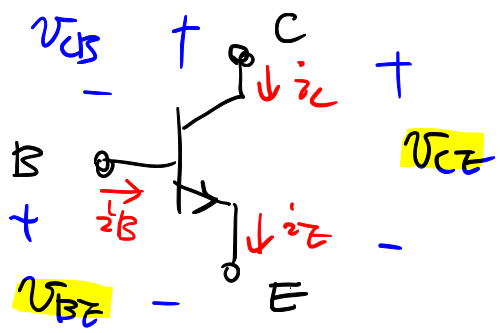


L22 – Power Electronics: Linear Amplifier

• BJT (npn)



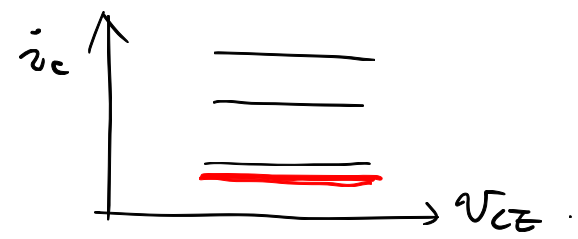
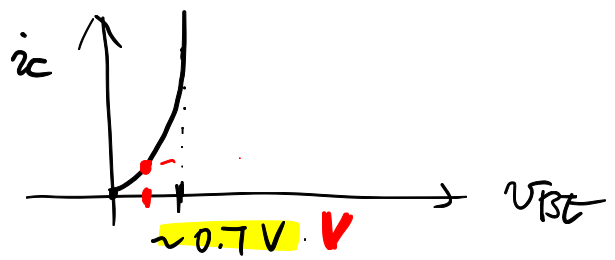
Terminal Variables

- Currents: i_B , i_C , i_E
- Voltages: V_{BE} , V_{CE} , V_{CB}

Terminal Relations

("Active" : $V_{BE} > 0$. AND $V_{CE} > V_{BE}$
 $V_{BC} > 0$

✓ $i_C \approx I_S \exp\left(\frac{V_{BE}}{V_T}\right)$



$$\cdot i_c = \beta i_B \Leftrightarrow i_B = \frac{1}{\beta} i_c$$

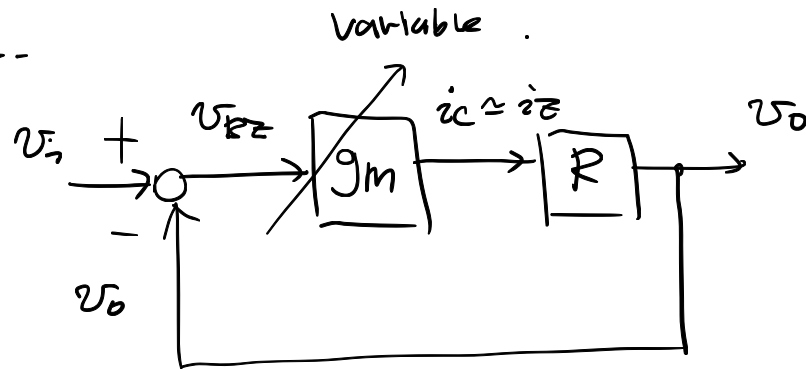
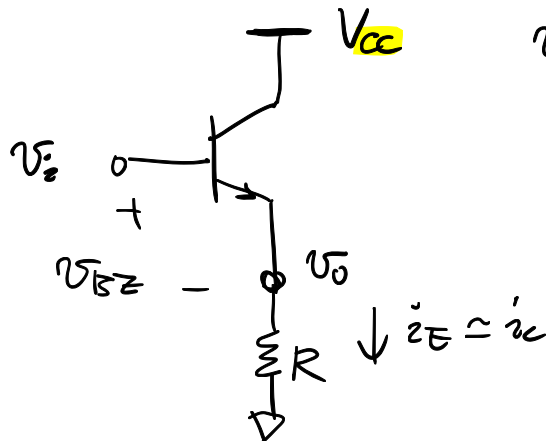
$$\begin{aligned} \cdot i_E &= i_C + i_B \\ &= i_C \left(1 + \frac{1}{\beta}\right) \\ &\approx i_C \end{aligned}$$

