



FORENSIC ANALYSIS OF FAILED SURGE ARRESTORS

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Presentation Flow:

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Introduction :

Surge Arrester

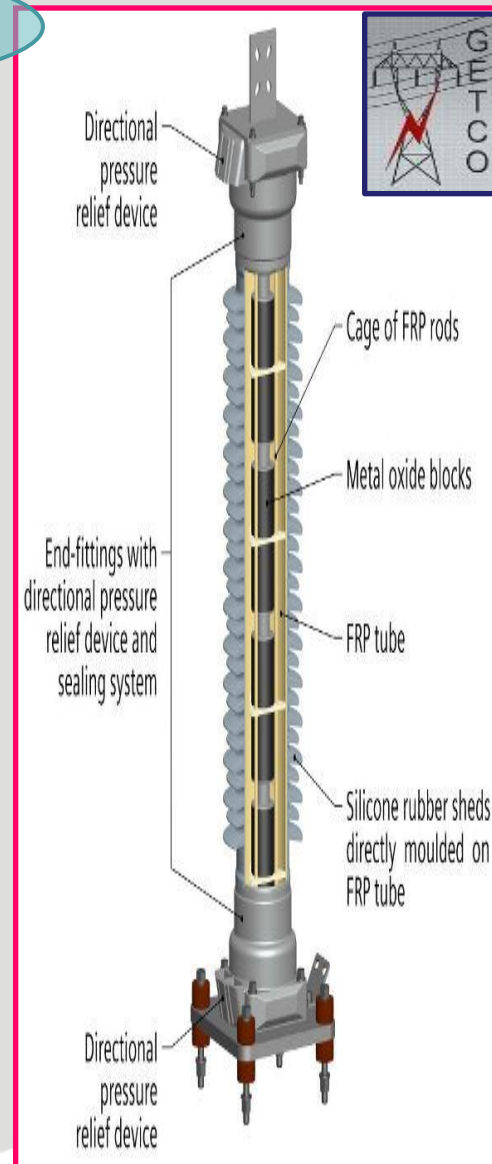


“Important” Equipment of the Grid

- Protects electrical power systems from Lighting/Switching surges
- Main component of SA: Semiconductor ZnO discs
 - highly voltage sensible
 - Insulating at low voltage
 - Conducting at high voltage

“MUST” conditions for Surge Arrester:

- ✓ Conducts only during over voltages/surges
- ✓ Minimal surge clearing Time
- ✓ Low power loss under normal operating conditions
- ✓ High resistance to power current
- ✓ High energy handling capability.
- ✓ No system disturbance while operation.
- ✓ Economical, reliable and having long life





Concept behind Analysis:

- Any failure, if analyzed, is useful to improve upon design, quality and operational aspects.
- **Forensic analysis:**
 - Allow to determine cause of end of life of arrestor, whether it is,
 - Normal or expected (i.e. while performing protecting function)
 - Or any other issue related to
 - Design
 - Manufacturing or
 - Maintenance
- This exercise is useful for continuous improvement to build up efficient , safe & uninterrupted power system.
- It is also important for OEM to become consistent in quality while design & manufacturing.

GETCO Approach:

