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4.1.1

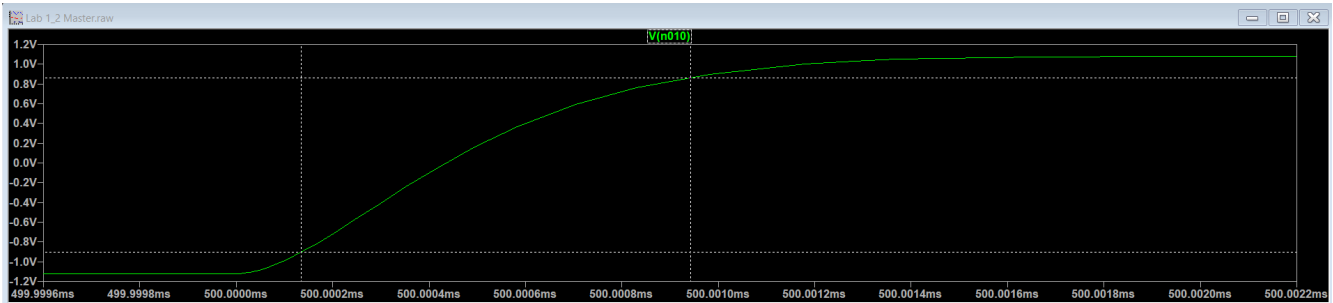


Figure 1: Vo of 0.2V p2p

Steady state = $1.0791816\text{V} - (-1.1206958\text{V}) = 2.1998774\text{V p2p}$

Overshoot = $1.0792908\text{V} = 2.1999867\text{V p2p} \rightarrow \% = 0.0049685\%$

90% = $860\text{mV} \rightarrow t = 500.00094\text{ms}$

10% = $-900\text{mV} \rightarrow t = 500.00013\text{ms} \rightarrow dt = .00081\text{ms}$

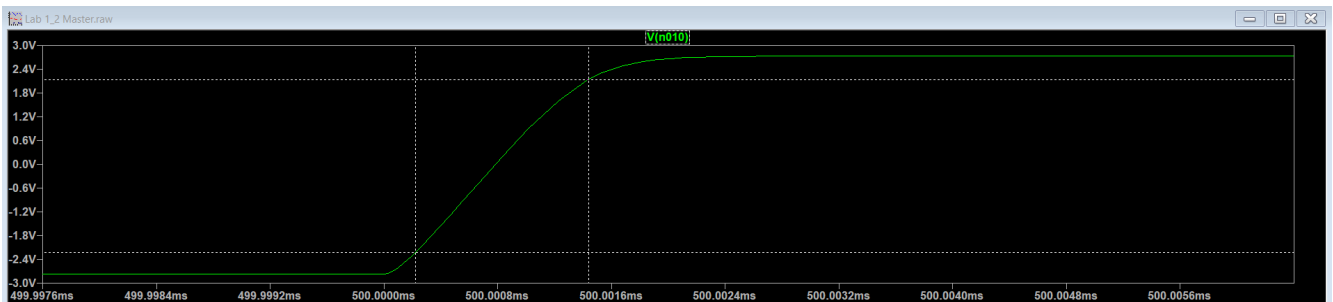


Figure 2: Vo of 0.5V p2p

SS = $2.7290895\text{V} - (-2.7706039\text{V}) = 5.4996934\text{V p2p}$

Overshoot = $2.7292024\text{V} = 5.4998107\text{V p2p} \rightarrow \% = 0.0021328\%$

90% = $2.18\text{V} \rightarrow t = 500.00144\text{ms}$

10% = $-2.22\text{V} \rightarrow t = 500.00022\text{ms} \rightarrow dt = .00122\text{ms}$

