One-port Elements

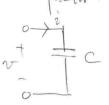
· Voltage Source

. Current Souce

· Resistor

$$Z = R$$

. Capactor.

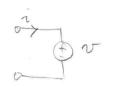


$$Z = \frac{Cs}{L}$$

o port

- · A pair of terminals that must comy the same current through the element.
- · power through a port: P= v.a (Check the polarity):

ex)
$$v = -vi$$
 $v = -vi$ $v = +vi$

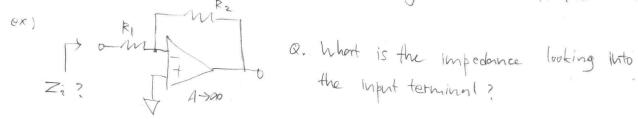


* Impedance seen "looking into" a part

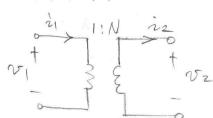
It means the apparent impedance between the two terminals

· Impedance seen. "looking Into" a terminal

It means the apparent impedance between a particular terminal of interest and the common (ground) of the circuit.







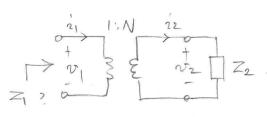
Block Piagroum:

$$V_1$$

$$v_2 = R \hat{z}_1$$

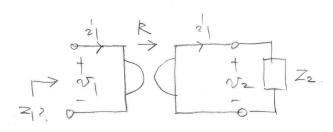
$$\dot{z}_2 = \frac{1}{R} v_1$$

o Impedance Transformation.



$$V_1$$
 V_2
 V_2

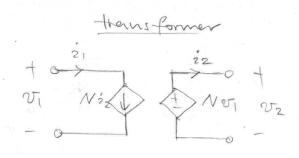
$$\begin{aligned}
\chi &= \frac{21}{V_1} = \frac{N^2}{Z_2} \\
Z_1 &= \frac{2}{21} = \frac{Z_2}{N^2}
\end{aligned}$$



$$\begin{array}{c|c}
 & V_2 \\
\hline
 & V_1 \\
\hline
 & V_2 \\
\hline
 & Z_2 \\
\hline
 &$$

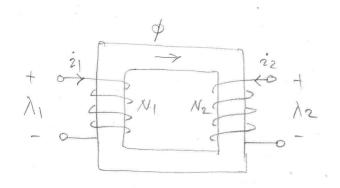
$$Z_1 \triangleq \frac{V_1}{2} = \frac{R^2}{Z_2}$$

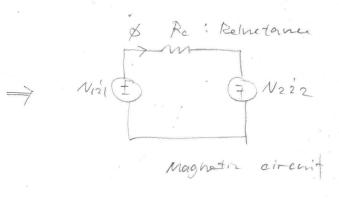
Alternative Representations. (using dependent sources)



$$rac{Giykator}{v_1}$$
 $rac{21}{Ri_2}$
 $rac{22}{Ri_1}$
 $rac{22}{Ri_1}$
 $rac{22}{Ri_2}$

· Transformer Modeling





Terminal variables & Flux linkage > Cornert 2

Terminal Relations:
$$\begin{bmatrix} \lambda_1 \\ \lambda_2 \end{bmatrix} = \begin{bmatrix} L_{11} & L_{12} \\ L_{21} & L_{22} \end{bmatrix} \begin{bmatrix} \dot{z}_1 \\ \dot{z}_2 \end{bmatrix}$$

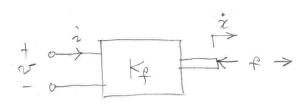
Votage Relation:
$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \frac{d}{dt} \begin{bmatrix} \lambda_1 \\ \lambda_2 \end{bmatrix} = \begin{bmatrix} N_1 \frac{d\phi}{dt} \\ N_2 \frac{d\phi}{dt} \end{bmatrix} \Rightarrow \begin{bmatrix} v_1 = v_2 \\ N_1 & \overline{N_2} \end{bmatrix}$$

* assuming he leakage

Contract Relation: Rep = Nis1 + N222 As undo Rodo = Nizi + Nziz =0



· Voice Coll.

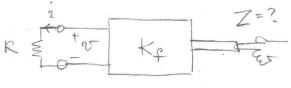


$$(Port)$$
 (Pin)
 $f \cdot \dot{x} = v \dot{n}$

Block Diagram

· Brushed DC Motor.

