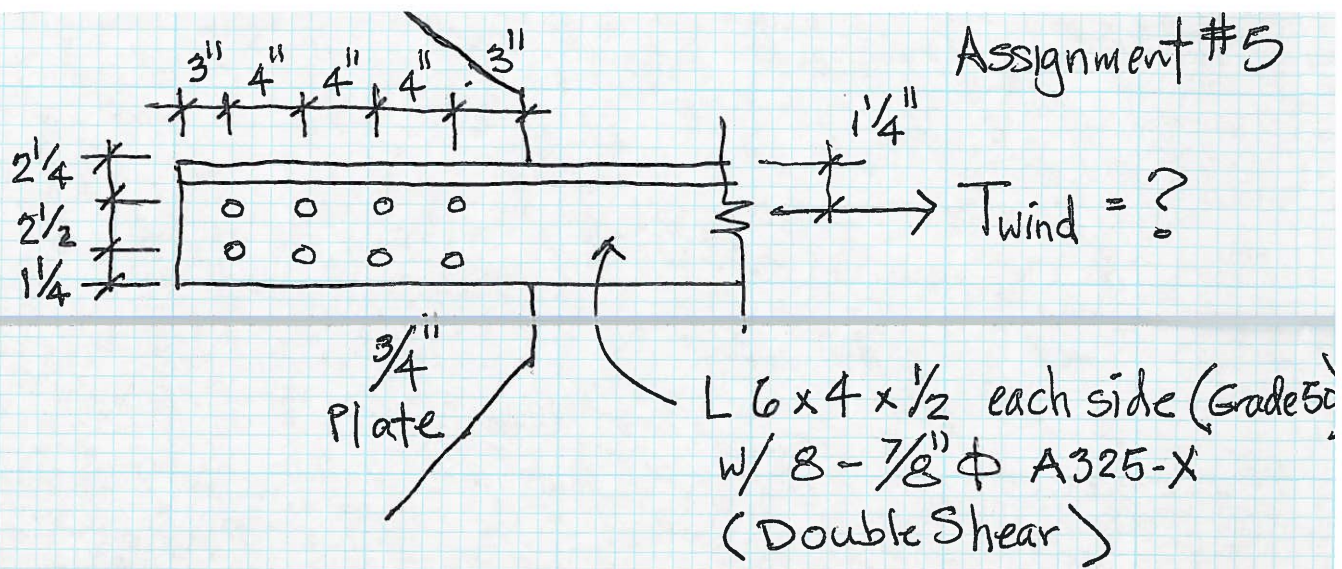
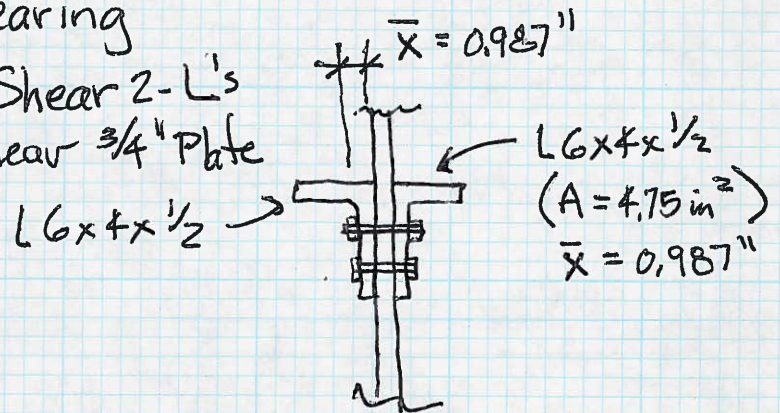


Assignment #5



A. Find T_{wind} (Note $T_u = 1.3 T_{wind}$)

- ① General Yielding of Members
- ② Fracture of Net Section
- ③ Bolt Shear
- ④ Bolt Bearing
- ⑤ Block Shear 2-L's
- ⑥ Block Shear $\frac{3}{4}"$ Plate