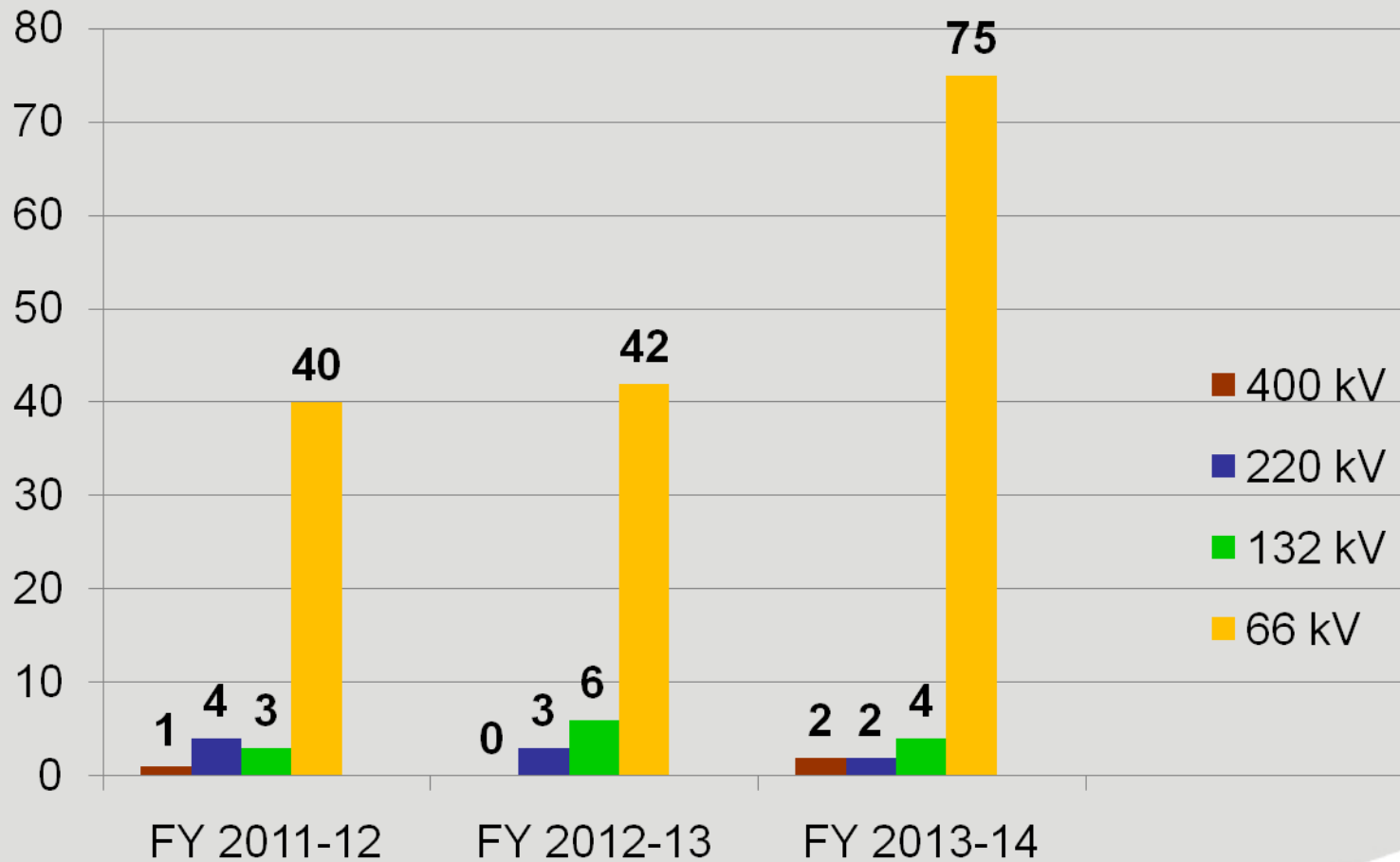


| Class | 400 kV | 220 kV | 132 kV | 66 kV | TOTAL |
|------------|--------|--------|--------|-------|-------|
| Population | 313 | 2600 | 1491 | 16196 | 20600 |

