

Capital Cost Evaluation for Optimum Process Design of Cryogenic Air Separation

Diploma Thesis
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1 Introduction

Air separation technology, or – more generally speaking – gas separation technology, lies at the heart of the modern process industry. Highly pure oxygen and nitrogen are used in many industrial applications. Modern power generation processes, such as the currently developed OXICOAL process, rely on incineration with pure oxygen to produce flue gases with very high carbon dioxide content for further storage. Nitrogen is essential to many widely used processes such as the production of ammonia in the Haber-Bosch synthesis, as fertilizer or in many organic reactions.

2 Air Separation Technology

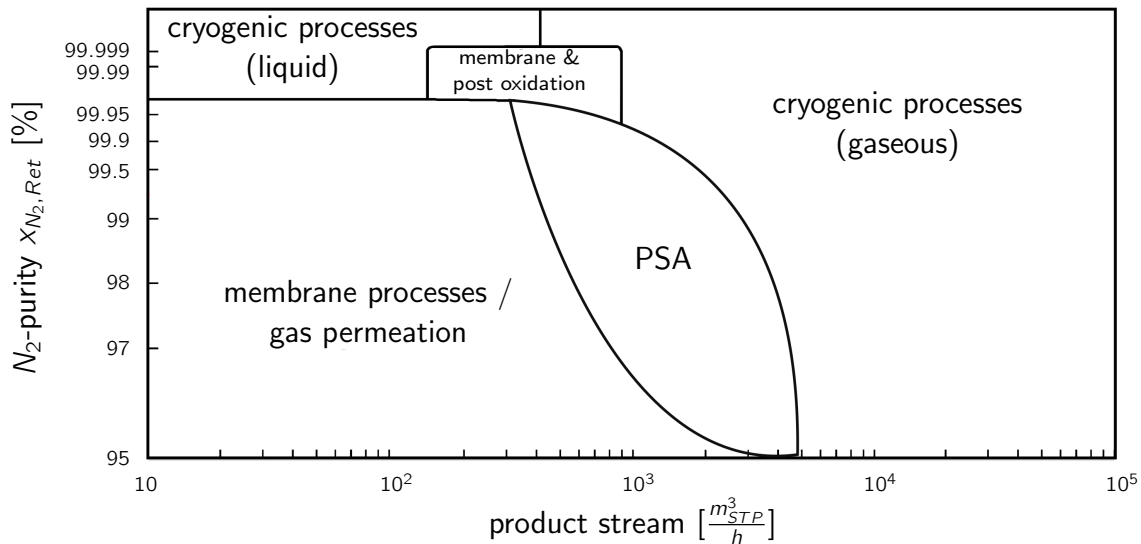


Figure 2.1: Comparison of Air Separation Technologies [3].

There are several ways besides cryogenic air separation that can be employed to separate gas mixtures. In this chapter different competing technologies and their main applications will be discussed. The predominately used technologies are cryogenic distillation, pressure swing adsorption (PSA) as well as gas permeation (GP). In the distillation process the gas is first liquefied. Separation is achieved by the different concentration differences in vapor and liquid phase. PSA relies on the different affinities of gaseous species to adsorb to certain materials in order to extract a component from a mixture. During gas permeation membranes are used. Each species migrates in different quantities through a given membrane depending on process parameters and membrane structure.

Fig. 2.1 illustrates the most economically viable processes depending on product purity and product stream volume. It can be seen that alternative air separation processes cannot supply the high quality or quantity of the cryogenic process. Due to that cryogenic air separation is thought to be the main supplier of highly pure gases in industrial quantities for years to come [1]. The alternative processes however offer some very appealing characteristics, which make them the favorable choice when lower quantities of product or more moderate purity is required. The cryogenic process is always connected with a considerable energy consumption for the liquefaction and compression. Due to that smaller implementations of the process are very unlikely to yield economically sound solutions to a separation problem.

