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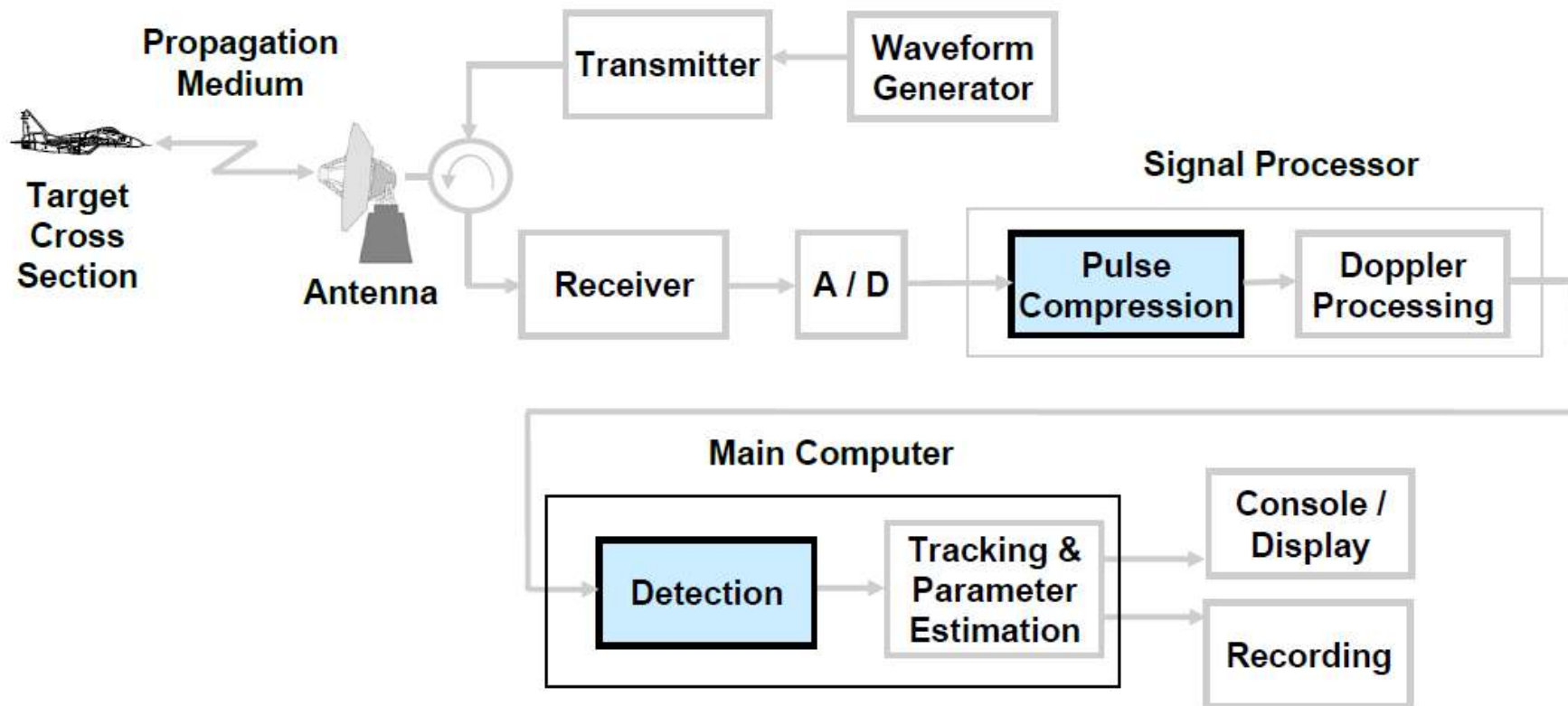
Radar Systems

Lecture 5.


Detection of Targets in Noise and Pulse Compression Techniques

구 자 열

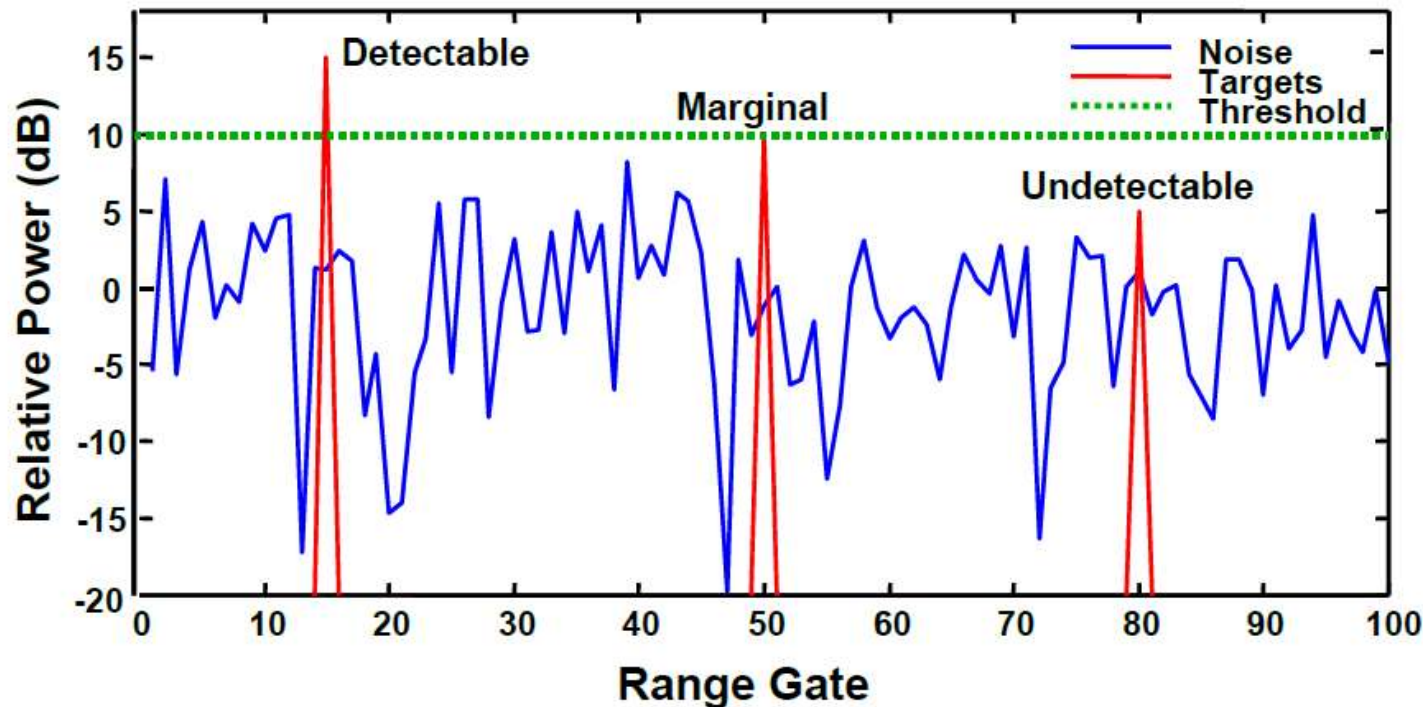
Detection and Pulse Compression



차 례

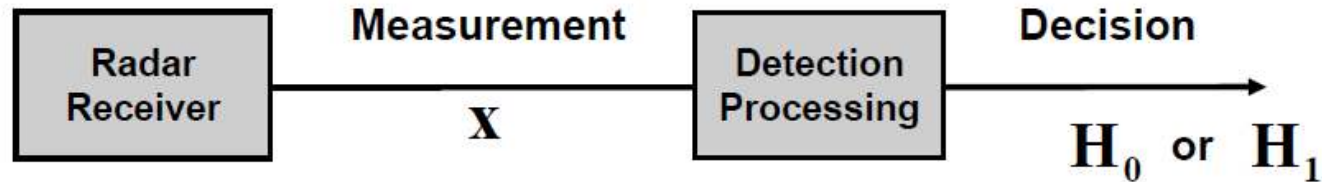
- **Detection of Target Echoes in Noise** 
 - Basic Concepts
 - Integration of Pulses
 - Fluctuating Targets Issues
 - Adaptive Thresholding Techniques
- **Pulse Compression**

Target Detection in the Presence of Noise



- The radar return is sampled at regular intervals with A/D (Analog to Digital) converters
- The sampled returns may include the target of interest and noise
- A threshold is used to reject noise

The Radar Detection Problem



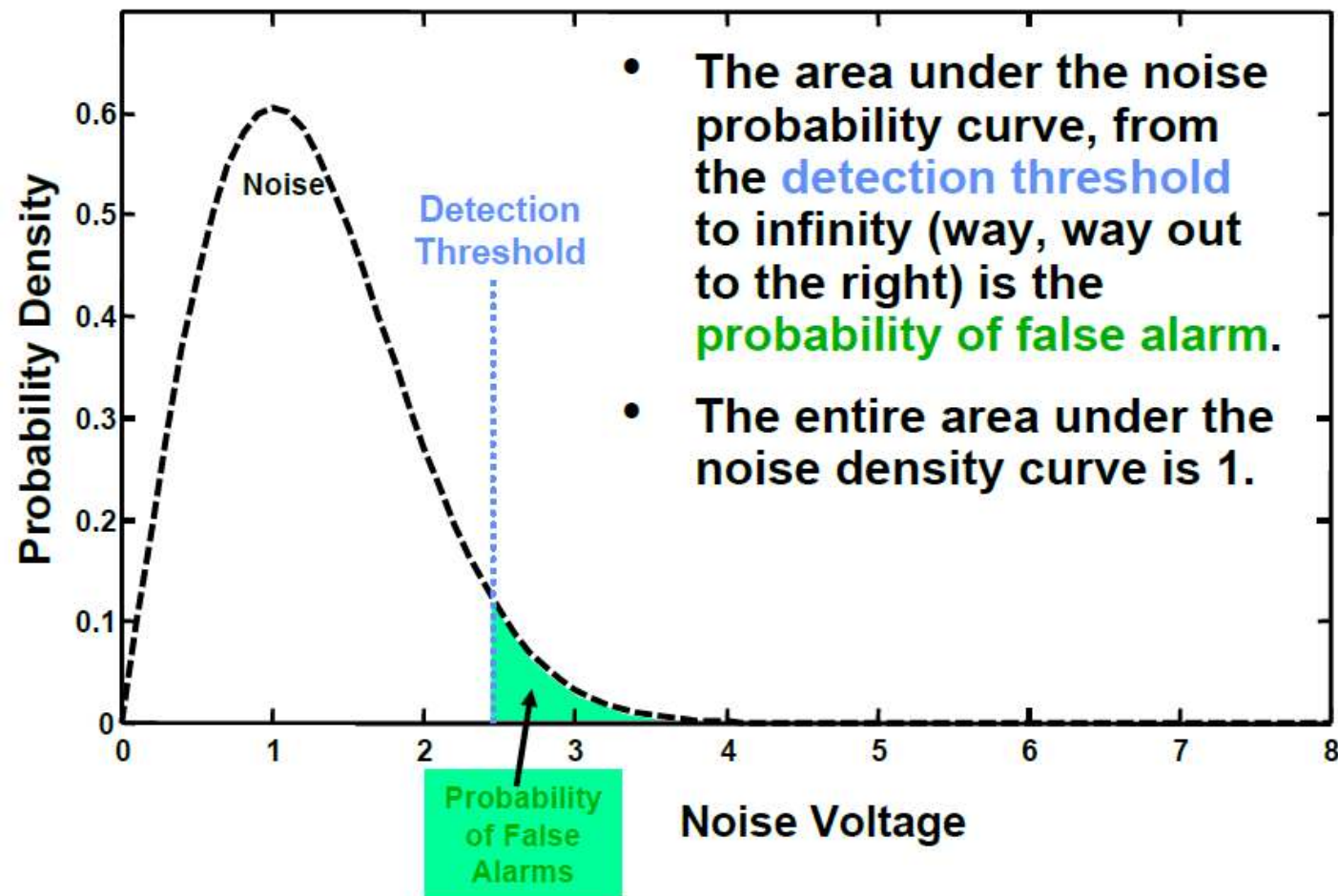
For each measurement
There are two possibilities:

	Measurement	Probability Density
Target absent hypothesis, H_0 Noise only	$\mathbf{x} = \mathbf{n}$	$p(\mathbf{x} H_0)$
Target present hypothesis, H_1 Signal plus noise	$\mathbf{x} = \mathbf{a} + \mathbf{n}$	$p(\mathbf{x} H_1)$

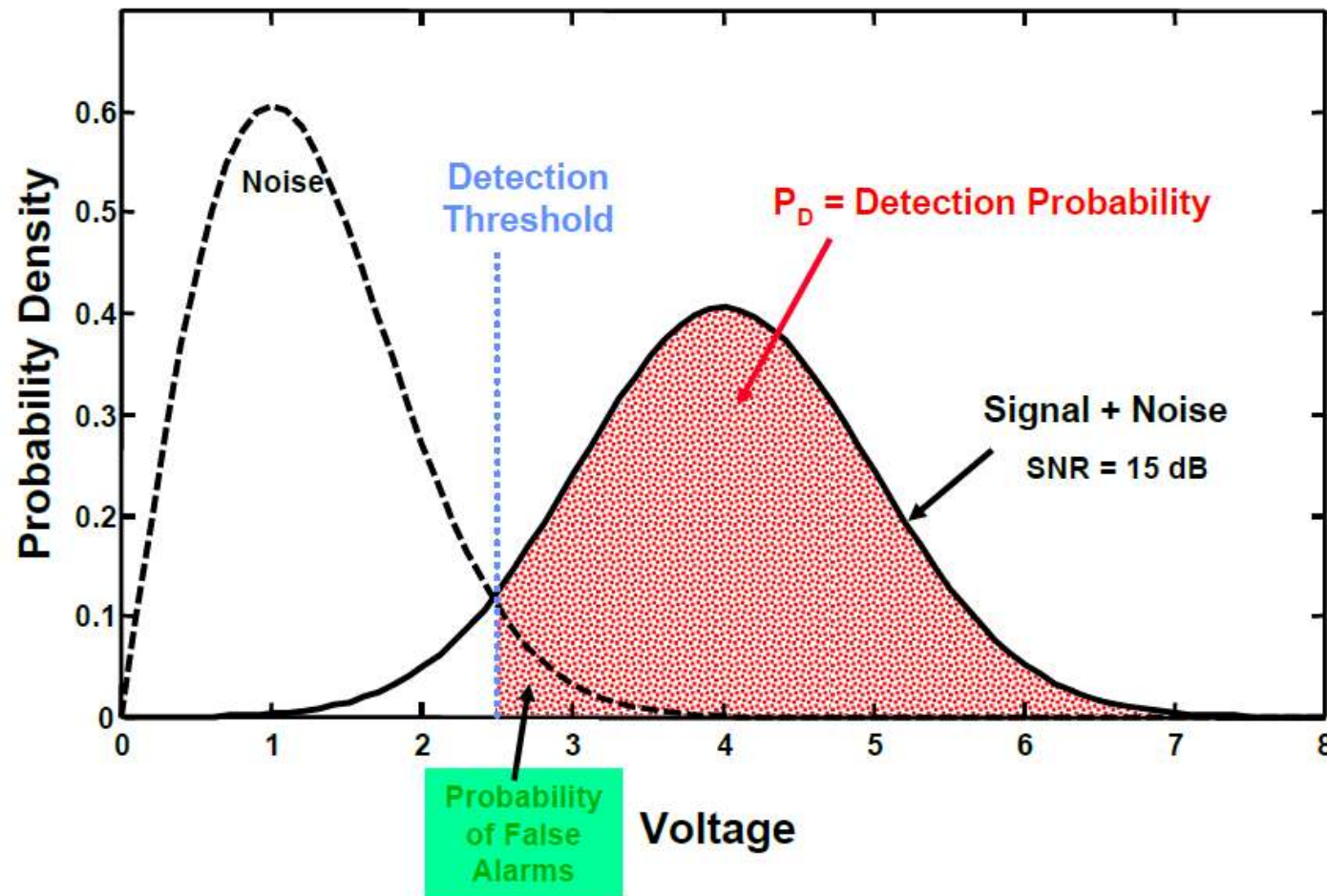
For each measurement
There are four decisions:

		Decision	
		H_0	H_1
Truth	H_0	Don't Report	False Alarm
	H_1	Missed Detection	Detection

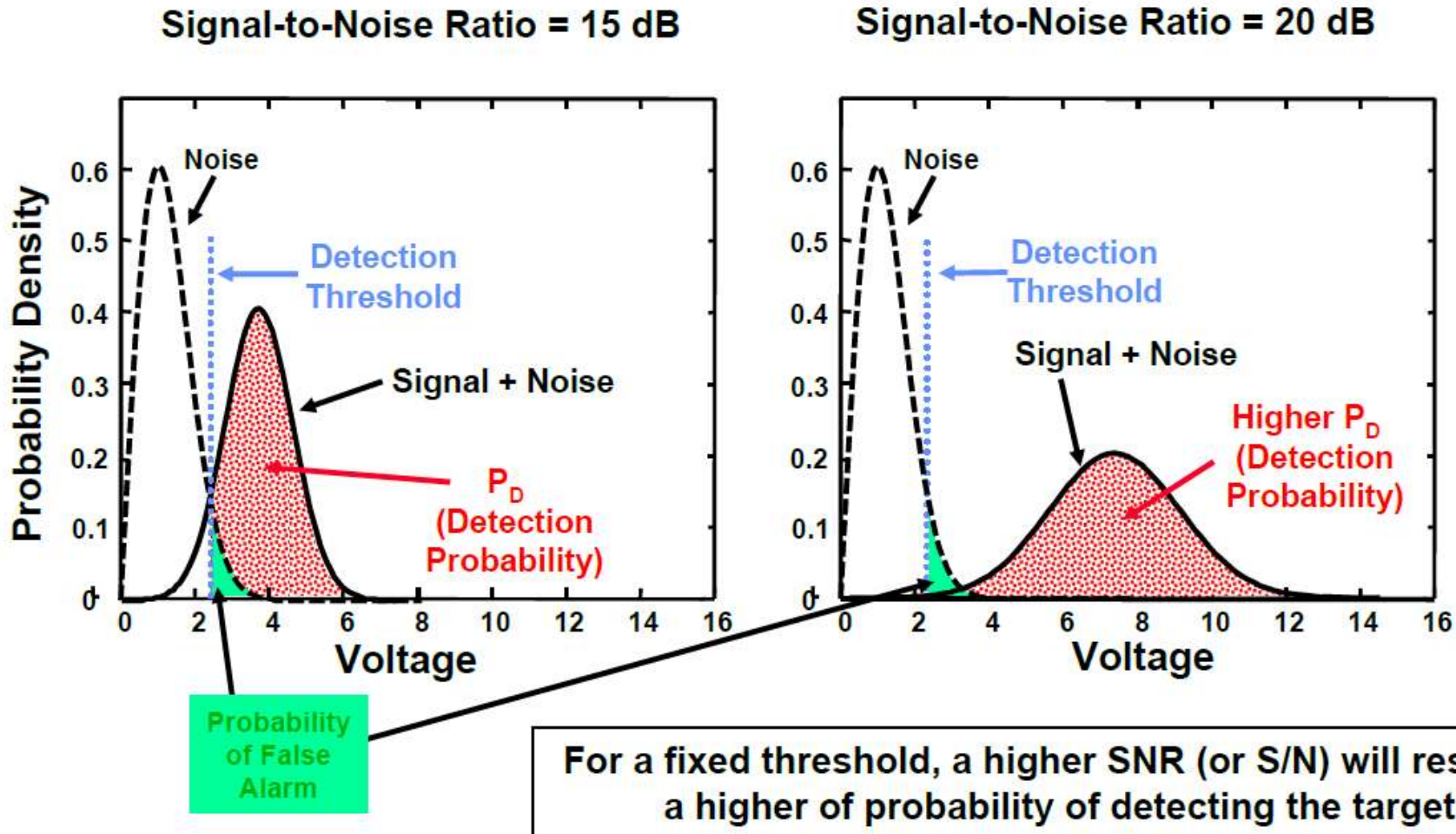
The Detection Problem



The Detection Problem



Detection Examples with Different SNR



Probability of Detection vs. SNR

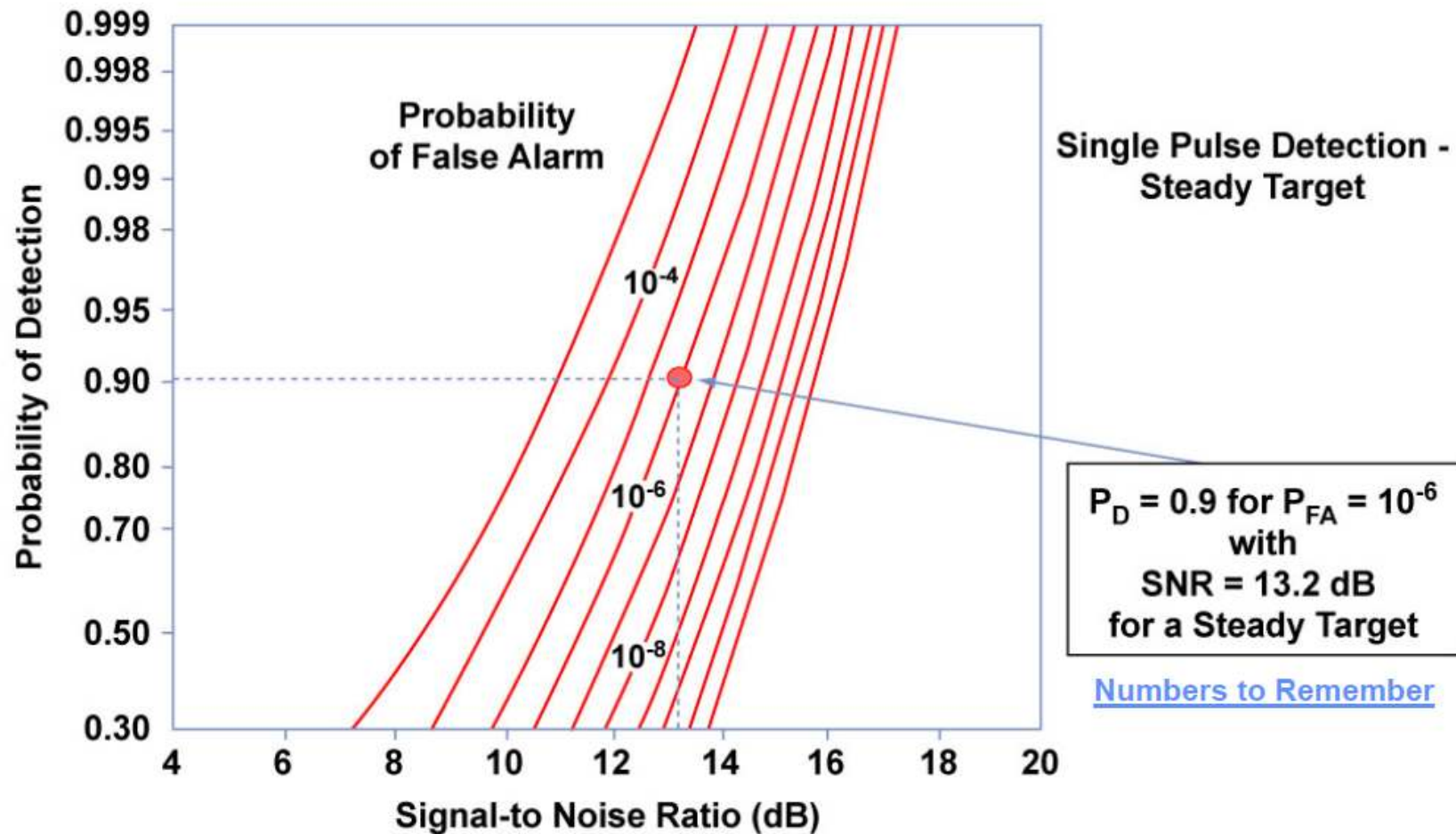


Figure by MIT OCW.



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차 례

- **Detection of Target Echoes in Noise**
 - Basic Concepts
 - Integration of Pulses ←
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 - Adaptive Thresholding Techniques
- **Pulse Compression**

Integration of Pulse

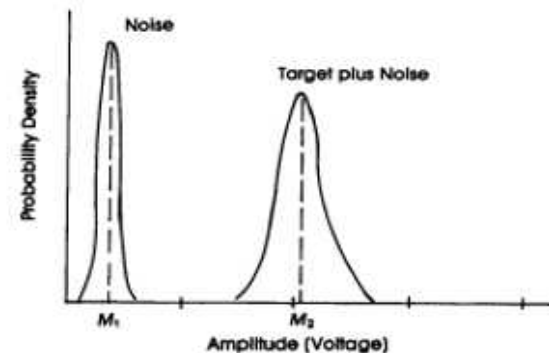
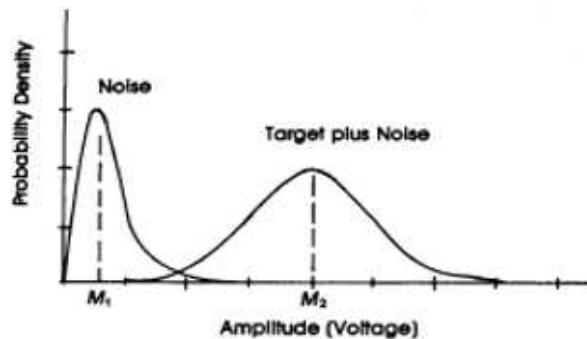
- The process of summing all the radar pulses to improve detection is known as “Pulse integration”
- A search-radar beam scans, the target will remain in the beam sufficiently long for more than one pulse to hit it. This number is known as hits per scan.

$$n_b = \frac{\theta_b f_p}{\dot{\theta}_s} = \frac{\theta_b f_p}{6\omega_m},$$

- For a ground based search radar with antenna scan rate 5 rpm, beam width 1.5° and PRF 300Hz, the number of hits would be 15/scan.

Integration of Pulse

- A pulse integrator is a improvement technique to address gains in probability of detection by using multiple transmit pulses.



- Depending on location of the pulse integrator in the signal processing chain this process is referred to as
 - coherent integration.
 - non-coherent integration.

Integration of Pulse

- Coherent Integration:
 - Insertion of a Pulse integrator between the matched filter and amplitude detector.
 - The signal processor samples the return from each transmit pulse at a spacing equal to the range resolution of the radar set and adds the returns from N pulses. After it accumulates the N pulses, performs the amplitude detection and threshold check.
- Non-Coherent Integration :
 - Integrator is placed after the amplitude or square law detector.
 - The name non-coherent integration derives from the fact that, since the signal has undergone amplitude or square law detection, the phase information is lost.
 - The non-coherent integrator operates in the same fashion as the coherent integrator in that it sums the returns from N pulses before performing the threshold check.

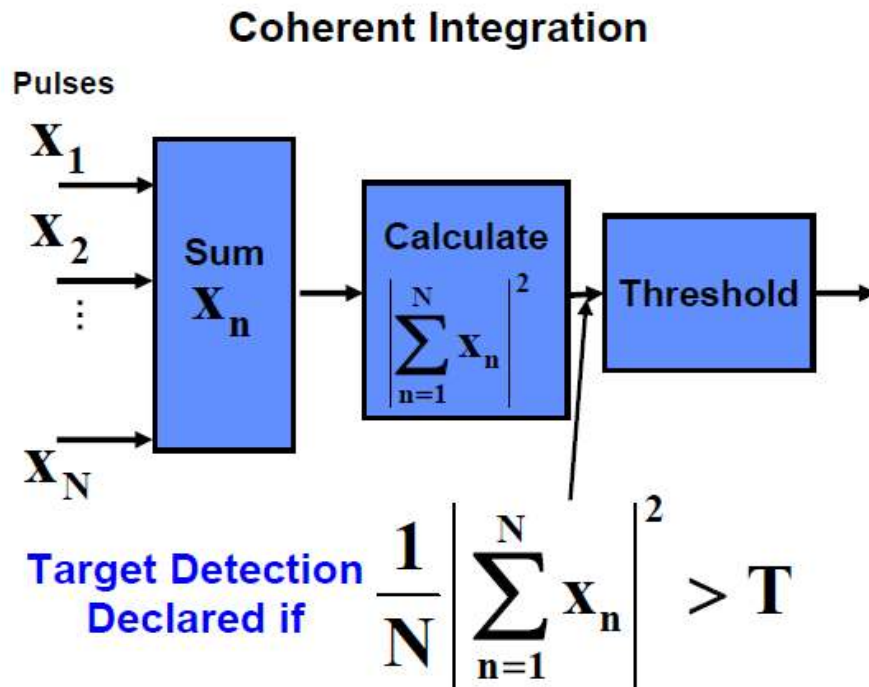
Integration of Pulse

Coherent Integration	Non-Coherent Integration
<u>Predetection</u> Integration	<u>Postdetection</u> Integration
Phase information of the echo signal is preserved	Detector destroys phase information. Less efficient than <u>predetection</u> .
If n pulse are integrated, the SNR of integrated signal is <u>nSNR</u> .	If n pulse are integrated, the SNR of integrated signal is lesser than <u>nSNR</u> .
Difficult to implement	Easy to implement

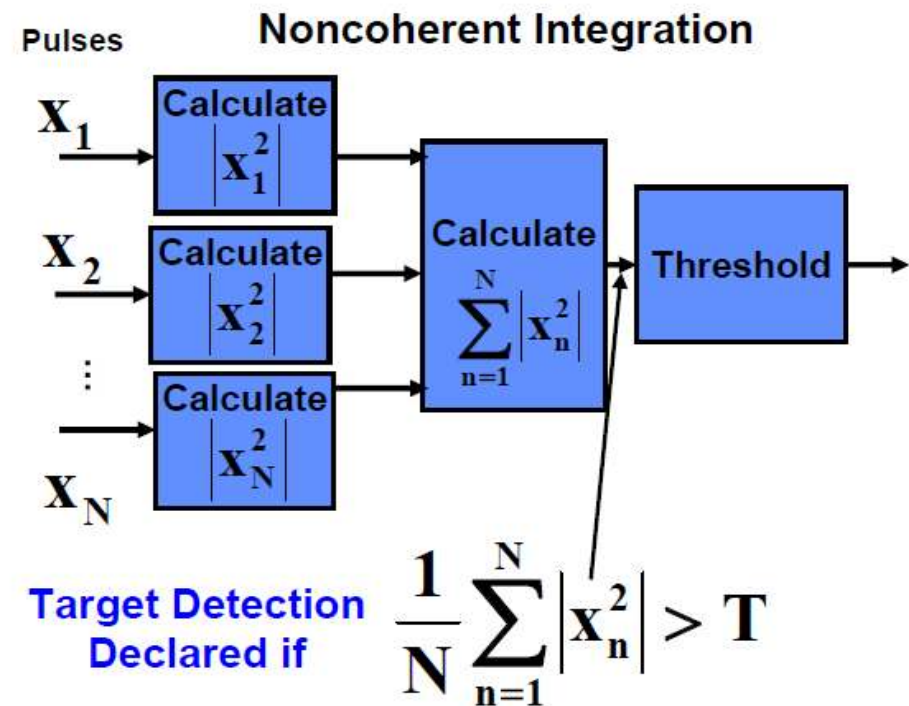
Integration of Radar Pulses

- Improve ability of radar to detect targets by combining the returns from multiple pulses
- Coherent Integration
 - No information lost (amplitude or phase)
- Non-coherent integration techniques
 - Some information lost (phase)
 - Non-coherent (video) Integration
 - Binary Integration
 - Cumulative detection
 - For most cases, coherent integration is more efficient than non-coherent integration

