

Name: _____ Section: _____

Question 1 [8 marks]

Compute the surface integral

$$\iint_S xy dS$$

over the surface S given by $z = x^2 + y^2$ with $0 \leq x \leq 1$ and $0 \leq y \leq 1$.

$$f(x, y) = x^2 + y^2 \quad f_x = 2x \quad f_y = 2y$$

$$\iint_S xy dS = \int_0^1 \int_0^1 xy \sqrt{1 + (2x)^2 + (2y)^2} dx dy$$

$$= \int_0^1 \int_0^1 xy \sqrt{1 + 4x^2 + 4y^2} dx dy$$

$$= \int_0^1 \left(y (1 + 4x^2 + 4y^2)^{3/2} \frac{2}{3} \frac{1}{8} \Big|_0^1 \right) dy$$

$$= \frac{1}{12} \int_0^1 \left(y (5 + 4y^2)^{3/2} - y (1 + 4y^2)^{3/2} \right) dy$$

$$= \frac{1}{12} \left((5 + 4y^2)^{5/2} \frac{2}{5} \cdot \frac{1}{8} - (1 + 4y^2)^{5/2} \frac{2}{5} \cdot \frac{1}{8} \right) \Big|_0^1$$

$$= \frac{1}{240} \left(9^{5/2} - 5^{5/2} - (5^{5/2} - 1) \right)$$

$$\boxed{= \frac{244 - 50\sqrt{5}}{240} \approx 0.5508}$$

$$= \frac{122 - 25\sqrt{5}}{120}$$

Question 2 [9 marks]Find the surface area of the surface S defined by the parameterization

$$\mathbf{r}(u, v) = (u^2 \sin v \cos v, u \sin v, u \cos v)$$

for $0 \leq u \leq 1$ and $0 \leq v \leq 2\pi$.

$$\vec{r}(u, v) = (u^2 \sin(v) \cos(v), u \sin(v), u \cos(v))$$

$$\vec{r}_u = (2u \sin(v) \cos(v), \sin(v), \cos(v))$$

$$\vec{r}_v = (u^2(\cos^2(v) - \sin^2(v)), u \cos(v), -u \sin(v))$$

$$\begin{aligned} \vec{r}_u \times \vec{r}_v &= \begin{pmatrix} \sin(v)(-u \sin(v)) - u \cos^2(v), \\ - (2u \sin(v) \cos(v)(-u \sin(v)) - u^2(\cos^2(v) - \sin^2(v)) \cos(v), \\ 2u \sin(v) \cos(v) u \cos(v) - u^2(\cos^2(v) - \sin^2(v)) \sin(v) \end{pmatrix} \\ &= \begin{pmatrix} -u, \\ -(-u^2 \sin^2(v) \cos(v) - u^2 \cos^2(v) \cos(v)), \\ u^2 \sin(v) \cos^2(v) + u^2 \sin^2(v) \sin(v) \end{pmatrix} \\ &= (-u, u^2 \cos(v), u^2 \sin(v)) \end{aligned}$$

$$\begin{aligned} \|\vec{r}_u \times \vec{r}_v\| &= \sqrt{(-u)^2 + (u^2 \cos(v))^2 + (u^2 \sin(v))^2} \\ &= u \sqrt{1 + u^2} \end{aligned}$$

$$\begin{aligned} \iint_S dS &= \int_0^{2\pi} \int_0^1 u \sqrt{1+u^2} \, du \, dv \\ &= 2\pi \cdot (1+u^2)^{3/2} \cdot \frac{2}{3} \frac{1}{2} \Big|_0^1 = \frac{2\pi}{3} (2\sqrt{2} - 1) \end{aligned}$$

Question 3 [9 marks]Find the surface integral $\iint_S \mathbf{F} \cdot d\mathbf{S}$ of the vector field

$$\mathbf{F}(x, y, z) = (z - y^2)\mathbf{i} + (xy + z)\mathbf{j} + (x + y)\mathbf{k}$$

over the surface S defined by $z = 2 - 3x^2 - y^2$ for $0 \leq x \leq 1$, $0 \leq y \leq 1$, and with unit normal vector \mathbf{n} pointing in the positive z direction.

