

Free body diagrams

Vertical force balances:

$$m\ddot{x}_1 + kx_1 - k(x_3 - x_1) = 0$$
  
 $(x_3 - x_1) - Possopt - k(x_2 - x_3) = 0$   
 $\frac{m}{2}\ddot{x}_2 + k(x_2 - x_3) = 0$ 

From 2nd 
$$\Rightarrow x_3 = \frac{x_1 + x_2}{2} + \frac{P \cos w_1 t}{2k}$$

Substitute 
$$m\ddot{x}_1 + \frac{3}{2}kx_1 - \frac{1}{2}kx_2 = \frac{2}{2}\cos \omega_f t$$
 with 1st +3rd  $\frac{m}{2}\ddot{x}_1 - \frac{1}{2}kx_1 + \frac{1}{2}kx_2 = \frac{2}{2}\cos \omega_f t$  equations

In matrix form 
$$\rightarrow \begin{bmatrix} m & 0 \\ 0 & \frac{m}{2} \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} \ddot{x}_2 \cdot k & -k k \\ -k k & k k \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \frac{N}{2} \\ \frac{N}{2} \end{bmatrix} \cos \omega_f t$$

Solution must be true for all t -> cos wft +0

$$X_{1} = \frac{-\frac{1}{2}\left(\frac{m\omega_{f}^{2}-k}{2}-k\right)}{\Delta},$$

$$X_{2} = -\frac{P\left(\frac{m}{2}\omega_{f}^{2} - k\right)}{\Delta}$$

where 
$$\Delta = (\frac{3}{2}k - m\omega_f^2)(\frac{1}{2}k - \frac{m}{2}\omega_f^2) - \frac{1}{4}s^2$$
  
 $= \frac{m^2}{2}\omega_f^4 - \frac{5}{4}mk\omega_f^2 + \frac{1}{2}k^2$   
 $= (\frac{m}{2}\omega_f^2 - k)(m\omega_f^2 - \frac{1}{2})$ 

$$\Rightarrow x_1 = \frac{y_2 x_2}{k - 2m \omega_f^2} \qquad \text{when } \left(\frac{m \omega_f^2 - k}{2}\right) \neq 0$$

$$\Rightarrow \omega_f^2 \neq \frac{2k}{m}$$

For natural frequency calculation, consider free vibrations

set right hand side = 0

$$\longrightarrow \begin{bmatrix} m & 0 \\ 0 & m_k \end{bmatrix} \begin{bmatrix} \ddot{x_i} \\ \ddot{x_2} \end{bmatrix} + \begin{bmatrix} \frac{3}{2}k & -\frac{1}{2}k \\ -\frac{1}{2}k & \frac{1}{2}k \end{bmatrix} \begin{bmatrix} x_i \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Try a harmonic solution  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} \cos \omega t$ 

$$= \frac{\left(\frac{m}{2}\omega^2 - k\right)\left(m\omega^2 - \frac{k}{2}\right) = 0}{\left(\text{from } \Delta\right)}$$

$$\frac{1}{2m}$$
 and  $\frac{2k}{m}$ 

Let the mode shape be 
$$\begin{bmatrix} u \end{bmatrix}$$

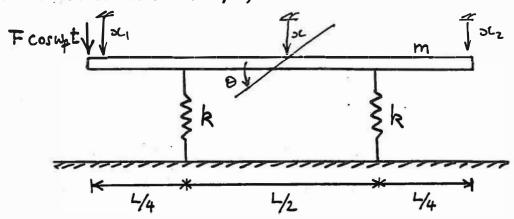
$$= \begin{bmatrix} \frac{3}{2}k - m\omega^2 & -\frac{1}{2}k \\ -\frac{1}{2}k & \frac{m}{2}\omega^2 \end{bmatrix} \begin{bmatrix} 1 \\ u \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

For 
$$\omega^2 = \frac{2m}{k}\omega^2$$

For  $\omega^2 = \frac{k}{2m}$   $\Rightarrow$   $\begin{bmatrix} 1 \\ u \end{bmatrix} = \begin{bmatrix} 1 \\ 2 \end{bmatrix}$ 

The second mode has a nodal point at the junction of the two lower springs. Thus, a harmonic force applied at this point cannot excite this mode. The force can only excite the first mode because this mode does not have a nodal point where the force is applied.