Transconductance

$$g_m \triangleq \frac{d i_C}{d v_{BE}} = \frac{I_S}{V_T} \exp\left(\frac{v_{BE}}{V_T}\right) = \frac{i_C}{V_T}$$

• KJT : VCCS . $v_{BE} \rightarrow [P] \rightarrow i_C$. CCCS

• Emitter follower -



$$\frac{v_o}{v_i} = \frac{g_m R}{1 + g_m R}$$

$$= \frac{R}{\frac{1}{g_m} + R} \approx 1 \quad \text{when } g_m R \gg 1$$

.. "power Amplification"

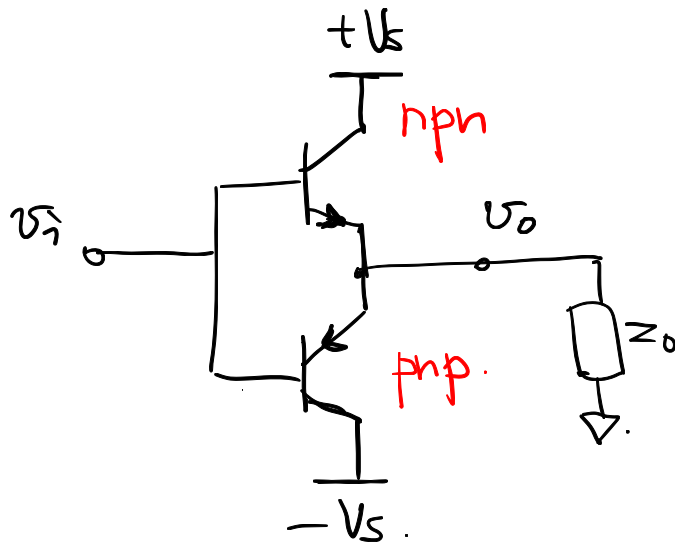
$$P_{in} = v_i i_b$$

$$P_{out} = v_o i_o \approx v_i i_b \beta$$

$$\Rightarrow \frac{P_{out}}{P_{in}} \approx \beta$$

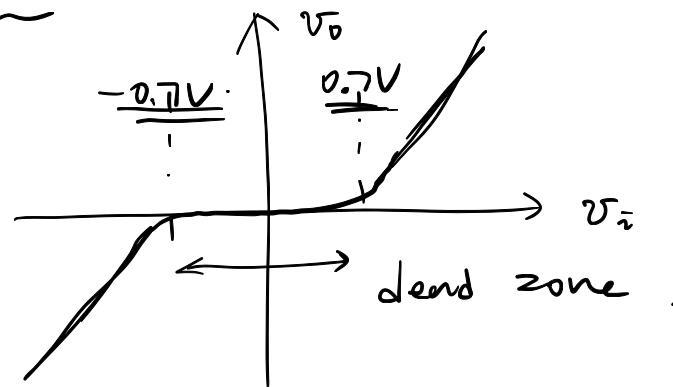
.. Cannot "Sink" current, $z_o > 0$

o Push-pull stage. (Class B).

