#### Tsai-Lenz Hand-eye calibration

we will derive a modified version of Rodrigues formula:

$$R = \left(1 - \frac{1}{2} \|P_r\|^2\right) I_3 + \frac{1}{2} (P_r P_r^T + \sqrt{4 - \|P_r\|^2} [P_r \times])$$

starting with,

$$R = [(q_4^2 - \|\mathbf{q}\|^2)I_3 + 2\mathbf{q}\mathbf{q}^T + 2q_4\mathbf{q}\times]$$

where

$$\mathbf{q} \times = \begin{bmatrix} 0 & -q_3 & q_2 \\ q_3 & 0 & -q_1 \\ -q_2 & q_1 & 0 \end{bmatrix}$$
$$q_4 = \cos \frac{\theta}{2}$$
$$\mathbf{q} = \sin \frac{\theta}{2} \hat{\mathbf{n}}$$

define,

$$\vec{P}_r = 2\sin\frac{\theta}{2}\hat{n}$$

$$\|\vec{P}_r\|^2 = 4\sin^2\frac{\theta}{2}$$

$$\frac{\|\vec{P}_r\|}{4} = 1 - \cos^2\frac{\theta}{2}$$

$$\cos^2\frac{\theta}{2} = 1 - \frac{\|\vec{P}_r\|^2}{4}$$

$$q_4 = \cos\frac{\theta}{2} = \sqrt{1 - \frac{\|P_r\|^2}{4}}$$

now,

$$\|\vec{q}\|^2 = \sin^2\frac{\theta}{2} = \frac{\|P_r\|^2}{4}$$

For the middle term,  $2\mathbf{q}\mathbf{q}^T$ 

$$2\vec{q}\vec{q}^T = 2\frac{\vec{P}_r}{2}\frac{\vec{P}_r^T}{2} = \frac{1}{2}\vec{P}_r\vec{P}_r^T$$

For the last term  $2q_4\mathbf{q}\times$ ,

$$2q_4\vec{q} \times = 2\sqrt{1 - \frac{\|\vec{P}_r\|^2}{4}} \frac{[\vec{P}_r \times]}{2} = \frac{1}{2}\sqrt{4 - \|\vec{P}_r\|^2} [\vec{P}_r \times]$$

summing up,

$$R = \left(1 - \frac{1}{2} \|P_r\|^2\right) I_3 + \frac{1}{2} P_r P_r^T + \frac{1}{2} \sqrt{4 - \|P_r\|^2} [P_r \times]$$
$$= \left(1 - \frac{1}{2} \|P_r\|^2\right) I_3 + \frac{1}{2} (P_r P_r^T + \alpha [P_r \times])$$

where  $\alpha = \sqrt{4 - \|P_r\|^2}$ , and  $[P_r \times] = skew(P_r)$ 

Figure 1 shows the relation:

$$H_{qj} \circ H_{qij} = H_{qi}$$

$$H_{cij} \circ H_{ci} = H_{cj}$$

where o denotes "followed by"

$$H_{cij} = H_{cj}H_{ci}^{-1}$$
$$H_{gij} = H_{gi}^{-1}H_{gi}$$

given:  $H_{gi}$  defines coordinate transformation from  $G_i$  to RW

$$H_{gi} = \begin{bmatrix} R_{gi} & T_{gi} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

 $\mathcal{H}_{ci}$  defines coordinate transformation from CW to  $\mathcal{C}_i$ 

$$H_{ci} = \begin{bmatrix} R_{ci} & T_{ci} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

 $H_{gij}$  defines coordinate transformation from  $G_i$  to  $G_j$ 

$$H_{gij} = \begin{bmatrix} R_{gij} & T_{gij} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

 $H_{cij}$  defines coordinate transformation from  $C_i$  to  $C_j$ 

$$H_{cij} = \begin{bmatrix} R_{cij} & T_{cij} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

 $H_{cg}$  defines coordinate transformation from  $C_i$  to  $G_i$ 

$$H_{cg} = \begin{bmatrix} R_{cg} & T_{cg} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

In the above i,j range from 1 to N, where N is the number of stations.

### Lemma 1

$$H_{gj}H_{cg}H_{cj} = H_{gi}H_{cg}H_{ci}$$

$$H_{cg}H_{cj}H_{ci}^{-1} = H_{gj}^{-1}H_{gi}H_{cg}$$

$$H_{cg}H_{cij} = H_{gij}H_{cg}$$

$$H_{gij}H_{cg} = H_{cg}H_{cij}$$

$$AX = XB$$

$$(1)$$

from the rotation terms,

Lemma 1: 
$$R_{gij} = R_{cg}R_{cij}R_{cg}^T$$

## Lemma 2: $P_{gij} = R_{cg}P_{cij}$

Proof: Suppose we have two coordinate frames, the transformation of a vector measured from one to the other is related by

$$\vec{u} = Q\vec{u}_a$$

where Q is a rotation matrix with the direction cosines of the axes of the rotated frame w.r.t to the original frame. Now, let's say we want to transform the vector  $\vec{u}$  to another vector  $\vec{v}$ ,