Integration of Radar Pulses



- Adds 'voltages', then square
- Phase is preserved
- pulse-to-pulse phase coherence required
- SNR Improvement = $10 \log_{10} N$



- Adds 'powers' not voltages
- Phase neither preserved nor required
- Easier to implement, not as efficient

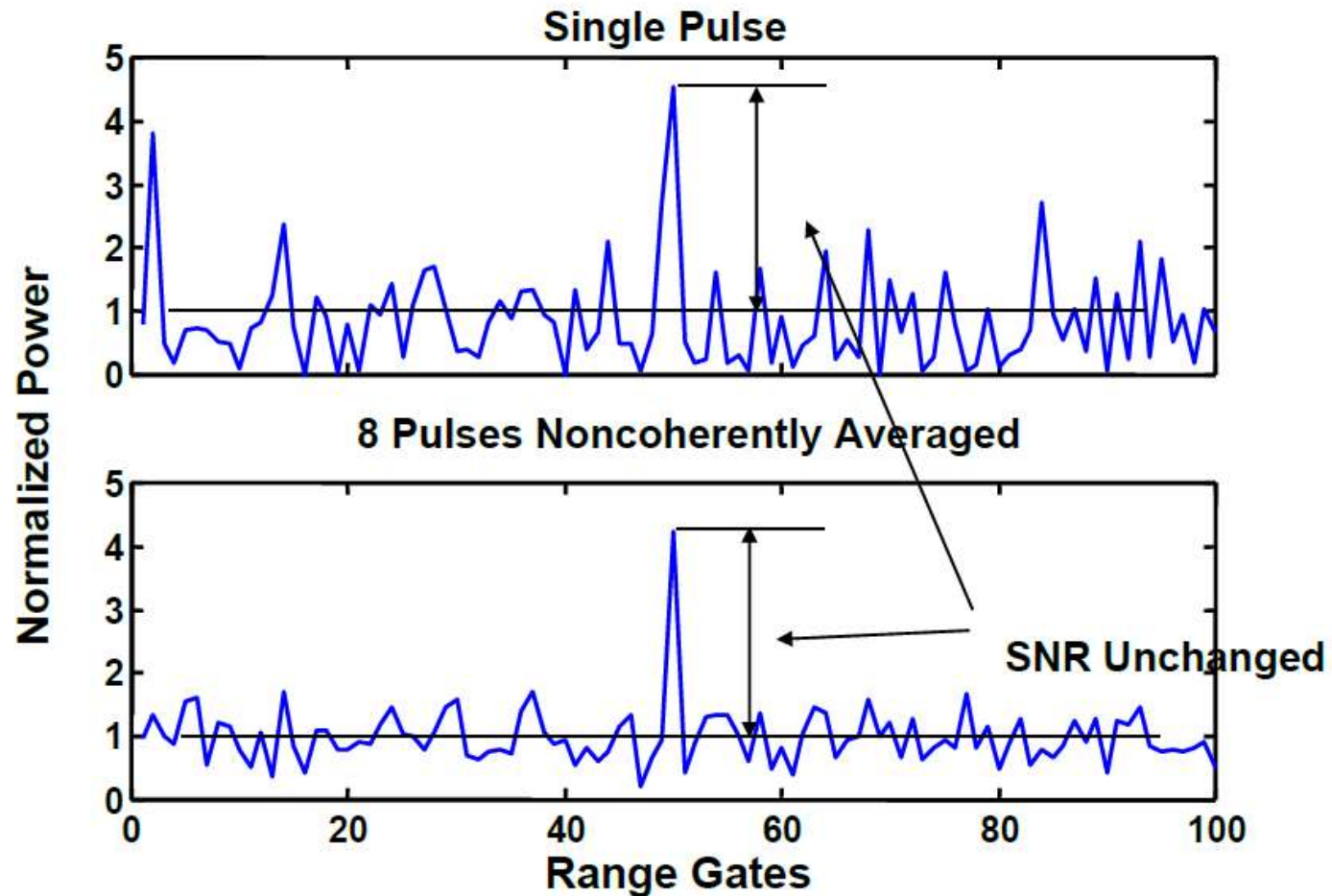
Detection performance can be improved by integrating multiple pulses

Coherent Integration

- Real and Imaginary (In-phase and Quadrature) parts of the complex radar return are added, and the magnitude of the voltage is calculated
 - $V = (I^2 + Q^2)^{1/2}$
- This quantity is then thresholded
- The coherent integration gain is equal to the number of pulses coherently integrated
 - 2 pulses 3 dB
 - 10 pulses 10 dB
 - 20 pulses 13 dB
- For this gain to be realized, the noise samples, from pulse to pulse must be independent
 - The background noise is white Gaussian noise

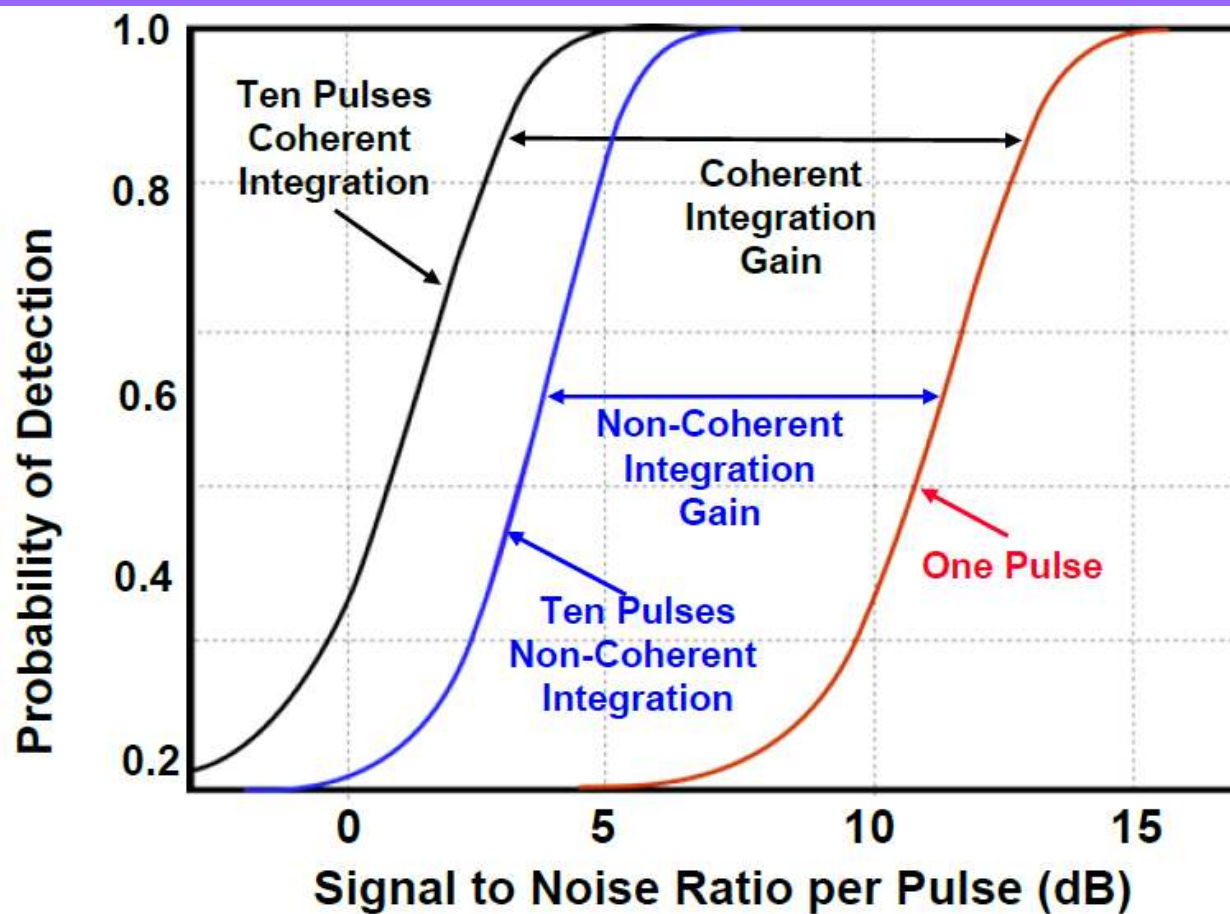
Noncoherent Integration

Steady Target



Noise Variance Reduced after Integration (Allows Lower Threshold)

Integration of Pulses



Steady
Target

$$P_{FA} = 10^{-6}$$

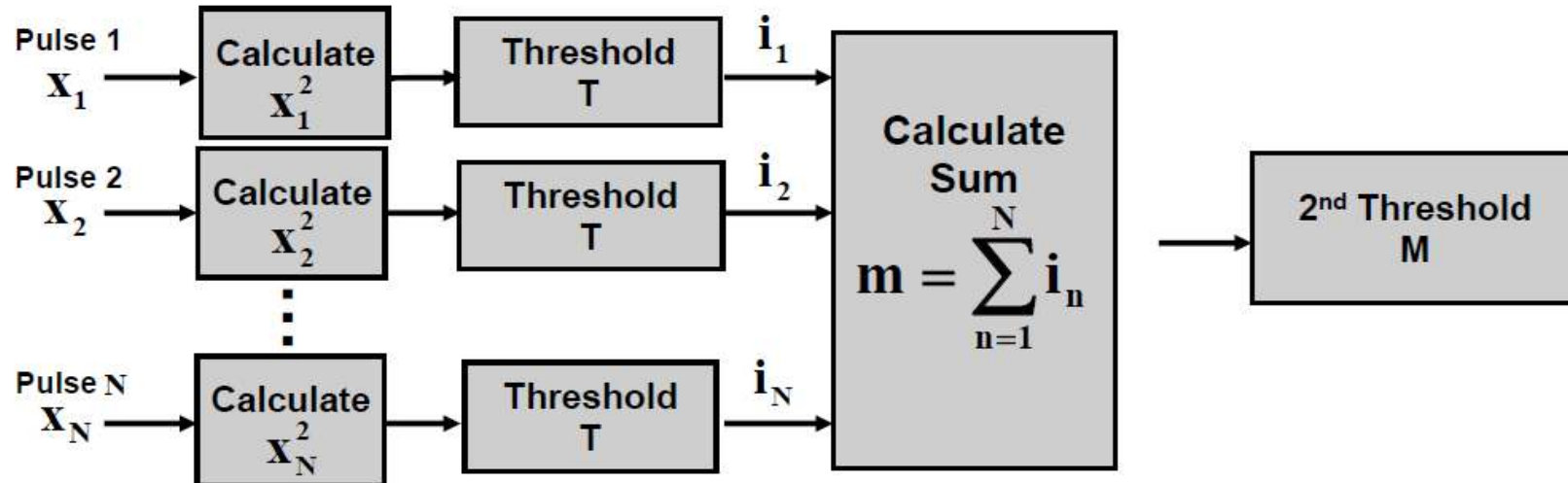
For Most Cases, Coherent Integration is More Efficient than Non-Coherent Integration



Different Types of Non-Coherent Integration

- **Non Coherent Integration – General (aka video integration)**
 - Generate magnitude for each of N pulses
 - Add magnitudes and then threshold
- **Binary Integration**
 - Generate magnitude for each of N pulses and then threshold
 - Require at least M detections in N scans
- **Cumulative Detection**
 - Generate magnitude for each of N pulses and then threshold
 - Require at least 1 detection in N scans

Binary (M -of- N) Integration



Individual pulse detectors:

$$\begin{aligned} |X_n|^2 &\geq T, & i_n &= 1 \\ |X_n|^2 &< T, & i_n &= 0 \end{aligned}$$

2nd thresholding:

$$\begin{aligned} m &\geq M, & \text{target present} \\ m &< M, & \text{target absent} \end{aligned}$$

