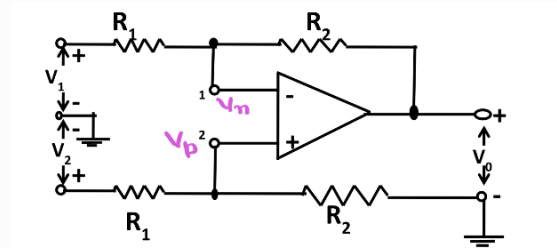


2. The differential input operational amplifier shown consists of a base amplifier of infinite gain. Find the expression of output voltage.



$$V_p = \frac{V_2}{R_1 + R_2} R_2 = V_n$$

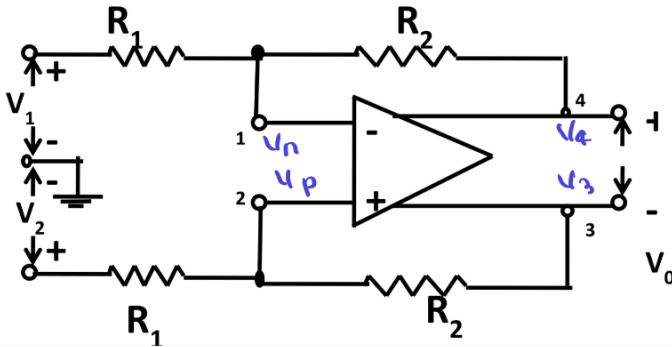
$$\frac{V_1 - V_n}{R_1} = \frac{V_n - V_0}{R_2}$$

$$\frac{V_0}{R_2} = V_n \left( \frac{1}{R_1} + \frac{1}{R_2} \right) - \frac{V_1}{R_1}$$

$$V_0 = -\frac{R_2}{R_1} V_1 + \frac{V_2}{R_1 + R_2} R_2 \frac{R_1 + R_2}{R_1}$$

$$V_0 = \frac{R_2}{R_1} (V_2 - V_1)$$

3. Repeat the above problem for the amplifier shown.



$$V_p = V_2 - \frac{V_2 - V_3}{R_1 + R_2} R_1$$

$$V_p = V_n$$

$$\frac{V_1 - V_n}{R_1} = \frac{V_n - V_4}{R_2}$$

$$\Rightarrow \frac{V_4}{R_2} = \frac{V_n}{R_2} + \frac{V_n}{R_1} - \frac{V_1}{R_1}$$

$$\Rightarrow V_4 = (R_1 + R_2) \frac{V_n}{R_1} - \frac{R_2}{R_1} V_1$$

$$V_4 = \frac{R_1 + R_2}{R_1} \left( V_2 - \frac{V_2 - V_3}{R_1 + R_2} R_1 \right) - \frac{R_2}{R_1} V_1$$

$$\Rightarrow V_4 = \left( \frac{R_1 + R_2}{R_1} \right) V_2 - (V_2 - V_3) - \frac{R_2}{R_1} V_1$$

$$\Rightarrow V_4 - V_3 = \left( 1 + \frac{R_2}{R_1} \right) V_2 - V_2 - \frac{R_2}{R_1} V_1$$

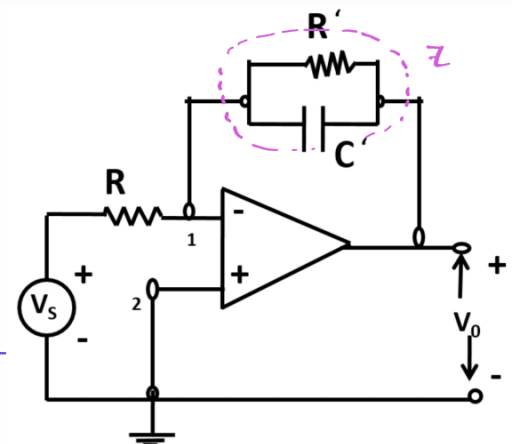
$$\Rightarrow V_0 = \frac{R_2}{R_1} (V_2 - V_1)$$

4. The circuit shown represents a low-pass de-coupled amplifier. Assuming an ideal operational amplifier determine the low-frequency gain  $A_v = V_0/V_s$ .

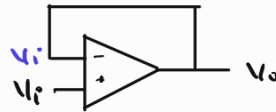
$$Z = \frac{R' \cdot \frac{1}{j\omega C}}{R' + \frac{1}{j\omega C}} = \frac{R'}{1 + j\omega C R'}$$

$$\frac{V_s}{R} = -\frac{V_0}{Z} \Rightarrow \frac{V_0}{V_s} = -\frac{Z}{R} = \frac{R'}{1 + j\omega C R'}$$

$$|A_v| = \left| \frac{V_0}{V_s} \right| = \frac{R'}{R} \cdot \frac{1}{1 + (\omega C R')^2}$$

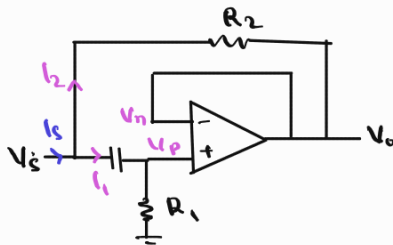


5) a) Show that if the inverting terminal of an OPAMP is shorted to output, then it acts as unit gain buffer (unit gain amplifier with high input impedance)