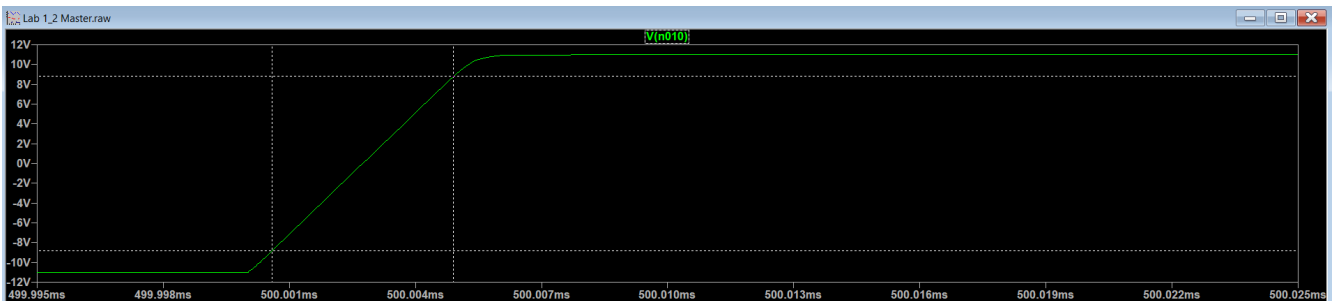


Figure 3: Vo of 2V peak to peak

SS = $10.97863\text{V} - (-11.020144\text{V}) = 21.998774\text{V p2p}$

Overshoot = $11.00192\text{V} = 22.022064\text{V p2p} \rightarrow \% = 0.1058695\%$

90% = $8.79\text{V} \rightarrow t = 500.00490\text{ms}$

10% = $-8.82\text{V} \rightarrow t = 500.00059\text{ms} \rightarrow dt = .00431\text{ms}$



Figure 4: V_o of 5V peak to peak

$$SS = 23.352053V - (-21.552312V) = 44.904366V \text{ p2p}$$

$$\text{Overshoot} = 23.37276V = 44.925072V \text{ p2p} \rightarrow \% = 0.0461113\%$$

$$90\% = 18.86V \rightarrow t = 500.0101ms$$

$$10\% = -17.06V \rightarrow t = 500.00132ms \rightarrow dt = .00878ms$$

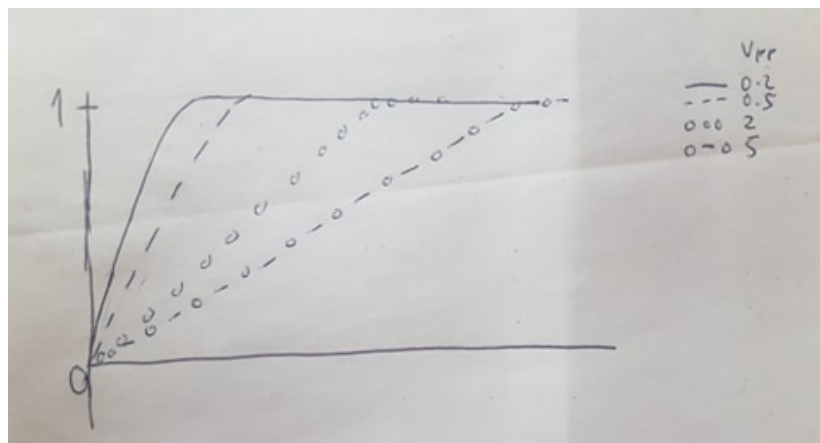


Figure 5: Drawn normalized ramp response of $V_r = 0.2V, 0.5V, 2V, 5V$ peak to peak

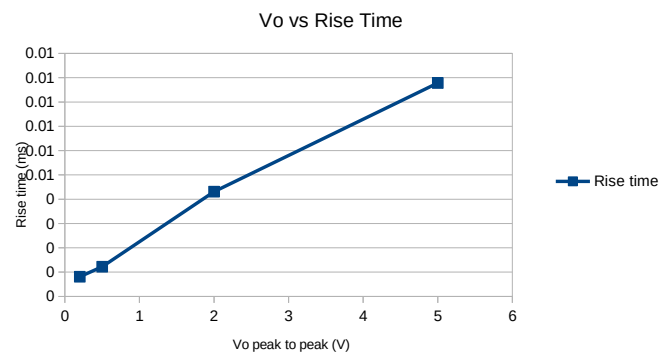


Figure 6: V_o vs rise time plot

It seems that rise time is linearly correlated with input voltage. This makes sense as it would take more time to rise to steady state if input voltage is higher.

