

# **FOREWORD**

THE SIMBAD NUMERICAL MODEL CAN BE USED TO SIMULATE THE BEHAVIOR OF A MOORED SHIP, USING THE CUMMINS EQUATION (TIME SIMULATION) AND TAKING INTO ACCOUNT THE FOLLOWING ELEMENTS:

- RANDOM WAVE FORCES (FIRST ORDER AND DRIFT FORCES)
- GUSTY WIND FORCES (GENERATION OF WIND SPEEDS ACCORDING TO A WIND SPECTRUM)
- FORCES INDUCED BY A PASSING SHIP
- LINEAR OR NON-LINEAR MOORING CHARACTERISTICS FOR MOORING LINES AND FENDERS,
   AS WELL AS RIGID CONNECTION TYPE MOORING SYSTEM

# **NOTICE**

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#### THE INPUT DATA ARE READ FROM THE FOLLOWING FILES:

## 1. FILES PROVIDED BY THE PRE-PROCESSING PROGRAM (SEE DOCUMENTATION):

- ➤ "HOUL\_IRR.TXT", FOR MAIN CHARACTERISTICS OF SHIP (LENGTH, DRAUGHT, POSITION OF CENTRE OF GRAVITY, MASSES AND INERTIA, HYDROSTATICS, "INFINITY" ADDED MASSES...)
- > "RAD\_IRF.TXT", FOR THE RADIATION DAMPING IMPULSE RESPONSE FUNCTIONS
- > "WAVE\_FOR.TXT" AND "DRIFT\_FOR.TXT" RESPECTIVELY FOR THE WAVE EXCITATION AND DRIFT FORCES TIME SERIES
- "WIND\_VEL.TXT" FOR THE WIND SPEED TIME SERIES

## 2. FILES SPECIFIC FOR THE SIMBAD NUMERICAL MODEL:

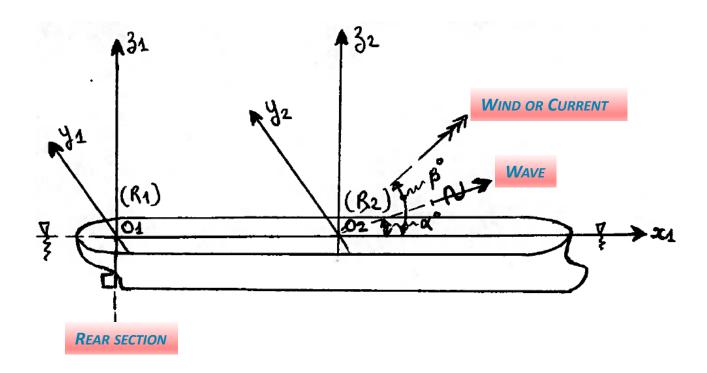
Unlike the previous files, the names of the following files can be changed at the beginning of each run, if necessary:

- > "VENT.DAT", FOR THE WIND CHARACTERISTICS (OTHER THAN DIRECTION AND VELOCITY)
- > "COURANT.DAT", FOR THE CURRENT CHARACTERISTICS
- "AMAR.DAT" FOR THE MOORING SYSTEM
- ➤ "POINT.DAT" FOR A PARTICULAR POINT ABOARD THE SHIP
- "CHENAL.DAT" FOR PASSING SHIP INDUCED FORCES

THESE FILES ARE DESCRIBED IN DETAILS HEREAFTER.

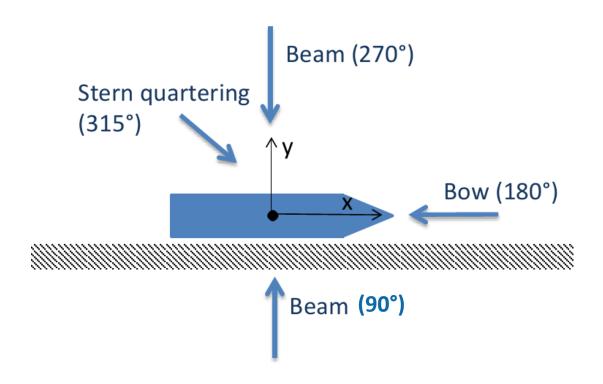
### **COORDINATE SYSTEMS:**

TWO COORDINATE SYSTEMS ARE USED IN THE SIMBAD PROGRAM. THESE COORDINATE SYSTEMS HAVE THE X AXIS POINTING FORWARD, Y TO PORT AND Z UPWARD. THE FIRST FIXED COORDINATE SYSTEM (R1) HAS ITS ORIGIN LOCATED AT THE INTERSECTION OF REAR SECTION, MIDSHIP PLANE AND WATERLINE PLANE. THE SECOND COORDINATE SYSTEM (R2) HAS ITS ORIGIN LOCATED AT THE POSITION OF THE CENTRE OF GRAVITY (WITH ITS X, Y AND Z VALUES SPECIFIED AS PER THE FIRST COORDINATE SYSTEM IN FILE "HOUL\_IRR.TXT").



