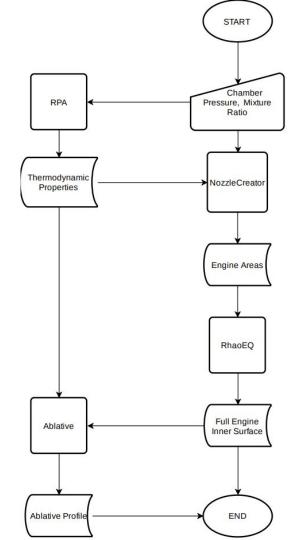


CODE REVIEW

Adam Poklemba

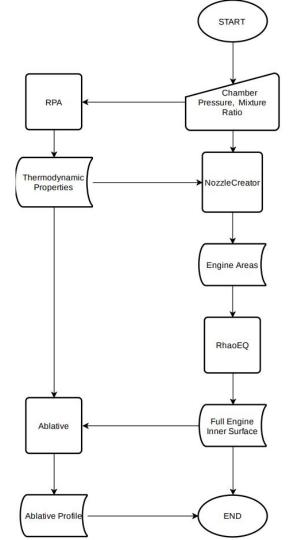
Section one -Engine Design



What this Codebase does

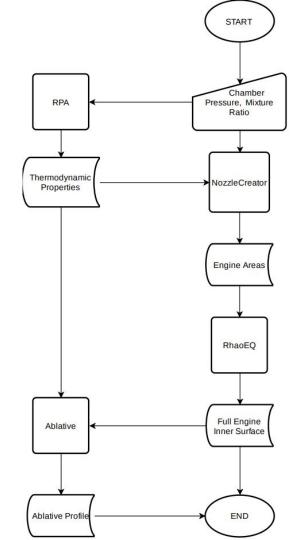
- Take in
 - Values for Chamber Pressure and Mixture Ratio
- Spit out
 - An engine profile and an ablative profile





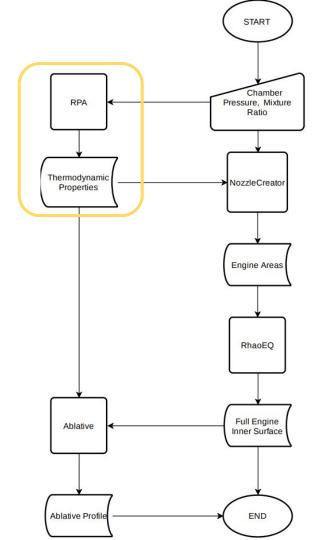
Why is it Like This

- For any given Thrust, PC, MR there exists
 ONE optimal nozzle and a family of optimal profiles
- Fix Thrust -> PC, MR determine system



What is RPA

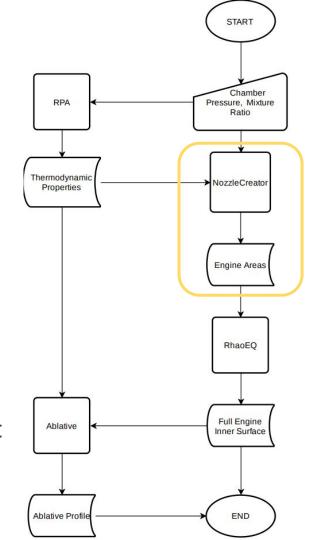
- It is our thermodynamics package
- Designed for rocketry
- Verified data validity over small range using CEA
- Their profiles agree with ours



Defines Throat and Exit Areas



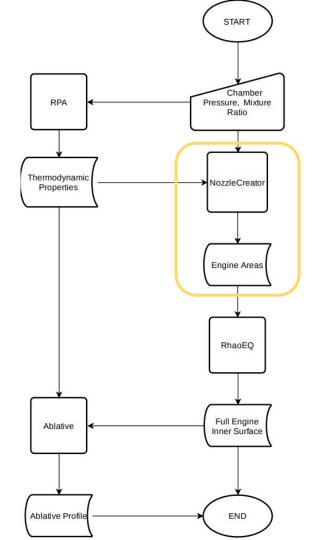
- We are designing around choked flow at A_t
- We assume the gas is radially and axially uniform
- We assume that the gas follows the adiabatic ideal gas law
- All equations are from (1) and (2)



$$C_{f} = \sqrt{\frac{2\gamma^{2}}{\gamma - 1} \left[\frac{2}{\gamma + 1} \right]^{\frac{\gamma + 1}{\gamma - 1}} \left[1 - \left(\frac{p_{e}}{(p_{c})_{ns}} \right)^{\frac{\gamma - 1}{\gamma}} \right]}$$