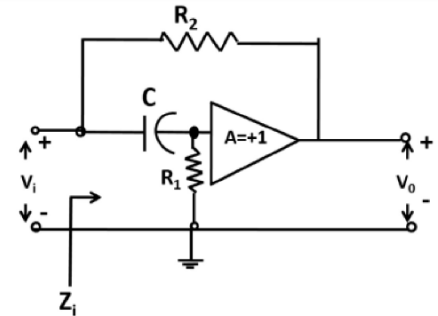


$$V_o = V_i \quad \Rightarrow \quad A_v = \frac{V_o}{V_i} = 1$$

b) show that the circuit of the accompanying figure can simulate a grounded inductor if  $R_1 > R_2$ . In other words, show that the reactive part of the input impedance of the circuit is positive if  $R_1 > R_2$ . In the circuit the OPAMP is a unit gain buffer.



$$(R_1 > R_2)$$



$$Z = \frac{V_s}{I_s}$$

$$I_s = I_1 + I_2 = \frac{V_s}{R_1 + \frac{1}{j\omega C}} + \frac{V_s - V_o}{R_2}$$

$$V_o = \frac{V_s(j\omega C) R_1}{1 + j\omega C R_1}$$

$$I_s = \frac{V_s(j\omega C)}{1 + R_1(j\omega C)} + \frac{V_s - \frac{V_s(j\omega C) R_1}{1 + j\omega C R_1}}{R_2}$$

$$= \frac{V_s(j\omega C)}{1 + R_1(j\omega C)} + \frac{V_s(1 + j\omega C R_1 - j\omega C R_1)}{(1 + j\omega C R_1) R_2}$$

$$= \frac{V_s(j\omega C) R_2 + V_s}{(1 + R_1(j\omega C)) R_2}$$

$$Z = \frac{V_s}{I_s} = \frac{R_2(1 + j\omega C R_1)}{1 + j\omega C R_2} \times \frac{1 - j\omega C R_2}{1 - j\omega C R_2}$$

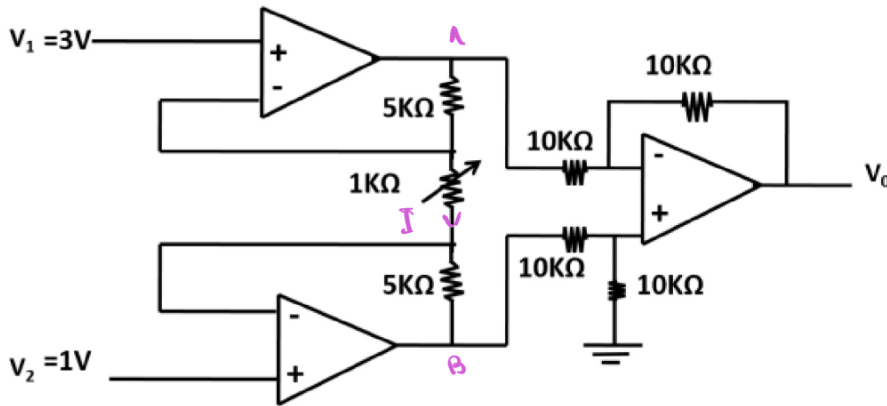
$$= \frac{R_2}{1 + (\omega C R_2)^2} \cdot \frac{1 + (\omega C)^2 R_1 R_2 + j\omega C(R_2 + R_1)}{1 - j\omega C R_2}$$

Analysing complex part

$$\text{Im}(Z) = \frac{R_2 \omega C (R_1 - R_2)}{1 + (\omega C R_2)^2}$$

$$R_1 > R_2 \quad \text{Im}(Z) > 0 \quad \Rightarrow \quad \text{inductor behaviour}$$

6) Calculate  $V_0$  in the circuit.



$$I = 2 \text{ mA}$$

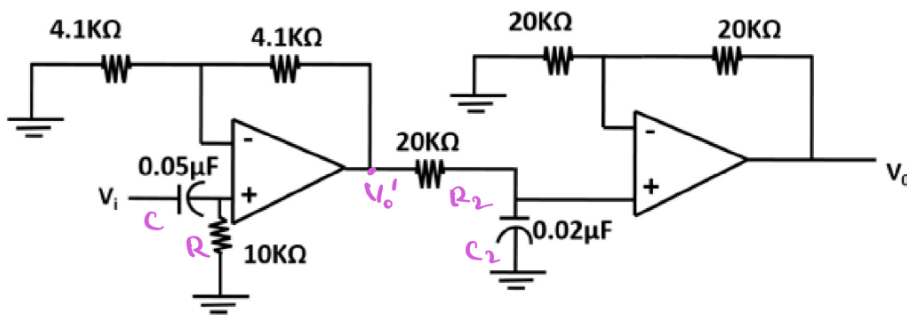
$$V_A = 13 \text{ V}$$

$$V_B = -9 \text{ V}$$

$$V_0 = V_B - V_A$$

$$= -22 \text{ V}$$

7) Calculate the lower and upper cutoff frequency in the band pass filter circuit.



$$V_p = \frac{V_i}{R_1 + \frac{1}{j\omega C}} R$$

$$-\frac{V_p}{R_1} = \frac{-V_0' + V_p}{R_1}$$

$$V_0' = 2V_p$$

$$V_p' = \frac{2V_p}{R_2 + \frac{1}{j\omega C_2}} \cdot \frac{1}{j\omega C_2}$$

$$= \frac{2V_p}{1 + j\omega R_2 C_2}$$

$$-\frac{V_p'}{R_3} = \frac{V_p' - V_0}{R_3}$$

$$\Rightarrow V_0 = 2V_p'$$

$$V_0 = \frac{4V_p}{1 + j\omega R_2 C_2}$$

$$V_0 = \frac{4}{1 + j\omega R_2 C_2} \cdot \frac{V_i(j\omega C)}{1 + R(j\omega C)} R$$

$$f_H = \frac{10^6}{2\pi(0.02)(20) \times 10^3}$$

$$f_L = \frac{10^6}{2\pi(0.05) 10 \times 10^3}$$