$$f(x, y) = 2 - 3x^2 - y^2 \quad f_x = -6x \quad f_y = -2y$$

$$\vec{r}(x, y) = (x, y, f(x, y))$$

$$\vec{r}_x = (1, 0, -6x) \quad \vec{r}_x \times \vec{r}_y = (6x, 2y, 1)$$

$$\vec{r}_y = (0, 1, -2y)$$

$$\iint_S \vec{F} \cdot d\vec{S} = \int_0^1 \int_0^1 (z - y^2, xy + z, x + y) \cdot (6x, 2y, 1) dx dy$$

$$= \int_0^1 \int_0^1 (6x(z - y^2) + 2y(xy + z) + (x + y)) dx dy$$

$$= \int_0^1 \int_0^1 (6x(2 - 3x^2 - y^2) + 2y(xy + 2 - 3x^2 - y^2) + x + y) dx dy$$

$$= \int_0^1 \int_0^1 (13x - 18x^3 - 10xy^2 + 5y - 6x^2y - 2y^3) dx dy$$

$$= \int_0^1 \left(\frac{13}{2}x^2 + \frac{18}{4}x^4 - 5x^2y^2 + 5yx - 2x^3y - 2y^3x \right) \Big|_0^1 dy$$

$$= \int_0^1 \left(\frac{13}{2} + \frac{9}{2} - 5y^2 + 5y - 2y - 2y^3 - (0) \right) dy$$

$$= \int_0^1 (2 + 3y - 5y^2 - 2y^3) dy$$

$$= 2y + \frac{3}{2}y^2 - \frac{5}{3}y^3 - \frac{1}{2}y^4 \Big|_0^1 = 2 + \frac{3}{2} - \frac{5}{3} - \frac{1}{2} = \frac{4}{3}$$

$$\boxed{= \frac{4}{3}}$$

Question 4 [9 marks]Find the surface integral $\iint_S \mathbf{F} \cdot d\mathbf{S}$ of the vector field

$$\mathbf{F}(x, y, z) = x^2 y \mathbf{i} + xz \mathbf{j} + yz \mathbf{k}$$

over the surface S of the sphere of radius 1.

Use the Divergence Theorem

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E \operatorname{div} \vec{F} dV$$

$$= \iiint_E (2xy + 0 + y) dV$$

$$= \int_0^{2\pi} \int_0^\pi \int_0^1 (2(p \sin \phi \cos \theta)(p \sin \phi \sin \theta) + p \sin \phi \sin \theta) \cdot p^2 \sin \phi dp d\phi d\theta$$

$$= \int_0^{2\pi} \int_0^\pi \int_0^1 (2p^4 \sin^3 \phi \cos \theta \sin \theta + p^3 \sin^2 \phi \sin \theta) dp d\phi d\theta$$

$$= \int_0^{2\pi} \int_0^\pi 2\left(\frac{1}{5}p^5\right) \sin^3 \phi \cos \theta \sin \theta \Big|_0^1 d\phi d\theta$$

$$+ \int_0^{2\pi} \int_0^\pi \frac{1}{4}p^4 \sin^2 \phi \sin \theta \Big|_0^1 d\phi d\theta$$

$$= \frac{2}{5} \int_0^{2\pi} \cos \theta \sin \theta d\theta \cdot \int_0^\pi \sin^3 \phi d\phi + \frac{1}{4} \int_0^{2\pi} \sin \theta d\theta \cdot \int_0^\pi \sin^2 \phi d\phi$$

$$\rightarrow \frac{2}{5} \frac{1}{2} \sin^2 \theta \Big|_0^{2\pi} = 0$$

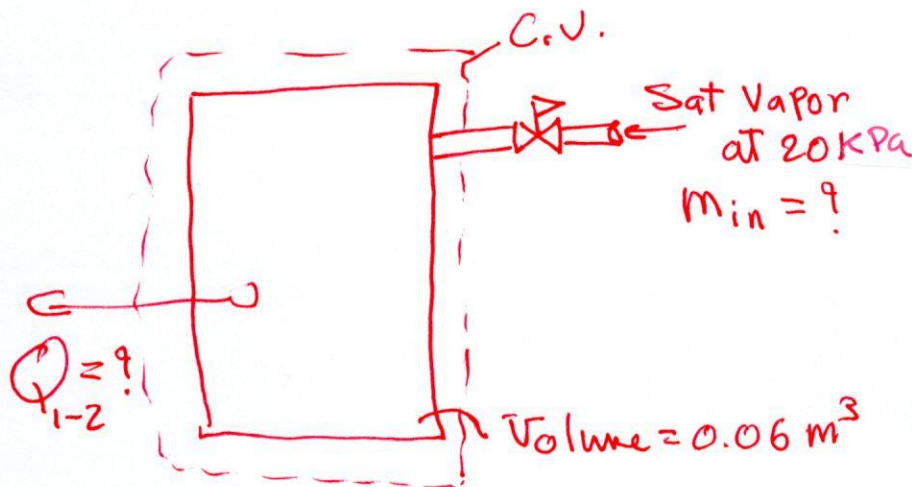
$$\Rightarrow \boxed{\iint_S \vec{F} \cdot d\vec{S} = 0}$$

Solutions

MECH 222-Thermo, Test 5, March 16, 2017

Question 1 (10 marks) A rigid tank has a volume of 0.06 m^3 and initially contains saturated vapor water at a pressure of 20 kPa . As heat is removed from the tank contents, a pressure regulating valve keeps the pressure constant in the tank by allowing saturated vapor to enter. Cooling continues until the quality reaches 15%. Determine:

- (5 marks) The amount of heat transfer, in kJ
- (5 marks) The mass of vapor that enters, in kg



* USUF Process.