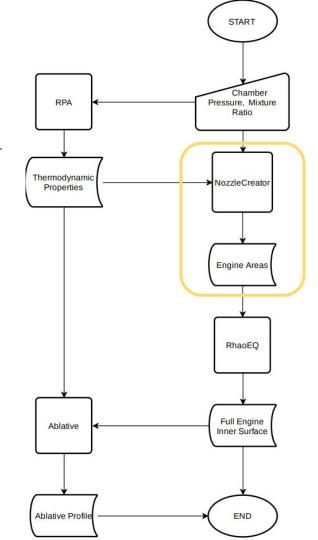
$$+ \epsilon \left[\frac{p_{e} - p_{a}}{(p_{c})_{ns}} \right] \qquad C_{f} = \frac{F}{A_{t}(p_{c})_{ns}}$$

- We get gamma from RPA as a function of (MR,PC)
- This gives us A_t



$$\frac{A_t}{A_x} = \frac{V_t v_x}{V_x v_t} = \left(\frac{k+1}{2}\right)^{1/(k-1)} \left(\frac{p_x}{p_1}\right)^{1/k} \sqrt{\frac{k+1}{k-1} \left[1 - \left(\frac{p_x}{p_1}\right)^{(k-1)/k}\right]}$$

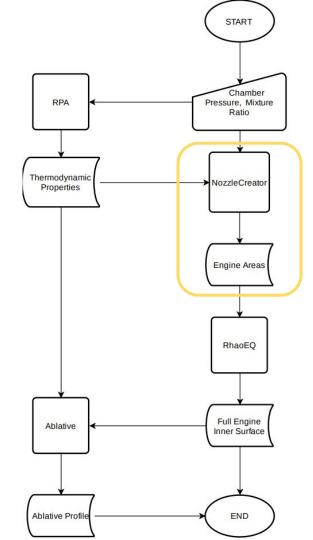
- K is the gamma from before
- P_x is set to exit pressure (1atm)
- P₁ is chamber pressure
- This gives us A_e



$$C_{f} = \sqrt{\frac{2\gamma^{2}}{\gamma - 1} \left[\frac{2}{\gamma + 1} \right]^{\frac{\gamma + 1}{\gamma - 1}} \left[1 - \left(\frac{p_{e}}{(p_{c})_{ns}} \right)^{\frac{\gamma - 1}{\gamma}} \right]} + \epsilon \left[\frac{p_{e} - p_{2}}{(p_{c})_{ns}} \right]$$

$$C_f = \frac{\mathbf{F}}{\mathbf{A}_t(\mathbf{p}_c)_{ns}}$$

- Setting P_e in the EQ gives us thrust as a function of altitude
- Epsilon is A_e/A_t

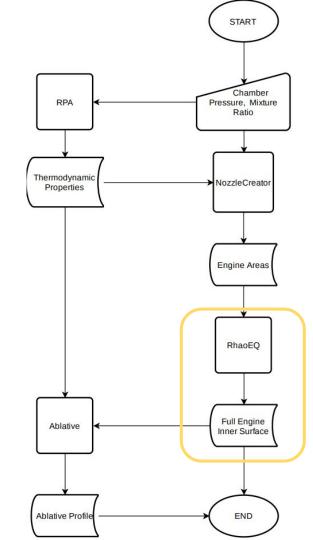


What is RaoEQ

- Defines inner engine surface



- Approximation of a MOC optimal nozzle
- 80% length, 99% efficiency
- All data from (3)