Target present if at least M detections in N pulses

Binary Integration

At Least
 M of N
Detections

$$P_{M/N} = \sum_{k=M}^N \frac{N!}{k!(N-k)!} p^k (1-p)^{N-k}$$

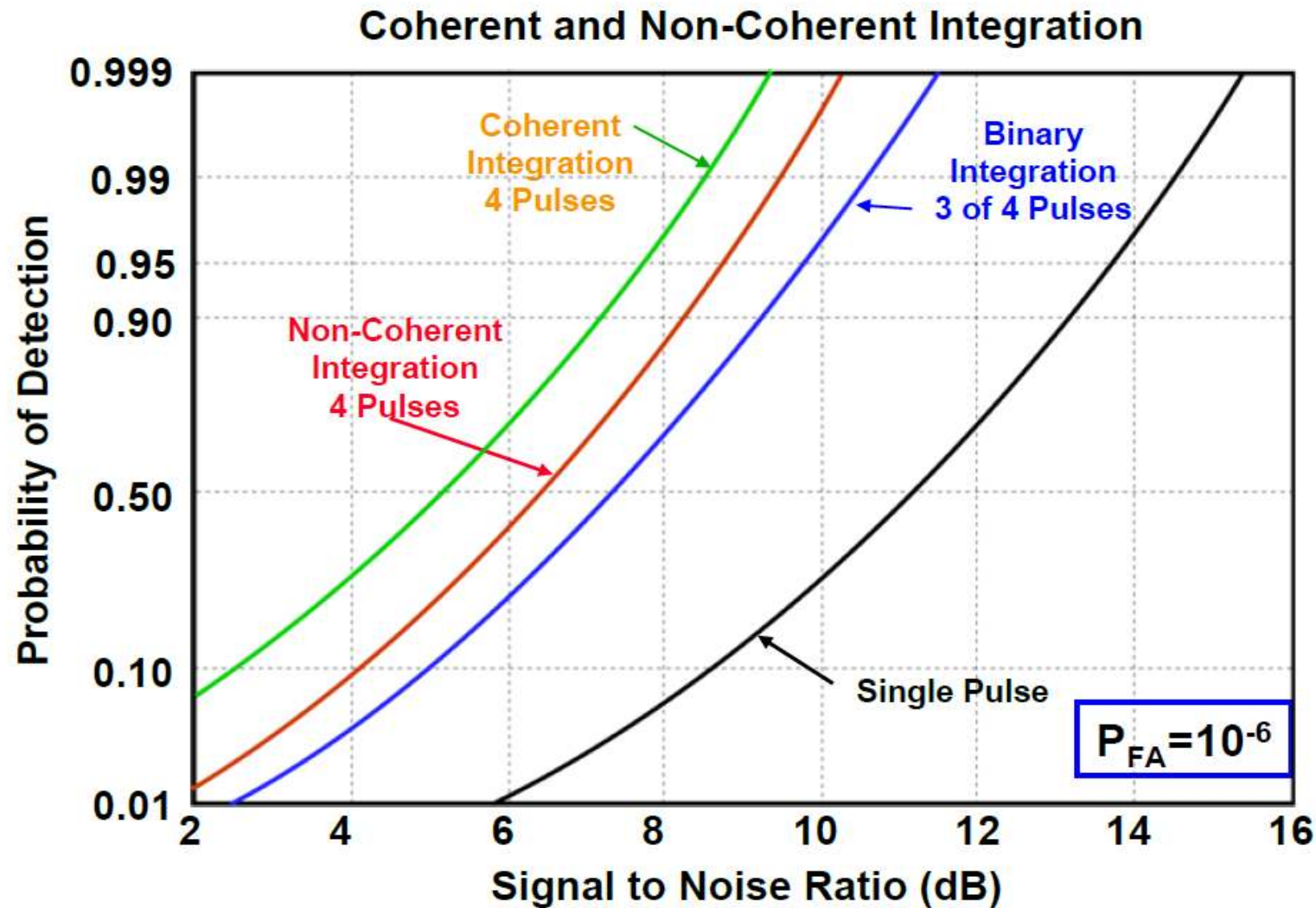
Cumulative Detection

At Least
1 of N

$$P_C = 1 - (1-p)^N$$



Detection Statistics for Different Types of Integration

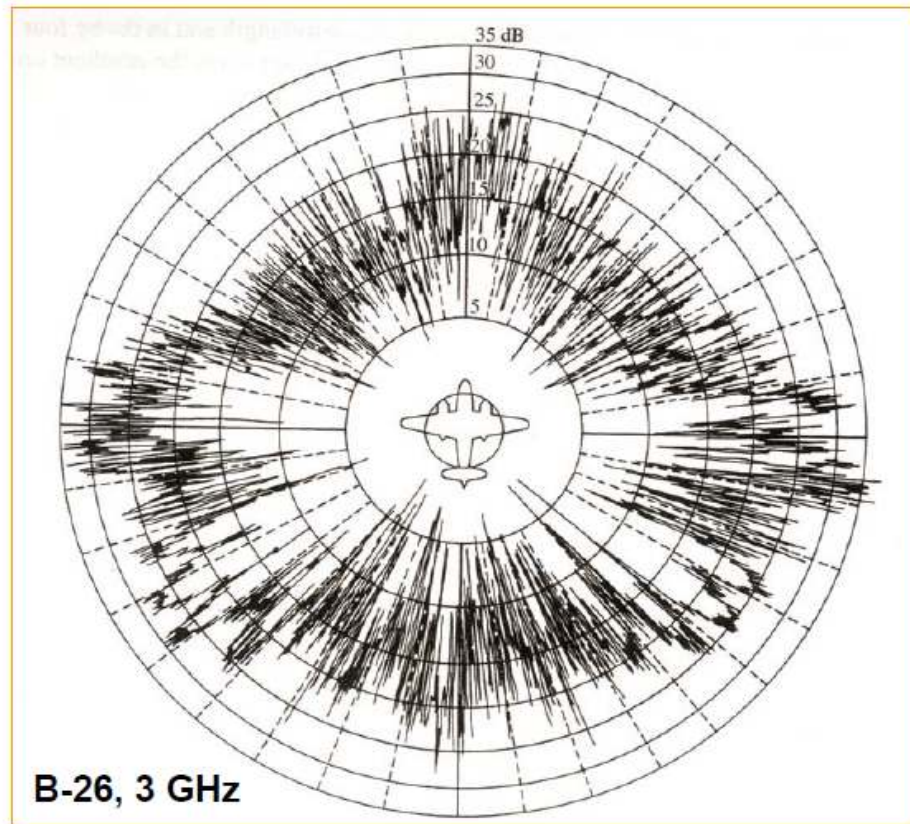


차 례

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Fluctuating Target Models

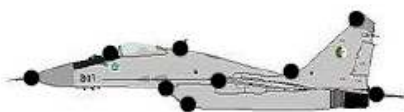
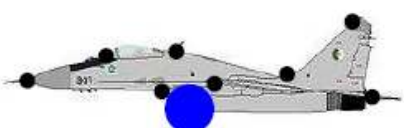
RCS vs. Azimuth for a Typical Complex Target



RCS versus Azimuth

- For many types of targets, the received radar backscatter amplitude of the target will vary a lot from pulse-to-pulse:
 - Different scattering centers on complex targets can interfere constructively and destructively
 - Small aspect angle changes or frequency diversity of the radar's waveform can cause this effect
- Fluctuating target models are used to more accurately predict detection statistics (P_D vs., P_{FA} , and S/N) in the presence of target amplitude fluctuations

Swerling Target Models

Nature of Scattering	RCS Model	Fluctuation Rate	
		Slow Fluctuation “Scan-to-Scan”	Fast Fluctuation “Pulse-to-Pulse”
Similar amplitudes 	Exponential (Chi-Squared DOF=2) $p(\sigma) = \frac{1}{\bar{\sigma}} \exp\left(-\frac{\sigma}{\bar{\sigma}}\right)$	Swerling I	Swerling II
One scatterer much Larger than others 	(Chi-Squared DOF=4) $p(\sigma) = \frac{4\sigma}{\bar{\sigma}^2} \exp\left(-\frac{2\sigma}{\bar{\sigma}}\right)$	Swerling III	Swerling IV

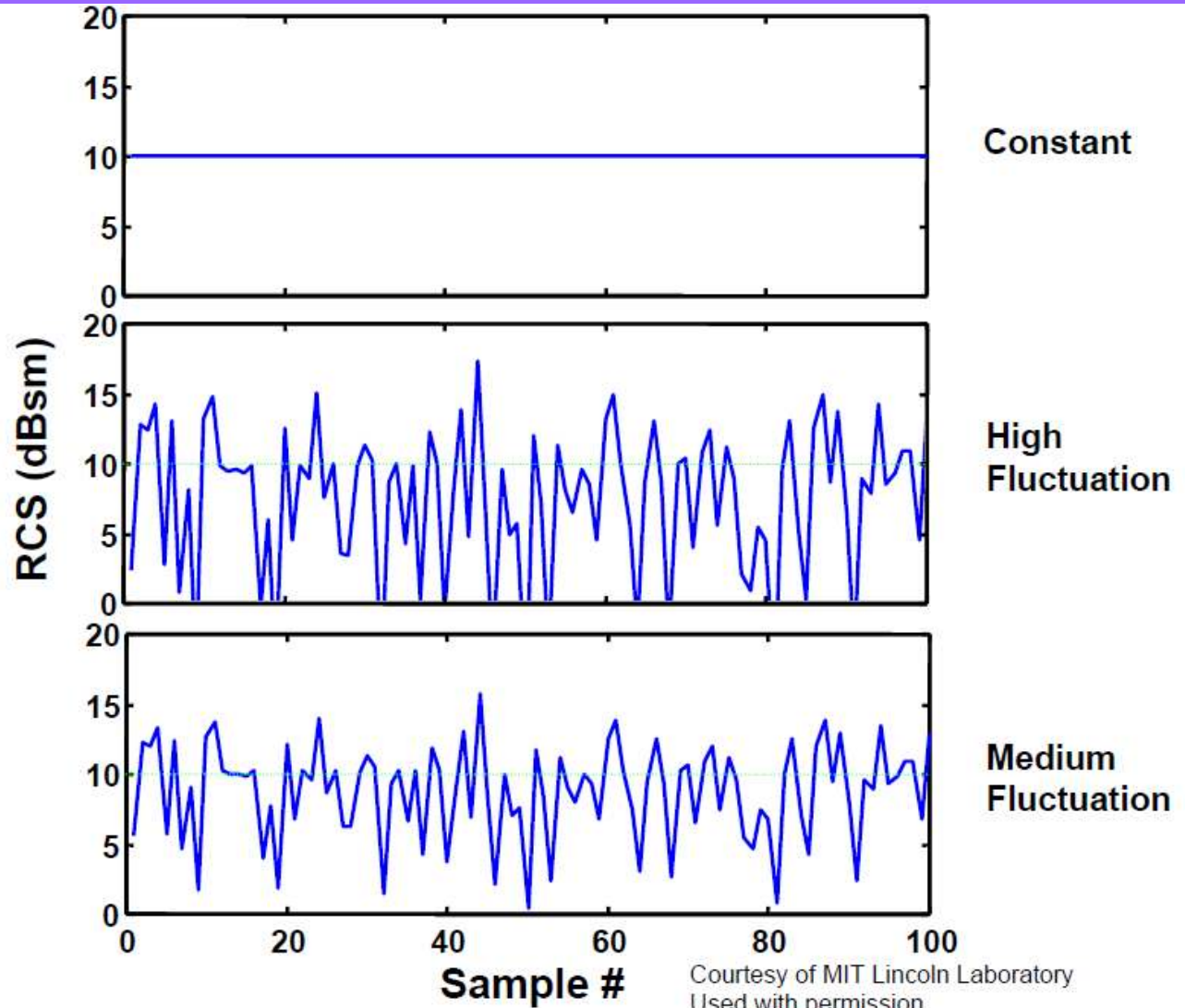
$\bar{\sigma}$ = Average RCS (m²)

Courtesy of MIT Lincoln Laboratory
Used with permission

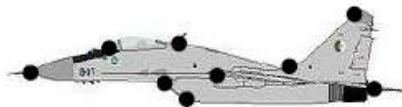


RCS Variability for Different Target Models

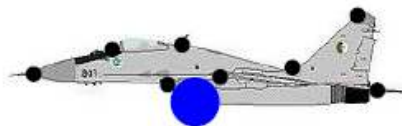
Non-fluctuating Target



Swerling I/II



Swerling III/IV



Detection Statistics for Fluctuating Targets

Single Pulse Detection

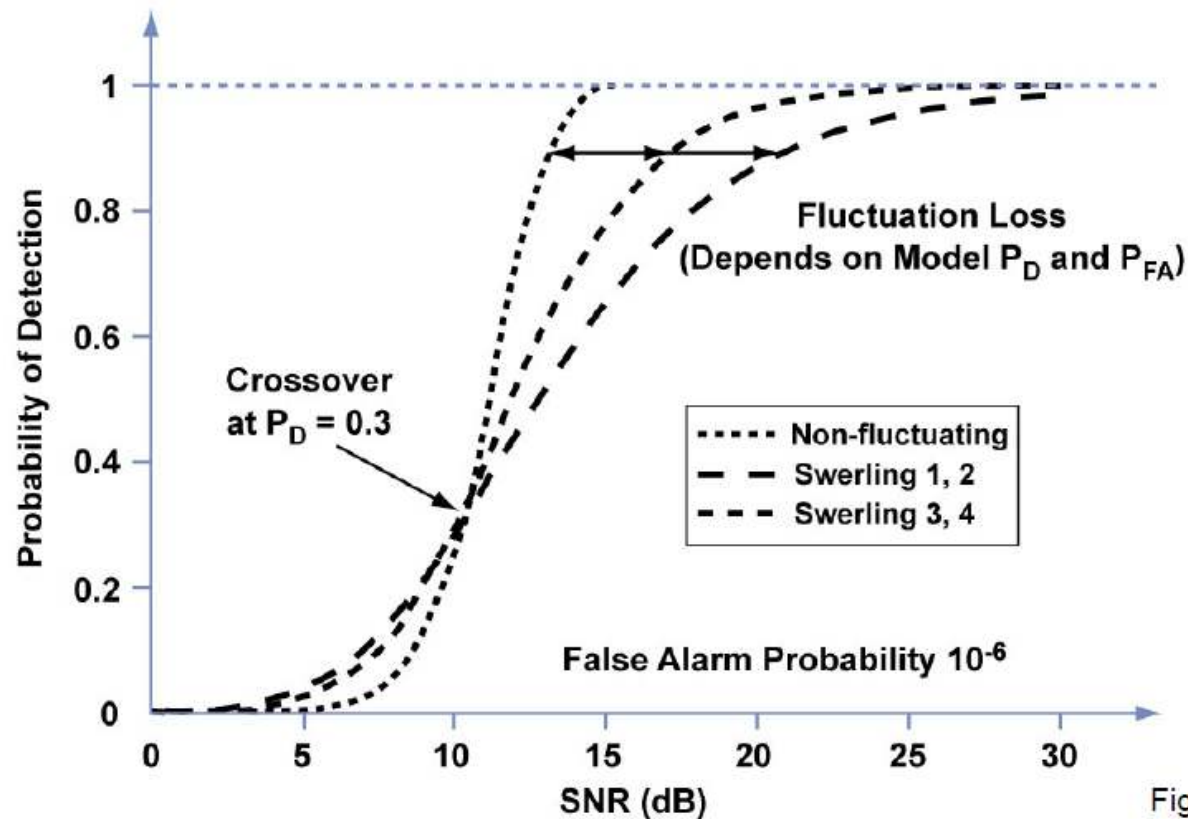


Figure by MIT OCW.

Fluctuating Targets Require More SNR than Non-fluctuating Targets to Maintain a High Probability of Detection



차 례

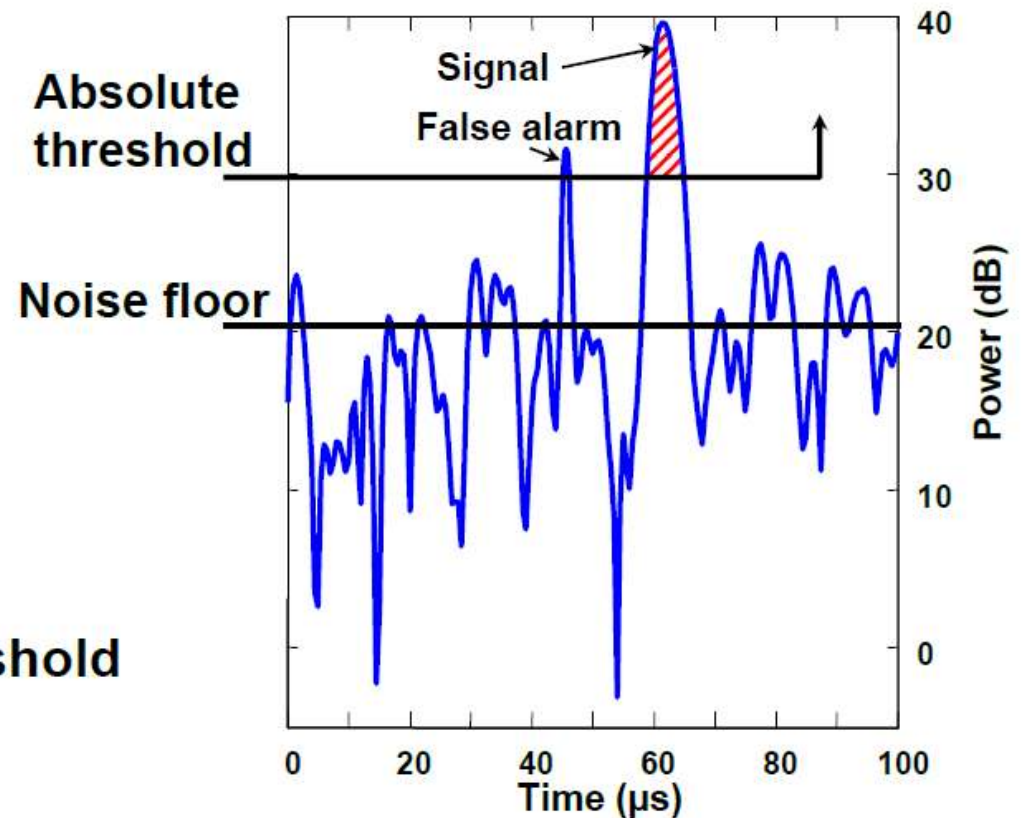
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Constant False Alarm Rate (CFAR) Thresholding