4.1.2

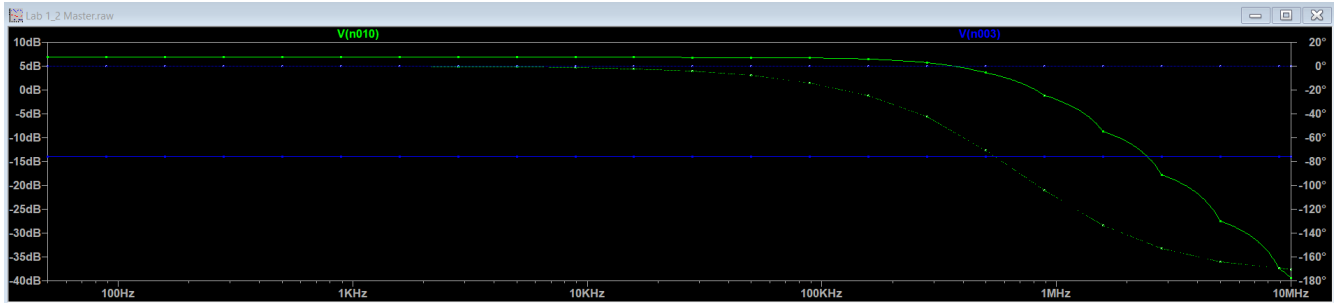


Figure 7: Magnitude and phase shift of V_o (gree) and V_r (blue), ~20 evenly spaced points in log scale

Freq.	Amp(V_r)	Phase(V_r)	Amp(V_o)	Phase(V_r)
5.00E+01	-1.39794000869111e+001dB	3.65415955283620e-011°	6.84796930399518e+000dB	-7.82226816450582e-003°
8.89E+01	-1.39794000869102e+001dB	6.41179539879428e-011°	6.84796922518541e+000dB	-1.39101783850246e-002°
1.58E+02	-1.39794000869074e+001dB	1.09423281561055e-010°	6.84796897596689e+000dB	-2.47361836334302e-002°
2.81E+02	-1.39794000868999e+001dB	1.72588274007045e-010°	6.84796818786744e+000dB	-4.39878450299245e-002°
5.00E+02	-1.39794000868844e+001dB	2.26124546579779e-010°	6.84796569567016e+000dB	-7.82226733954377e-002°
8.89E+02	-1.39794000868648e+001dB	2.19640359662025e-010°	6.84795781462347e+000dB	-1.39101737097464e-001°
1.58E+03	-1.39794000868509e+001dB	1.60979564282671e-010°	6.84793289254070e+000dB	-2.47361571986863e-001°
2.81E+03	-1.39794000868446e+001dB	1.01377282717127e-010°	6.84785408219072e+000dB	-4.39876960141184e-001°
5.00E+03	-1.39794000868423e+001dB	6.16213693078168e-011°	6.84760486429657e+000dB	-7.82218347252086e-001°
8.89E+03	-1.39794000868416e+001dB	3.98413129284320e-011°	6.84681679143969e+000dB	-1.39097019901218e+000°
1.58E+04	-1.39794000868413e+001dB	3.10636049476373e-011°	6.84432491959997e+000dB	-2.47335044444741e+000°
2.81E+04	-1.39794000868411e+001dB	3.27282856427863e-011°	6.83644726452959e+000dB	-4.39727788680390e+000°
5.00E+04	-1.39794000868407e+001dB	4.53163127918395e-011°	6.81155935208278e+000dB	-7.81379582304535e+000°
8.89E+04	-1.39794000868396e+001dB	7.22104275108035e-011°	6.73309303188532e+000dB	-1.38625534669257e+001°
1.58E+05	-1.39794000868362e+001dB	1.17927643835620e-010°	6.48737812743140e+000dB	-2.44688590802319e+001°
2.81E+05	-1.39794000868278e+001dB	1.78938231521920e-010°	5.73574080420971e+000dB	-4.25005110551812e+001°
5.00E+05	-1.39794000868118e+001dB	2.26926989042268e-010°	3.61723092138714e+000dB	-7.03544554287762e+001°
8.89E+05	-1.39794000867907e+001dB	2.12057279637381e-010°	-1.14737172275953e+000dB	-1.04299658873330e+002°
1.58E+06	-1.39794000867771e+001dB	1.20954409519144e-010°	-8.70062751730764e+000dB	-1.33497032545443e+002°
2.81E+06	-1.39794000867755e+001dB	3.98398655824271e-011°	-1.78118053645444e+001dB	-1.52731072608755e+002°
5.00E+06	-1.39794000867770e+001dB	-4.81279650966443e-012°	-2.75182384551393e+001dB	-1.63855431469172e+002°
8.89E+06	-1.39794000867786e+001dB	-3.90113419046287e-011°	-3.74212734144427e+001dB	-1.69695236766898e+002°
1.00E+07	-1.39794000867790e+001dB	-4.65011374385602e-011°	-3.94520754791024e+001dB	-1.70421645504360e+002°