What is RaoEQ: Nozzle

- Arc, Arc, Bezier Curve



$$x = 1.5 R_t \cos \theta$$

$$y = 1.5 R_t \sin \theta + 1.5 R_t + R_t$$

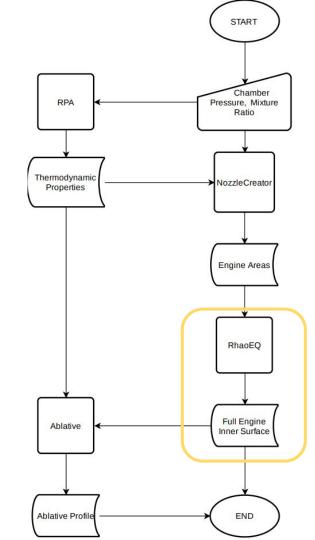
where: $-135 \le \theta \le -90$

$$x = 0.382 R_t \cos \theta$$

$$y = 0.382 R_t \sin \theta + 0.382 R_t + R_t$$

where: $-90 \le \theta \le (\theta_n - 90)$

Converging arc, Diverging arc



What is RaoEQ: Nozzle

- Bezier Curve Definition

$$\begin{split} x(t) &= (1-t)^2 N_x + 2(1-t)t \, Q_x + t^2 E_x &\quad 0 \leq t \leq 1 \\ y(t) &= (1-t)^2 N_y + 2(1-t)t \, Q_y + t^2 E_y &\quad 0 \leq t \leq 1 \end{split}$$

- N is the end of the last arc
- E is the exit of the nozzle
- Q is the intersection of the tangent lines at N and E

 θ_n 35 Parabola angles, degs $-\theta_{\rho}$ 100% 100 Nozzle expansion ratio

The radius of the nozzle exit:
$$R_e = \sqrt{\epsilon} R_t$$
 equ. 2

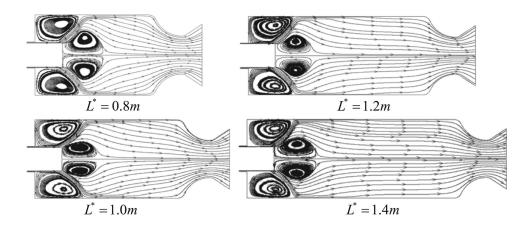
and nozzle length
$$L_N=0.8\left(rac{\left(\sqrt{\epsilon}-1
ight)R_t}{ an(15)}
ight)$$
 equ. 3

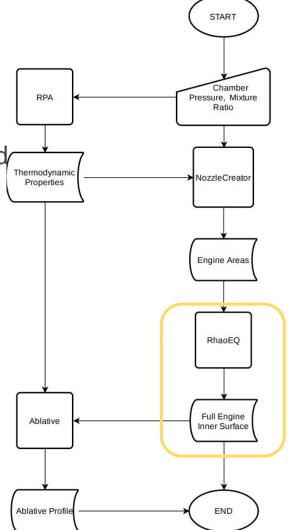
What is RaoEQ: Chamber

 Chamber is a cylinder whose volume is defined by characteristic length L* (4)

- $L*A_t = V_c$

- Set A_c to A_e

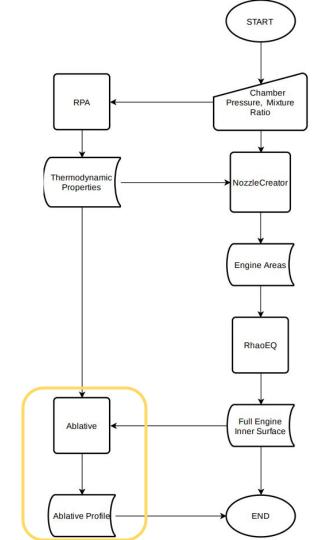




- Defines the thickness of ablative material
- Material parameters from (5)

Thermal Overview

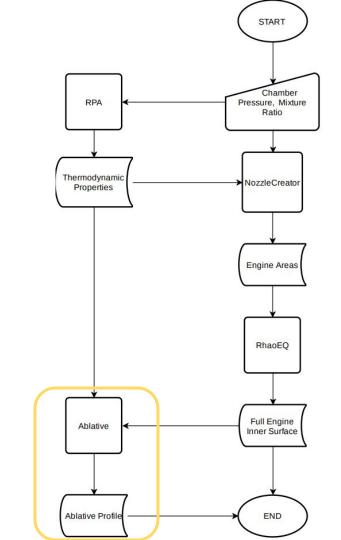
- Material is two-phase: resin and fibre
- Very low thermal conductivity (.9 W/MK)
- Resin vaporises, taking heat away
- Fibre retains structure