- **Problem:** Must know (or estimate) noise floor to set threshold
- **Solution:** Estimate noise floor using noise-only samples
 - Adaptive thresholding
- **CFAR thresholding:**

$$\frac{\text{test cell}}{\text{noise floor estimate}} > \text{threshold}$$

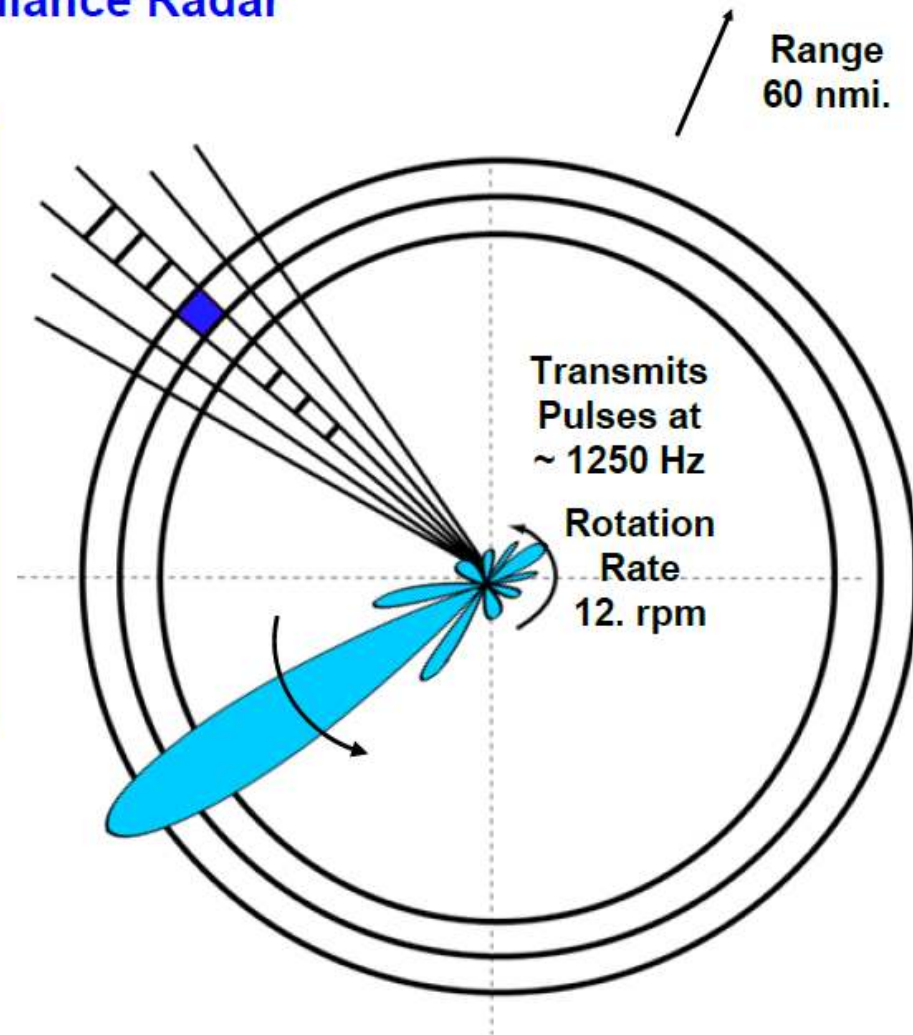


Radar Detection – “The Big Picture”

Example – Typical Aircraft Surveillance Radar ASR-9

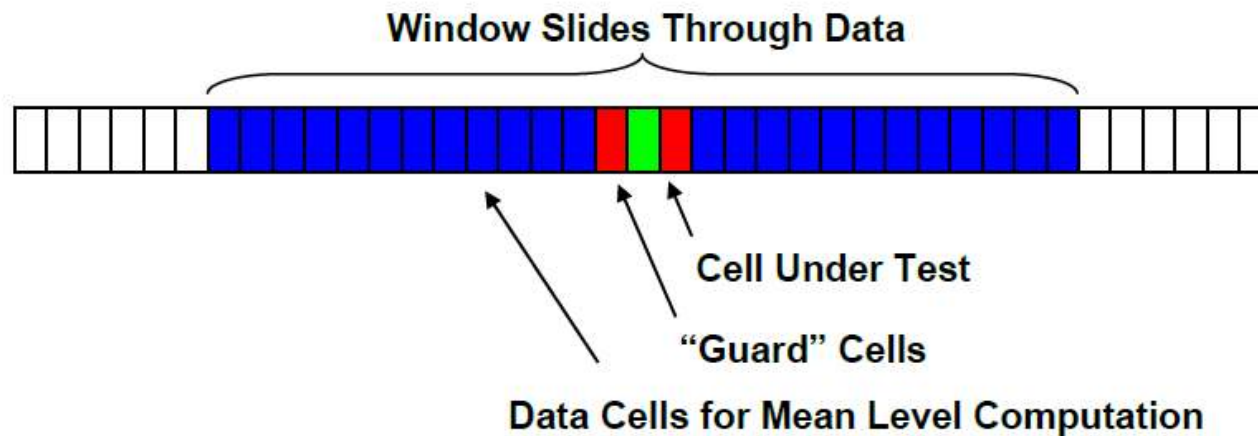


- **Mission – Detect and track all aircraft within 60 nmi of radar**
- **S-band $\lambda \sim 10$ cm**



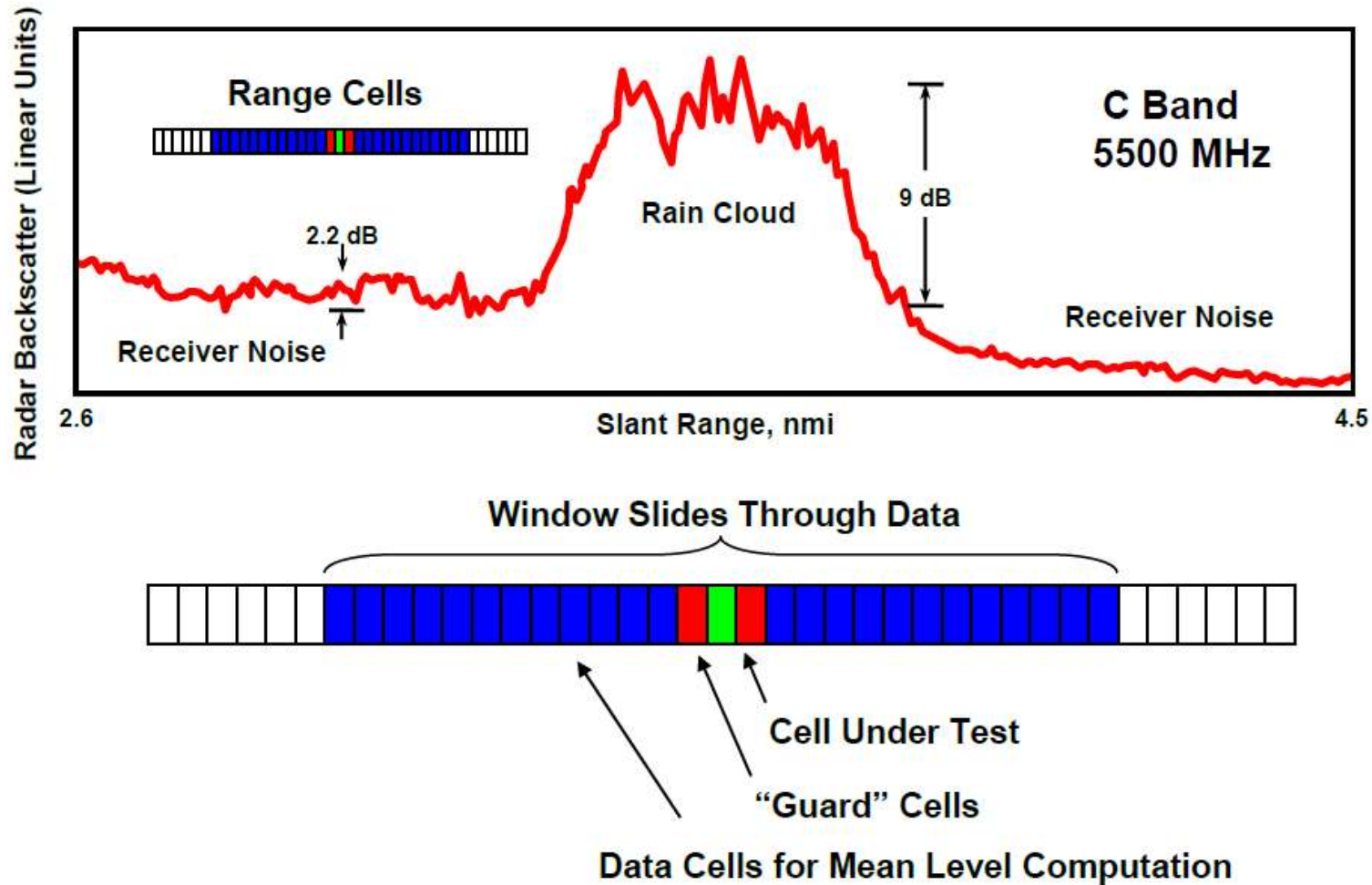
The Mean Level CFAR

- Use mean value of surrounding range cells to determine threshold for cell under test

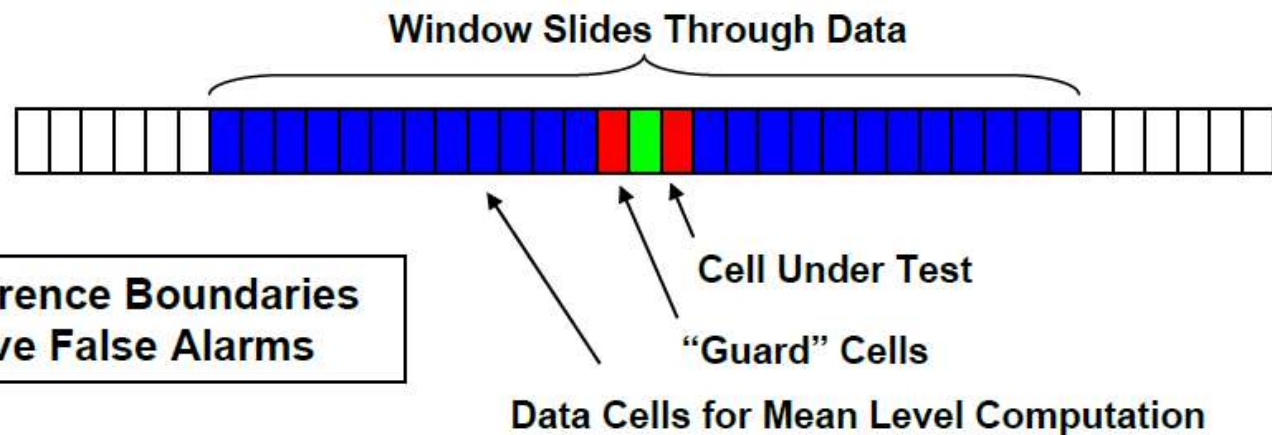
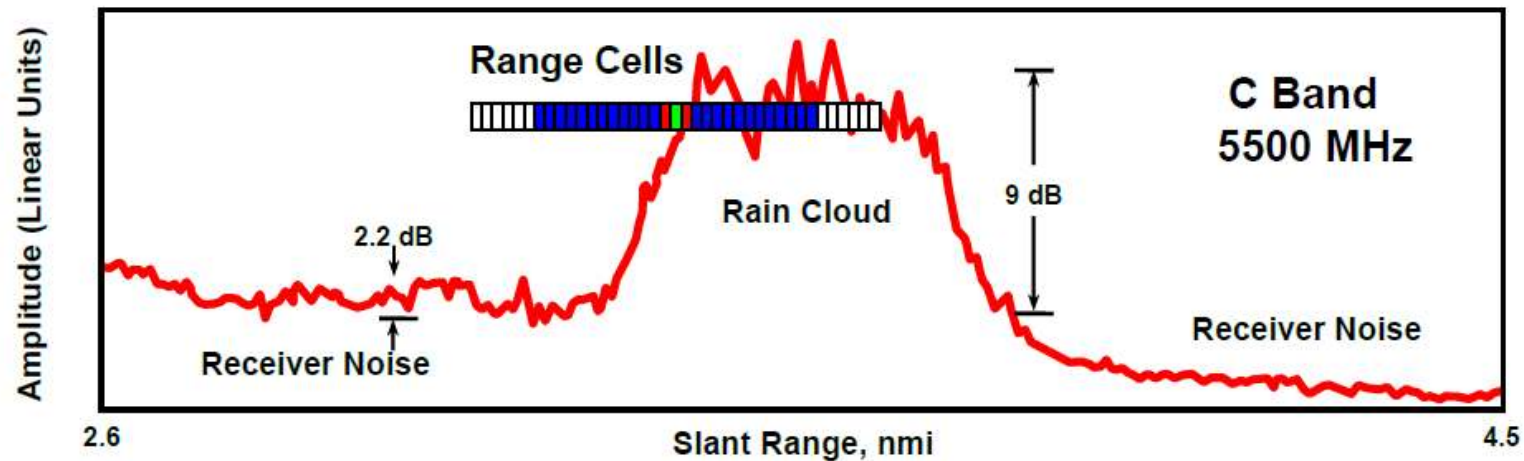


- Nearby targets can raise threshold and suppress detection

Effect of Rain on CFAR Thresholding



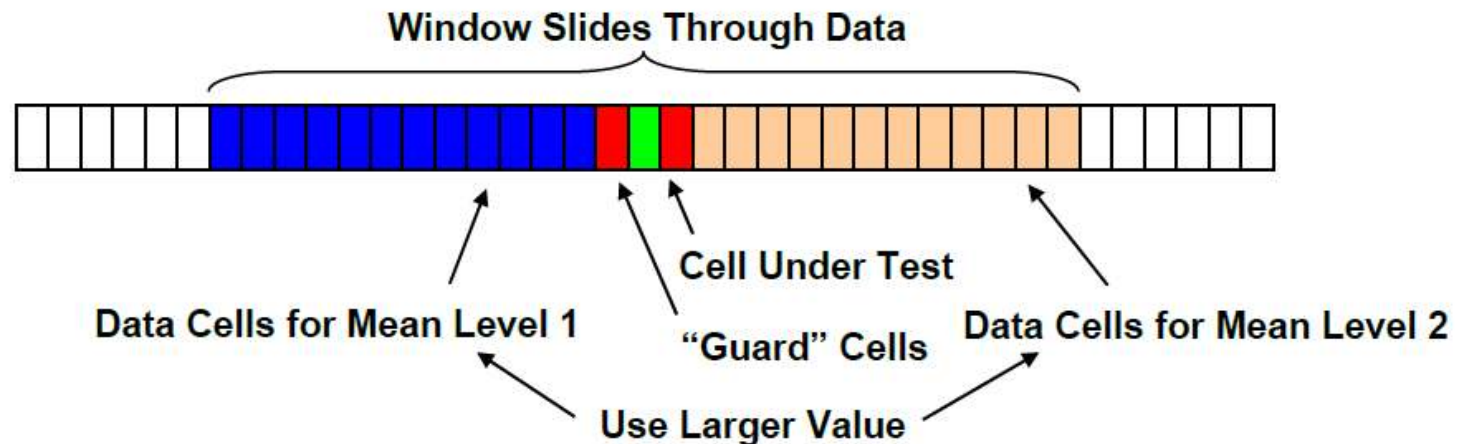
Effect of Rain on CFAR Thresholding



**Sharp Clutter or Interference Boundaries
Can Lead to Excessive False Alarms**


Greatest-of Mean Level CFAR

- Find mean value of $N/2$ cells before and after test cell separately
- Use larger noise estimate to determine threshold