2. A very idealized model of an automobile consists of a uniform slender rod of mass m and length L. The rod is supported at its quarter points by two springs, each of stiffness k. A force  $f(t) = F \cos \omega_t t$  is applied at one end of the rod. Derive an expression for the vibrational displacement at that point. (Hint: The centroidal moment of inertia of a slender rod is  $J = mL^2/12$ )



There are many possible choices of coordinates that are reasonable here. Of course, any choice will work, but a may be more or less convenient.

Coordinate choice 1: - ends of rod.

This choice gives the required displacement directly as X,. However it involves both slynamic and static coupling, as well as awkward expressions for the invertia and spring force.

For upt 
$$m^{\frac{3}{2} + \frac{1}{2}}$$

$$\frac{\sqrt{\frac{1}{4}x_1 + \frac{1}{4}x_2}}{\sqrt{\frac{1}{4}x_1 + \frac{3}{4}x_2}} \times (\frac{1}{4}x_1 + \frac{3}{4}x_2)$$

Put J= 12ml and divide second equation by ==

$$\Rightarrow \begin{bmatrix} \frac{M}{2} & \frac{M}{2} \\ \frac{M}{4} & -\frac{M}{6} \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} + \begin{bmatrix} k & k \\ k/4 & -k/4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F \\ F \end{bmatrix} \cos \omega_F t$$

Solving using

Cramer's rule

$$X_1 = \frac{|F| k - \frac{m}{2} \omega_1^2}{|F| - \frac{k}{4} + \frac{m}{6} \omega_1^2}$$
 $|k - \frac{m}{4} \omega_2|^2 k - \frac{m}{4} \omega_2^2$ 

$$\begin{vmatrix} k - \frac{m}{2} \omega_{p}^{2} & k - \frac{m}{2} \omega_{p}^{2} \\ \frac{k}{4} - \frac{m}{6} \omega_{p}^{2} & -\frac{k}{4} + \frac{m}{6} \omega_{p}^{2} \end{vmatrix}$$

$$X_{1} = \frac{F(-\frac{5}{4}k + \frac{2}{3}m\omega_{4}^{2})}{(k - \frac{m}{2}\omega_{4}^{2})(-\frac{k}{4} + \frac{m}{6}\omega_{4}^{2})}$$
vibration amplitude at force application point.

Static displacement Xo, = X, when we =0

We can see from the denominator that the two natural frequencies are  $w_i^2 = \frac{3k}{2m}$  and  $w_i^2 = \frac{2k}{m}$ 

Coordinate choice 2: - displacement and rotation

This choice gives no at centre of mass dynamic coupling. For this symmetrical system, we also get no static coupling. It and I are the principal coordinates.

Put  $J = \frac{1}{12} mL^2$  and divide second equation by  $\frac{L}{2}$   $\Rightarrow \begin{bmatrix} m & 0 \\ 0 & \frac{L}{6}mL \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{\theta} \end{bmatrix} + \begin{bmatrix} 2k & 0 \\ 0 & \frac{kL}{4} \end{bmatrix} \begin{bmatrix} xl \\ 0 \end{bmatrix} = \begin{bmatrix} F \\ F \end{bmatrix} \cos \omega_{\phi} t$ 

For convenience, define  $y = 0.\frac{L}{2} = displacement of L.H. end$ relative to centre of mass

$$\longrightarrow \begin{bmatrix} m & 0 \\ 0 & \frac{1}{3}m \end{bmatrix} \begin{bmatrix} si \\ jj \end{bmatrix} + \begin{bmatrix} 2k & 0 \\ 0 & \frac{1}{2}k \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} F \\ F \end{bmatrix} \cos \omega_{f} t$$

Try solution  $\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} x \\ y \end{bmatrix}$  cos with for the steady state solution.

Displacement amplitude at LH end = X+1

$$X + 1 = \frac{F(\pm k - \frac{1}{3}m\omega_f^2) + F(2k - m\omega_f^2)}{(2k - m\omega_f^2)(\pm k - \frac{1}{3}m\omega_f^2)} = \frac{F(\frac{5}{2}k - \frac{4}{3}m\omega_f^2)}{(2k - m\omega_f^2)(\pm k - \frac{1}{3}m\omega_f^2)} = X + Y$$

-> same as before.