### **RELATIVE DIRECTIONS OF ENVIRONMENTAL CONDITIONS:**

The relative direction has been defined in the ship axis system in which waves propagating, wind blowing or current flowing in the direction of the positive X2-axis is defined as  $0^\circ$  and waves propagating, wind blowing or current flowing in the positive Y2-axis as  $90^\circ$ 



# RUNNING THE SIMBAD PROGRAM: NAMES OF INPUT FILES AT BEGINNING OF EACH RUN

```
USED FILES:
1 Houl_irr.txt
2 VENT.DAT
3 wind_vel.txt
4 COURANT.DAT
5 AMAR.DAT
6 POINT.DAT
7 CHENAL.DAT
```

**N**AME OF FILE NOT TO BE CHANGED

INPUT FILE NAME THAT CAN BE CHANGED (FILE NAME: 12 CHARACTERS MAX. WITH EXTENSION)

NAME OF FILE NOT TO BE CHANGED

INPUT FILE NAMES THAT CAN BE CHANGED (FILE NAME: 12 CHARACTERS MAX. WITH EXTENSION)

### INPUT FILE "WIND\_VEL.TXT" PROVIDES THE WIND VELOCITY TIME SERIES

210.0000 | RELATIVE WIND DIRECTION 0.00 10.22 13.02 2.00 16.32 4.00 6.00 18.22 8.00 20.16 19.90 10.00 12.00 19.19 14.00 23,30 16.00 18.96 18.00 19.95 20.00 22.05 22.00 16.86 24.00 18.02 26.00 13,48 28.00 15.77 30.00 20.65 32.00 18.27 34.00 18.07 36.00 19.52 16.74 38.00 40.00 18.35 42.00 16.90 44.00 15,13 46.00 20.91 48.00 17.20 50.00 20.08 52.00 20.88 54.00 17.19 56.00 17,49 58.00 16.30 60.00 19.09 62.00 22,00 64.00 17.98 66.00 13.65

WIND SPEED TIME SERIES (TIME IN S VS. WIND SPEED IN M/S). IT IS MANDATORY TO END WITH A NEGATIVE TIME VALUE. THE NUMBER OF TIME STEPS IS LIMITED TO 28800. IF THE SIMULATION TIME IS GREATER THAN THE DURATION OF THE TIME SERIES, THE SERIES IS REPEATED CYCLICALLY. THE DURATION OF TIME SERIES SHALL BE LESS THAN (OR EQUAL TO) THE TOTAL SIMULATION TIME.

# RUNNING THE SIMBAD PROGRAM: INPUT FILE "WIND\_VEL.TXT" PROVIDES THE WIND VELOCITY TIME SERIES (FOLLOWING)

1968.00 17.69 1970.00 17.34 1972.00 21.37 1974.00 16.50 1976.00 19.60 1978.00 18.94 1980.00 15.30 1982.00 13.70 1984.00 10.65 1986.00 11.59 1988.00 16.70 1990.00 11.93 1992.00 10.10 1994.00 11.96 1996.00 10.55 -1

WIND SPEED TIME SERIES (TIME IN S VS. WIND SPEED IN M/S). IT IS MANDATORY TO END WITH A NEGATIVE TIME VALUE. THE NUMBER OF TIME STEPS IS LIMITED TO 28800. IF THE SIMULATION TIME IS GREATER THAN THE DURATION OF THE TIME SERIES, THE SERIES IS REPEATED CYCLICALLY. THE DURATION OF TIME SERIES SHALL BE LESS THAN (OR EQUAL TO) THE TOTAL SIMULATION TIME.

```
123.0000
0.0000000E+00 0.0000000E+00
10000.00 0.0000000E+00
-1 0
```