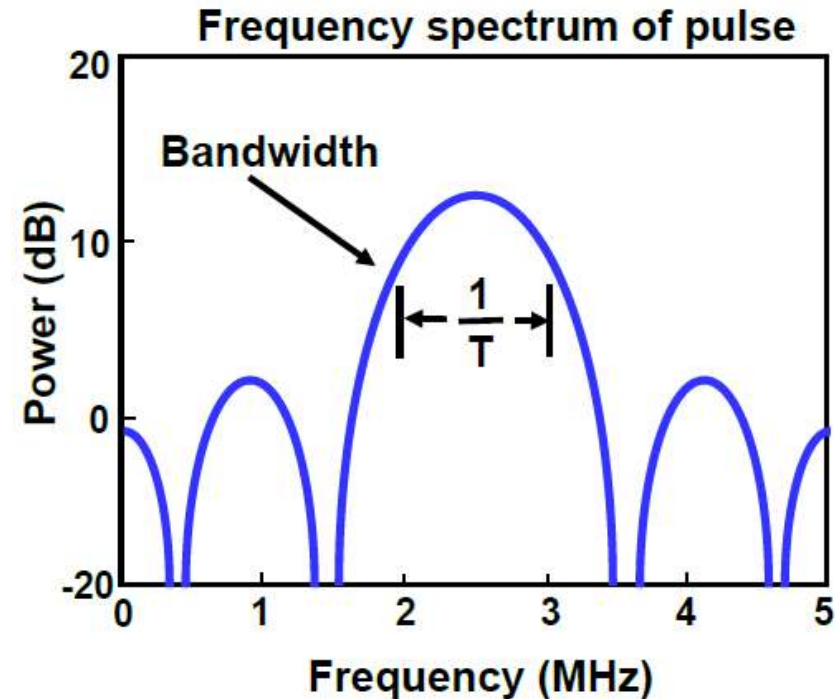
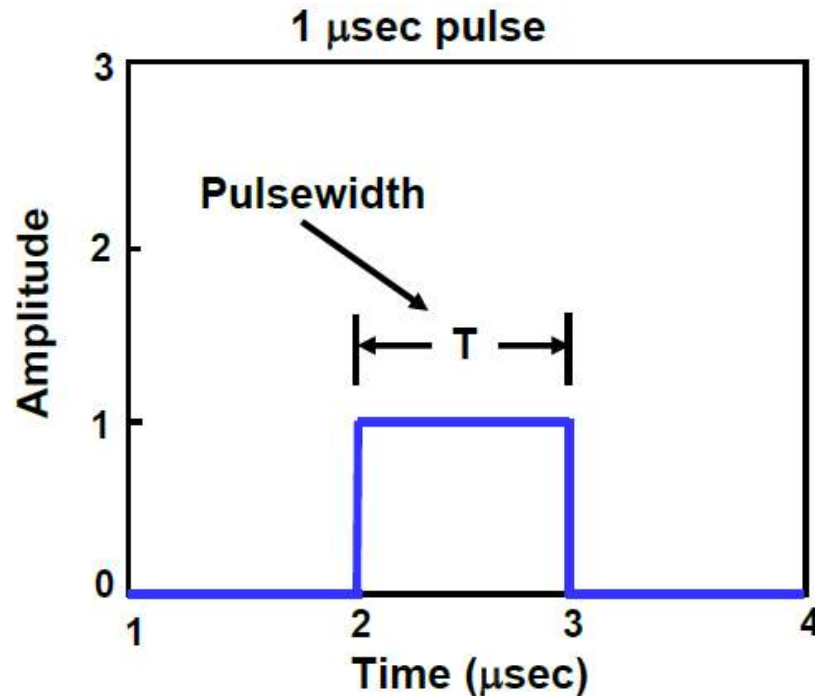
- Helps reduce false alarms near sharp clutter or interference boundaries
- Nearby targets still raise threshold and suppress detection

차 례

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Pulsed CW Radar Fundamentals

Range Resolution



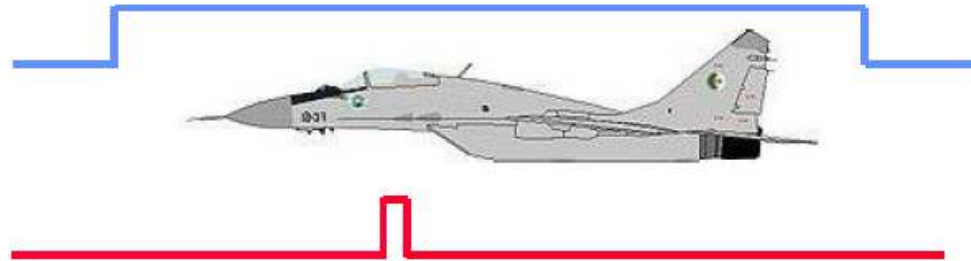
- Range Resolution (Δr)
 - Proportional to pulse width (T)
 - Inversely proportional to bandwidth ($B = 1/T$)
- 1 MHz Bandwidth \Rightarrow 150 m of range resolution

$$\Delta r = \frac{cT}{2}$$

$$\Delta r = \frac{c}{2B}$$

Pulse Width, Bandwidth and Resolution for a Square Pulse

Resolution: Pulse Length is Larger than Target Length
Cannot Resolve Features Along the Target

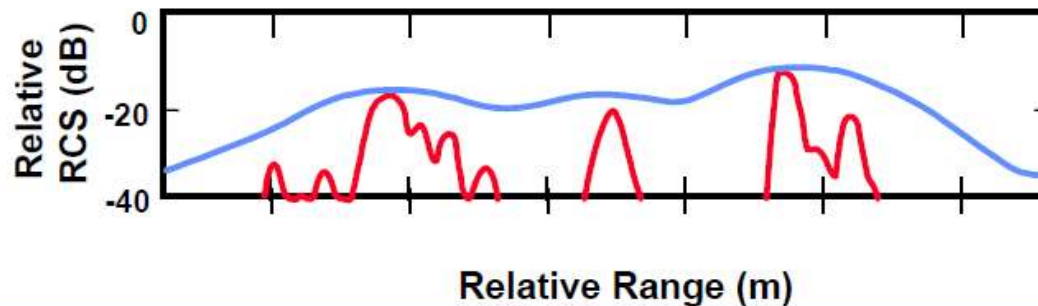


$$\Delta r = \frac{cT}{2}$$

$$\Delta r = \frac{c}{2B}$$

Pulse Length is Smaller than Target Length
Can Resolve Features Along the Target

Metaphorical
Example :



High Bandwidth

$$\Delta r = .1 \times \Delta r$$

$$BW = 10 \times BW$$

Low Bandwidth

Shorter Pulses have Higher Bandwidth and Better Resolution

Viewgraph courtesy of MIT Lincoln Laboratory
Used with permission

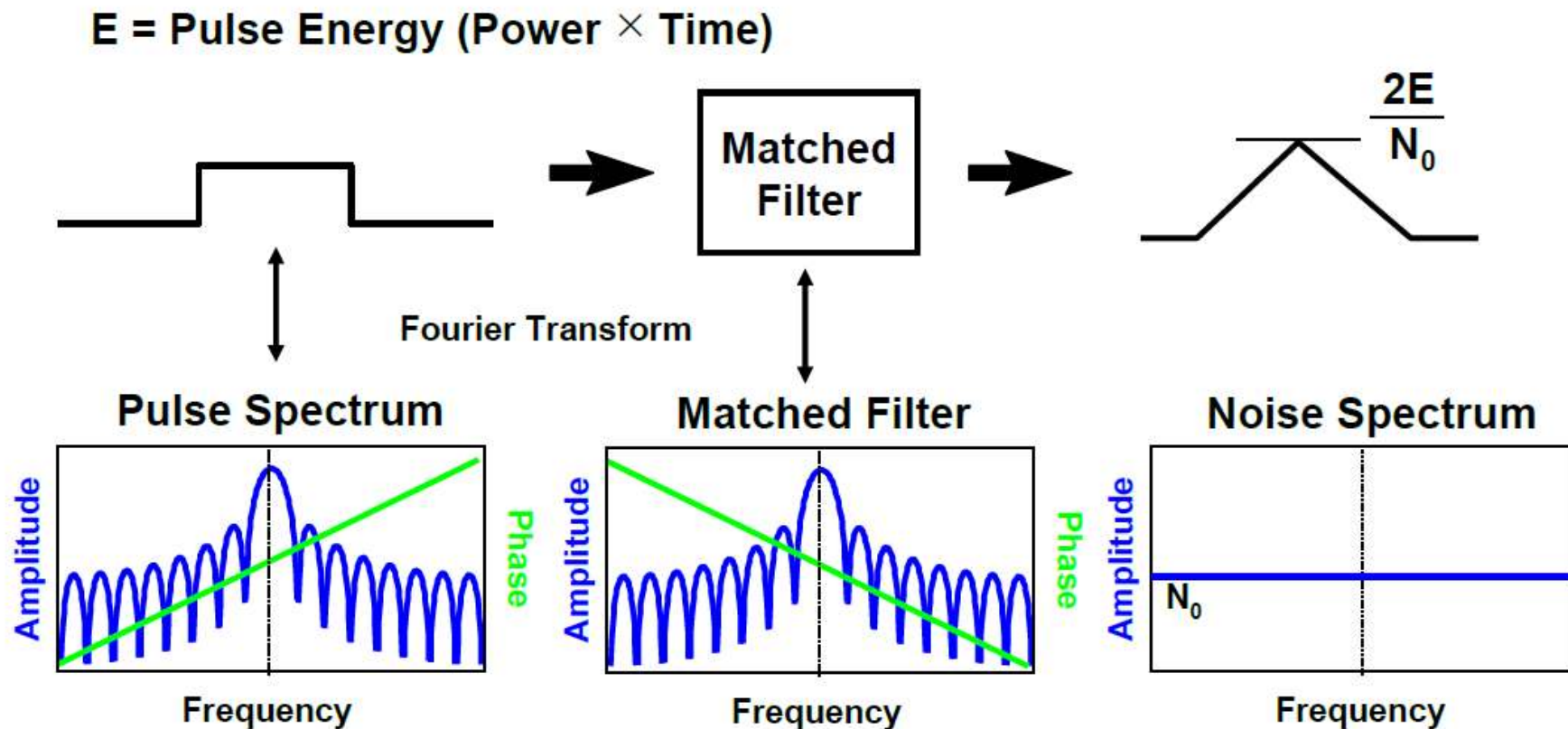


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Motivation for Pulse Compression

- Hard to get “good” average power and resolution at the same time using a pulsed CW system
 - Higher average power is proportional to pulse width
 - Better resolution is inversely proportional to pulse width
- A long pulse can have the same bandwidth (resolution) as a short pulse if the long pulse is modulated in **frequency or phase**
- These pulse compression techniques allow a radar to simultaneously achieve the energy of a long pulse and the resolution of a short pulse

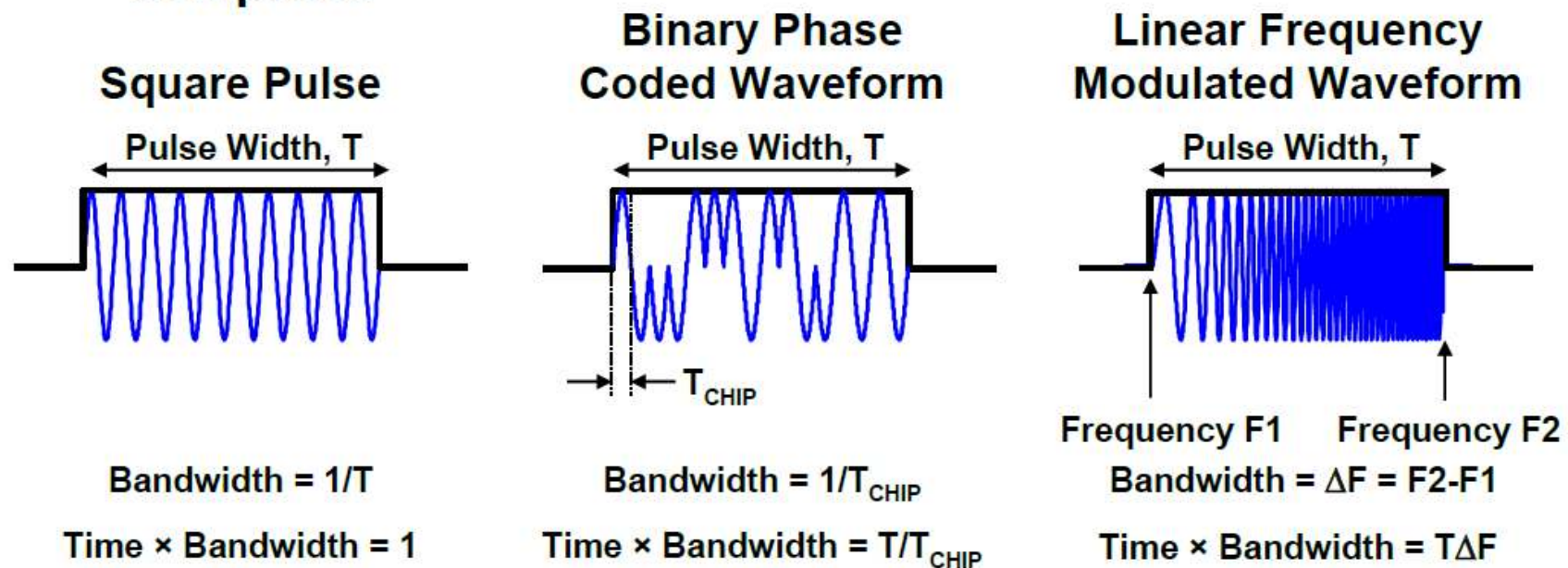
Matched Filter Concept



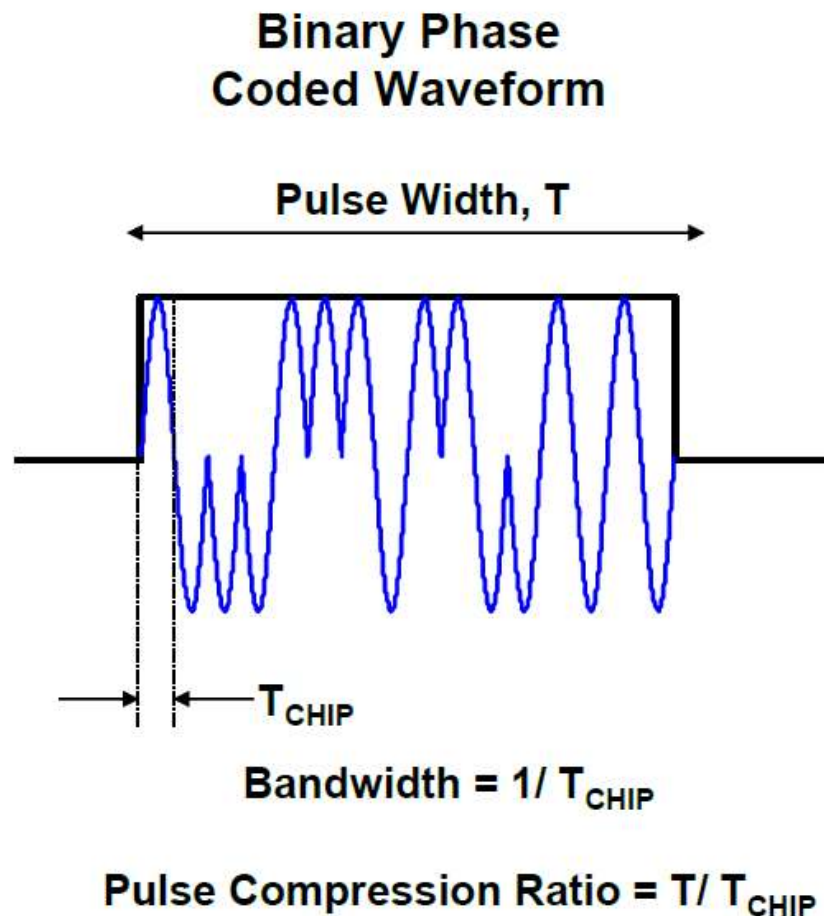
- Matched Filter maximizes the peak-signal to mean noise ratio
 - For rectangular pulse, matched filter is a simple pass band filter