Grade 50 Steel
 $F_y = 50 \text{ ksi}$
 $F_u = 65 \text{ ksi}$

Assignment #5 A

A. ① $\phi_t T_n = \phi_t F_y A_g$
 $= 0.9(50)(4.75 \times 2) = \underline{427.5^k}$

② $A_n = 2(4.75 - 2(0.5'')(7/8 + 1/8)) = 7.5 \text{ in}^2$

$U = 1 - \frac{\bar{x}}{L} = 1 - \frac{0.987''}{12''} = 0.92 > \underline{0.9}$

$A_e = U A_n = 0.9 \times 7.5 = 6.75 \text{ in}^2$

$\phi_t T_n = \phi_t F_u A_e = 0.75(65)(6.75) = \underline{329.1^k}$

③ $\phi R_n = 54.1^k$ A325-X Double Shear

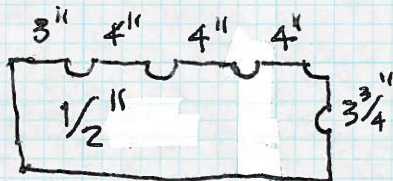
$\phi_t T_n = 54.1 \times 8 \text{ bolts} = \underline{432.8^k}$

④ Check $3/4''$ plate $3/4'' < 2 \times 0.5''$

$L_e > 2d \quad L_e = 3'' - \left(\frac{7}{8} + \frac{1}{8}\right)\frac{1}{2} = 2\frac{1}{2}'' > 2 \times 7/8''$

$\phi R_n = 0.75(2.4 \times 7/8'' \times 3/4'' \times 65 \text{ ksi})$
 $= 76.8^k/\text{bolt} > \phi R_n \text{ Bolt shear}$

⑤



$A_{gv} = 1/2 \times 15'' = 7.5$

$A_{nv} = 1/2(15 - 3\frac{1}{2} \times 1'') = 5.75$

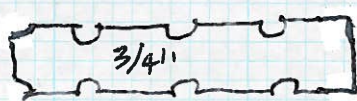
$A_{gt} = 1/2(3\frac{3}{4}) = 1.875$

$A_{nt} = 1/2(3\frac{3}{4} - 1\frac{1}{2} \times 1'') = 1.125$

$\phi R_n = \phi[0.6 F_y A_{gv} + F_u A_{nt}] = 0.75[0.6 \times 50 \times 7.5 + 65 \times 1.125] = 223.6^k$

$\phi R_n = \phi[0.6 F_u A_{nv} + F_y A_{gt}] = 0.75[0.6 \times 65 \times 5.75 + 50 \times 1.875] = 238.5^k$

$\phi T_n = 2 \times 223.6^k = \underline{447.2^k} \text{ (two L's)}$



$A_{gv} = 3/4 \times 15 \times 2 = 22.5$

$A_{nv} = 3/4(15 - 3\frac{1}{2} \times 1'') \times 2 = 17.25$

$A_{gt} = 3/4 \times 2\frac{1}{2} = 1.875$

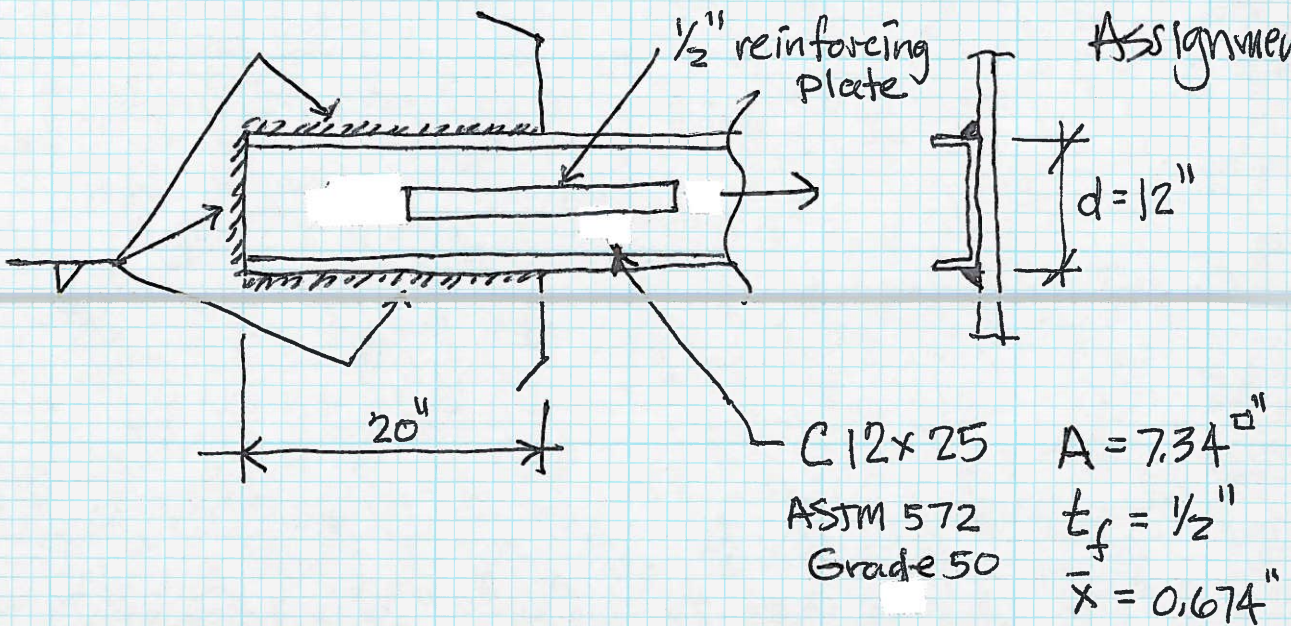
$A_{nt} = 3/4 \times (2\frac{1}{2} - 1 \times 1'') \times 2 = 1.125$