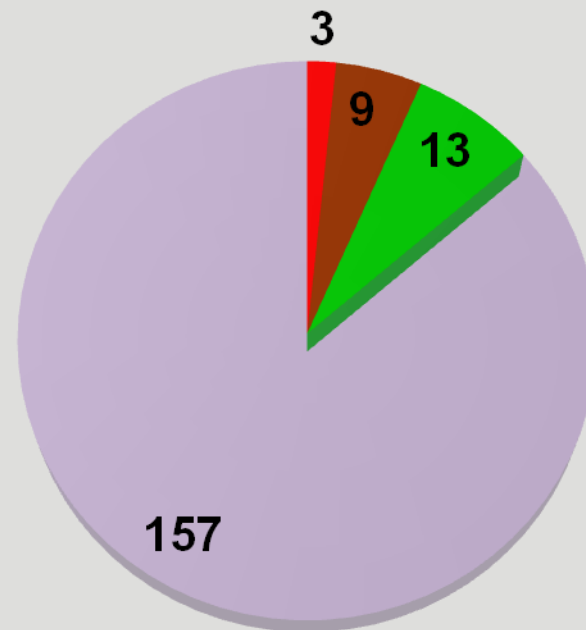
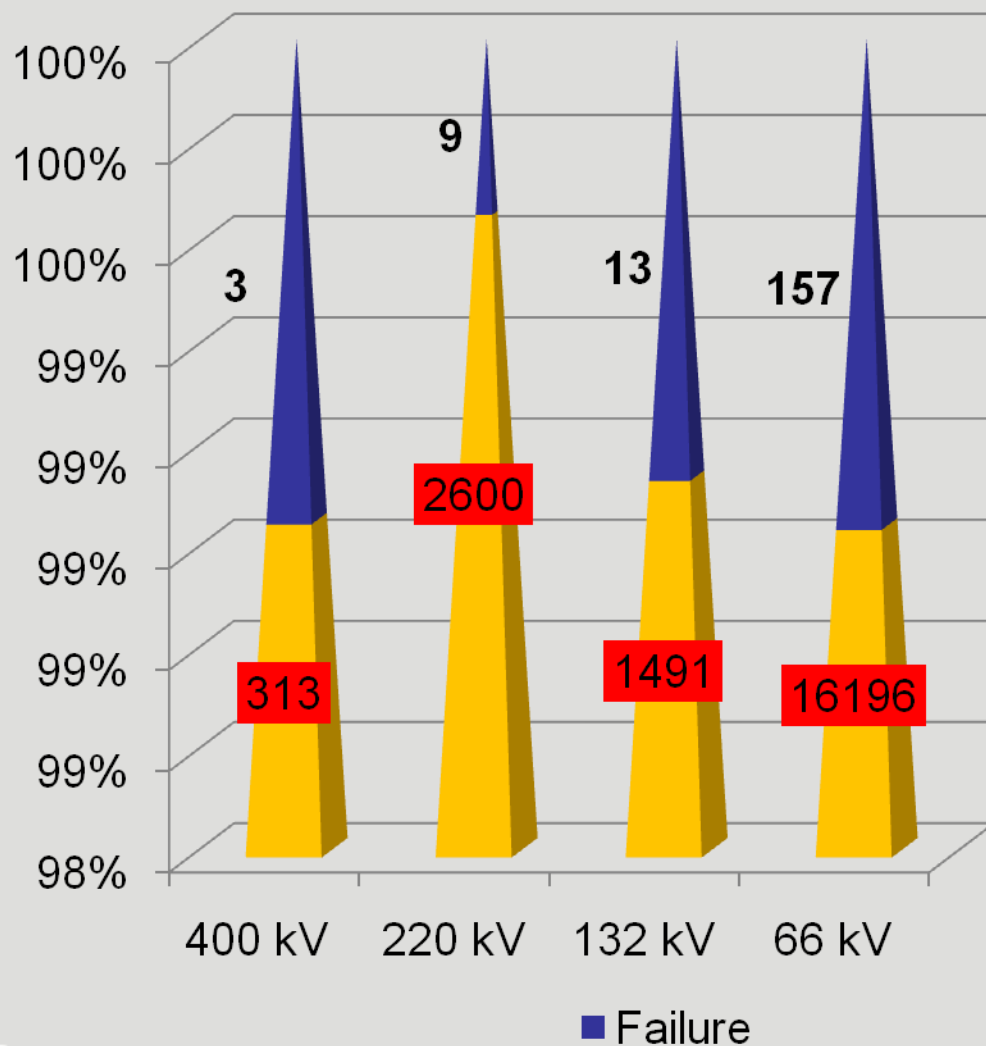
- Increasing failure rates observed in recent years (Year: 2011-12, 2012-13, 2013-14).
- Monitoring of leakage current of each and every SA is already in place.
- Knowing the reason of failure, we can identify areas of improvement like design, manufacturing, quality or service conditions.
- To identify the reason of failure, root cause analysis of each failure is essential.

| Class | 400 kV | 220 kV | 132 kV | 66 kV | TOTAL |
|---|--------|--------|--------|-------|-------|
| No. of failures | 3 | 9 | 13 | 157 | 182 |
| Rate of failure out of total population | 1 % | 0.35 % | 0.9 % | 1 % | 0.9 % |