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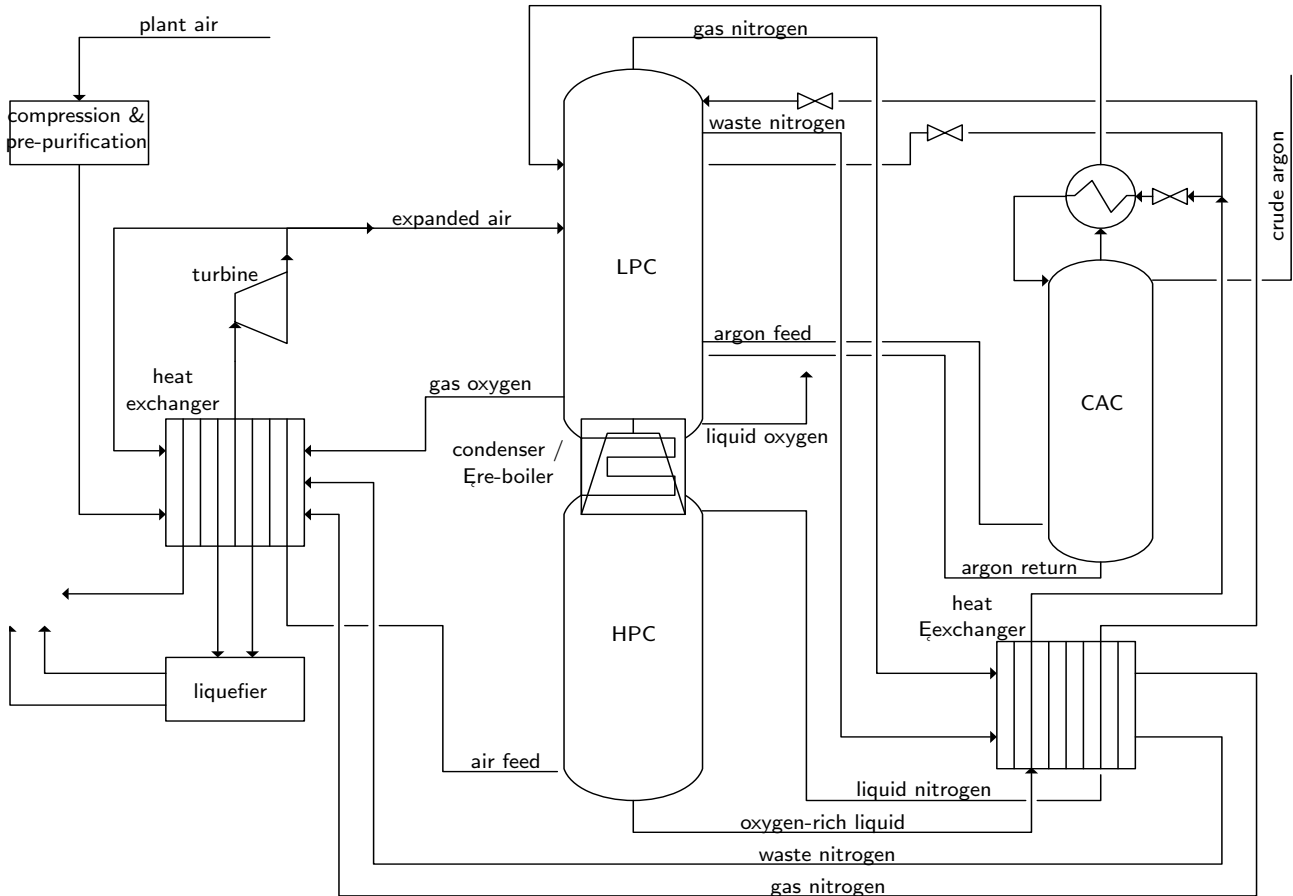


Figure 2.2: Schematic representation of the cryogenic air separation process.

2.1 Cryogenic Air Separation

Cryogenic Air Separation finds applications over a great variety of industries among others refining, petrochemicals, medical, food & beverages and environmental [4]. Furthermore prospective processes for power generation from fossil sources in form of the integrated gaseous combined cycle (IGCC) integrates the air separation process in order to enable more environmentally friendly power generation [2].

As can be seen in Fig. 2.2 double effect heat integrated distillation column lies at the heart of the air liquefaction processes. It consists of a high pressure column (HPC) operating at 0.68 MPa and temperatures below 130 K as well as a low pressure column (LPC) which operates at around 0.13 MPa and comparable temperatures. In order to also attain highly pure argon as a product the process may also include a crude argon column (CAC) which works at slightly lower pressures than the LPC.

