-78.17	-23.45 ✓
B-Gas flow	3.69	1	11.87	-23.67	31.05
C-Power	153.06	1	11.87	125.70	180.42 ✓
AB	-12.44	1	11.87	-39.80	14.92
AC	-76.81	1	11.87	-104.17	-49.45 ✓
BC	-1.06	1	11.87	-28.42	26.30
ABC	2.81	1	11.87	-24.55	30.17

Example III

ANOVA Table

■ TABLE 6.6

Analysis of Variance for the Plasma Etching Experiment

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F_0	P -Value
Gap (A)	41,310.5625	1	41,310.5625	18.34	0.0027
Gas flow (B)	217.5625	1	217.5625	0.10	0.7639
Power (C)	374,850.0625	1	374,850.0625	166.41	0.0001
AB	2475.0625	1	2475.0625	1.10	0.3252
AC	94,402.5625	1	94,402.5625	41.91	0.0002
BC	18.0625	1	18.0625	0.01	0.9308
ABC	126.5625	1	126.5625	0.06	0.8186
Error	18,020.5000	8	2252.5625		
Total	531,420.9375	15			

Example IV

Reduced Model

$$y = \beta_0 + \beta_1 x_1 + \beta_3 x_3 + \beta_{13} x_1 x_3 + \epsilon$$

Model Coefficients for Reduced Model

Factor	Coefficient Estimate	DF	Standard Error	95% CI Low	95% CI High
Intercept	776.06	1	10.42	753.35	798.77
A-Gap	-50.81	1	10.42	-73.52	28.10
C-Power	153.06	1	10.42	130.35	175.77
AC	-76.81	1	10.42	-99.52	-54.10

Example V

Model Summary Statistics

- R^2 and adjusted R^2 for reduced model

$$R^2 = \frac{SS_{Model}}{SS_T} = \frac{5.106 \times 10^5}{5.314 \times 10^5} = 0.9608$$

$$R^2_{Adj} = 1 - \frac{SSE/df_E}{SS_T/df_T} = 1 - \frac{20857.75/12}{5.314 \times 10^5/15} = 0.9509$$

- Standard error of full model coefficients

$$se(\hat{\beta}) = \sqrt{\frac{MSE}{n2^k}} = \sqrt{\frac{2252.56}{2 \times 8}} = 11.87$$

Example VI

- Confidence interval on model coefficients

$$\hat{\beta} - t_{\alpha/2, df_E} SE(\hat{\beta}) \leq \beta \leq \hat{\beta} + t_{\alpha/2, df_E} SE(\hat{\beta})$$