Year wise Failure



Voltage class wise Failures



■ 400 kV ■ 220 kV
■ 132 kV ■ 66 kV

Total 182 SAs failed during 3 years

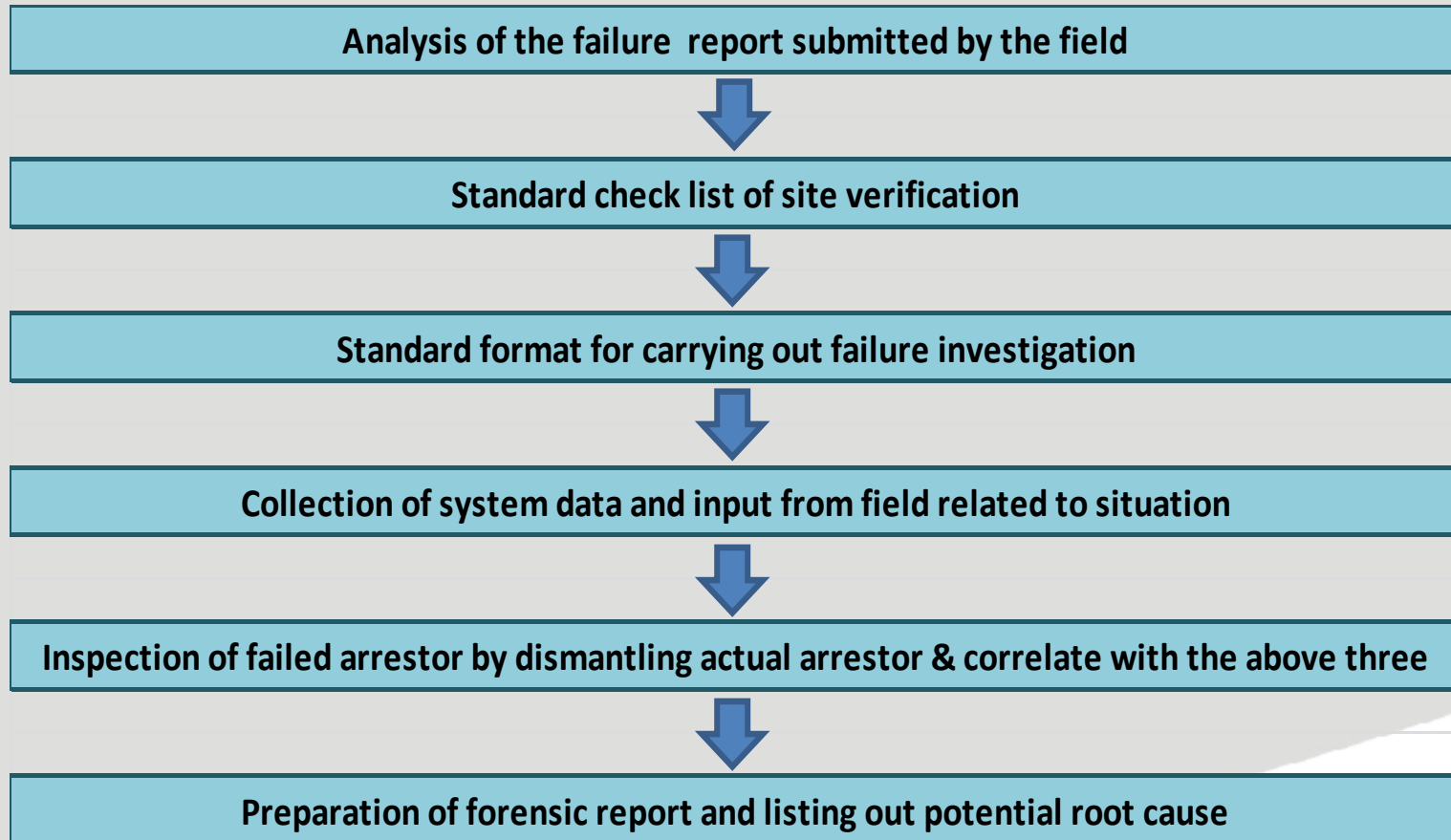


Forensic Analysis of Failed Surge Arrestors:

Out of 182 nos. of failures, preliminarily 20 nos. of SAs were selected randomly for study & analysis, considering practical as well as theoretical facets.



Failure Analysis Strategy





1. Analysis of preliminary field reports

Preliminary field failure reports comprise of

- Name plate data
- Date of commissioning
- Application (Line, Transformer or Capacitor bank)
- System conditions at the time of failure
- Weather conditions at the time of failure
- Any other specific data

2. Standard Check list for site verification

Standard

The standard check list/format, describing post failure condition of SA, was prepared to maintain uniformity & precision in data collection during site visits.

:: CHECK LIST FOR LIGHTNING ARRESTER ::