- Note that these elements behave like "multi-domain gyrator"
- · Apparent damping.



Suppose you connected a resistor across the two terminals of a voice coil.

Ignoring Its Internal Inductornae (L=0).
What is the mechanical impedance you
"feel" at the mechanical port?

$$Z = \frac{F}{\dot{x}} = \frac{K\rho^2}{R}$$
 2> "Apparent damping".

As RV, you feel more damping.

· Mechanical Impedance.

- . We can define mechanical impedance at a "mechanical port"
- · "port" is a channel of power flow.

When you push a doshpot with your finger (with force of & velocity is) the area of contact becomes a mechanical port.

Power Into your finger: -fx
power into the dashpot: fx

The ratio between the force and velocity, i.e. $\frac{f}{x^2}$ can be defined as mechanical impedance.

Here, $Z = \frac{f}{x^2} = \frac{bx}{x^2} = b$.

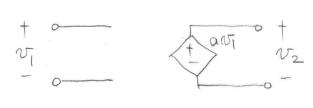
· Dynamiz Stiffness.

For mechanical systems where we care more about "position" than velocity, it is more convinient to use the concept of dynamic stiffness. $K = \frac{F}{X}$ Here, $K = \frac{bx}{x} = bs$, $s \in \mathbb{C}$.

Note: many people use the word "Mechanical Impedance" for.
"Dynamiz stiffness", We should check the meaning from the context.

o Two-port Elements (Active: Amplifier)

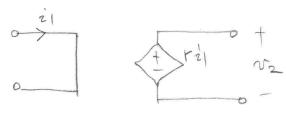
· Voltage - controlled Voltage Source.



V2 = a. VI



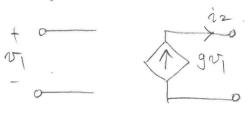
· Current-controlled Voltage Source



Nz = r.21

t: trans impedance [2]

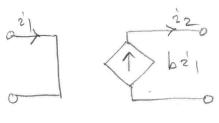
· Voltage - controlled Current Source



12 = 9 VI

9: transconductorne [2]

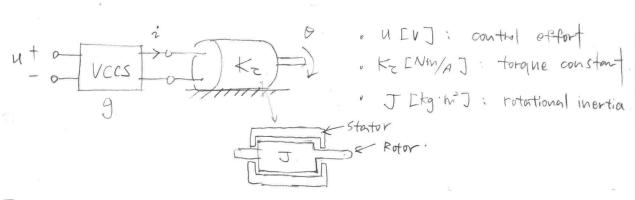
· Current - controlled Current Source



12 = 6.21

b: current gain [-]

- Q1. What is the output impedance of vccs when the Input terminals are shorted? (Answer 1 00)
- Q2. A brushed be motor is driven with a VCCS.



Find the transfer function from U [V] to O [rad].

(Answer: teg)

o Inter connection Constraints

: Kirchhoff's Voltage Law
$$(KVL)$$
 : $\sum_{k=1}^{n} v_k = 0$

· Node Method.

apply KCL to each of the nodes.

- Collect all the equations and solve for the unknown voltages.

ex)

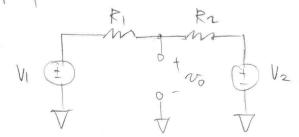
$$V_1 \leftarrow V_2$$

$$\dot{z}_1 = \frac{v_0 - V_1}{R_1}, \quad \dot{z}_2 = \frac{v_0 - V_2}{R_2}$$

$$v_0 = \frac{R_2}{R_1 + R_2} V_1 + \frac{R_1}{R_1 + R_2} V_2$$

It is a shre-fire way to solve linear circuit, BUT the complexity in algebra builds up rapidly & it does not help you build intuition.

o Superposition Method.



$$rospasse when
$$V_{2} = \frac{R_{2}}{R_{1}+R_{2}} \cdot V_{1} + \frac{R_{1}}{R_{1}+R_{2}} \cdot V_{2}$$

$$respasse when
$$V_{2} = 0 \qquad V_{1} = 0$$$$$$

o Thevenin Equivalent Circuit.

You are asked to solve for vo

$$V_1 \oplus V_2$$
 $V_1 \oplus V_2$

Would you solve this circuit from schartch?

OR is there a more elegant way to re-use the provious result?

- The venin Voltage (V+h) is open-circuited. V+h = $\frac{R_2}{R_1 + R_2}$ V_1 + $\frac{R_1}{R_1 + R_2}$ V_2

2> Which we already know.

