

Department of Biomedical Informatics

# A Primer on Dynamic Systems

(Kalman Filtering Lecture Prerequisite)

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# Background

### Signal

Any waveform or time-series represented as a function of an independent variable (time, space, samples, etc.).

### Example

Blood pressure variations in time, change of pressure vs altitude, stock market daily charts, electrocardiogram and electroencephalogram waveforms, etc.

### System

- General definition: a set of entities interacting together as parts of a mechanism forming a complex whole.
- In our context: a mathematical/algorithmic process that maps an input to an output.

### Example

Cardiovascular system, thermal regulation system, glucose control system, etc.

# System Properties: Structure

• Static: No temporal evolution in the system or its output

### Example

$$y = x^2 + 2x + \sqrt{x} \tag{1}$$

• **Dynamic:** The system evolves in time, i.e., the input-output process is not point-wise; besides the instantaneous input, the output also depends on the rate changes in the input

### Example

$$\ddot{y}(t) + 2\alpha \dot{y}(t) + \omega_0^2 y(t) = x(t) \tag{2}$$



# System Properties

(continued)

### Linearity

- Linear: The input-output relationship is linear: additivity and homogeneity hold
- Nonlinear: The input-output relationship is nonlinear (the system is either non-additive or non-homogeneous)

### Time Dependence

- Time-variant: The input-output mapping depends on the time origin
- **Time-invariant:** The input-output mapping *does not* depend on the time origin

### Input-Output Mathematical Description

Dynamic systems are of great interest in biological systems modeling. The input-output relationship of these systems can be expressed as follows:

• Explicit: The output can be directly calculated from the input

### Example

$$y(t) = x^2(t) + kt (3)$$

• Implicit: Only an implicit relation between the input and output are available

### Example

$$\ddot{y}(t) + \alpha \dot{y}(t) + b\sqrt{y(t)} = x(t)$$
 (4)



# Differential Equations

In many systems, the *rate* of output and input of a system are related (instead of the input or outputs themselves). This relationship can be modeled by differential equations. The general form of a linear differential equation is:

$$\sum_{k=0}^{N-1} a_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^{M-1} b_k \frac{d^k x(t)}{dt^k}$$
 (5)

- If the coefficients in (5) are constant, the system is time-invariant
- If the initial states are zero, the system is linear; otherwise it is incrementally linear (affine)

# Differential Equations

(continued)

The solution of (5) is

$$y(t) = y_h(t) + y_p(t) \tag{6}$$

where

- $y_h(t)$ : the homogeneous response to initial states
- $y_p(t)$ : the particular response to the system input



The system is only linear when  $y_h(t) = 0$ , i.e., initial states are zero

### Transfer Functions

For linear time-invariant systems, using Laplace (or Fourier) transform, a transfer function can be assigned to the system:

$$H(s) \stackrel{\triangle}{=} \frac{Y(s)}{X(s)} \tag{7}$$

where X(s) and Y(s) are Laplace transforms of x(t) and y(t).

- H(s) is used for *steady-state* analysis but not (explicitly) for *transient* analysis. For *stable* systems, the response to initial states converge to zero. Hence, in steady-state, the output can be exactly determined using H(s)
- The system is stable if the poles are in the left half plane.
- The farther the poles are from the origin, the faster the effect of initial states vanish

### Transfer Functions

(continued)

#### Transfer Function Limitations

- It is restricted to LTI systems (or systems which can be approximated by LTI systems)
- It can only be used for steady-state analysis and and not for transient analysis (although the transfer function has indirect implications on the transient properties of a system)

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(continued)

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Alternative Approach: State-space analysis



# State Space

#### States

- States are properties of a system (usually represented as a vector), through
  which the system's response to a given input can be uniquely found. States
  are properties of a system, knowing which make us needless of its past.
- In a physical system, storage of the 'past information' requires energy saving elements (capacitors, inductors, neurons, cells, etc.). In digital systems memory elements (registers) are required to preserve states
- State variables are not necessarily unique; but for linear systems their total number (known as the *system's order*) is fixed
- A system's order can be infinite

(continued)

### Example

$$y(t) + \alpha y(t) = \beta x(t) \tag{8}$$

(continued)

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This system has one state; knowledge of  $y(t_0)$  is sufficient to determine y(t) for all  $t \in [t_0, \infty)$ .