Table 1: Values from ramp response

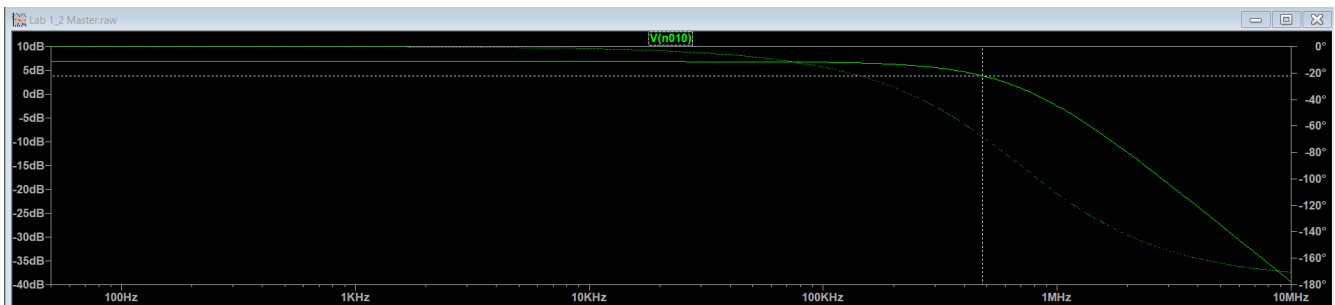


Figure 8: V_r magnitude and phase shift

SS = 6.85dB

ss - 3dB = 3.85dB \rightarrow Freq = 480kHz

This is very different from the calculated 2.28e6 Hz. This could result from some bad estimation from PA13 response plot.

4.2.1



Figure 9: Vio ramp response

$$SS = 67.42\text{mV} - (-70.02\text{mV}) = 137.45\text{mV}$$

$$t(v = -70.02\text{mV}) = 499.9757\text{ms}$$

$$0.63 \cdot SS = 16.57\text{mV} \rightarrow t(16.57\text{mV}) = 503.32871\text{ms}$$

$$dt = 352.01\mu\text{s}$$

$$\text{Time constant from prelab} = 1/3200 \text{ s}^{-1} \rightarrow t = 312.5\mu\text{s}$$

Observed time constant and calculated time constant are approximately equal.

