

### Assignment #3

Design the typical floor composite beam & girder using the same loads as in Assignment #1

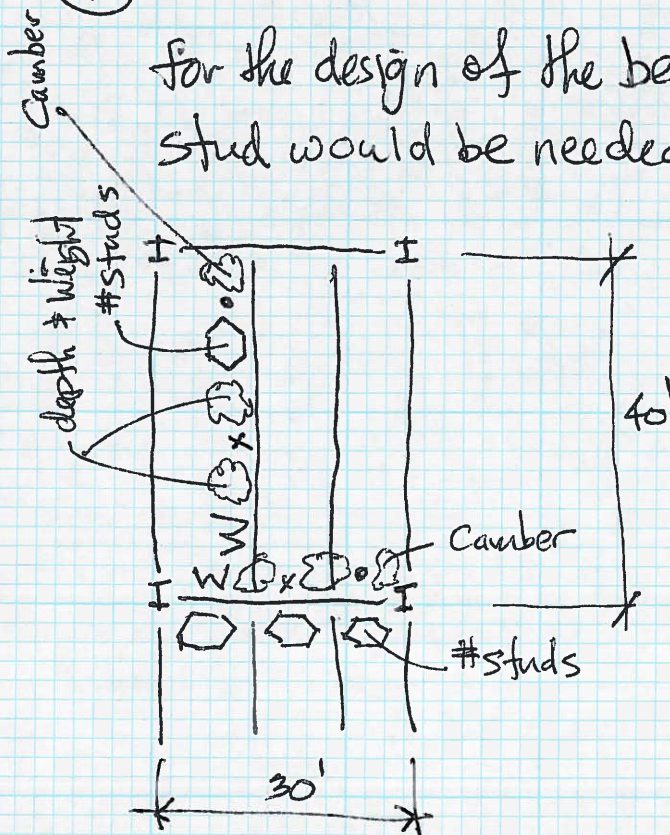
Choose W sections based on the following requirements:

Beams Unshored construction  
Camber  $\leq 1\frac{1}{2}"$

Girders Unshored construction  
Camber  $\leq \frac{3}{4}"$

Find the following for both Beams & Girders:

- ①  $\phi M_n > M_u$
- ② Number of studs for partial composite
- ③ Check  $\Delta_L < L/360$
- ④ Can the live load be increased to 100 psf for the design of the beam? How many stud would be needed?





# Assignment #3

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## Typical Beam

Loads from Assignment #1  $w_D = 860 \text{ #/}$ ,  $w_L = 400 \text{ #/}$   
Const DL = 56 psf LL = 20 psf.

$$w_u = 1.2(0.056 \times 10') + 1.6(0.020 \times 10') = 0.992 \text{ k/}$$

$$M_u = 0.992 \times 40^2 / 8 = 198 \text{ k}$$

$$\text{Req'd } Z = \frac{M_u}{\phi F_y} = \frac{198 \times 12}{0.9 \times 50} = 53 \text{ in}^3$$

$$\text{Camber} \leq 1\frac{1}{2}" \quad \Delta_{DL} \leq 1.50 / 0.8 = 1.875"$$

$$\text{Req'd } I = \frac{5(0.056 \times 10) 40^4 \times 12^3}{384 \times 29000 \times 1.875"} = 593 \text{ in}^4$$

$$\text{Try W18} \times 40 \quad Z = 78.4 \text{ in}^3 \quad I = 612 \text{ in}^4 \quad A = 11.8 \text{ in}^2 \quad d = 17.9"$$

$$\left. \begin{aligned} b &= 10' \times 12 = 120" \\ b &= 40 \times 12 / 4 = 120" \end{aligned} \right\} b = 120"$$

$$A_s F_y = 11.8 \times 50 = 590 \text{ k}$$

$$\alpha = 590 / (0.85 \times 120 \times 3 \text{ ksi}) = 1.93" < 2\frac{1}{2}" \text{ OK}$$