- The venin Impedance (2th)

: the impedance looking into the port when all the independent sources are turned off $R + C = R + R + R = \frac{R + R + R}{R + R}$

Rth = RIII R2 = RITR2. 27 which we come quickly figure out via inspection.
Thus, the original circuit problem can be simplified to

Thus, the original circuit problem can be simplified to $\frac{Z_{th}}{V_{th}} = \frac{Z_{i}}{Z_{i}^{2} + Z_{th}^{2}} \cdot \nabla f_{h}$ Where $\sum_{i=1}^{N} V_{i} = \frac{Z_{i}^{2}}{Z_{i}^{2} + Z_{th}^{2}} \cdot \nabla f_{h}$

$$= \frac{Z_1^2 + R_1 ||R_2|}{Z_1^2 + R_1 ||R_2|} \left(\frac{R_2}{R_1 + R_2} V_1 + \frac{R_1}{R_1 + R_2} V_2 \right)$$

Therenin Egulvalent circulity.

Note that Theren's equivalent tells us the equivalent system only in terms of the port voltage and current.

For example. Fower dissipation from the original circuit and that from the Therenin equivalent can be different.

$$V_1 \stackrel{R_1}{=} V_2$$

$$V_1 \stackrel{R_2}{=} V_2$$

$$V_1 \stackrel{R_1}{=} V_2$$

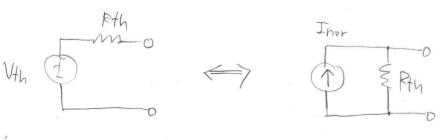
$$V_2 \stackrel{R_1+R_2}{=} V_3$$

$$V_3 \stackrel{R_1+R_2}{=} V_4$$

$$V_4 \stackrel{R_1}{=} V_5$$

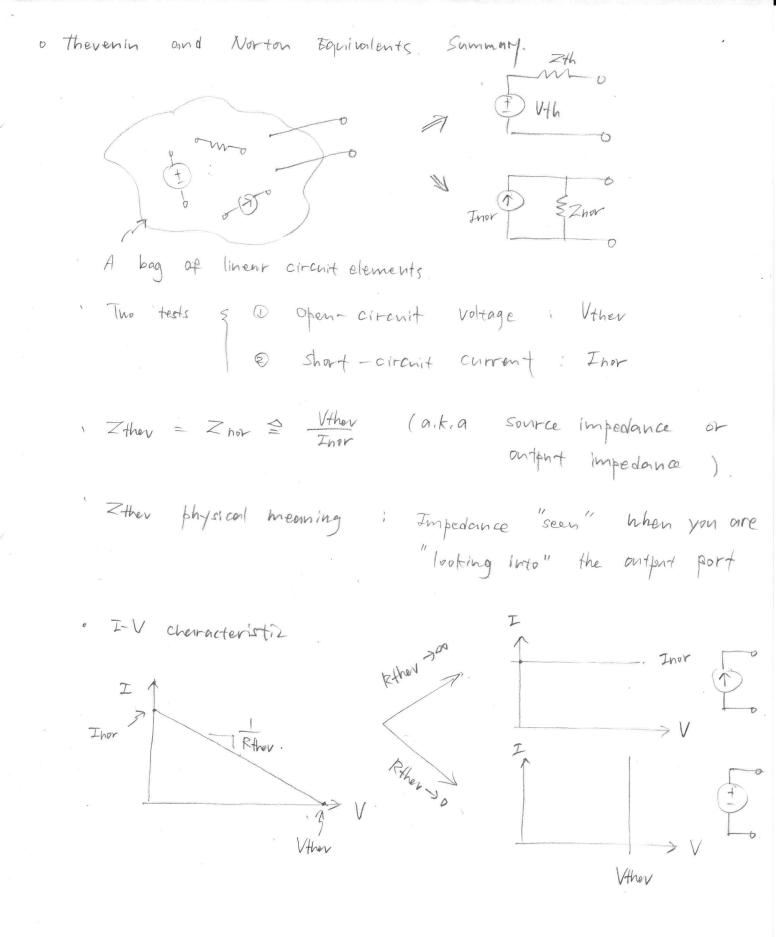
$$V_5 \stackrel{R_1+R_2}{=} V_5$$

o Norton Equivalent Circuit.