(continued)

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#### Example

$$y(t) = x(t - t_0)$$
 or  $H(s) = e^{-t_0 s}$   
 $H(s) = 1 - st_0 + \frac{(st_0)^2}{2} - \dots = \frac{1}{1 + st_0 + \frac{(st_0)^2}{2} + \dots}$  (9)

(continued)

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This system has infinite number of states. For  $|st_0| \ll 1$ , the system can be approximated with lower order systems. A small value of  $st_0$  implies a narrow-band system working at a relatively low frequency.

### State-space equations

Set of first-order differential (difference) equations relating the system inputs, outputs, and states

$$\begin{cases}
\dot{s}(t) = f(x(t), s(t)) \\
y(t) = g(x(t), s(t))
\end{cases}$$
(10)

where x(t), y(t), and s(t) are the input, output and state vectors.

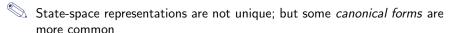


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For LTI systems, differential and state-space equations can be converted to one another

Scalar differential equations of order n, are converted into n first order state-space differential equations (if the system is irreducible)



(continued)

### State-space equations for multi-input multi-output (MIMO) systems

$$\begin{cases}
\dot{s_1} = f_1(s_1, \dots, s_n, x_1, \dots, x_p) \\
\vdots \\
\dot{s_n} = f_n(s_1, \dots, s_n, x_1, \dots, x_p)
\end{cases}$$
(11)

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\dot{s_1} = f_1(s_1, \dots, s_n, x_1, \dots, x_p) \\
\vdots \\
\dot{s_n} = f_n(s_1, \dots, s_n, x_1, \dots, x_p)
\end{cases}$$

$$\begin{cases}
y_1 = g_1(s_1, \dots, s_n, x_1, \dots, x_p) \\
\vdots \\
y_m = g_m(s_1, \dots, s_n, x_1, \dots, x_p)
\end{cases}$$
(12)

(continued)

#### Linear Case

$$\mathbf{s} = \begin{bmatrix} s_1 \\ \vdots \\ s_n \end{bmatrix}, \mathbf{A} = \begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \vdots & & \vdots \\ a_{n1} & \cdots & a_{nn} \end{bmatrix}, \mathbf{x} = \begin{bmatrix} x_1 \\ \vdots \\ x_p \end{bmatrix}, \mathbf{y} = \begin{bmatrix} y_1 \\ \vdots \\ y_m \end{bmatrix}$$
(13)

$$\begin{cases}
\dot{\mathbf{s}}_{n\times 1} = \mathbf{A}_{n\times n} \mathbf{s}_{n\times 1} + \mathbf{B}_{n\times p} \mathbf{x}_{p\times 1} \\
\mathbf{y}_{m\times 1} = \mathbf{C}_{m\times n} \mathbf{s}_{n\times 1} + \mathbf{D}_{m\times p} \mathbf{x}_{p\times 1}
\end{cases} (14)$$

#### Nonlinear Case

$$\begin{cases}
\dot{\mathbf{s}}_{n\times 1} = \mathbf{f}_{n\times 1}(\mathbf{s}_{n\times 1}, \mathbf{x}_{p\times 1}) \\
\mathbf{y}_{m\times 1} = \mathbf{g}_{m\times 1}(\mathbf{s}_{n\times 1}, \mathbf{x}_{p\times 1})
\end{cases}$$
(15)

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# Canonical State-Space Representations

### Controllable state-space forms

Controllability is the ability to drive the system states to arbitrary values through the input signal or noise in finite time (Kailath, 1980; Tsakalis, 2001)

### Example

Controlling blood pressure through drug intake.

### Observable state-space forms

Observability describes the ability to infer the system states given output measurements (Kailath, 1980; Tsakalis, 2001)

#### Example

Output demonstration of internal body infections as fever.

Question: Are physiological systems necessarily controllable and/or observable?

(continued)

### Example

$$a\frac{d^{2}y(t)}{dt^{2}} + b\frac{dy(t)}{dt} + cy(t) = x(t)$$
 (16)

$$s_1 \stackrel{\triangle}{=} y(t) \qquad \dot{s}_1 = s_2$$
  

$$s_2 \stackrel{\triangle}{=} \dot{y}(t) \Rightarrow \quad \dot{s}_2 = \ddot{y}(t) = \frac{1}{a}(x(t) - bs_2 - cs_1)$$
(17)

State-space representation:

$$\begin{bmatrix} \dot{s}_{1} \\ \dot{s}_{2} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{c}{a} & -\frac{b}{a} \end{bmatrix} \cdot \begin{bmatrix} s_{1} \\ s_{2} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{a} \end{bmatrix} x(t)$$