WHEN THERE IS NO WIND, SUCH AN INPUT FILE WITH A NIL SPEED IS REQUIRED

# RUNNING THE SIMBAD PROGRAM: INPUT FILE "VENT DAT" PROVIDES TH

INPUT FILE "VENT.DAT" PROVIDES THE WIND CHARACTERISTICS

SIDE WIND AREA/FRONT WIND AREA/VESSEL LENGTH/HEIGHT OF SIDE WIND AREA
CENTRE OF GRAVITY ABOVE THE WATERLINE PLANE

			٦.		
5300.000	1320.000	274.0000	8.500000		C,
0.0000000E+00	0.3500000	0.0000000E+00	0.0000000E+00	0.0000000E	+00
10.00000	0.3500000	0.1300000	-2.5000000E-02	-0.3300000	
20.00000	0.2500000	0.2900000	-2.999999E-02	-0.5400000	
30.00000	0.2000000	0.4300000	-7.5000003E-02	-0.8200000	
40.00000	0.2100000	0.5500000	-9.0000004E-02	-1.080000	
50.00000	0.2600000	0.6300000	-0.1150000	-1.240000	
60.00000	0.3000000	0.6800000	-9.0000004E-02	-1.350000	
70.00000	0.2200000	0.7100000	-2.999999E-02	-1.410000	
80.00000	0.1300000	0.7200000	-2.5000000E-02	-1.480000	
90.00000	0.0000000E+00	0.7200000	0.0000000E+00	-1.530000	
100.0000	-5.0000001E-02	0.7100000	1.5000000E-02	-1.490000	
110.0000	-7.9999998E-02	0.6800000	2.9999999E-02	-1.400000	
120.0000	-0.1000000	0.6400000	5.0000001E-02	-1.270000	
130.0000	-0.1500000	0.5500000	7.5000003E-02	-1.100000	
140.0000	-0.2000000	0.4300000	5.0000001E-02	-0.9100000	
150.0000	-0.2500000	0.3000000	3.999999E-02	-0.6200000	
160.0000	-0.3000000	0.1900000	2.9999999E-02	-0.3800000	
170.0000	-0.3500000	9.0000004E-02	1.5000000E-02	-0.2200000	
180.0000	-0.4000000	0.0000000E+00	0.0000000E+00	0.0000000E	+00

RELATIVE WIND DIRECTION (FROM 0° TO 180°) / WIND COEFFICIENTS CX, CY, CN, CK (SEE NOTE HEREAFTER)

#### **N**OTE ON THE WIND FORCES CALCULATION:

THE FOLLOWING FORMULAS ARE USED, RELATIVE TO COORDINATE SYSTEM R2:

SURGE WIND FORCE:  $F_{xv} = \frac{1}{2} \rho_a \cdot C_x \cdot A_l \cdot V^2$ 

SWAY WIND FORCE:  $F_{yy} = \frac{1}{2} \rho_a \cdot C_y \cdot A_T \cdot V^2$ 

YAW WIND MOMENT:  $M_{nv} = \frac{1}{2} \rho_a \cdot C_n \cdot A_T \cdot V^2 \cdot L_{pp}$ 

ROLL WIND MOMENT:  $M_{kv} = \frac{1}{2} \rho_a \cdot C_k \cdot A_T \cdot V^2 \cdot H$ 

WITH:

CX, CY, CN, CK: WIND COEFFICIENTS VS. RELATIVE DIRECTION

V, WIND SPEED (M/S)

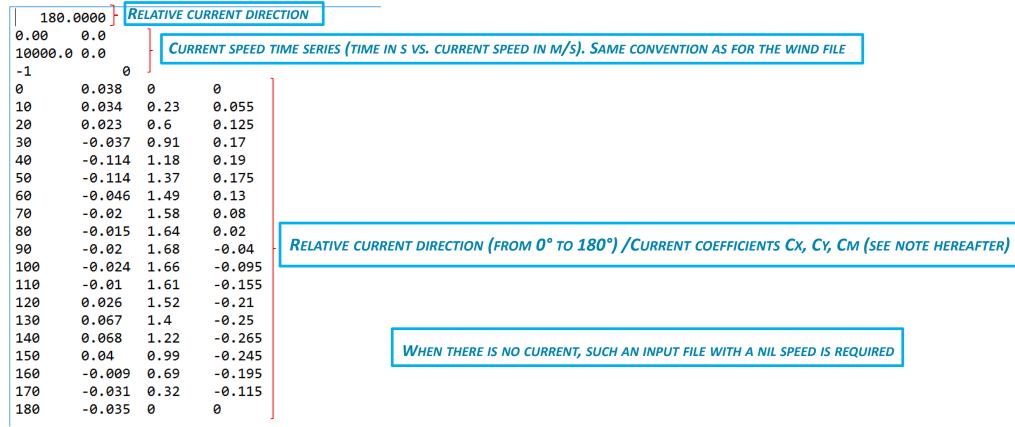
AT, AL: SIDE WIND AND FRONT WIND AREAS (M2)

LPP: SHIP LENGTH (M)

H: HEIGHT OF SIDE WIND AREA CENTRE OF GRAVITY ABOVE SHIP COG

 $P_a$ : AIR DENSITY (KG/M3)

#### INPUT FILE "COURANT.DAT" PROVIDES THE CURRENT CHARACTERISTICS



#### **NOTE ON THE CURRENT FORCES CALCULATION:**

THE FOLLOWING FORMULAS ARE USED, RELATIVE TO COORDINATE SYSTEM R2:

**SURGE WIND FORCE:**  $F = \frac{1}{2} \rho C_F U^2 A_C$ 

**SWAY WIND FORCE:**  $F = \frac{1}{2} \rho C_F U^2 A_c$ 

**YAW WIND MOMENT:**  $M = \frac{1}{2} \rho C_M U^2 A_c L_{pp}$ 

WITH:

CF = Cx , CY: CURRENT COEFFICIENTS IN SURGE OR SWAY VS. RELATIVE DIRECTION

CM = CURRENT COEFFICIENTS IN YAW VS. RELATIVE DIRECTION

**U**, CURRENT SPEED (M/S)

Ac: Current area  $(M2) = LPP \times T$ 

LPP: SHIP LENGTH (M)