$\phi R_n = 0.75[0.6 \times 50 \times 22.5 + 65 \times 1.125] = 561.1^k$

$\phi R_n = 0.75[0.6 \times 65 \times 17.25 + 50 \times 1.875] = 574.3^k$

$\phi T_n = 561.1^k$

② Controls $\phi T_n = 329.1$
 $\phi T_n = 329.1/1.3 = 253.1$



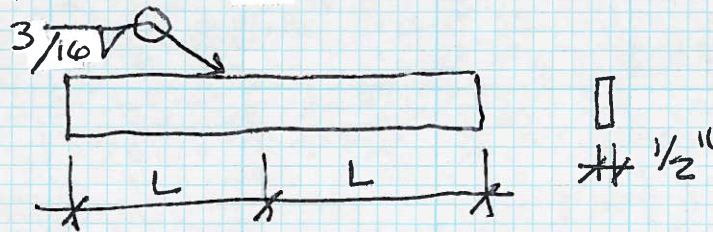
B. Design Connection for Expected Yield Strength of the Channel

① $P_n = R_y F_y A_g$

② Weld (Fillet) size w

③ Width of $\frac{1}{2}"$ reinforcing plate

④ Length of reinforcing plate L
 (Assume $\frac{3}{16}"$ Fillet weld on two sides)



Assignment 5B

$$\textcircled{1} P_u = R_g F_y A_g = 1.1 \times 50 \times 7.34 = \underline{\underline{404^k}}$$

$$\textcircled{2} \text{ Available weld length } L = 20'' + 12'' + 20'' = 52''$$

$$w = \frac{P_u}{0.707 \times L \times \phi F_w} = \frac{404}{0.707 \times 52'' \times 31.5} = 0.35''$$

$$\text{Max } w = \frac{1}{2}'' - \frac{1}{16}'' = \frac{7}{16}'' \quad \text{use } \underline{\underline{\frac{3}{8}''}}$$

$$\textcircled{3} U = 1 - \frac{\bar{x}}{L} = 1 - \frac{0.674}{20} = 0.97 \quad \text{use } \underline{\underline{0.9}}$$

check Rupture

$$\phi P_n = 0.75 (65 \text{ ksi}) (7.34 \times 0.9) = 322^k$$

Reinforce channel

$$(A_n + A_{rn}) U > A_g$$

$$A_{rn} = \frac{A_g - U A_n}{U} = \frac{7.34 - 0.9 \times 7.34}{0.9} = 0.82''$$

$$\boxed{\times} \quad x = \frac{0.82}{0.5} = 1.63'' \sim \underline{\underline{1\frac{3}{4}''}}$$

~~1\frac{1}{2}''~~

$$\textcircled{4} P_u = 1.1 \times 50 \times \left(\frac{1}{2} \times 1\frac{3}{4}\right) = 48.2^k$$

$$D=3 \quad \phi R_n = 4.18^k$$

$$L_{\text{total}} = \frac{48.2}{4.18} = 11.5'' = 1\frac{1}{2}'' + 5'' + 5'' \quad \leftarrow \text{end}$$

$$L_{\text{min}} = \underline{\underline{5''}}$$