Frequency and Phase Modulation of Pulses

- Resolution of a short pulse can be achieved by modulating a long pulse, increasing the time-bandwidth product
- Signal must be processed on return to “pulse compress”



Binary Phase Coded Waveforms



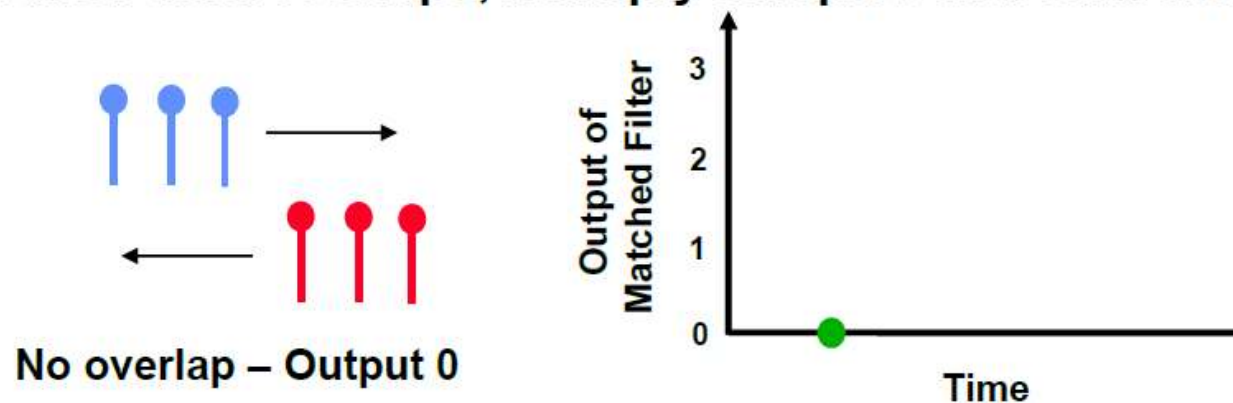
- Changes in phase can be used to increase the signal bandwidth of a long pulse
- A pulse of duration T is divided into N sub-pulses of duration T_{CHIP}
- The phase of each sub-pulse is changed or not changed, according to a **binary phase code**
- Phase changes 0 or π radians (+ or -)
- Pulse compression filter output will be a compressed pulse of width T_{CHIP} and a peak N times that of the uncompressed pulse

Implementation of Matched Filter

- Matched filter is implemented by “convolving” the reflected echo with the “time reversed” transmit pulse



- Convolution process:
 - Move digitized pulses by each other, in steps
 - When data overlaps, multiply samples and sum them up

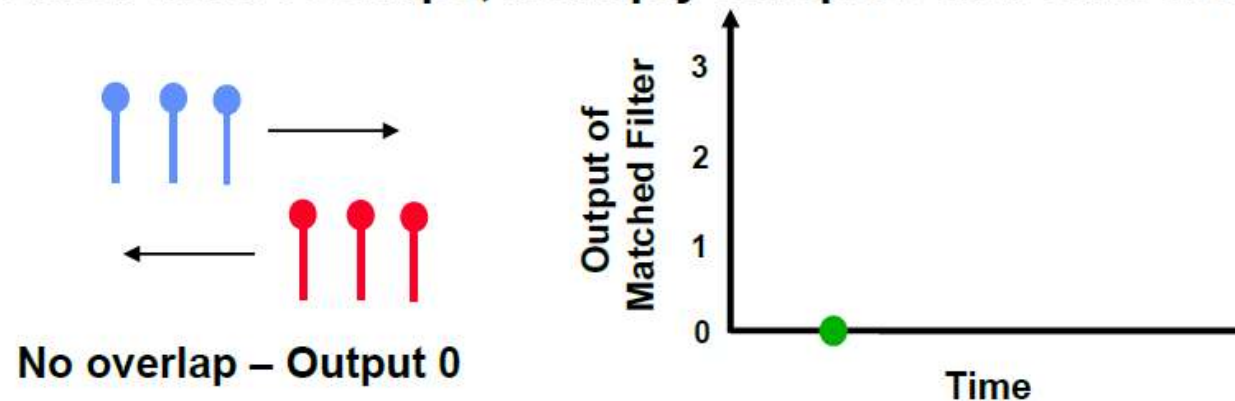


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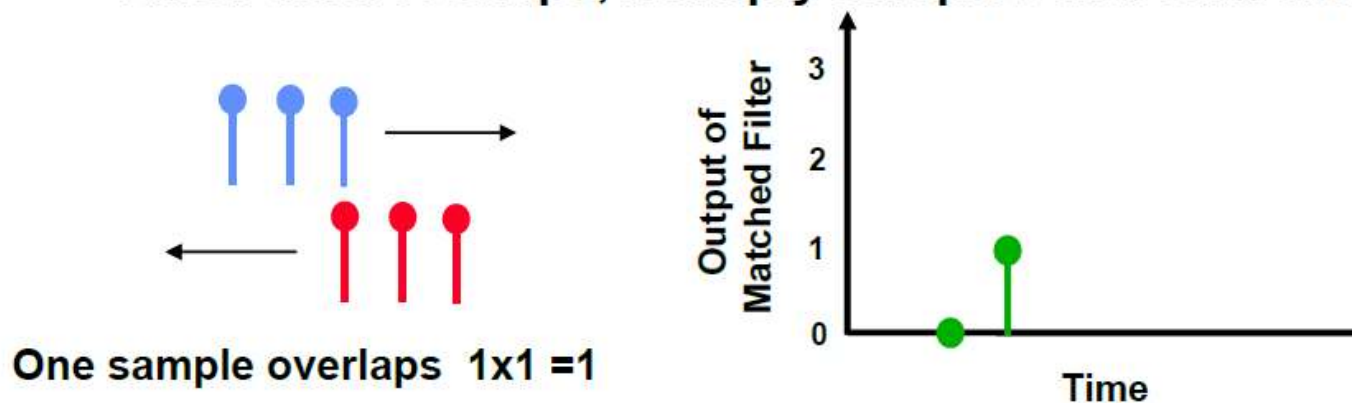


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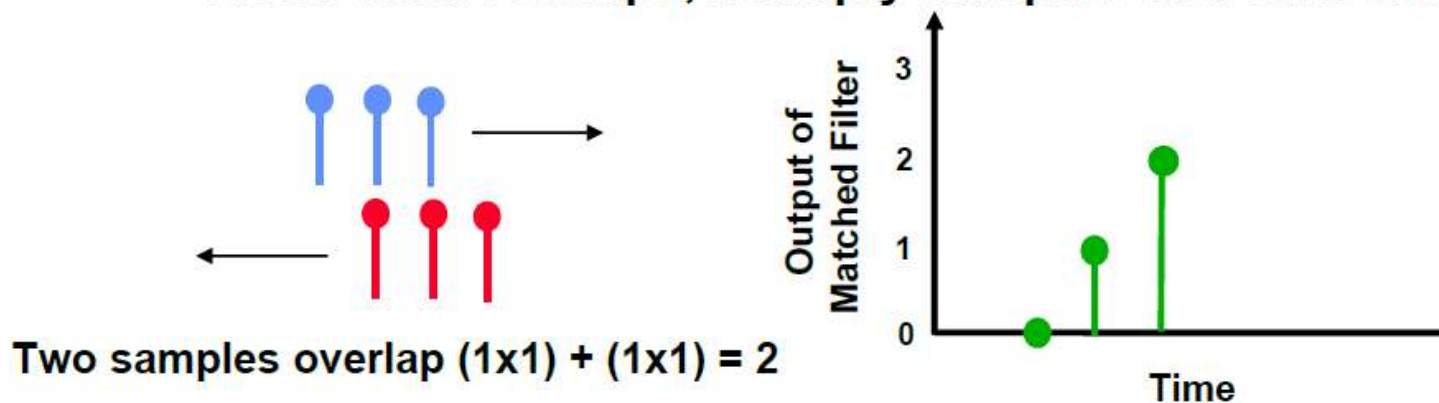


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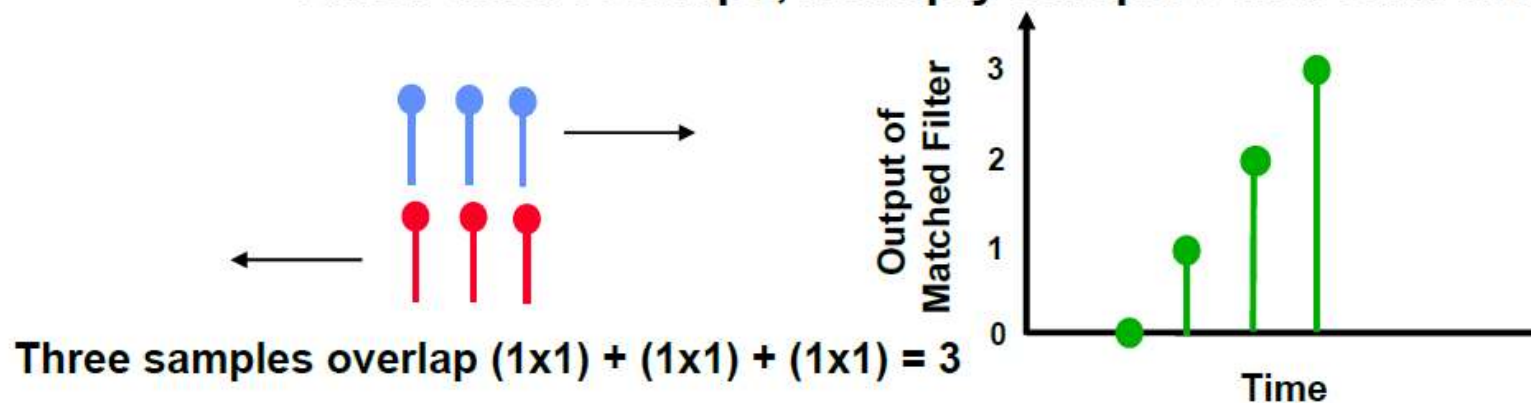


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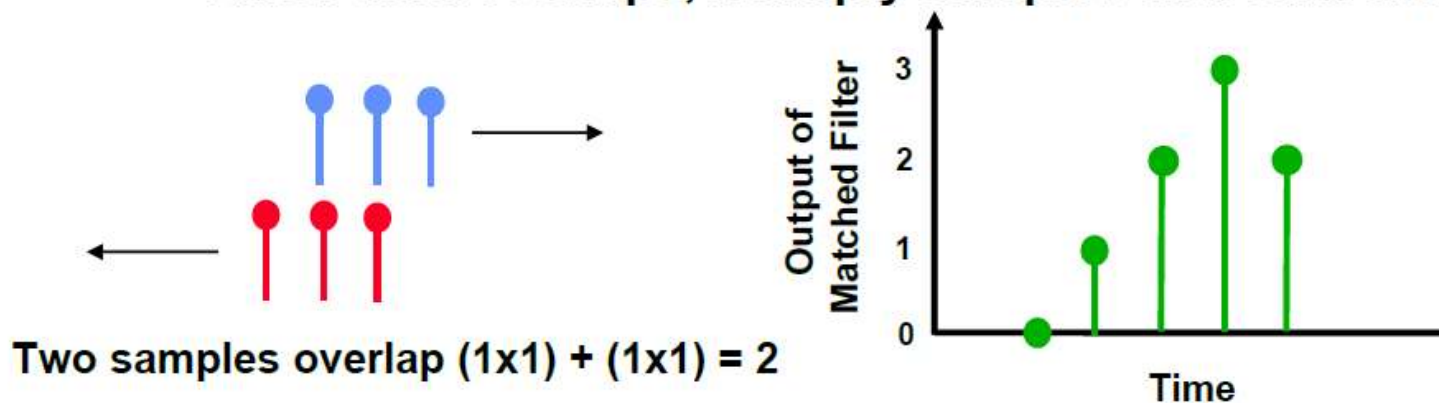


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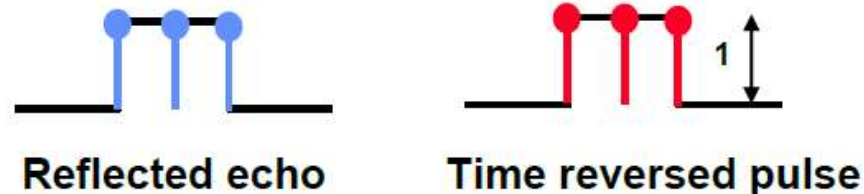


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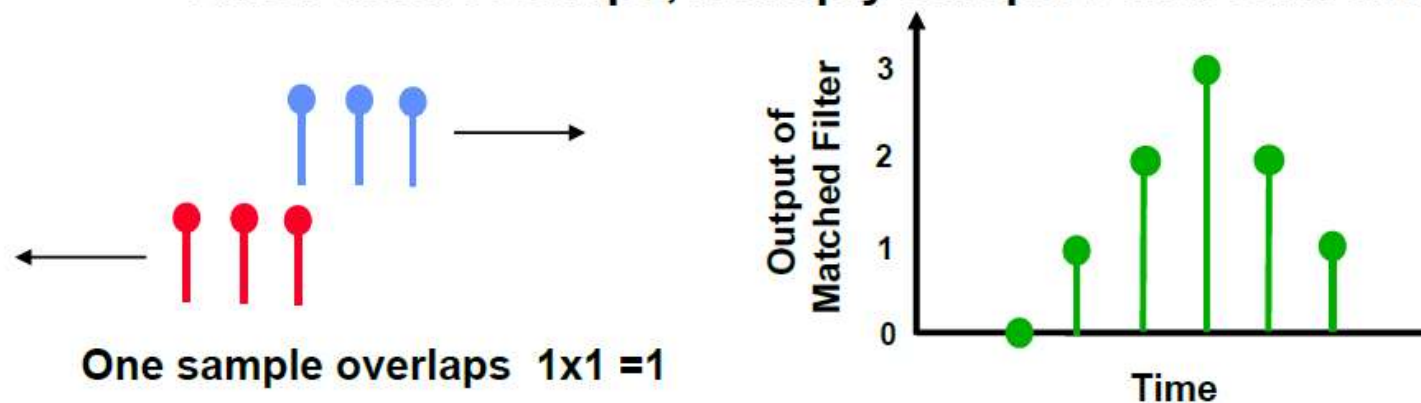