$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s_{1} \\ s_{2} \end{bmatrix}$$
(18)

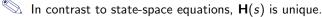
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# State-Space to Transfer Functions and Differential Equations

Taking the Laplace transform of (14):

$$\mathbf{Y}(s) = \left[ \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1} \mathbf{B} + \mathbf{D} \right] \mathbf{X}(s) \tag{19}$$

Transfer matrix:  $\mathbf{H}(s) \stackrel{\triangle}{=} \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$ 



Taking the inverse Laplace transform, takes the system back to the time domain (in differential equation or impulse response form)



# Temporal Solutions from State-Space Representation

Scalar Case

### Example

Consider the system  $\dot{y}(t) = ay(t) + bx(t)$ , with initial condition y(0). Taking the Laplace transform, we find:

$$sY(s) - y(0) = aY(s) + bX(s)$$

$$Y(s) = \frac{y(0)}{s - a} + \frac{bX(s)}{s - a} \Rightarrow$$

$$y(t) = y(0)e^{at}u(t) + be^{at}u(t) * x(t) \Rightarrow$$

$$y(t) = y(0)e^{at}u(t) + b\int_0^t e^{a(t - \tau)}x(\tau)d\tau$$
(20)

When a < 0, the effect of initial conditions vanish in time

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# Temporal Solutions from State-pace Representation

#### Vectorial Case

The vectorial differential equation  $\dot{\mathbf{y}}(t) = \mathbf{A}\mathbf{y}(t) + \mathbf{B}\mathbf{x}(t)$  yields:

$$s\mathbf{Y}(s) - \mathbf{y}(0) = \mathbf{A}\mathbf{Y}(s) + \mathbf{B}\mathbf{X}(s)$$

$$\mathbf{Y}(s) = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{y}(0) + (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}\mathbf{X}(s)$$

$$\Phi(s) \stackrel{\Delta}{=} (s\mathbf{I} - \mathbf{A})^{-1} = L\left\{e^{\mathbf{A}t}\right\} = L\left\{\phi(t)\right\}$$
(21)

where  $\phi(t) = e^{\mathbf{A}t}u(t)$  is the state transition matrix.

Hence:

$$\mathbf{y}(t) = \phi(t)\mathbf{y}(0) + \int_0^t \phi(t-\tau)\mathbf{B}\mathbf{x}(\tau)d\tau$$
 (22)

Or, if the initial states are given at  $t = t_0$ :

$$\mathbf{y}(t) = \phi(t - t_0)\mathbf{y}(t_0) + \int_{t_0}^{t} \phi(t - \tau)\mathbf{B}\mathbf{x}(\tau)d\tau$$
 (23)



Whenever  $\mathbf{x}(t) = \mathbf{0}$  we have:  $\mathbf{y}(t) = \phi(t - t_0)\mathbf{y}(t_0)$ 

### State Transition Matrix

Example

$$\dot{\mathbf{y}}(t) = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \mathbf{y}(t) \tag{24}$$

with  $\mathbf{y}(0) = \mathbf{0}$ .

Solution:

$$(s\mathbf{I} - \mathbf{A}) = \begin{bmatrix} s & -1 \\ 2 & s+3 \end{bmatrix}$$

$$(s\mathbf{I} - \mathbf{A})^{-1} = \frac{1}{s^2 + 3s + 2} \begin{bmatrix} s+3 & 1 \\ -2 & s \end{bmatrix} \Rightarrow (25)$$

$$\phi(t) = L^{-1} \{ \Phi(s) \} = \begin{bmatrix} -e^{-2t} + 2e^{-t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix} u(t)$$

This matrix indicates variation of each state over time with respect to the specific initial condition.

### State Transition Matrix

(continued)

### **Properties**

- $\phi(0) = \mathbf{I}$ : No state transition without time elapse (state transition requires time)
- $\phi^{-1}(\tau) = \phi(-\tau) \Rightarrow \mathbf{x}(t_0) = \phi^{-1}(t t_0)\mathbf{x}(t)$ : Time is reversible using the inverse transition matrix
- $\phi(t_1 + t_2) = \phi(t_1)\phi(t_2) = \phi(t_2)\phi(t_1)$ : Time epochs can be split into smaller segments (special case:  $[\phi(\Delta)]^k = \phi(k\Delta)$ )
- $\phi(t_2 t_0) = \phi(t_2 t_1)\phi(t_1 t_0)$ : State transition is independent of the time path (like the work done in a conservative system)

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### Continuous vs. discrete models

- Models can be continuous or discrete in time.
- With current digital simulation and modeling systems, models are either discrete by definition or are discretized during the modeling and simulation procedure.
- Discretization in time consists of converting a continuous-time signal/system to a discrete-time signal/system.