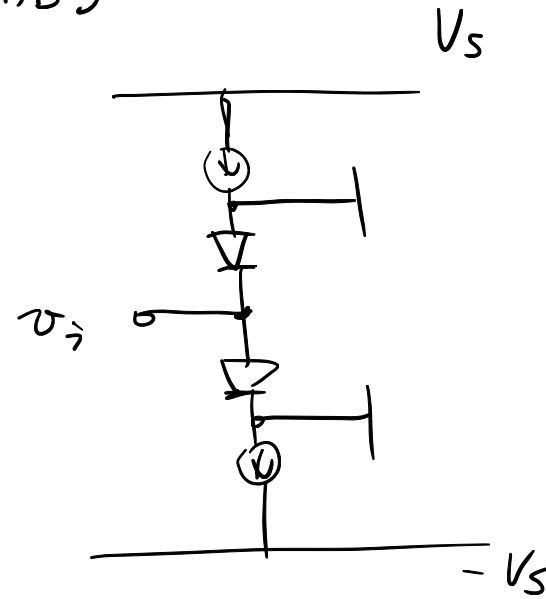
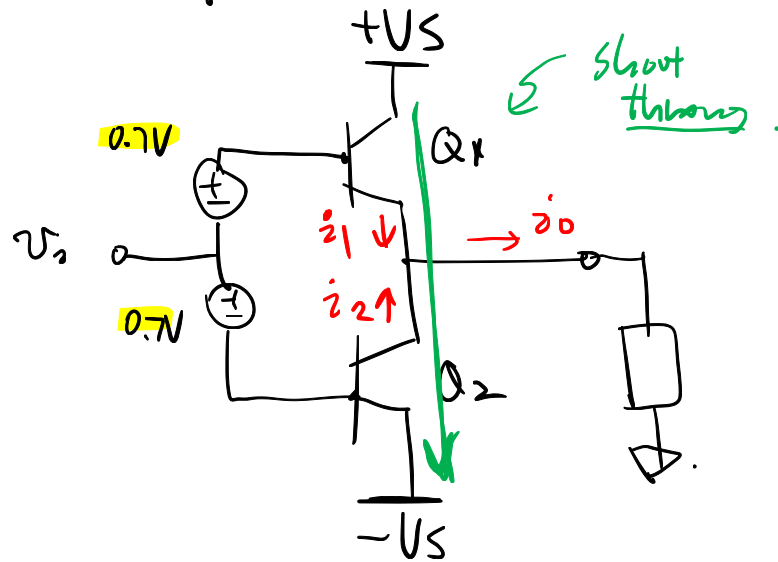


.. Now. Both source & sink i_o .

$$\frac{v_o}{v_i} = \frac{g_m z_o}{1 + g_m z_o} \approx 1$$

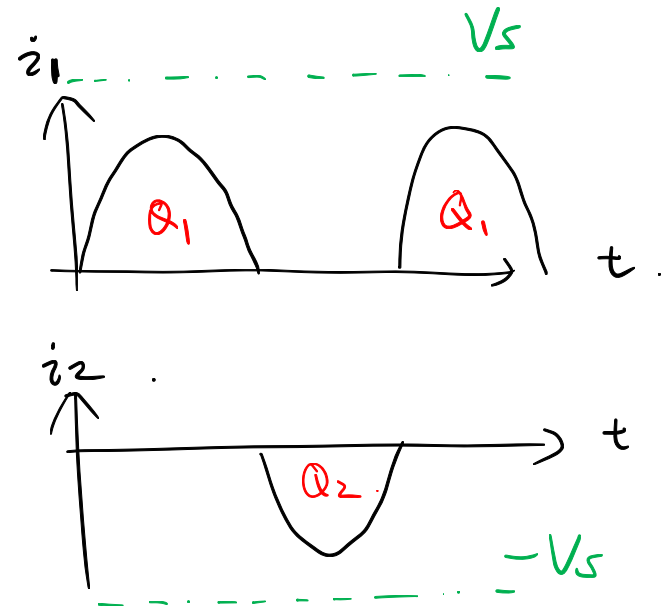
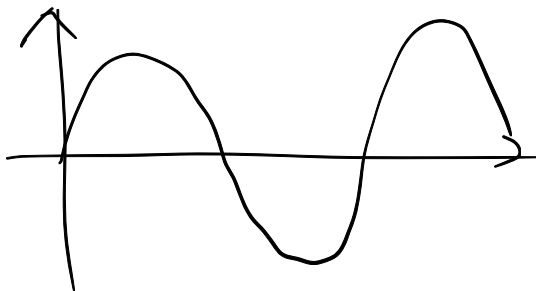