The Math

$$\frac{dT}{dt} = \alpha \frac{d^2T}{dx^2} - \frac{H_{vap}\rho \frac{dV}{dt}}{V\rho c_p}$$
$$\rho_0^p \frac{\partial V^p}{\partial t} = -J^p$$
$$\rho_0^c \frac{\partial V^c}{\partial t} = J^p (1 - \Gamma^p)$$
$$J^p = A_0 \frac{V^p}{V_0} \exp\left(-\frac{E_a}{RT}\right)$$

$$Q = h_g(T_{aw} - T^0)$$

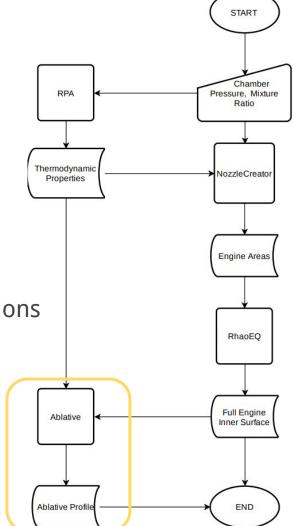


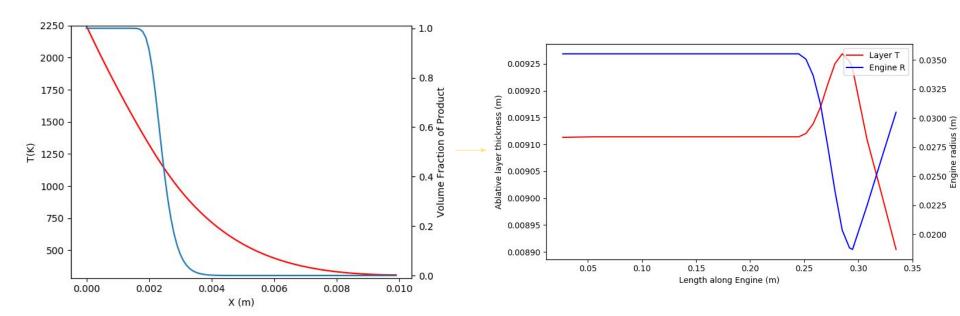
Methodology



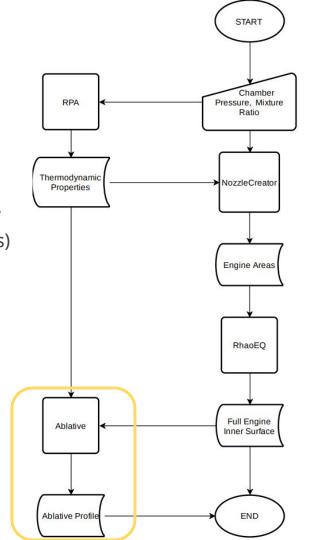
- Split nozzle into toroidal stations

- Split toroidal station into circular hoop stations



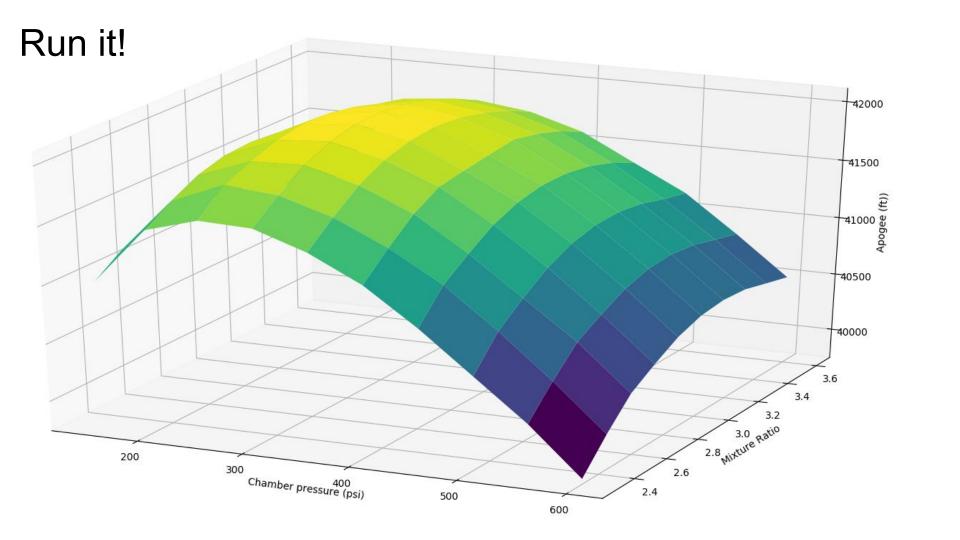


- Underlying assumptions
 - Geometrically imperfect
 - Longitudinal and Tangential q = 0
 - Data from paper was modified to make paper