T: SHIP DRAFT (M)

P: WATER DENSITY (KG/M3)

INPUT FILE "AMAR.DAT" DEFINES THE MOORING SYSTEM

```
12}
                                                           TOTAL NUMBER OF MOORING LINES AND FENDERS. MAX.: 22
                   4 336500.0 -188320.0 82873.0
       1
       1 0.0000000E+00
 -66,000
              65.50000
                             7.50000
 -15.0000
                5.00000
                              22,0000
 98100.0
             0.0000000E+00
                   4 596520.0 -415490.0 186330.0 -18592.0
       1 0.0000000E+00
 -21,0000
              65.50000
                              7,50000
 -6.0000
           16.50000
                            22.00000
147200.0
             0.0000000E+00
                   4 394520.0 -272190.0 121920.0 -12132.0
       1 0.0000000E+00
              65.50000
                             7.50000
25,00000
1.50000
            18.50000
                            22.00000
123600.0
             0.0000000E+00
                   4 358580.0 -219240.0 97027.0 -9332.8
       1 0.0000000E+00
 93,0000
              29.00000
                             7.50000
 25.0000
              23,00000
                            22,00000
129500.0
             0.0000000E+00
                   4 354470.0 -213390.0 94326.0 -9034.9
       1 0.0000000E+00
151,0000
              29.00000
                             7.50000
221,0000
             23,00000
                            22,00000
 68700.0
             0.0000000E+00
                   4 375670.0 -244040.0 108590.0 -10621.0
       1 0.0000000E+00
221,0000
              65.50000
                             7.50000
252,0000
              13,50000
                            22,00000
 88300.0
             0.0000000E+00
                   4 580970.0 -391990.0 175120.0 -17314.0
       1 0.0000000E+00
263.0000
              65.50000
                             7.50000
262.0000
             10,00000
                            22,00000
132400.0
             0.0000000E+00
                   4 352330.0 -210370.0 92935.0 -8882.0
```

**EACH MOORING LINE OR FENDER DEFINED AS FOLLOWS:** FIRST LINE:

PARAMETER FOR THE TYPE OF CONNECTION: 1 FOR A CLASSIC MOORING LINE. **2** FOR A SPECIFIC CONNECTION, -1 FOR A FENDER

FOR CLASSIC MOORING LINE AND FENDER (PARAMETERS 1 AND -1), THE STIFFNESS MAY BE DEFINED WITH A POLYNOMIAL CURVE UP TO DEGREE 5. DEFINING THE MOORING LOAD AS A FUNCTION OF ELONGATION OR THE **REACTION FORCE AS A FUNCTION OF DEFLECTION, SUCH AS:** 

 $A * x + B * x^2 + C * x^3 + D * x^4$  (x being the elongation or DEFLECTION), THEN FOR A STRONG NON-LINEAR STIFFNESS: INDICATE (DEGREE) 4 (AND COEFFICIENTS:) A (N/M), B(N/M2), C(N/M3), D(N/M4) AND FOR A LINEAR STIFFNESS: (DEGREE) 1 (AND) A(N/M)

A SPECIFIC CONNECTION (PARAMETER 2) IS A UNIT THAT RESPONDS TO THE ERROR IN DISPLACEMENT (X AND Y DIRECTIONS) WITH A REACTION FORCE WITH THE AIM OF GETTING THE UNIT, AND THUS THE SHIP, BACK IN THE NEUTRAL POSITION. THE MODEL OF THE UNITS IS WRITTEN TO CALCULATE THE ANGLE AND MAGNITUDE OF THIS REACTION FORCE. THE ERROR IN DISPLACEMENT IS RUN THROUGH A PID CONTROLLER. THE CONTROL VALUE AND THE ANGLE, DEFINING THE MAXIMUM FORCE, ARE USED TO DETERMINE THE MAXIMUM FORCE. IN ANY CASE, TO PREVENT THE FORCES LARGER THAN THE MAXIMUM FORCE, THE CONTROL VARIABLE HAS A MAXIMUM OF 1. EACH UNIT IS ALLOCATED TO EXERT A SWAY FORCE OF 230 KN AND A SURGE FORCE OF 100 KN. FOR THIS SPECIFIC CONNECTION, THE NUMBER INDICATING THE DEGREE OF THE POLYNOMIAL IS NOW THE NUMBER OF COUPLED UNITS. IT MUST BE FOLLOWED BY AS MANY NIL VALUES AS THERE ARE NUMBER OF UNITS (EXAMPLE: 2 / 0. / 0.)