| 1] LA Details: | | | |
|--|--|----------|----------|
| a) | Make of Lightning arresters | | |
| b) | Rating of LA. | | |
| c) | MCOV of LA. | | |
| d) | Sl. No. of LA. | | |
| e) | Year of manufacturing. | | |
| f) | No. of units per arrester. | | |
| g) | Rating of each unit. | | |
| h) | Date of Commissioning | | |
| i) | Date of Failure | | |
| 2] PHYSICAL VERIFICATION OF ARRESTER:- | | | |
| S. N. | ITEM | YES / NO | REMARKS. |
| EXTERNAL VERIFICATION. | | | |
| 1. | BUSHING. (SHORT CIRCUIT MARKS, FLASHOVER MARKS | | |
| 2. | BUSHING BROKEN. | | |
| 3. | FLASHOVER MARKS ON CASTINGS | | |
| | • TOP | | |
| | • BOTTOM | | |
| 4. | FLASHOVER MARKS ON LINE TERMINAL CONNECTOR. | | |
| 5. | FLASHOVER MARKS ON LINE TERMINAL BRACKET. | | |
| INTERNAL VERIFICATION AFTER OPENING. | | | |
| 1. | CONDITION OF END COVER PLATES | | |
| | • TOP | | |
| | • BOTTOM | | |
| 2. | CONDITION OF PRESSURE RELEASE DEVICE OPERATED | | |
| | • TOP | | |
| | • BOTTOM | | |
| 3. | GASKET CONDITION | | |
| | • TOP | | |
| | • BOTTOM | | |
| | MOISTURE INGRESS | | |
| 4. | STACK POSITION, CARBON CONTAMINATION. | | |
| 5. | NO. OF BLOCKS PER STACK / UNIT. | | |
| 6. | BLOCK DETAILS IF ANY (PRINTED ON BLOCK) | | |
| 7. | NO. OF BLOCKS DAMAGED. | | |
| 8. | NO. OF FRP RODS PER UNIT/STACK. | | |
| 9. | FLASHOVER MARK/DAMAGE OF FRP ROD. | | |
| 10. | MELTING OF STACK SEPARATORS. | | |
| 11. | FLASHOVER OF STACK SUPPORTERS. | | |
| 12. | SPRING CONDITION | | |
| SURGE MONITOR. | | | |
| 1. | SERIAL NO. | | |
| 2. | FLASH OVER. | | |
| 3. | NO. OF IMPULSES COUNTED. | | |
| 4. | IMPULSE MARKS ON SURGE MONITOR. | | |
| 3] Remarks if any:- | | | |

3. Standard format for carrying out failure investigation

Matrix of Root cause, Failure mechanism and Symptoms

Matrix

1. External Flashover

| | |
|-------------------|--|
| Typical reasons | Lightning. |
| | Severe contamination with presence of moist atmosphere |
| | Caused by animals, like monkey, snake etc. |
| Failure mechanism | <p>Due to electrocution of animal, external arc can be created over the external housing of LA.</p> <p>However, LA may not always get affected due to external flashover if the protection system is properly operated</p> |
| Indicators | Marking of arcs on HV side of LA or on housing and base |

2. Moisture Ingress

| | |
|-------------------|---|
| Typical reasons | Manufacturing defect |
| | Mishandling |
| | External flashover damaging seal |
| Failure mechanism | Due to entry of moisture, relative humidity reaches inside same as outside. With low temperature condensation occurred along electrically stressed components leads to dry band arcing & dielectric tracking along wet surface and eventually results in a short circuit of unit. |
| Indicators | Brown rust on metal parts |
| | White rust on aluminum parts |
| | Increased watt loss at operating voltage |
| | Tracking along electrically stressed components |
| | Increased temperature in infrared image |
| | Green copper oxidation |
| | Hardened rubber seal left with lower compressive strength |
| | Old rust covered by carbon by-products of arcing which indicates rust was there prior to failure |
| | Tracking inside |
| | Cracks and damp on discs |

3. Excessive Internal Partial Discharge

| | |
|-------------------|---|
| Typical reasons | Excessive PD lead to degradation of ZnO discs as well as dielectric capability. |
| | Happened in significant internal air space. |
| | Manufacturing defects, moisture ingress, mishandling, excessive contamination & moisture on external surfaces. |
| Failure mechanism | Minor PD activity starts & then grows. After long exposure, the dielectric in this area of arrester degrades & leads to flashover of electrically stressed parts. |
| | PD can also reduce the oxygen content of the air around the discs and in some cases changes characteristics of disc. |
| Indicators | PD is indicated by high freq spikes near edges & corners, discoloration of components & contact points etc. |
| | Multi colored growths on rubber components |
| | Corroded internal parts, oxidization etc. |



4. Lightning

| | |
|-------------------|--|
| Typical reasons | Terminal overload occur due to lightning stroke above designed value. |
| | However, failure can occur later if the damage due to this is minimal. |
| | Excessive single current surge or a significant multi-stroke surge |
| | Improper lightning duty specified |
| | Successive strokes on same unit |
| | TOV followed by a surge due to fault on that circuit exceeding SA's capability |
| Failure mechanism | This minor damage triggers PD in turn leads to tracking and causes electrical failure. If capability is exceeded by LI stroke, the ZnO discs will initially take surge, heat up, may get cracked and then flashover. If minor damage is there, it may fail later on. |
| Indicators | ZnO discs get punctured |
| | Porcelain gets cracked or broken |