$$M_n = 590 \left( \frac{17.90}{2} + 5.5" - \frac{1.93}{2} \right) / 12 = 590 (13.49") / 12 = 663 \text{ k}$$

$$\phi M_n = 0.9 \times 663 = 597 \text{ k} \gg M_u = 408 \text{ k}$$

## Partial Composite

$$V = \frac{(408 / 0.9) \times 12}{13.49"} = 403.4 \text{ k}$$

$$\text{No. studs} = 403.4 / 17.2 = 23 > 20 \text{ or 1 per flange}$$

Try 5 flanges w/ 2 studs + 15 flanges w/ 1 stud

$$\Sigma Q_n = 5 \times 2 \times 14.6 \text{ k} + 15 \times 17.2 = 404 > V$$

25 stud per 1/2 beam

$$\% \text{ Partial Composite} = \frac{404}{590} \times 100 = 68\%$$



## Deflection Calculations ( $n=8$ )

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$$\bar{y} = \frac{(120/8)(2.5'')2.5/2 + (5.5'' + 17.90/2)11.8}{11.8 + (120/8)2.5} = 4.41''$$

$$I_{tr} = \frac{(120/8)2.5^3}{12} + 612 + (4.41 - 2.5/2)^2 \left( \frac{120}{8} \times 2.5 \right) + \left( \frac{17.9}{2} + 5.5 - 4.41 \right)^2 11.8$$

$$= 19.5 + 612 + 374.5 + 1189.5 = 2196 \text{ in}^4$$

$$I_{eff} = 0.75 I_{tr} = 1647 \text{ in}^4$$

$$I_{eff} = I_s + \sqrt{\frac{E A_n}{C_f}} (I_{tr} - I_s) = 612 + \sqrt{\frac{403.4}{590}} (2196 - 612)$$

$$= 1922 \text{ in}^4$$

Use  $I_{eff} = 1647 \text{ in}^4$

$$\Delta_{LL} = \frac{5(0.4040^4 \times 12^3)}{384 \times 29000 \times 1647} = 0.48'' < \frac{L}{360} = \frac{40 \times 12}{360} = 1.33''$$

$< 1''$  AISC

## Typical Girder

Loads from Assignment #1  $W_D = 3560 \text{ #/ft}$ ,  $W_L = 1120 \text{ #/ft}$   
 $M_u = 682 \text{ k}$

Const DL =  $59 \text{ #/ft}$  LL = 20

$$W_u = 1.2(59 \times 40) + 1.6(20 \times 40) = 412 \text{ #/ft}$$

$$M_u = 4.112 \times 30^2 / 8 = 462.6 \text{ k}$$

$$\text{Req'd } Z = \frac{462.6 \times 12}{0.9 \times 50} = 123.4 \text{ in}^3$$

Camber  $\leq 3/4''$   $\Delta_D = 0.75/0.8 = 0.94''$

$$\text{Req'd } I = \frac{5(0.059 \times 40) 30^4 \times 12^3}{384 \times 29000 \times 0.94} = 1578 \text{ in}^4$$

Try W24x68  $Z = 177 \text{ in}^3$   $I = 1830 \text{ in}^4$   $A = 20.1$   $d = 23.73''$

$$\left. \begin{array}{l} b = 40' \times 12 = 480'' \\ b = 30' \times 12/4 = 90'' \end{array} \right\} b = 90''$$

$$A_s F_y = 20.1 \times 50 = 1005 \text{ k}$$

$$a = 1005 \text{ k} / (0.85 \times 90'' \times 3 \text{ ksi}) = 4.38'' > a_{max} = 3\frac{1}{2}'' + 2\frac{1}{2}'' = 4''$$