## INPUT FILE "AMAR.DAT" DEFINES THE MOORING SYSTEM (FOLLOWING)

```
1
                 4 336500.0 -188320.0 82873.0 -7786.7
       1 0.0000000E+00
 -66,000
           65.50000
                           7.50000
 -15.0000
            5.00000
                          22.0000
 98100.0 0.0000000E+00
                 4 596520.0 -415490.0 186330.0 -18592.0
       1 0.0000000E+00
 -21.0000
           65,50000
                          7,50000
 -6.0000 16.50000
                          22.00000
147200.0
           0.0000000E+00
                 4 394520.0 -272190.0 121920.0 -12132.0
       1 0.0000000E+00
          65.50000
                         7.50000
25.00000
1.50000 18.50000
                          22.00000
123600.0 0.0000000E+00
                 4 358580.0 -219240.0 97027.0 -9332.8
       1 0.0000000E+00
93,0000
             29,00000
                         7.50000
25.0000
           23.00000
                          22,00000
129500.0 0.0000000E+00
                 4 354470.0 -213390.0 94326.0 -9034.9
       1 0.0000000E+00
151.0000
           29.00000
                         7.50000
221,0000
           23,00000
                          22,00000
 68700.0 0.0000000E+00
                 4 375670.0 -244040.0 108590.0 -10621.0
       1 0.0000000E+00
221.0000
             65.50000
                          7.50000
252,0000
                          22,00000
           13,50000
 88300.0
            0.0000000E+00
                 4 580970.0 -391990.0 175120.0 -17314.0
       1 0.0000000E+00
263.0000
             65.50000
                         7.50000
262,0000
           10.00000
                          22.00000
132400.0 0.0000000E+00
                 4 352330.0 -210370.0 92935.0 -8882.0
```

**EACH MOORING LINE OR FENDER DEFINED AS FOLLOWS:** 

#### **SECOND LINE:**

A DAMPING MAY BE DEFINED WITH A POLYNOMIAL CURVE UP TO DEGREE 5, AS A FUNCTION OF ELONGATION OR DEFLECTION SPEED. CONVENTIONS ARE THE SAME AS FOR THE INTRODUCTION OF STIFFNESS. IF THERE IS NO DAMPING: PUT 1/0.

#### THIRD LINE:

POSITION OF THE BOLLARD AT QUAY (PARAMETER 1) OR OF FENDER SUPPORT (GENERALLY THE QUAY OR WHARF)(PARAMETER -1), IN THE FIRST FIXED COORDINATE SYSTEM (R1). FOR A SPECIFIC CONNECTION (PARAMETER 2), IT IS THE POINT ON THE SHIP'S HULL WHERE THE CONNECTION IS FIXED.

#### **FOURTH LINE:**

POSITION OF THE MOORING POINT ON-BOARD THE SHIP (PARAMETER 1). IF THERE IS A LONG MOORING LENGTH ON-BOARD THE SHIP, IT IS PREFERABLE TO POSITION THE POINT AT THE FAIRLEAD AND TO TAKE THIS LENGTH INTO ACCOUNT IN THE CALCULATION OF THE STIFFNESS.

FOR A FENDER (PARAMETER -1), IT IS THE POINT ON THE SHIP'S HULL WHERE THE FENDER IS IN TOUCH. ONLY THE Y COORDINATES ARE DIFFERENT BETWEEN THE TWO POSITIONS.

FOR A SPECIFIC CONNECTION (PARAMETER 2), ONLY THE Y COORDINATE DIFFERS FROM THE PREVIOUS POINT AND IT SHOULD BE PLACED 1 M IN FRONT OF THIS POINT.

#### **FIFTH LINE:**

**PRETENSION (IN N) FOR THE MOORING LINE AND PRE-DAMPING, IF ANY.** 

# RUNNING THE SIMBAD PROGRAM: INPUT FILE "AMAR.DAT" DEFINES THE MOORING SYSTEM (FOLLOWING)

```
1 8675000.
       -1
       1 0.0000000E+00
 68,0000
             26.00000
                           5.000000
 68,0000
             23,00000
                         5.000000
0.0000000E+00 0.0000000E+00
                1 8675000.
       1 0.0000000E+00
            26.00000
 93.0000
                           5.000000
                       5.000000
 93.0000
            23.00000
0.0000000E+00 0.0000000E+00
                  1 8675000.
       1 0.0000000E+00
             26.00000
151.0000
                           5.000000
151,0000
             23,00000
                           5,000000
0.000000E+00 0.000000E+00
             1 8675000.
       1 0.0000000E+00
185.0000 26.00000
                           5.000000
185.0000
         23.00000
                       5.000000
0.0000000E+00 0.0000000E+00
       2 2 0.0 0.0
       1 0.0000000E+00
 72,9000
         -15.95000
                         3,000000
 72.9000 -14.95000
                         3.000000
  0.0
        0.0000000E+00
                2 0.0 0.0
       1 0.0000000E+00
102,9000
         -15.95000
                         3,000000
102,9000
            -14.95000
                        3,000000
  0.0
        0.0000000E+00
                 2 0.0 0.0
       1 0.0000000E+00
132,9000
         -15.95000
                         3.000000
132,9000
         -14.95000
                         3.000000
  0.0
        0.0000000E+00
       2 0.0 0.0
       1 0.0000000E+00
162.9000 -15.95000
                         3.000000
162.9000
         -14.95000
                         3.000000
  0.0
        0.0000000E+00
```