5. Temporary Over Voltages (TOV)

| | |
|-------------------|---|
| Typical reasons | Terminal overload caused by PF voltage beyond design capability. |
| | A TOV overload can be immediate but, it can also occur a long term failure triggered by unrelated other issues. |
| | Excessive voltage rise in healthy (un-faulted) phase |
| | Misapplication of arrester |
| | Change in neutral configuration, loss of neutral on system |
| | Ferro resonance |
| | Ageing of ZnO discs |
| Failure mechanism | During TOV overload, the voltage across the arrester rises to a level where the disks conduct much more than during the steady state condition. |
| | Discs get heated up significantly in turn lowers its resistance and leads to more conduction and ultimately fails. |
| Indicators | Change in disc characteristics |
| | Cracking of few discs in stack |
| | Flashover of discs |
| | Opening of vent |

6. Switching Surge Overload

| | |
|-------------------|---|
| Typical reasons | It may occur due to surges generated from switching of capacitor banks, long lines, exceeding design limits of arresters. |
| | Re-strike or prestrike of breakers and/ or pre strike of capacitor switches. |
| Failure mechanism | Same as for lightning mechanisms. |
| Indicators | Numerous small holes in the aluminum electrode of the discs generally around circumference of disc electrode. |
| | Polarization of disc at low levels |
| Remarks | Damage due to fault current after the initial overload can disguise the real cause. |

7. Ageing of Discs

| | |
|-------------------|---|
| Typical reasons | Due to ageing, long term changes are observed in MOV arresters. |
| | More losses due to ageing occur. |
| | Improper manufacturing of disc. |
| Failure mechanism | At normal operating voltage, losses gradually increase leading to internal heating. When this heat exceeds arrester's ability to dissipate in to environment, this leads to dielectric failure and a fault on system. |
| | Thermal run away |
| Indicators | Hot arrester at normal operating temperature |
| | Excessive electrical losses at operating voltage |

8. Other Causes

| | |
|---|---|
| External contamination | Lead to external flashover and excessive internal partial discharge |
| Improper selection of U_c or TOV rating | U_c value lower than steady state value of system voltage. |
| Unbalance electric field | Clearance between each phase and with ground, overheating of discs due to voltage imbalance and inappropriate grading ring can cause this type of failure. |
| Misalignment of disc column | Off centered column of discs along the length of housing, physical damage to edges of disc, misalignment during transport & handling, improper spring pressure can lead to PD and ultimately failure. |
| Mechanical stress | Excessive mechanical stress due to jumper, failure of seals due to mechanical load on one side etc. |
| Burrs | Sharp points on conductive parts used inside lead to internal discharge. Design or manufacturing defects also can contribute to this. |
| Insufficient Dielectric strength | Any of the material used inside having inadequate dielectric strength to withstand steady or impulse states can track or flashover. And it will worsen with surge event. |
| Assembly | Improper verification of internal arrangement as per drawings. |





4. Collection of system data and input from field related to situation

- Any additional information like brief history of equipment, last LCM readings, maintenance records etc. were asked from field and final database prepared.

5. Inspection of failed arrestor by dismantling actual arrestor

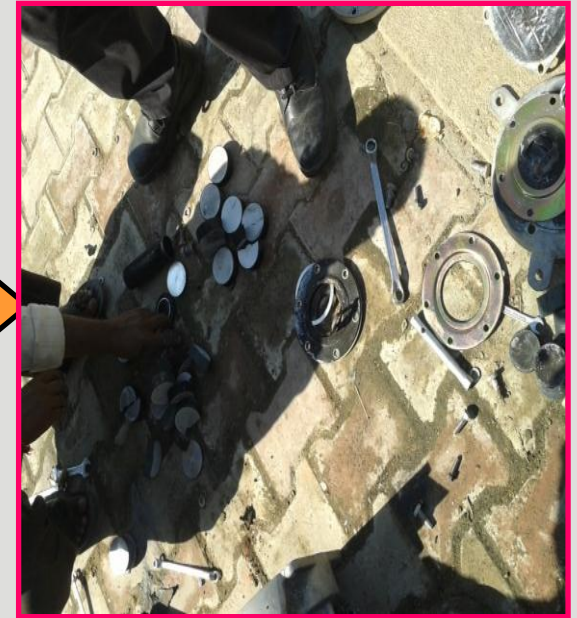
- During site visit each failed SA was dismantled.
- Photographs of various internal & external parts of SA were taken.
- The condition of various parts of SA is matched with the indicators or symptoms given in matrix.
- Some of the photographs of dismantled SAs, pointing out their root causes of failures are shown here.