 consistent with our simulation (real sin hours)
- This code is a heavy WIP
 - Disagrees with Compositex's input



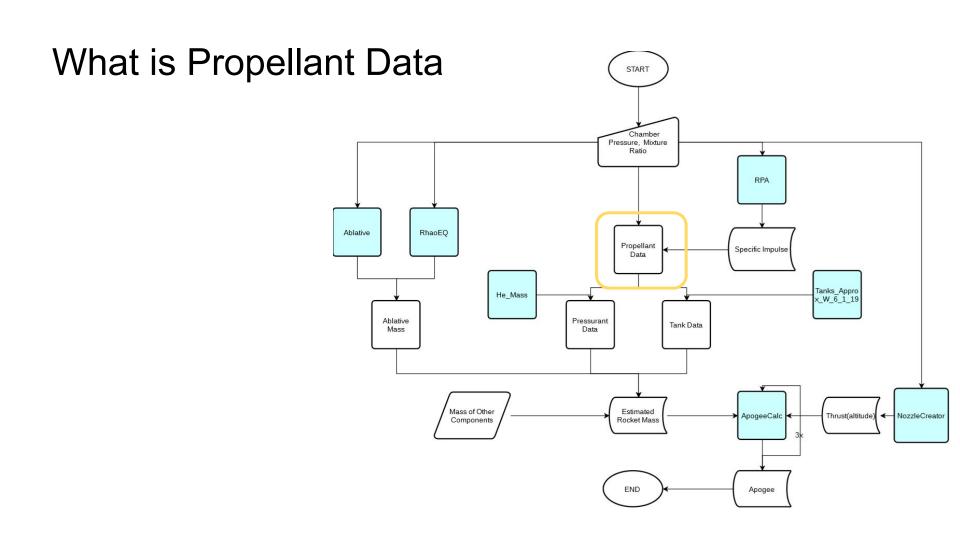
Section Two-**Engine OPT** Chamber Pressure. Mixture **RPA** Ablative RhaoEQ Propellant Specific Impulse Data Tanks_Appro x_W_6_1_19 He_Mass Ablative Pressurant Tank Data Mass Mass of Other Estimated ApogeeCalc Thrust(altitude NozzleCreator Components Rocket Mass

Apogee



Why is it like this START Chamber Pressure, Mixture RPA Ablative RhaoEQ Propellant Specific Impulse Data Tanks_Appro x_W_6_1_19 He_Mass Ablative Pressurant Tank Data Data Mass Mass of Other Estimated ApogeeCalc Thrust(altitude) NozzleCreator Rocket Mass Components