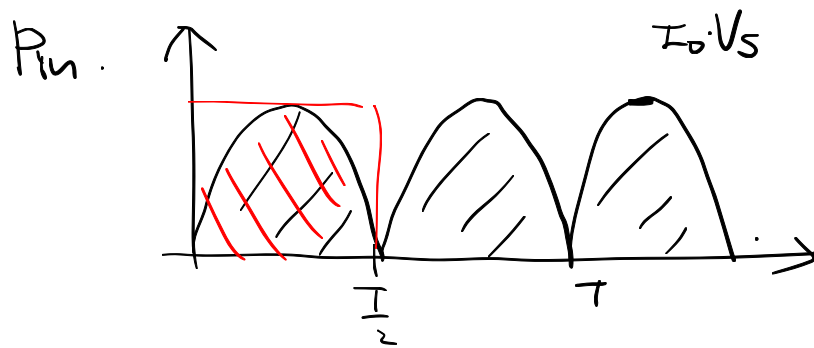
Improved push-pull (Class AB)



Power Dissipation:

Suppose $\begin{cases} Z \approx L_S \\ i_o = I_o \text{ shoot.} \end{cases}$





$$\overline{P_{in}} = \frac{2}{T} \int_0^{\frac{T}{2}} I_0 V_s \sin \omega t \cdot dt$$

$$= \frac{2}{\pi} I_0 V_s$$

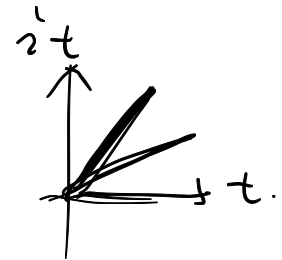
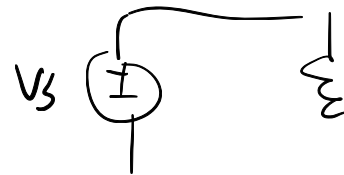


$\overline{P_{out}} = 0$ for pure inductor.

$$\overline{P_{diss}} = \frac{2}{\pi} I_0 \underline{V_s} !$$

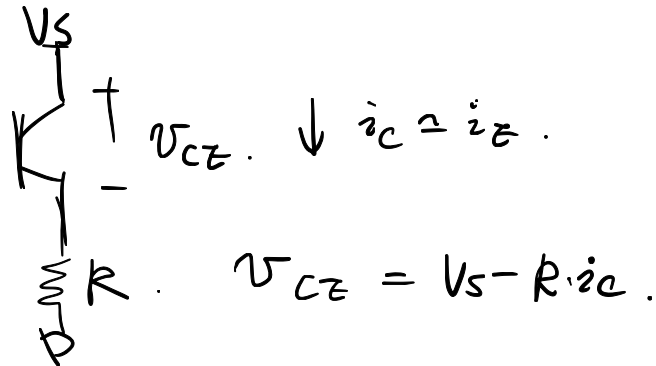
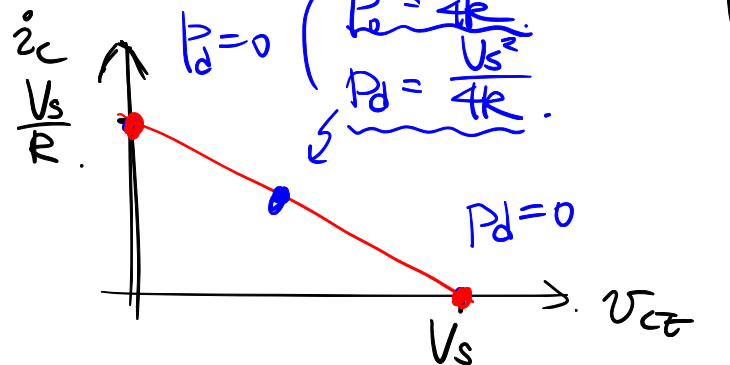
- For efficiency, we want $V_s \downarrow$.
- For control, we want $V_s \uparrow$

$$\max \left(\frac{di}{dt} \right) = \frac{V_s}{L}$$



- Large $\overline{P_{diss}}$ limits device downsizing.
 - \uparrow size of power semiconductors.
 - Requires add. comps (Heat sinks, fans).

o Switched-mode
 $P_d = 0$ $\left(P_e = \frac{V_s^2}{4R} \right)$
 $P_d = \frac{V_s^2}{4R}$



$$P = i_c \cdot v_{ce} = 0 \quad \begin{cases} i_c = 0 \\ v_{ce} = \infty \end{cases}$$