$$\vec{v} = T\vec{u}$$

then,

$$Q\vec{v}_a = TQ\vec{u}_a$$

# robot End Effector

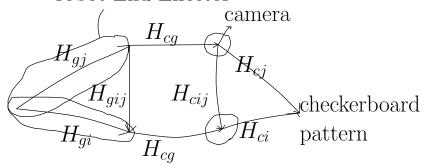


Figure 1: hand-eye calibration

$$\vec{v}_a = Q^{-1}TQ\vec{u}_a$$
 
$$\vec{v}_a = T_a\vec{u}_a \Rightarrow T_a = Q^{-1}TQ = Q^TTQ$$

now let  $B = T_a$  and A = T. Then  $B = Q^T A Q$ 

$$B\vec{v} = \lambda \vec{v}$$

with  $\lambda$  and  $\vec{v}$  being the eigenvalue and eigenvector pair of B. Then

$$Q^{T}AQ\vec{v} = \lambda \vec{v}$$
$$AQ\vec{v} = \lambda Q\vec{v}$$
$$A(Q\vec{v}) = \lambda (Q\vec{v})$$
$$A\vec{w} = \lambda \vec{w}$$

with  $\vec{w} = Q\vec{v}$  being the eigenvector of A corresponding to the same eigenvalue  $\lambda$ . Hence, given the similarity transform  $R_{cij} = R_{cg}^T R_{gij} R_{cg}$  from lemma 1 and letting  $B = R_{cij}$  and  $A = R_{gij}$ ,

by comparison, we can observe

$$P_{qij} = \vec{w} = Q\vec{v} = R_{cq}P_{cij}$$

**Lemma 3:**  $P_{cg} \perp (P_{gij} - P_{cij})$ , Before we prove that  $P_{cg} \perp (P_{gij} - P_{cij})$ , we will digress to show that the eigenvalues of a rotation matrix, R are  $\lambda_1 = 1$  and  $\lambda_{2,3} = e^{\pm i\phi}$  for  $\phi \in [0,\pi]$ :

$$R\mathbf{x} = \lambda \mathbf{x}$$

Since a rotation matrix consists of only real entries, complex conjugation on both sides yields:

$$\overline{R}\overline{\mathbf{x}} = R\overline{\mathbf{x}} = \overline{\lambda}\overline{\mathbf{x}}$$
$$(R\mathbf{x}) \cdot (R\overline{\mathbf{x}}) = (\lambda \mathbf{x}) \cdot (\overline{\lambda}\overline{\mathbf{x}})$$
$$\mathbf{x}^T R^T R\overline{\mathbf{x}} = \lambda \overline{\lambda}\mathbf{x} \cdot \mathbf{x}$$

Since  $R^T R = I$ ,

$$\mathbf{x} \cdot \mathbf{x} = \lambda \bar{\lambda} \mathbf{x} \cdot \mathbf{x}$$
$$\|\mathbf{x}\|^2 = \lambda \bar{\lambda} \|\mathbf{x}\|^2$$

Since  $\|\mathbf{x}\| \neq 0$ ,

$$\lambda \bar{\lambda} = 1$$

This can be satisfied for the eigenvalues  $\lambda_1 = 1$  and  $\lambda_{2,3} = e^{\pm i\phi}$  for  $\phi \in [0,\pi]$ . The eigenvalue  $\lambda = 1$  correspond to the eigenvector  $\hat{\mathbf{n}}$ . This implies  $R\hat{\mathbf{n}} = \hat{\mathbf{n}}$ . Furthermore, since  $det(A^T - \lambda I) = det((A - \lambda I)^T) = det(A - \lambda I)$ , implies  $A^T\hat{\mathbf{n}} = \hat{\mathbf{n}} \Rightarrow (A^T - I)\hat{\mathbf{n}} = 0$ .

Now, to prove  $P_{cg} \perp (P_{gij} - P_{cij})$  (we will ommit the subscript ij for clarity).

$$(P_g - P_c)^T P_{cg} = (P_g - P_c)^T R_{cg}^T R_{cg} P_{cg}$$

$$= [R_{cg}(P_g - P_c)]^T R_{cg} P_{cg}$$

$$= (R_{cg}P_g - P_g)^T P_{cg}$$

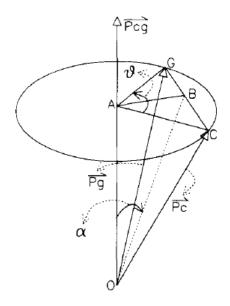
$$= [(R_{cg} - I)P_g]^T P_{cg}$$

$$= P_g^T (R_{cg}^T - I) P_{cg} = 0$$

Since it was shown before that  $(R^T - I)\hat{\mathbf{n}} = 0$ .

Obviously  $P_{cg} = R_{cg}P_{cg}$ ,

Figure 2: Geometrical relationships, the plane containing the circle is perpendicular to  $P_{cg}$ . B is the midpoint of point C and G.