Moisture Ingress



Green Copper
Oxidation

Cracked Discs



Excessive Internal PD



Multicolor
Growth

Corroded
Internal Parts

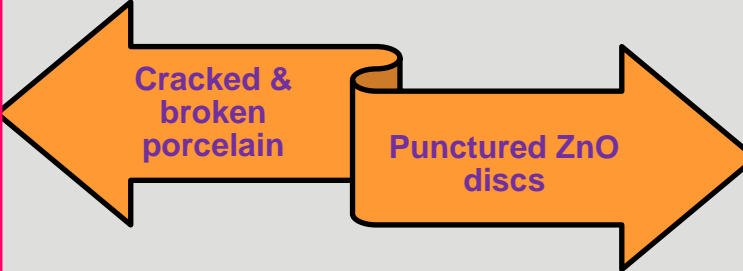


Broken edges
& corners

Discoloration
of internal
parts



Lightning



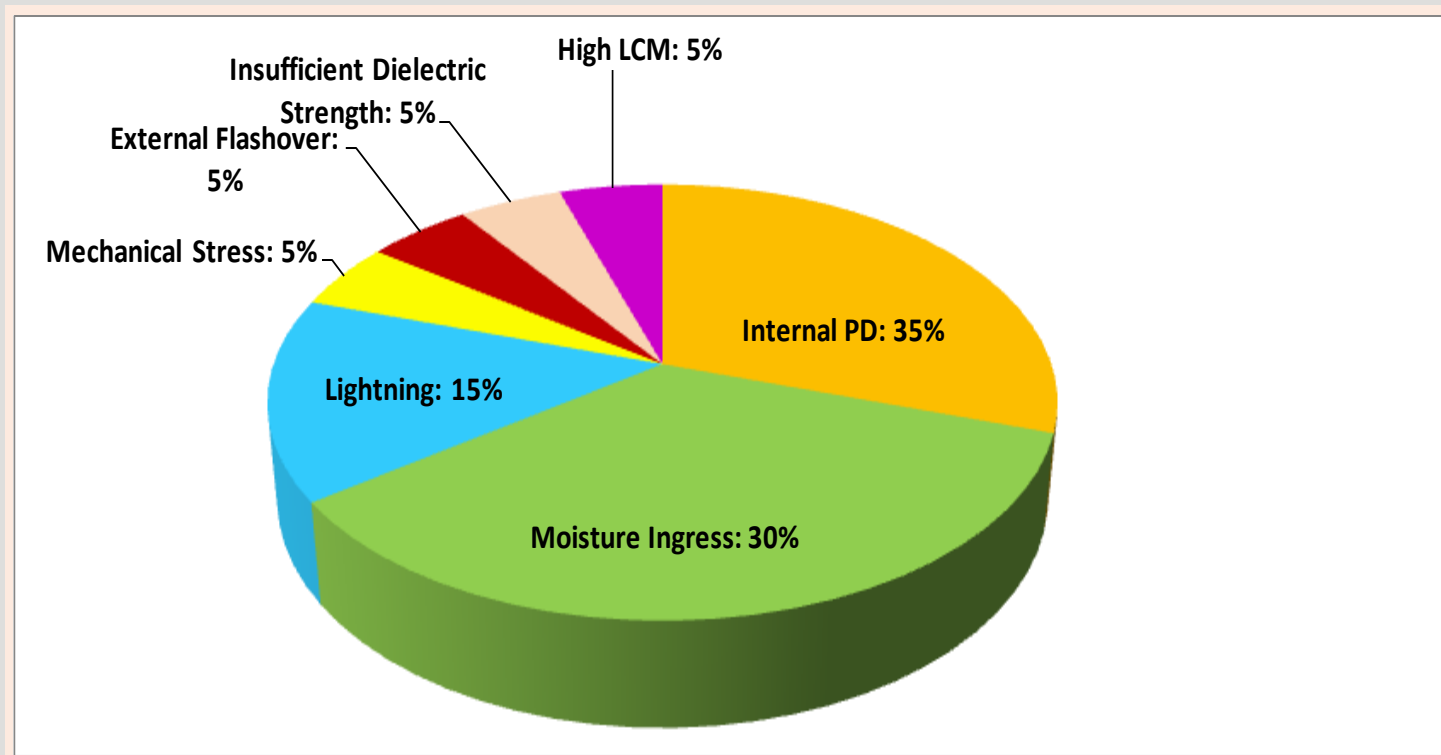
External Flashover



6. Preparation of forensic report and listing out potential root cause

After matching the conditions of failed SA with indicators or symptoms given in the matrix, the potential root causes of 20 nos. of Surge Arrestors are concluded as follows:

Analysis



Various Case Studies:



Case Study -1

60 kV Line SA at 66 kV Chhaya Substation,
Year of Manu.-2010, Failed on 06.09.2013

(A) External Inspection

1) Condition of components:

- Bushing & casting found intake.
- No any flashover marks observed .
- Top end cover plate found open.
- Seal damaged.