**EXAMPLES OF FENDER SYSTEM DEFINITION** 

**EXAMPLES OF SPECIFIC CONNECTION DEFINITION** 

# RUNNING THE SIMBAD PROGRAM: INPUT FILE "POINT.DAT" FOR PARTICULAR POINTS ABOARD THE SHIP

1 148.000 23.0000 26.2500

NUMBER OF PARTICULAR POINTS AND COORDINATES OF EACH POINT IN THE FIRST FIXED COORDINATE SYSTEM (R1)

#### INPUT FILE "CHENAL.DAT" FOR A PASSING SHIP

```
0.0
200.0 0.0
               0.0
                       0.0
204.49 4175.07 0.0
208.97 5365.54 0.0
213.46 7155.45 422.6 0.0
217.94 8945.37 1056.5 0.0
222.43 9540.61 1687.7 0.0
226.92 14310.91 2110.3 0.0
231.40 17291.29 2427.3 0.0
235.89 20271.68 2532.9 0.0
240.38 22656.83 2744.2 0.0
244.86 28621.82 5065.9 0.0
249.35 31006.97 6333.7 -81054.8
253.83 36372.51 6967.6 -188933.6
258.32 42928.51 9923.2 -350897.5
262.81 52469.12 13090.1 -701940.7
267.29 59624.57 16888.1 -971929.2
271.78 67375.26 23010.5 -1349796.3
276.27 77515.32 28921.6 -1835833.8
280.75 87651.16 36945.8 -2348695.2
285.24 95401.84 49401.9 -2969581.1
289.72 102557.30 62489.1 -3779546.3
294.21 96592.31 80222.4 -4400432.2
298.70 82880.85 97113.3 -5075403.3
303.18 48298.27 111891.0 -5129342.6
307.67 7155.45 122445.4 -4589365.8
312.15 -54854.27 128567.8 -3320624.3
316.64 -115078.29 127514.0 -1619784.7
321.13 -172912.94 118224.7 944813.7
325.61 -232541.73 103024.4 4049534.7
330.10 -292166.30 86344.8 6992146.1
334.59 -345830.10 61224.1 9286901.9
339.07 -390548.53 27445.2 11338639.0
343.56 -414995.28 -12667.4 12958423.7
348.04 -419170.35 -55313.0 14038231.6
352.53 -413205.36 -97113.3 14389274.9
357.02 -392933.68 -143556.8 13714303.8
```

Time series of forces induced by passing ship relative to coordinate system R2 (surge force X, sway force Y in Newton and yaw moment M in Nm). It is mandatory to end with a negative time value. The number of time steps is limited to 1000. As there is no ramp-up time for this type of simulation, a "blank time" of about 200s is to be introduced at the beginning of the time series.

```
540.95 -11330.53 0.0 0.0

545.44 -9540.61 0.0 0.0

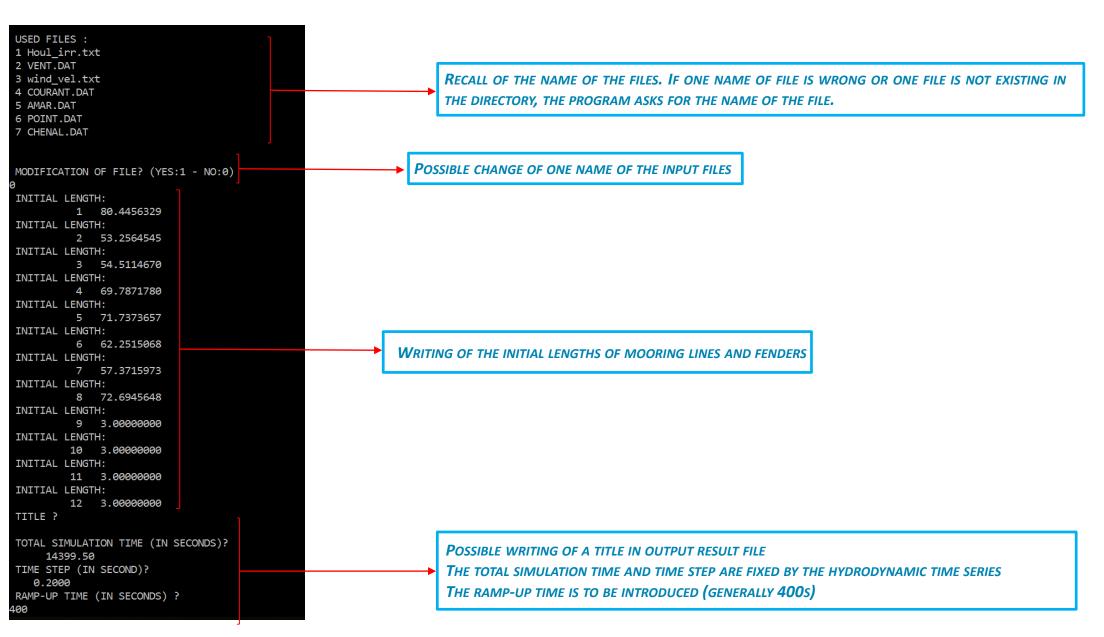
549.92 -7750.69 0.0 0.0

554.41 -6560.22 0.0 0.0

558.89 -4770.30 0.0 0.0

600.00 0.0 0.0 0.0

-1 0.0 0.0 0.0
```



```
TOTAL SIMULATION TIME (IN SECONDS)?
  14399.5000
 TIME STEP (IN SECOND)?
 0.200000003
RAMP-UP TIME (IN SECONDS) ?
*** CALCULATION IN PROGRESS ***
0 ---> PROGRAM EXIT
  ---> WRITING OF RESULTS FILES
                                                           CHOICE OF DIFFERENT OPTIONS (0 IS ALWAYS TO EXIT)
  ---> ADDITIONAL DURATION
  ---> ANALYSIS OF RESULTS
START OF ANALYSIS (IN SECONDS)?
END OF ANALYSIS (IN SECONDS)?
14300
0 ---> PROGRAM EXIT
1 ---> ANALYSIS: TABLE OF RESULTS
                  AVERAGE
                               MIN.
                                            MAX.
                                                        MAX-MIN
                1.702E+01 8.710E+00
                -2.027E-01
                            -8.676E-01
  PITCH (DEG) | -9.075E-04 | -7.916E-01 | 7.733E-01 |
                                                     1.565E+00
```