The plant air entering the process is initially purified, where carbon and nitrogen oxides as well as solid contaminants are removed, and then compressed to process conditions. The compressed air is then cooled against product streams namely liquefied nitrogen, oxygen and argon. The air stream is then divided into several sub-streams. One of those is fed into the HPC bottom, while another is expanded by means of a turbine and further cooled down through the Joule- Thompson effect. Aside from further cooling energy from the initial compression is thus partially recovered. This expanded air stream is then fed into the LPC. At the bottom of the LPC liquid as well as gaseous oxygen are

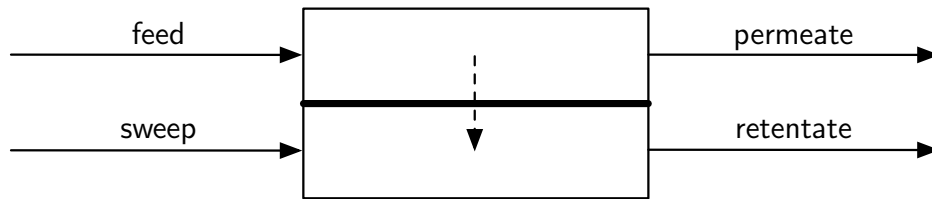


Figure 2.3: Gas permeation process.

recovered as desired products. The bottom and top streams from the HPC are made up of an oxygen rich liquid as well as liquid nitrogen. The liquid nitrogen stream is led through a heat exchanger and fed as reflux into the top of the LPC. The bottom stream is, after heat integration, partially fed into the LPC as well as CAC. From the lower part of the LPC a side stream is drawn and led into the bottom of the CAC. At the same point the reflux from the CAC is fed back into the LPC [5].

2.2 Pressure Swing Adsorption

2.3 Gas Permeation

find paper: DOI: 10.1002/cite.330480804

The separation of mixed gases by membrane process is called gas permeation. Its main strength in comparison with alternative processes are the low energy consumption and the possibility to produce flexible mobile units. As mentioned before it is not however capable of producing high quantity highly pure product streams. As Fig. 2.1 illustrates the main application for the gas permeation process are small to moderate product streams at intermediate purities.

Fig. 2.3 shows the schematic for a single stage membrane unit. Within the feed stream the gaseous mixture is fed into the unit, which can quickly be implemented. Within the unit one or more species migrate favorably through the membrane. In this case mostly dense polymer membranes are employed used. There have been some impressive results with metallic membranes, but due to the very high material costs they have not been adapted by the industry. Furthermore, since gaseous phases often have rather small molecular species, porous membranes cannot achieve desired separation. The driving force for the separation process is a difference in partial pressure or species activity across the membrane. According to the molecular structure of each species, the structure of the separating membrane as well as the process parameters pressure and temperature, they permeate through the membrane in different quantities.

The process of permeation can be subdivided into three separate steps. Sorption at the membrane / feed interface, diffusion through the mostly dense polymer membrane and finally desorption at the permeate side of the membrane.

3 Process Design

3.1 Process Model

3.2 Uncertainty in Process Modeling

3.3 Economic Considerations

4 Cryogenic Air Separation

4.1 Process Model

4.1.1 Distillation Columns

4.1.2 Heat Exchanger

4.1.3 Compressors

4.1.4 Turbine

4.2 Process Economics

5 Conclusion and Further Research

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Bibliography

- [1] W. F. Castle. Air separation and liquefaction: recent developments and prospects for the beginning of the new millennium. *International Journal of Refrigeration*, 25(1):158–172, 2002.
- [2] P. Mahapatra and B. W. Bequette. Process design and control studies of an elevated-pressure air separations unit for IGCC power plants: American Control Conference (ACC), 2010: American Control Conference (ACC), 2010 DOI -. *American Control Conference (ACC), 2010*, pages 2003–2008, 2010.
- [3] R. Prasad, F. Notaro, and D.R Thompson. Evolution of membranes in commercial air separation. *Journal of Membrane Science*, 94(1):225–248, 1994.
- [4] Avinash R. Sirdeshpande, Marianthi G. Ierapetritou, Mark J. Andreovich, and Joseph P. Nau-movitz. Process synthesis optimization and flexibility evaluation of air separation cycles. *AIChE Journal*, 51(4):1190–1200, 2005.
- [5] Yu Zhu, Sean Legg, and Carl D. Laird. Optimal design of cryogenic air separation columns under uncertainty: Selected papers from the 7th International Conference on the Foundations of Computer-Aided Process Design (FOCAPD, 2009, Breckenridge, Colorado, USA. *Computers & Chemical Engineering*, 34(9):1377–1384, 2010.