# Continuous vs. Discrete Models

(continued)

### Examples of signal discretization and discrete signals

- Discretized signal: An ECG signal sampled and stored in a computer
- Intrinsically discrete signal: The heart rate time-series is discrete by definition

#### Examples of system discretization vs discrete systems

- **Discretized system:** Simulation of the respiratory system or cell-growth in a computer
- Discrete systems: Digital cardiac pacemakers, biofeedback systems, etc.

# Signal Discretization

### Signal discretization

- Signal discretization is the subject of digital signal processing
- The question is how to go from a continuous-time signal x(t) to a discrete-time signal x[n]
- In the real world, discrete signals are achieved by sampling a continuous-time signal in a *uniform* or *non-uniform* manner.

# System Discretization

### Static system discretization

Since static systems do not evolve in time, the discretization is straightforward:  $t \to nT_s$ , where  $T_s$  is the sampling time.

### Dynamic system discretization

Differential forms are approximated with difference equations of the appropriate order.

#### First-order discretization

For small  $\Delta$ :  $\frac{d}{dt}x(t) \approx \frac{x(t+\Delta)-x(t)}{\Delta}$ . If  $T_s$  is small 'enough' (an order of magnitude smaller than the Nyquist frequency is typically fine),  $\Delta$  can be replaced by  $T_s$ . Hence:

$$\frac{d}{dt}x(t) \to \frac{x[n+1] - x[n]}{T_s} \tag{26}$$

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# System Discretization

(continued)

- The same procedure can be used for state-space representations of models.
- For higher-order discretizations, the first-order can be extended or one may use an appropriate approximation of the desired order.



The discretization error increases if  $T_s$  is not small enough.

# System Discretization

(continued)

Discrete systems can be obtained from continuous ones using various approaches:

- Time-domain: The system is discretized from the implicit or explicit forms of its input/output equation
- Frequency-domain: H(s) is transferred to H(z) using a conformal mapping (cf. DSP textbooks)



Discretized models are not unique

Consider a static system: 
$$y = f(\mathbf{u}) (\mathbf{u} = [u_1, \dots, u_n]^T)$$
.



Consider a static system:  $y = f(\mathbf{u}) (\mathbf{u} = [u_1, \dots, u_n]^T)$ . A first-order Taylor expansion around  $y_0 = f(\mathbf{u}_0)$  results in:

$$y = f(\mathbf{u}_0) + \frac{\partial f(\mathbf{u})}{\partial \mathbf{u}} \bigg|_{\mathbf{u} = \mathbf{u}_0} (\mathbf{u} - \mathbf{u}_0) + \cdots$$

$$y \approx f(\mathbf{u}_0) + \frac{\partial f(\mathbf{u})}{\partial \mathbf{u}} \bigg|_{\mathbf{u} = \mathbf{u}_0} (\mathbf{u} - \mathbf{u}_0)$$
(27)

$$\frac{\partial f(\mathbf{u})}{\partial \mathbf{u}} = \left[ \frac{\partial f(\mathbf{u})}{\partial u_1}, \cdots, \frac{\partial f(\mathbf{u})}{\partial u_n} \right]^T \bigg|_{\mathbf{u} = u_0} \triangleq \mathbf{g}_0$$
 (28)

$$y \approx f(\mathbf{u}_0) + \mathbf{g}_0^T (\mathbf{u} - \mathbf{u}_0) \Rightarrow$$

$$y - y_0 \approx \mathbf{g}_0^T (\mathbf{u} - \mathbf{u}_0) \Rightarrow$$

$$\delta y \approx \mathbf{g}_0^T \delta \mathbf{u}$$
(29)

(continued)

### Example

Linearize the following static system around  $\bar{u}_1 = \bar{u}_2 = 0, \bar{y} = 0$ :

$$y = u_1^2 u_2^2 + u_2 + 3u_1^2 (30)$$

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(continued)

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### Approach 1 (Taylor expansion):

$$g^{T} = \begin{bmatrix} 2u_{1}u_{2}^{2} + 6u_{1} & 2u_{2}u_{1}^{2} + 1 \end{bmatrix} |_{u_{1}=u_{2}=0} = \begin{bmatrix} 0 & 1 \end{bmatrix} \Rightarrow \delta y \approx \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \delta u_{1} \\ \delta u_{1} \end{bmatrix} = \delta u_{2}$$
(31)