IF OPTION 3 IS CHOSEN ("ANALYSIS OF RESULTS"), THE START AND END TIME OF THE ANALYSIS ARE REQUESTED. FOR THE END TIME, ALWAYS INDICATE A TIME WHICH IS SHORTER (ABOUT 100s) THAN THE REAL END TIME. TO OBTAIN THE RESULTS OF THE ANALYSIS ON THE SCREEN ("RESULRES" FILE), TAKE OPTION 1 ("ANALYSIS: TABLE OF RESULTS")

# RUNNING THE SIMBAD PROGRAM: OUTPUT FILE "RESULRES" FOR ANALYSIS OF SIMBAD RESULTS

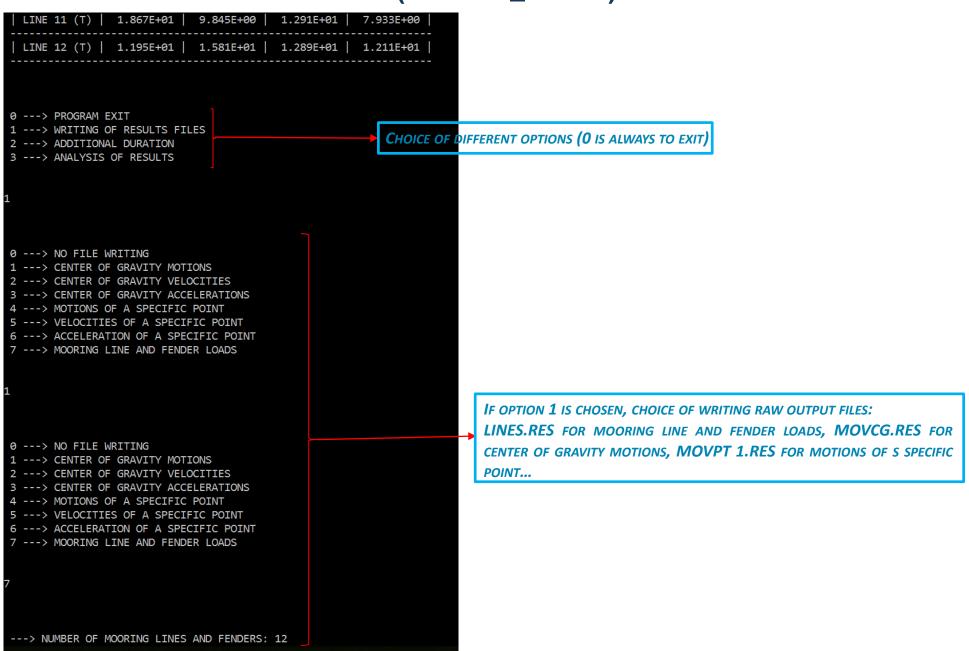
	AVERAGE   MIN.	MAX.	MAX-MIN   RMS
WIND (M/S)	0.000E+00   0.000E+00	0.000E+00	0.000E+00   0.000E+00
SURGE (M)	9.676E-03   -4.941E-02	7.246E-02	1.219E-01   1.924E-02
SWAY (M)	-2.753E-01   -2.676E+00	1.120E+00	3.796E+00   5.058E-01
HEAVE (M)	-1.452E-03   -1.281E+00	1.381E+00	2.662E+00   3.387E-01
ROLL (DEG)	-1.201E-01   -3.810E+00	3.443E+00	7.254E+00   9.614E-01
PITCH (DEG)	1.493E-03   -3.463E-02	4.147E-02	7.609E-02   1.025E-02
YAW (DEG)	-4.091E-02   -4.943E-01	3.937E-01	8.880E-01   1.210E-01
POINT 1	:		
SURGE (M)	2.239E-02   -1.376E-01	1.872E-01	3.248E-01   4.344E-02
SWAY (M)	-2.484E-01   -2.801E+00	1.318E+00	4.119E+00   5.355E-01
HEAVE (M)	-3.842E-02   -1.371E+00	1.237E+00	2.608E+00   3.055E-01
TENSION	:		
LINE 1 (T)	3.118E+01   0.000E+00	1.121E+02	1.121E+02   1.631E+01
LINE 2 (T)	3.187E+01   0.000E+00	1.184E+02	1.184E+02   1.763E+01
LINE 3 (T)	3.126E+01   0.000E+00	1.138E+02	1.138E+02   1.665E+01
LINE 4 (T)	2.588E+01   1.799E+01	4.229E+01	2.430E+01   2.895E+00
LINE 5 (T)	2.823E+01   1.655E+01	5.038E+01	3.382E+01   3.922E+00