* ΔKE and ΔPE negligible

* Work = 0

* Constant Pressure Process.

Initial conditions

Sat. Vapor at 20 bars

Final conditions

two-phase mixture at $x = 15\%$

Sat. Table

$P = 20 \text{ kPa}$

Table B.1.2

$$\left\{ \begin{array}{l} u_g = 2456.71 \\ u_f = 251.35 \\ h_g = 2609.7 \\ v_g = 7.64937 \end{array} \right.$$

$$h_f = 271.90$$

$$v_f = 0.001017$$

Continuity

$$\sum m_{in} - \sum m_{out} = (m_p - m_{init})_{C.V.}$$

$$m_{in} - 0 = m_{p_{final}} - m_{initial}$$

$$m_{initial} = \frac{V}{v_{initial}}$$

$$P_{sat} = 20 \text{ bars}$$

$$v_{\text{initial}} = v_g|_{20\text{bars}}$$

$$m_{\text{initial}} = \frac{0.06}{7.64937} = 7.844 \times 10^{-3} \text{ kg}$$

$$m_{\text{final}} = m_{\text{in}} + m_{\text{initial}} = m_{\text{in}} + 7.844 \times 10^{-3}$$

Energy balance

$$m_{\text{final}} u_{\text{final}} - m_{\text{initial}} u_{\text{initial}} = \cancel{Q_{1-2}} + m_{\text{in}} h_{\text{in}}^o$$

$$u_{\text{final}} = (1-x) u_f + x u_g = 0.85 \times 251.35 + 0.15 \times 2456.71$$

$$u_{\text{final}} = 582.15 \text{ kJ/kg}$$

$$u_{\text{initial}} = u_g = 2456.71 \text{ kJ/kg}$$

$$m_{\text{final}} = \frac{V}{v_{\text{final}}} ; v_{\text{final}} = (1-x) v_f + x v_g$$

$$v_{\text{final}} = (1-0.15) \times 0.001017 + 0.15 \times 7.64937$$

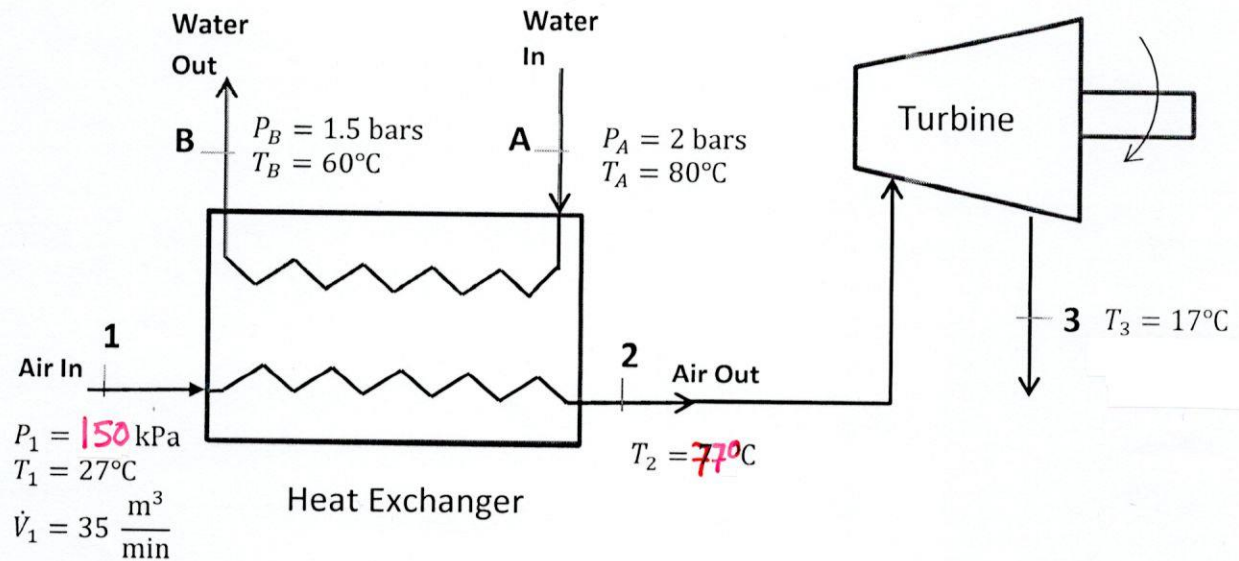
$$m_{\text{final}} = \frac{0.06}{1.148} = 0.052 \text{ kg} \quad v_{\text{final}} = 1.148$$