Apogee



What is Propellant Data

$$\dot{m}g\mathrm{Isp} = T$$

 $mg\mathrm{Isp} = I$

$$MR = \frac{m_o}{m_f}$$

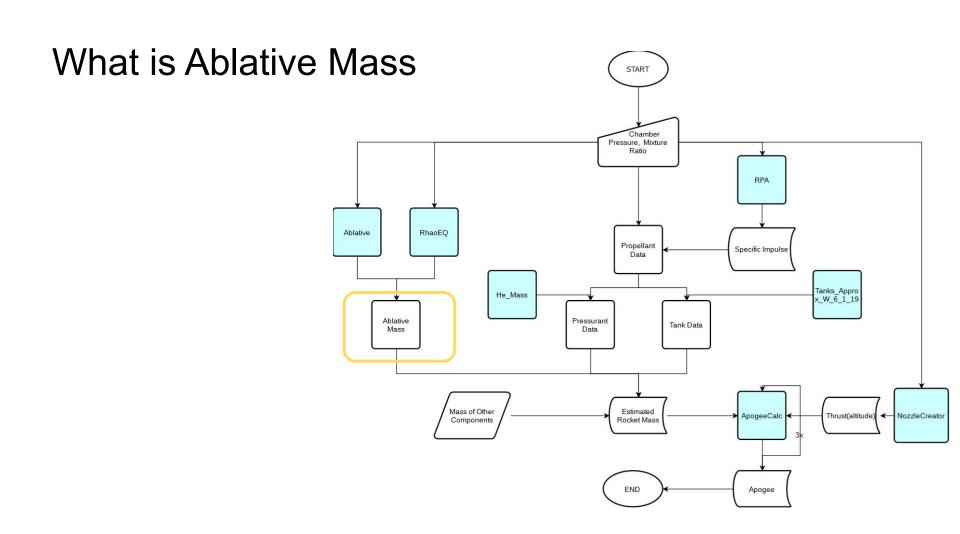
$$m_o + m_f = m$$

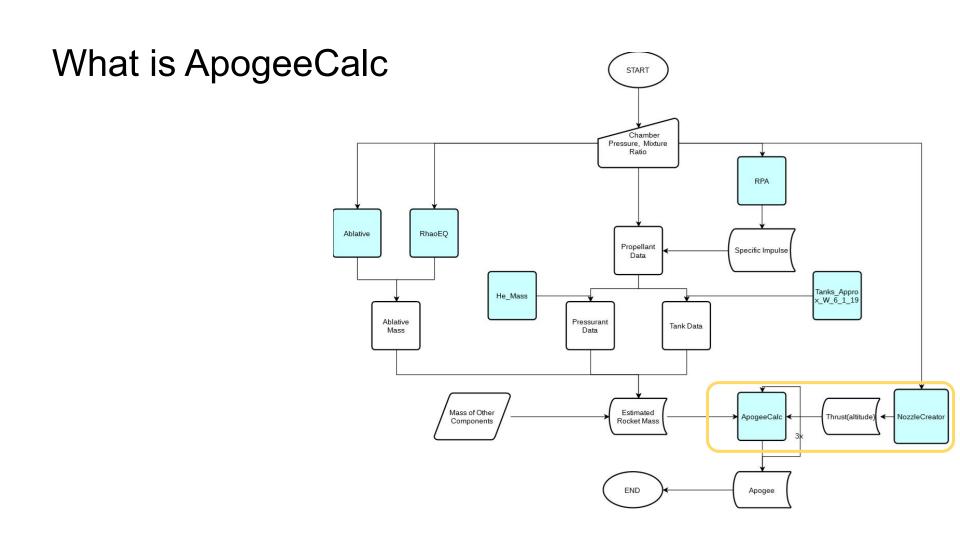
$$m_o = \frac{m}{1 + \frac{1}{MR}} \ m_f = \frac{m}{1 + MR}$$

Takes IN:

- Isp from RPA
- Gives us:
 - Prop mass, Prop volumes

What are Pressurant, Tank Data Chamber Pressure. Mixture RPA Ablative RhaoEQ Propellant Specific Impulse Data Tanks_Appro x_W_6_1_19 He_Mass Ablative Pressurant Tank Data Mass of Other Estimated ApogeeCalc Thrust(altitude) NozzleCreator Components Rocket Mass Apogee





Why do we Repeat Apogee Calc (START) Chamber Pressure, Mixture RPA Ablative RhaoEQ Propellant Specific Impulse Data Tanks_Appro x_W_6_1_19 He_Mass Ablative Pressurant Tank Data Mass of Other Estimated ApogeeCalc Thrust(altitude) NozzleCreator Components Rocket Mass Apogee

Source List

- 1. Rocket Propulsion Elements by Sutton and Biblarz
- 2. Modern Rocket Engine Design by Huzel and Huang
- 3. The Thrust Optimised Parabolic nozzle by Newlands
- Study on atomization and combustion characteristics of LOX/methane pintle injectors by Fang and Shen
- 5. Modeling of one-dimensional thermal response of silica-phenolic composites with volume ablation by Shi, Yi, Fang