$\therefore$  Partial composite  $T = C_{max}$



$$T = C_{max} = 0.85 \times 90'' \times 4'' \times 3 \text{ ksi} = 918^k$$

$$M_n = 918 \left( \frac{23.73}{2} + 5.5'' - \frac{4''}{2} \right) / 12 = 918 (15.37'') / 12 = 1174^k$$

$$\phi M_n = 0.9 \times 1174 = 1057^k > M_u = 682^k$$

### Partial Composite

$$V = \frac{(682 / 0.9) \times 12}{15.37''} = 592^k$$

$$\text{No. studs} = \frac{592^k}{21.5} = 27.5 \sim 28 \text{ studs over } 10'$$

2 rows @ 8 1/2"

$$\% \text{ Composite} = \frac{28 \times 21.5}{1005} \times 100 = 60\%$$

### Deflection Calculations (n=8)

$$\bar{y} = \frac{(90/8)(4)(4/2) + (5.5 + 23.73/2) 20.1}{20.1 + (90/8)(4'')} = 6.744''$$

$$I_{tr} = \frac{(90/8)4^3}{12} + 1830 + (6.744 - 4/2) \left( \frac{90}{8} \times 4 \right) + \left( \frac{23.73}{2} + 5.5 - 6.744 \right)^2 20.1$$

$$= 60 + 1830 + 1013 + 2267 = 5170 \text{ in}^4$$

$$I_{eff} = 0.75 \times 5170 = 3878 \text{ in}^4$$

$$I_{eff} = I_s + \sqrt{\frac{EQ_n}{C_f}} (I_{tr} - I_s) = 1830 + \sqrt{\frac{28 \times 21.5}{918}} (5170 - 1830)$$

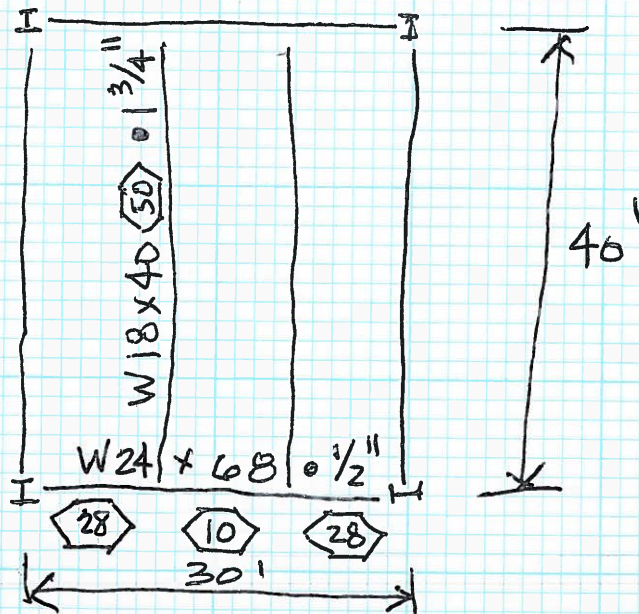
$$= 4535 \text{ in}^4 > \underline{3878 \text{ in}^4}$$

$$\Delta_{LL} = \frac{5(1.20) 30^4 \times 12^3}{384 \times 29000 \times 4535} = 0.18'' < \frac{L}{360} = \frac{30 \times 12}{360} = 1''$$

< 1" AISC



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100 psf LL on Beams

$$L = 100 \left( 0.25 + \frac{15}{\sqrt{2 \times 10 \times 40}} \right) = 78 \text{ psf.}$$

$$W_u = 1.2(860) + 1.6(78 \times 10') = 2280 \text{ \#/'}$$

$$M_u = 2.280 \times 40^2 / 8 = 456 \text{ k} < \phi M_n = 597 \text{ k} \quad \underline{\text{OK}}$$

$$V = \frac{(456 / 0.9) \times 12}{13.49''} = 451 \text{ k}$$

Try 9 flutes w/ 2 studs + 11 flutes w/ 1 stud

$$\Sigma Q_n = 9 \times 2 \times 14.6 + 11 \times 17.2 = 452 \text{ k} > V$$

29 studs per 1/2 beam