(continued)

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(31)

**Approach 2 (Perturbation theory):** Insert  $u_1 = \bar{u}_1 + \delta u_1$ ,  $u_2 = \bar{u}_2 + \delta u_2$ , and  $y = \bar{y} + \delta y$  in (30) and discard the second and higher-order terms:

$$(\bar{y} + \delta y) = (\bar{u}_1 + \delta u_1)^2 (\bar{u}_2 + \delta u_2)^2 + (\bar{u}_2 + \delta u_2) + 3(\bar{u}_1 + \delta u_1)^2$$
(32)

which results in  $\delta y \approx \delta u_2$  (Note: this is only valid at  $\bar{u}_1 = \bar{u}_2 = 0$ ).

# Dynamic System Linearization

The perturbation approach can also be used for linearizing dynamic systems:

### Example

Linearize 
$$y \frac{d^2y}{dt^2} + u^2 \frac{dy}{dt} + \sqrt{y} = u$$
 around  $\sqrt{y_0} = u_0$ 

### Dynamic System Linearization

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### Example

Linearize 
$$y \frac{d^2y}{dt^2} + u^2 \frac{dy}{dt} + \sqrt{y} = u$$
 around  $\sqrt{y_0} = u_0$ 

**Solution:** Replacing  $u(t) = u_0 + \delta u(t)$  and  $y(t) = y_0 + \delta y(t)$  gives:

$$(y_0 + \delta y)\frac{d^2}{dt^2}(y_0 + \delta y) + (u_0 + \delta u)^2\frac{d}{dt}(y_0 + \delta y) + \sqrt{y_0 + \delta y} = u_0 + \delta u$$
 (33)

Replacing  $\sqrt{y_0 + \delta y}$  with its Taylor expansion:

$$\sqrt{y_0 + \delta y} = (y_0 + \delta y)^{\frac{1}{2}} = y_0^{\frac{1}{2}} + \frac{1}{2\sqrt{y_0}} \delta y + (\text{second and higher-order terms}) \quad (34)$$

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# Dynamic System Linearization

(continued)

### Example (continued)

By discarding the second and higher-order terms, we find

$$y_0 \frac{d^2}{dt^2} (\delta y) + u_0^2 \frac{d}{dt} (\delta y) + \sqrt{y_0} + \frac{1}{2\sqrt{y_0}} \delta y \approx u_0 + \delta u$$
 (35)

$$y_0\ddot{\delta y} + u_0^2\dot{\delta y} + \frac{1}{2\sqrt{y_0}}\delta y \approx \delta u \tag{36}$$

This approximation is only valid around  $(u_0, y_0)$ . The transfer function (at this point) is:

$$H(s) = \frac{\Delta Y(s)}{\Delta U(s)} \approx \frac{1}{y_0 s^2 + u_0^2 s + \frac{1}{2\sqrt{y_0}}}$$
 (37)

Depending on the application,  $\delta u(t)$  and  $\delta y(t)$  should be small enough to ensure the validity of these approximations.

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# Nonlinear State-Space System Linearization

Linearize the following system around  $(\mathbf{u}_0, \mathbf{x}_0, \mathbf{y}_0)$ :

$$\begin{cases} \dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}) \\ \mathbf{y} = \mathbf{g}(\mathbf{x}, \mathbf{u}) \end{cases}$$
 (38)

The overall approach is similar:

$$\begin{cases}
\mathbf{u}(t) = \mathbf{u}_0 + \delta \mathbf{u}(t) \\
\mathbf{y}(t) = \mathbf{y}_0 + \delta \mathbf{y}(t) \\
\mathbf{x}(t) = \mathbf{x}_0 + \delta \mathbf{x}(t)
\end{cases}$$
(39)

$$\dot{\mathbf{x}}_0 + \delta \dot{\mathbf{x}}(t) = \mathbf{f}(\mathbf{x}_0 + \delta \mathbf{x}(t), \mathbf{u}_0 + \delta \mathbf{u}(t)) \\
= \mathbf{f}(\mathbf{x}_0, \mathbf{u}_0) + \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \begin{vmatrix} \mathbf{x} = \mathbf{x}_0 \\ \mathbf{y} = \mathbf{y}_0 \end{vmatrix} \mathbf{x} = \mathbf{x}_0 \quad \delta \mathbf{u}(t) + \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \begin{vmatrix} \mathbf{x} = \mathbf{x}_0 \\ \mathbf{y} = \mathbf{y}_0 \end{vmatrix}$$