$$0.052 \times 582.15 - 7.844 \times 10^{-3} \times 2456.71 = Q_{1-2} + [0.052 - 7.844 \times 10^{-3}] \times 2609.7$$

$$\checkmark \underline{Q_{1-2}} = 11 - 115.23 = -104.23 \text{ kJ}$$

$$\checkmark \underline{m_{\text{in}}} = m_{\text{final}} - m_{\text{initial}} = (0.052 - 7.844 \times 10^{-3}) = 0.044 \text{ kg}$$

Question 2 (20 marks) Air as an ideal gas is preheated at steady-state through a heat exchanger before entering a turbine generating power. The processes are shown schematically below. Data for various flow streams are shown on the figure. Heat transfer to surroundings can be neglected.



- (10 marks) Calculate the Turbine power in kW
- (10 marks) Assuming water specific volume is constant ($v = 0.001 \frac{\text{m}^3}{\text{kg}}$); Calculate the mass flowrate of the heating water in kg/s

Assumptions

- * steady state
- * Heat transfer to surroundings negligible
- * ΔPE and ΔKE negligible
- * air behaves as an ideal gas.
- * Water is incompressible with $v = 0.001 \frac{\text{m}^3}{\text{kg}}$ constant.
- * No pressure drop on the Heat exchanger air side

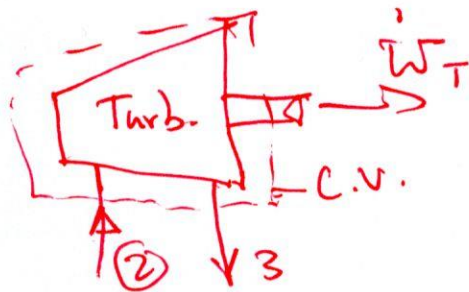
$$\dot{m}_{\text{air}} = \rho_1 \dot{V}_1 = \dot{V}_1 / v_1$$

$$P_1 v_1 = RT_1 \rightarrow v_1 = \frac{0.287 \times 300}{150} = 0.574 \frac{\text{m}^3}{\text{kg}}$$

$$\dot{m}_{\text{air}} = \frac{35}{60} \times \frac{1}{0.574} = 1.016 \text{ kg/s}$$

Table A7.1 \rightarrow $\begin{cases} T_1 = 300 \text{ K} & h_1 = 300.47 \text{ kJ/kg} \\ T_2 = 350 \text{ K} & h_2 = 350.78 \\ T_3 = 290 \text{ K} & h_3 = 290.43 \end{cases}$

air ideal gas



$$\dot{W}_T = \dot{m}_{\text{air}} (h_2 - h_3)$$

$$\dot{W}_T = 1.016 \times (350.78 - 290.43)$$

$$\dot{W}_T = 60.35 \text{ kW}$$

b) $\dot{Q}_{1-2} = -\dot{Q}_{AB}$

$$\dot{Q}_{1-2} = \dot{m}_{\text{air}} (h_2 - h_1) = 1.016 \times (350.78 - 300.47)$$

$$\dot{Q}_{1-2} = 51.1 \text{ kW} = -\dot{Q}_{AB} \Rightarrow \dot{Q}_{AB} = -51.1 \text{ kW}$$

$$\dot{Q}_{AB} = \dot{m}_w (h_B - h_A)$$

Incompressible $h_B \approx u_f|_{T_B} + v P_B$

$$h_A \approx u_f|_{T_A} + v P_A$$

$$h_B = 251.09 + 0.001 \times 150 = 251.24 \text{ kJ/kg}$$

$$h_A = 334.84 + 0.001 \times 200 = 335.04 \text{ kJ/kg}$$

Table B.1.1. $\begin{cases} T_A = 80^\circ \text{C} \\ \Rightarrow u_f = 334.84 \text{ kJ/kg} \\ T_B = 60^\circ \text{C} \\ \Rightarrow u_f = 251.09 \end{cases}$

$$-51.1 = \dot{m}_w (251.24 - 335.04)$$

$$\dot{m}_w = \frac{51.1}{83.8} = 0.61 \text{ kg/s}$$