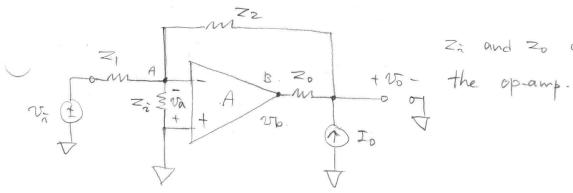


" Short-Circuited Current"

Goffil in magnetic circuits



Example I: Inverting Amplifier with finite Zi, Zo, and A



Zi and Zo are pulled art of the op-amp.

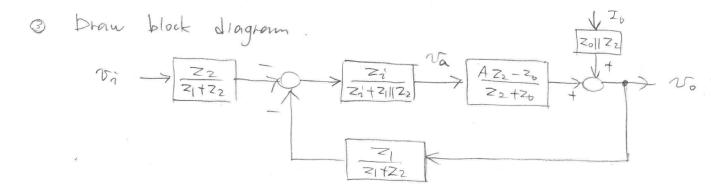
1 Find vo via superposition.

$$-v_{a} = \frac{Z_{2}}{v_{b}} - v_{a} = \frac{Z_{0}}{v_{b}} - v_{a} + \frac{Z_{2}}{v_{b}} + \frac{Z$$

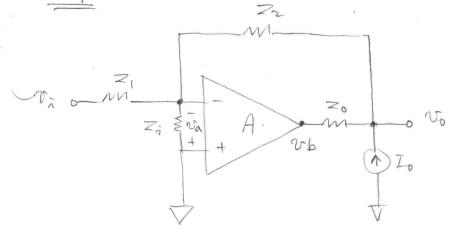
@ Find Va Via Thevenin method

$$\frac{z_{2}}{v_{n}} = \frac{z_{2}}{v_{n}} = \frac{z_{2}}{v$$

$$V_{th} = \frac{Z_2}{z_{1}+Z_2} v_n + \frac{z_1}{z_{1}+z_2} v_0$$



solved with Node Method.



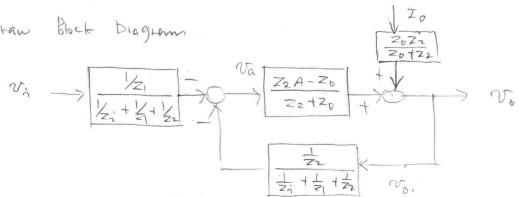
Find No Via Node Method

$$\frac{v_0 - v_0}{z_0} + \frac{v_0 + v_0}{z_2} = I_0$$

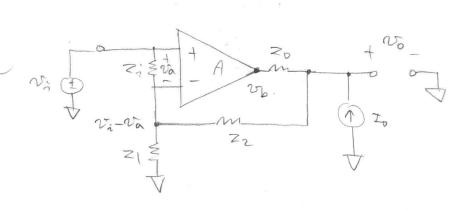
3 Find va via Node Method

$$\frac{v_a}{z_i} + \frac{v_i + v_a}{z_1} + \frac{v_0 + v_a}{z_2} = 0$$

@ Draw Block Diagram



Example I: Non-Inverting Amplifier with finite Zi, Zo, and A:



Zi and Zo are pulled and of the op-amp.

1) Find vo via superposition.

$$\frac{Z_{0}}{V_{0}} = \frac{Z_{2}}{Z_{2}+Z_{0}} \frac{V_{0}}{V_{0}} + \frac{Z_{0}}{Z_{2}+Z_{0}} \left(V_{n}^{2}-V_{0}^{2}\right) + \left(Z_{0}||Z_{2}\right) I_{0}$$

$$\frac{Z_{0}}{Z_{2}+Z_{0}} = \frac{AZ_{0}-Z_{0}}{Z_{2}+Z_{0}} V_{0} + \frac{Z_{0}}{Z_{2}+Z_{0}} V_{0} + \left(Z_{0}||Z_{2}\right) I_{0}.$$

@ Find va Via Therenin method.

$$v_{i}$$
 of z_{i} z

$$Vth = \frac{Z_1}{Z_1 + Z_2} v_0.$$

$$Z_n = \frac{Z_n}{Z_n + Z_n + Z_n + Z_n} \left(v_n - \frac{Z_1}{Z_1 + Z_n} v_0 \right)$$

$$Z_n + Z_n = \frac{Z_n}{Z_n + Z_n + Z_n} \left(v_n - \frac{Z_1}{Z_1 + Z_n} v_0 \right)$$

· 3 Draw block diagram.

