TM-modes of a planar waveguide are described by the field components Hy, Ex and Ez. These are related as the following:

$$E_{\chi} = \frac{\beta}{\omega \epsilon_{o} n^{2}} Hy$$

$$E_{\chi} = \frac{1}{i \omega \epsilon_{o} n^{2}} \frac{\partial Hy}{\partial x}$$
and  $i\beta E_{\chi} + \frac{\partial E_{\chi}}{\partial x} = i \omega \mu_{o} Hy$ 

Eliminating Ex and Ez from the above equs, we get  $n'(n) \frac{d}{dx} \left( \frac{1}{n'(n)} \frac{d+y}{dx} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n) - \beta^2}{r^2 N(n)} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n) - \beta^2}{r^2 N(n)} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n) - \beta^2}{r^2 N(n)} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n) - \beta^2}{r^2 N(n)} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n) - \beta^2}{r^2 N(n)} \right) + \left( \frac{r^2 N(n) - \beta^2}{r^2 N(n)} + \frac{r^2 N(n)}{r^2 N(n)} + \frac{r^2 N$ 

$$\frac{d^2Hy}{dx^2} - \left[\frac{1}{n^2(x)}\frac{dn^2}{dx}\right]\frac{dHy}{dx} + \left[\frac{2}{k_0}\frac{n^2(x)}{n^2(x)} - \beta^2\right]Hy = 0$$

This equation is different from the TE-modes' equation we discussed lartis (the Ey equation). However for a step-violex waveguide, the R.I. is constant in each region; therefore x-dependence of  $n^2 \left[\frac{d}{dx^2}\right]$  does not exist. So, we may write the Hy-equation for the TM-modes as

$$\frac{d^{2}H_{y}}{dn^{2}} + (R_{0}^{2}m_{1}^{2} - \beta^{2})H_{y} = 0 \qquad |x| < \frac{d_{2}}{2}$$

$$\frac{d^{2}H_{y}}{dn^{2}} - (\beta^{2} - R_{0}^{2}m_{2}^{2})H_{y} = 0 \qquad |x| > \frac{d_{2}}{2}$$

In this case, the boundary conditions require that tangential field components, ie, they and Ez to be continuous

across the interfaces ie, at  $n=\pm\frac{d}{2}$ But for TM-mode,  $E_3 = \frac{1}{2} \omega E_0 n_{(n)} \sqrt{3} \pi$ Hence the required conditions are Hy and  $\frac{1}{n^2}\frac{\partial Hy}{\partial n}$  be continuous at  $z=\pm\frac{d}{2}$ . The above equations yield the solutions for the symmetric  $H_{y}(x) = A c_{0} \times x |x| < \frac{d_{2}}{2} : core$   $B e^{-\gamma |x|} |y| > \frac{d_{2}}{2} : cladding$ The boundary conditions give

A cos (2d/2) = B e - rd/2 and  $\frac{1}{n_2}\left[-A \times Sin(2d_2)\right] = \frac{1}{m_2}\left(-B \times e^{-2d_2}\right)$ above two egns constitute the eigenvalue Dividing, the equation as  $\chi \tan(\chi d_2) = \chi \frac{m_1}{m_2^2}$ This can be written as  $2 \tan x = y$  where x = x dy where y = x dy y = x dyConsidéring the antisymmetric mode soluting Hyla) = C Sin x2 /x/2 dy: core = De-8/21 (21) dy : classings We avrive at the eigenvalue equation, on applying the boundary conditions, as  $tan(xd_2) = -\frac{x}{y} \cdot \frac{n_2^2}{n_1^2}$ In the same way on the TE-case, this can be withen  $x \cot x = -y$ 

The V-number can be defined in the same way as befre  $N = k_0 \cdot \frac{1}{2} \cdot \sqrt{n_1^2 - n_2^2} \quad \text{with} \quad x^2 + \frac{y^2}{(n_1^2)^2} = V^2.$ 

The solutions of the eigenvalue equations can be discussed in the same way as the TE-case, except the difference that the RHs of the equations now describe an ellipse whose semi major aris b  $\frac{n_1^2}{n_2^2}$  and semi-minor axis is V.

All the quantities related to the TM-modes, namely, the cut-off frequency, no. of zeros etc. are similar to the ones discussed in TE-mode.

A waveguide harnig v liging between  $0-17_2$ , is referred to as a single mode. But actually for this case there will be two modes me TE- and the other TM which are having slightly different B-values: BTE, BTM. However, if the incident field is planized to excite only TF or only Try -mode, the no. of modes nie be due to the respective conditions.

Mote:  $X_2^d = x$   $\left(\frac{\gamma_2^d}{2}\right)\frac{h_1}{h_2} = y$ ie,  $\frac{7d}{2} = \frac{1}{2}$  $V^2 = (\chi \frac{1}{2})^2 + (\frac{\pi d}{2})^2 = \chi^2 + y^2 (\frac{m^2}{m_1^2})^2$  $\frac{n^2}{\sqrt{2}} + \frac{n^2}{\sqrt{2}(n^2)^2} = 1$  8emi-major 8emi-major 19