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Use of Matched Filter Maximizes S/N

Pulse Compression

Binary Phase Modulation Example

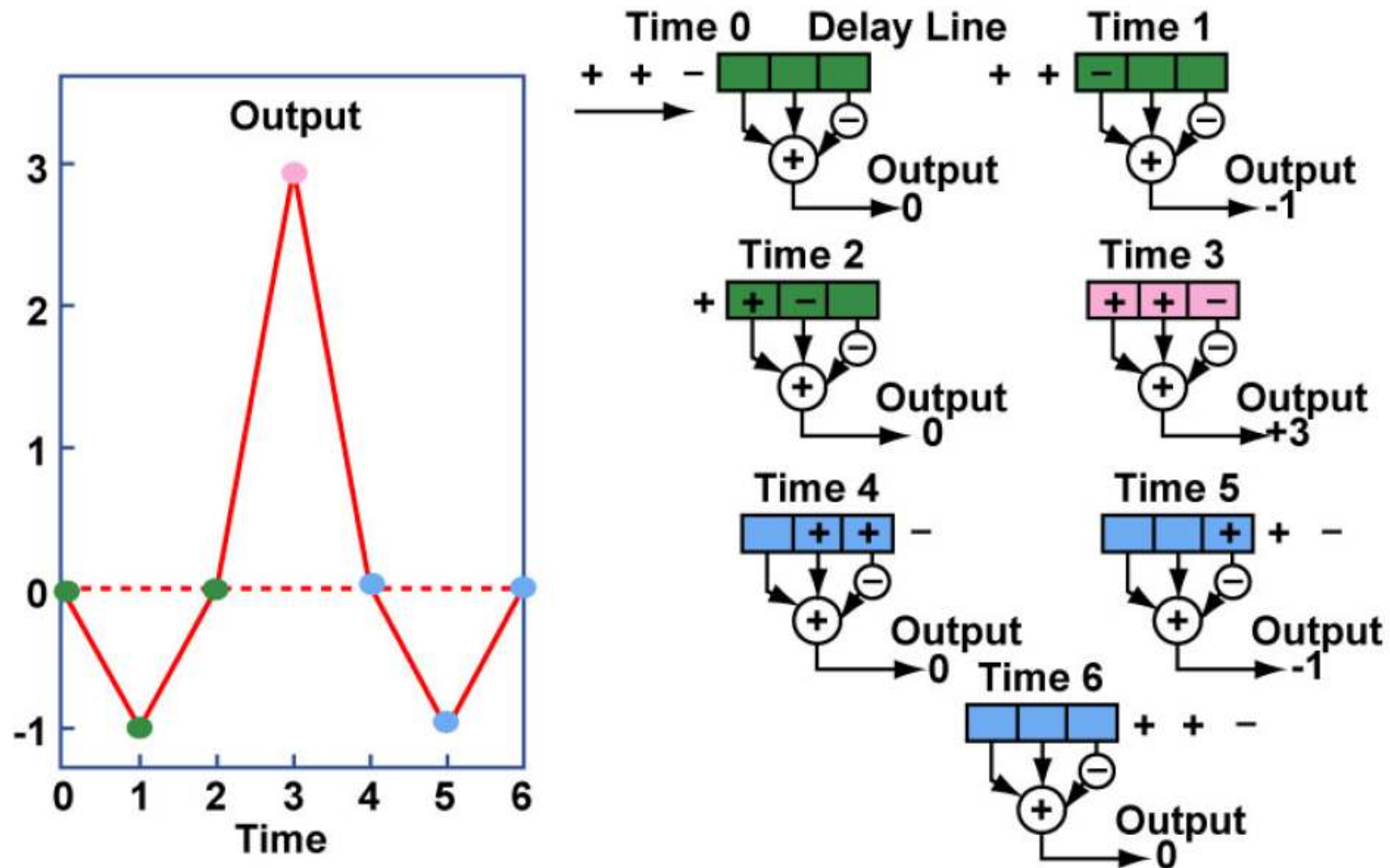
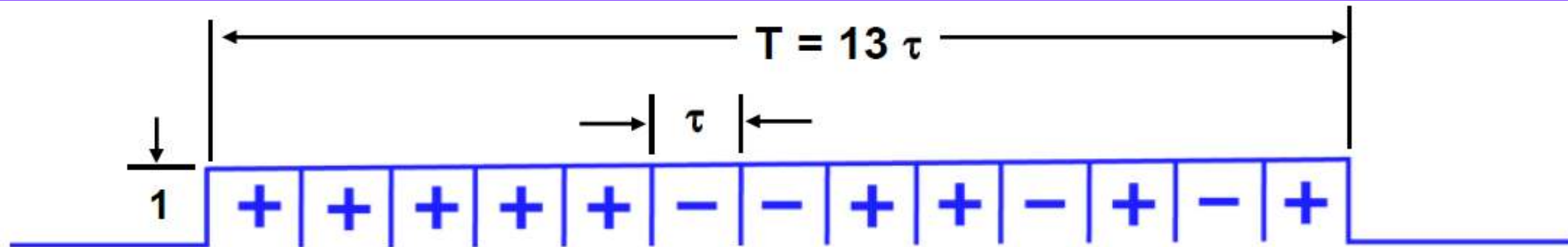
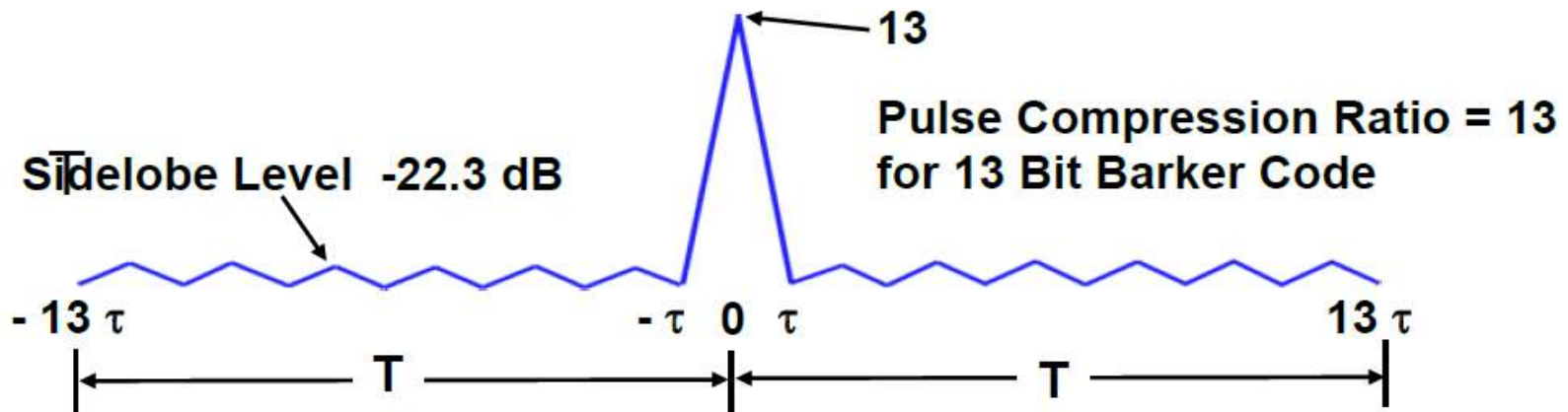


Figure by MIT OCW.

Example - 13 Bit Barker Code



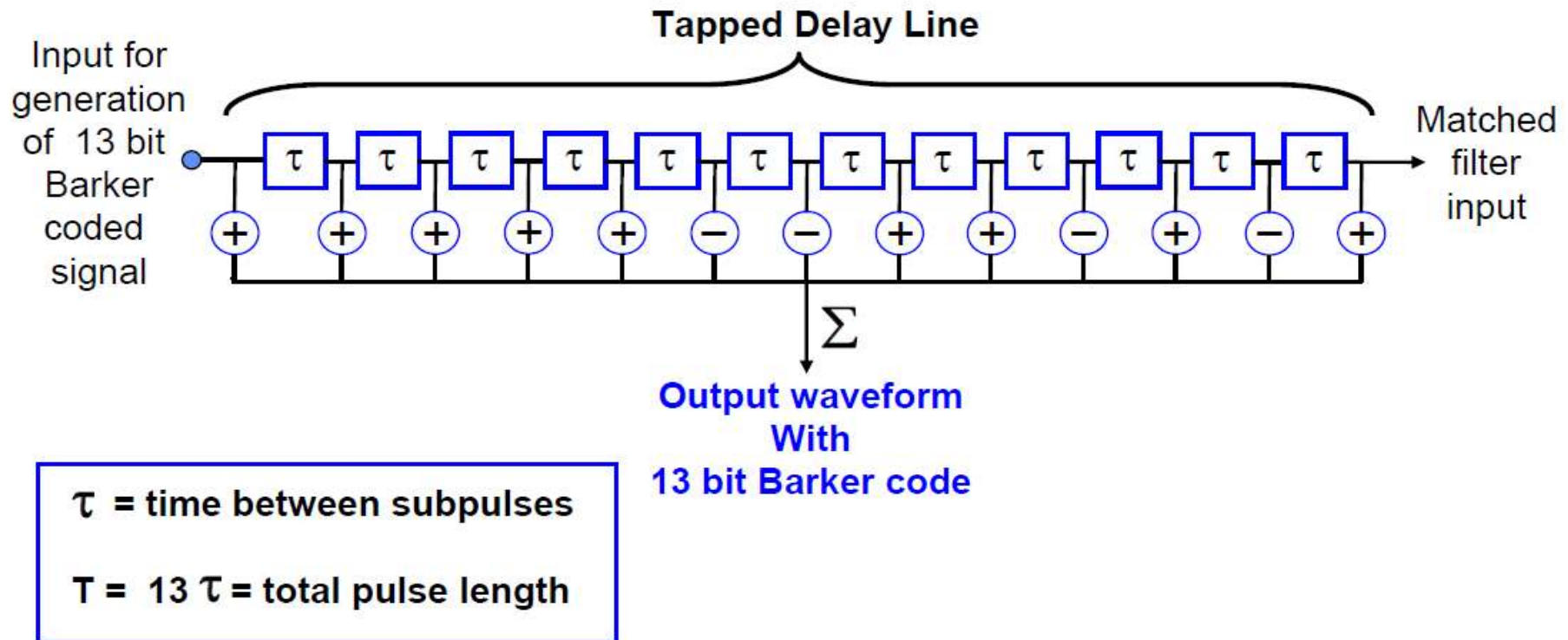
A long pulse with 13 equal sub-pulses, whose individual phases are either 0 (+) or π (-) relative to the un-coded pulse



Auto-correlation function of above pulse, which represents the output of the matched filter

Tapped Delay Line

Generating the Barker Code of Length 13



Barker Codes

<u>Code Length</u>	<u>Code Elements</u>	<u>Sidelobe Level (dB)</u>
2	+ - , + +	- 6.0
3	+ + -	- 9.5
4	+ + - + , + + + -	- 12.0
5	+ + + - +	- 14.0
7	+ + + - - + -	- 16.9
11	+ + + - - - + - - + -	- 20.8
13	+ + + + + - - + + - + - +	- 22.3

- The 0, and π binary phase codes that result in equal time sidelobes are called **Barker Codes**
- Sidelobe level of Barker Code is $1 / N^2$ that of the peak power (N = code length)
- None greater than length 13



Linear FM Pulse Compression

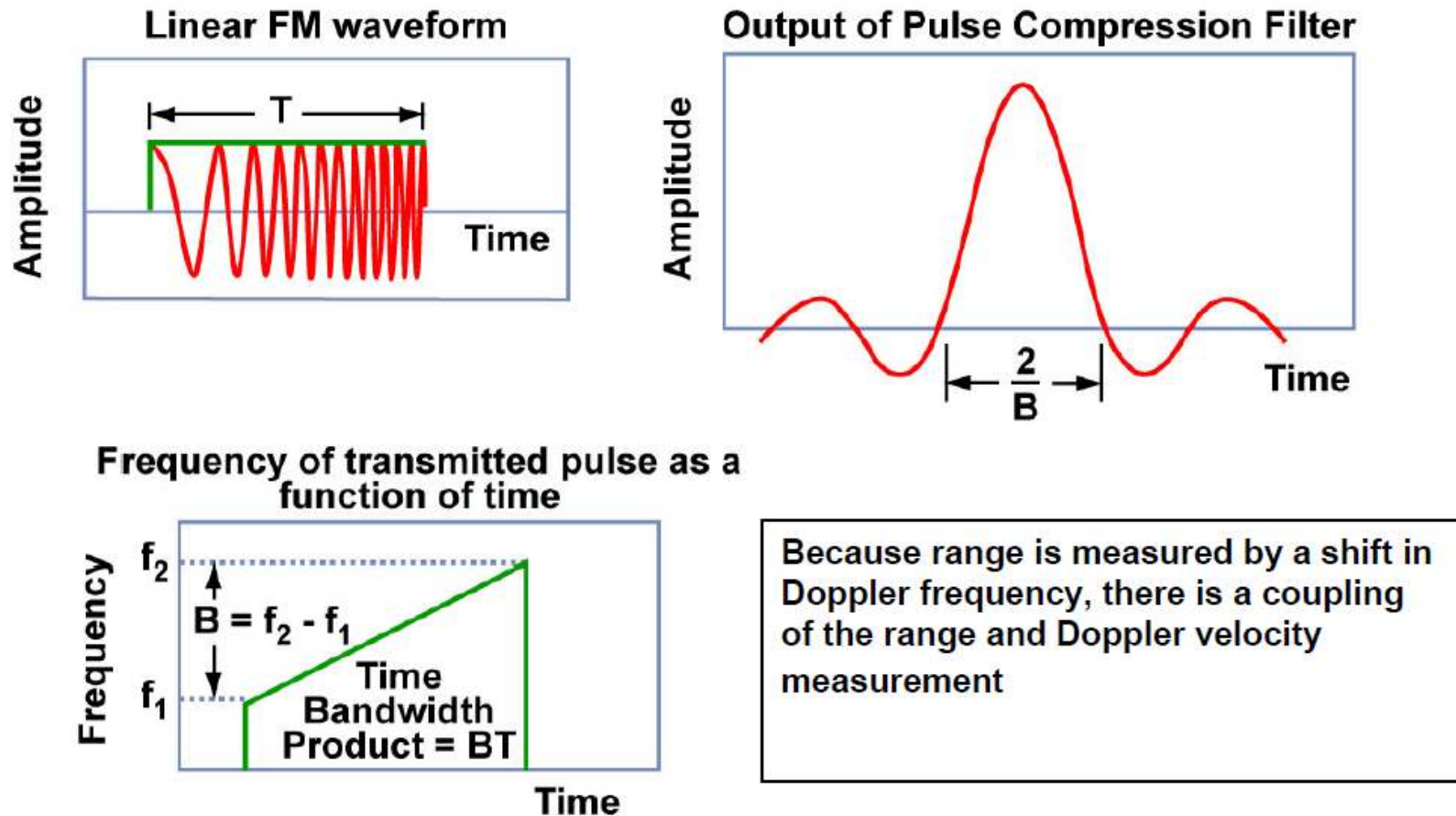


Figure by MIT OCW.

Q & A