DETERMINATION OF AVERAGE, MINIMUM, MAXIMUM AND STANDARD DEVIATION VALUES FOR MOTIONS, MOORING LINE AND FENDER LOADS. BY CONVENTION, MOORING LINE LOADS ARE POSITIVE AND FENDER LOADS ARE NEGATIVE.

	PERIOD 1 (S)  AMPLITUDE 1 PERIOD 2 (S)  AMPLITUDE 2
WIND (M/S)	0.000E+00   0.000E+00   0.000E+00   0.000E+00
SURGE (M)	8.436E+01   2.660E-02   7.816E+01   2.349E-02
SWAY (M)	2.986E+01   5.954E-01   1.427E+01   5.270E-01
HEAVE (M)	1.518E+01   4.266E-01   1.010E+01   3.629E-01
ROLL (DEG)	1.518E+01   1.639E+00   1.427E+01   1.364E+00
PITCH (DEG)	1.010E+01   1.574E-02   1.034E+01   9.014E-03
YAW (DEG)	2.988E+01   5.421E-01   2.610E+01   2.226E-01
POINT 1	:
SURGE (M)	2.988E+01   1.821E-01   2.611E+01   7.044E-02
SWAY (M)	1.427E+01   6.347E-01   1.518E+01   5.984E-01
HEAVE (M)	1.518E+01   2.883E-01   1.701E+01   2.803E-01
TENSION	:
LINE 1 (T)	1.518E+01   1.858E+01   1.427E+01   1.445E+01
LINE 2 (T)	1.518E+01   2.042E+01   1.427E+01   1.623E+01

**DETERMINATION OF MAIN PERIODS AND AMPLITUDES OF TIME-SERIES FROM A FFT PROCEDURE** 

OTHER RAW OUTPUT FILES ARE ALSO AVAILABLE FOR LATER ANALYSIS (SEE HEREAFTER): MOTIONS, SPEEDS, ACCELERATIONS OF THE CENTER OF GRAVITY OR OF A SPECIFIC POINT; MOORING LINE AND FENDER LOADS.



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0 ---> NO FILE WRITING
1 ---> CENTER OF GRAVITY MOTIONS
2 ---> CENTER OF GRAVITY VELOCITIES
3 ---> CENTER OF GRAVITY ACCELERATIONS
4 ---> MOTIONS OF A SPECIFIC POINT
5 ---> VELOCITIES OF A SPECIFIC POINT
6 ---> ACCELERATION OF A SPECIFIC POINT
7 ---> MOORING LINE AND FENDER LOADS
---> SPECIFIC POINT NUMBER: BETWEEN 1 AND 1
                                                                   CHOICE OF DIFFERENT OPTIONS (O IS ALWAYS TO EXIT)
0 ---> NO FILE WRITING
1 ---> CENTER OF GRAVITY MOTIONS
2 ---> CENTER OF GRAVITY VELOCITIES
  ---> CENTER OF GRAVITY ACCELERATIONS
 ---> MOTIONS OF A SPECIFIC POINT
5 ---> VELOCITIES OF A SPECIFIC POINT
6 ---> ACCELERATION OF A SPECIFIC POINT
7 ---> MOORING LINE AND FENDER LOADS
0 ---> PROGRAM EXIT
  ---> WRITING OF RESULTS FILES
2 ---> ADDITIONAL DURATION
3 ---> ANALYSIS OF RESULTS
ANOTHER RUN ? (YES:1 - NO:0)
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