2) Indicators of failure:

Sealing at top flange found damaged which indicates possibility of moisture ingress inside surge arrester.

Case Study-1

(B) Internal Inspection:

1) Condition of components:

- ZnO discs found flashover.
- Carbon contamination observed at stack.
- FRP rod found damaged.
- Stack separators and supporters melt partially.
- Spring corroded slightly.
- Gasket found damaged.



2) Indicators of failure:

- Brown rust on metal parts, white rust on aluminium parts, corroded spring and damaged gasket denote entrance of moisture inside.
- Discoloration on some of the discs, multi colored growths on rubber components and colored internal parts were observed which points out possibility of Partial Discharge.

Case Study-1



(C) Root Cause:

Rusting on metal parts and carbon contamination confirm presence of moisture inside surge arrestor. Due to this moisture, partial discharge activity accelerated and finally resulted in thermal runaway of surge arrestor.

Case Study-2

60 KV Line SA at 220 kV Shivilakha Substation,
Year of Manu.-2007, Failed on 24.09.2013:

(A) External Inspection

1) Condition of components:

- Bushing completely broken in pieces
- Both end cover plates damaged

2) Indicators of failure:

Totally broken bushing and end cover plates designate heavy pressure produced inside the surge arrestor.



Case Study-2



(B) Internal Inspection:

1) Condition of components:

- Gaskets totally damaged
- Stack found displaced
- All discs damaged
- Presence of flashover marks on FRP rod
- Stack supporters and few of stack separators partially melted

(C) Root Cause:

There was no lightning stroke at the time of failure but the atmosphere was rainy and humid.

So it is certain that there was an exchange of moist air between atmosphere and surge arrestor which resulted in internal flashover with heavy pressure developed inside.

Due to this acute pressure, bushing was broken into pieces with blast.

Case Study-3

120 KV Capacitor Bank SA at 220 kV Gondal Substation, Year of Manu.-1999, Failed on 02.04.2013:

1) Condition of components:

- Flashover marks on bushing
- Castings ,Terminal connectors and terminal bracket & Support insulators broken.
- Bottom portion of surge arrester damaged completely.

2) Indicators of failure:

Marking of arcs on housing & base envisage possibility of external flashover.



Case Study-3

Root Cause:

As per field report, the surge arrestor was having high leakage current (LCM reading- **444 μA**) which indicates degrading of property of ZnO discs at rated voltage.

Moreover, this surge arrestor was installed at 132 kV **capacitor bank**, so it is prone to frequent switching surges.

In view of this, it can be concluded that during any switching operation the surge arrestor might get failed while withstanding voltage swing and consequently flashed.

Remedial Measures:



Majority of the Surge Arrestors, in quantity, have failed in 66 kV class. So utilities have to focus on manufacturing, quality and system operation aspects, as the 66 kV Surge Arrestors are closed to distribution system.

The following remedial actions are planned by GETCO:

- 1) Condition monitoring data shall be recorded in a **live asset management module** and such in built analysis should bring out defective SAs for replacement.
- 2) Detailed engineering exercise to **select gasket as well as sealing arrangement** is required to be done to improve design.
- 3) GETCO will carry out this exercise **in association with OEMs & material experts**.
- 4) The approach will also be to compare 66 kV SA design with 400/220 kV SA designs, with respect to sealing arrangements, constructional features, gasket material etc.



- 5) It is intended to revise the acceptable limit of Partial Discharge level, measured at 1.05 times Continuous Operating Voltage, from 50 pC to 10 pC.
- 6) GETCO is also looking forward to implement online leakage current monitoring (**Digital Surge Monitoring**) and to integrate the same with substation automation system.

Conclusion:



The high failure rate of Surge Arrestor has been a matter of concern for GETCO in spite of condition monitoring system in place.

This exercise is useful not only to utilities, but also important to OEM to improve upon design & manufacturing process and become consistent in quality.



Thank You !