4.2.2

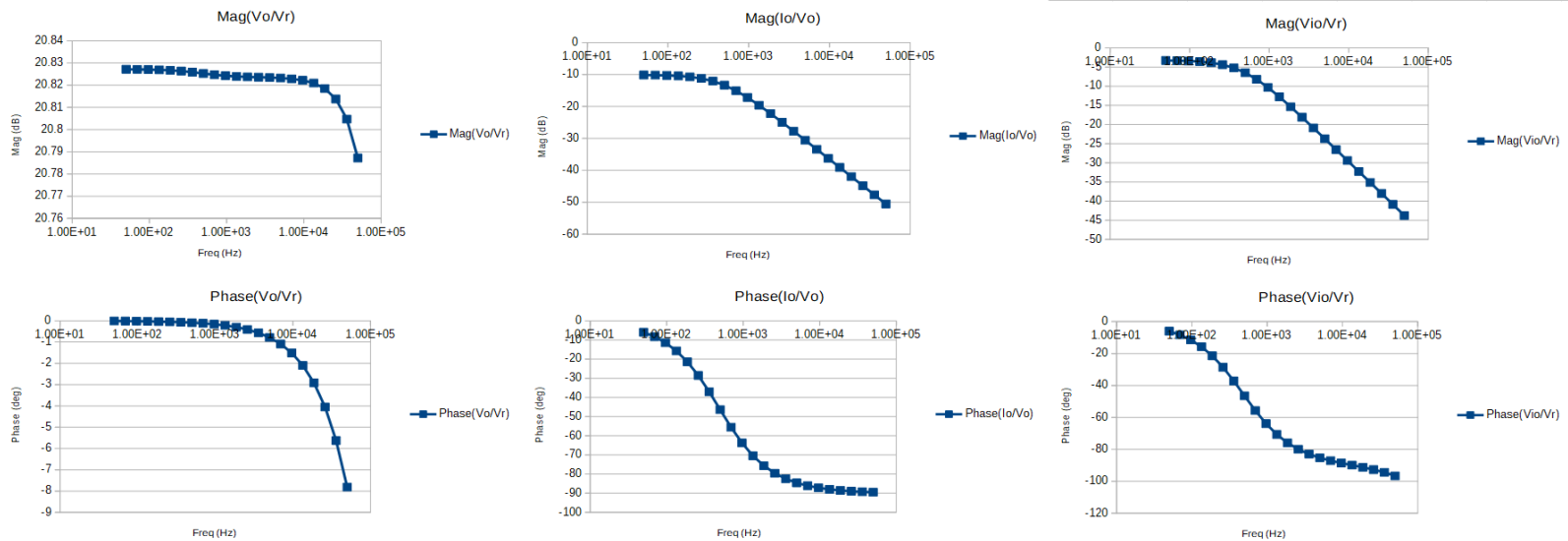


Figure 10: Frequency responses

Based on prelab, we can see that function of $I_o/V_o = 1/(R+sL) = a/(1+s/b)$. Looking at the plot, we can see that $a = -10\text{dB} = .316$ and $b = 3000 \text{ Hz}$, approximately. This results in $R = 1/a = 3.16\Omega$, and $L = 1/(ab) = .00105\text{H}$; both values are approximately same as given in lab manual.

4.3

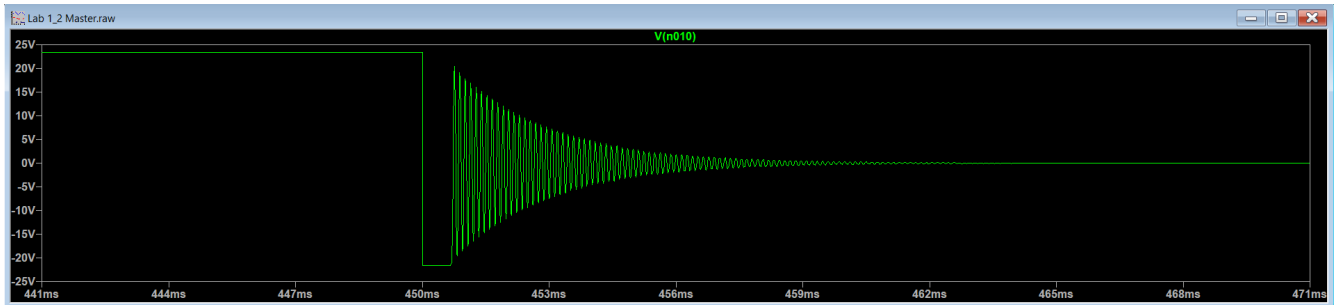


Figure 11: Response with added capacitor

Adding a capacitor causes circuit to behave like a RC circuit, where current can't drop to 0V suddenly, and so there's a sinusoidal, curved discharge.