$$\mathbf{y}_{0} + \delta \mathbf{y}(t) = \mathbf{g}(\mathbf{x}_{0} + \delta \mathbf{x}(t), \mathbf{u}_{0} + \delta \mathbf{u}(t))$$

$$= \mathbf{g}(\mathbf{x}_{0}, \mathbf{u}_{0}) + \frac{\partial \mathbf{g}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \begin{vmatrix} \mathbf{x} = \mathbf{x}_{0} & \delta \mathbf{x}(t) + \frac{\partial \mathbf{g}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \end{vmatrix} \mathbf{x} = \mathbf{x}_{0}$$

$$\mathbf{y} = \mathbf{y}_{0}$$

$$\mathbf{y} = \mathbf{y}_{0}$$

# Nonlinear State-Space System Linearization (continued)

Defining

$$\begin{array}{c|c}
\mathbf{A}(t) \stackrel{\triangle}{=} \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \middle| & \mathbf{x} = \mathbf{x}_{0} \\
\mathbf{y} = \mathbf{y}_{0} \\
\mathbf{C}(t) \stackrel{\triangle}{=} \frac{\partial \mathbf{g}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{x}} \middle| & \mathbf{x} = \mathbf{x}_{0} \\
\mathbf{y} = \mathbf{y}_{0} \\
\mathbf{y} = \mathbf{y}_{0}
\end{array}$$

$$\begin{array}{c|c}
\mathbf{B}(t) \stackrel{\triangle}{=} \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \middle| & \mathbf{x} = \mathbf{x}_{0} \\
\mathbf{y} = \mathbf{y}_{0} \\
\mathbf{y} = \mathbf{y}_{0}
\end{array}$$

$$\begin{array}{c|c}
\mathbf{D}(t) \stackrel{\triangle}{=} \frac{\partial \mathbf{g}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \middle| & \mathbf{x} = \mathbf{x}_{0} \\
\mathbf{y} = \mathbf{y}_{0}
\end{array}$$

$$\mathbf{A}(t) \stackrel{\triangle}{=} \frac{\partial \mathbf{f}(\mathbf{x}, \mathbf{u})}{\partial \mathbf{u}} \middle| & \mathbf{x} = \mathbf{x}_{0} \\
\mathbf{y} = \mathbf{y}_{0}$$

$$\mathbf{y} = \mathbf{y}_{0}$$

$$\mathbf{y} = \mathbf{y}_{0}$$

and considering that

$$\begin{cases}
\dot{\mathbf{x}}_0 = \mathbf{f}(\mathbf{x}_0, \mathbf{u}_0) \\
\mathbf{y}_0 = \mathbf{g}(\mathbf{x}_0, \mathbf{u}_0)
\end{cases} (42)$$

Results in:

$$\begin{cases}
\delta \dot{\mathbf{x}}(t) \approx \mathbf{A}(t)\delta \mathbf{x}(t) + \mathbf{B}(t)\delta \mathbf{u}(t) \\
\delta \mathbf{y}(t) \approx \mathbf{C}(t)\delta \mathbf{x}(t) + \mathbf{D}(t)\delta \mathbf{u}(t)
\end{cases} (43)$$

which is a linear approximation of the original nonlinear state-space equations around  $(\mathbf{u}_0, \mathbf{x}_0, \mathbf{y}_0)$ .

# Stability Analysis of Nonlinear Systems

### In linear systems

All the system poles should be in the left half plane

#### In nonlinear systems

- The system is first linearized around the desired point
- The state transition matrix is calculated for the linearized system:  $\phi(s) = (s\mathbf{I} \mathbf{A})^{-1} \ (\phi(t) = L^{-1} \{\phi(s)\})$
- **1** In order to have a stable system, the poles of  $\phi(s)$  should be in the left half plane (or  $\lim_{t\to\infty} \phi(t) = 0$ ), around the point of interest

# Further Reading

- Kailath, T. (1980). Linear Systems.
   Prentice Hall
- Dorf, R. C. & Bishop, R. H. (2021). Modern Control Systems.
   Pearson Prentice Hall, 13th edition
- Ogata, K. (2010). Modern control engineering.
   Prentice hall, 5th edition
- Oppenheim, A., Schafer, R., & Buck, J. (1999). Discrete-time signal processing.
   Prentice-Hall signal processing series. Prentice Hall
- Tsakalis, K. S. (2001). Stability, controllability, observability.
   Lecture Notes