**Lemma 4:**  $P_{cij} - P_{gij}$  is collinear with  $(P_{gij} + P_{cij}) \times P_{cg}$ . This means  $P_{cij} - P_{gij} = s(P_{gij} + P_{cij}) \times P_{cg}$  for some scale factor s. This follows from the fact that  $(P_{gij} - P_{cij})$  is perpendicular to  $(P_{gij} + P_{cij})$ . Proof:

$$(P_{gij} - P_{cij})^{T} (P_{gij} - P_{cij})$$

$$= P_{gij}^{T} P_{gij} + P_{gij}^{T} P_{cij} - P_{cij}^{T} P_{gij} - P_{cij}^{T} P_{cij}$$

$$= \|P_{gij}\|^{2} - \|P_{cij}\|^{2}$$

$$= (R_{cg} P_{cij})^{T} (R_{cg} P_{cij}) - \|P_{cij}\|^{2}$$

$$= \|P_{cij}\|^{2} - \|P_{cij}\|^{2} = 0$$

**Lemma 5**;  $P_{cij} - P_{gij}$  and  $(P_{gij} + P_{cij}) \times P_{cg}^{'}$  have the same length. Define  $P_{r}^{'}$ ,

$$P_r^{'} = \frac{P_r}{2\cos\frac{\theta_r}{2}}$$

This definition will be useful in calculating  $\theta$  later. Since,

$$\frac{2\sin\frac{\theta}{2}}{2\cos\frac{\theta}{2}} = \frac{\|P_r\|}{\|P_r\|} \Rightarrow \tan\frac{\theta}{2} = \|P_r^{'}\|$$

$$\theta = 2\tan^{-1}\|P_r^{'}\|$$

Also, with this definition  $P_r$  can be calculated using,

$$P_r = \frac{2P_r'}{\sqrt{1 + \|P_r'\|^2}}$$

by definition,

$$\begin{split} |(P_g + P_c) \times P_{cg}^{'}| &= |P_g + P_c| 2 \sin \frac{\theta}{2} \\ &\cdot \left( 4 - 4 \sin^2 \frac{\theta}{2} \right)^{-1/2} \sin \alpha \\ &= |P_g + P_c| \tan \frac{\theta}{2} \sin \alpha \\ &= 2|\overline{OB}| \sin \alpha \tan \frac{\theta}{2} \\ &= 2|\overline{AB}| \tan \frac{\theta}{2} = 2|\overline{CB}| \\ &= |\overline{CG}| = |P_c - P_g| \end{split}$$

**Lemma 6:**  $(P_{gij} + P_{cij}) \times P'_{cg} = P_{cij} - P_{gij}$ . Proof: direct consequence of Lemmas 4 and 5.

**Lemma 7:** Skew $(P_{gij} + P_{cij})$  is singular and has rank 2. Consequence: it is impossible to compute  $R_{cg}$  with only two stations, i.e. i=1, j=2 (two stations), we therefore need a minimum of j=3.

**Lemma 8:**  $(R_{gij} - I)T_{cg} = R_{cg}T_{cij} - T_{gij}$ . This follows from the translation terms of eq. (1).

**Lemma 9:**  $R_{gij} - I$  is singular and has rank 2. Consequence: it is impossible to compute  $R_{cg}$  with only two stations.

**Lemma 10:** If  $\theta_{R_{cg}} \neq \pi$ , or equivalently,  $|P_{cg}| \neq \pm 2$ , then

$$\begin{bmatrix} Skew(P_{gi_1j_1} + P_{ci_1j_1}) \\ Skew(P_{gi_2j_2} + P_{ci_2j_2}) \end{bmatrix}$$

has full column rank if and only if  $P_{gi_1j_1}$  and  $P_{gi_2j_2}$  have different directions (or equivalently  $P_{ci_1j_1}$  and  $P_{ci_2j_2}$  have different directions.

## Lemma 11:

$$\begin{bmatrix} R_{gi_1j_1} - I \\ R_{gi_2j_2} - I \end{bmatrix}$$

has full column rank if and only if we have different pairs of  $P_{gi_1j_1}$  and  $P_{gi_2j_2}$ .

In summary, procedure for computing  $R_{cg}$ :

1. Compute  $P'_{cg}$ . For each pair of stations i,j such that the rotation angle  $R_{gij}$  or  $R_{cij}$  is as large as possible, Figure 2. Set up a system of linear equations with  $P'_{cg}$  as the unknown

$$Skew(P_{gij} + P_{cij})P'_{cg} = P_{cij} - P_{gij}$$

Since  $Skew(P_{gij} + P_{cij})$  is always singular, it takes at least two pairs of stations to solve for a unique solution for  $P'_{cg}$  using least squares technique. **Exception handling:** If  $P_{gi_1j_1} + P_{ci_1j_1}$  is collinear with  $P_{gi_2j_2} + P_{ci_2j_2}$  while  $P_{gi_1j_1}$  is not collinear with  $P_{gi_2j_2}$ , then the rotation angle of  $R_{cg}$  must be  $180^o$  and the rotation axis the same as  $P_{gi_1j_1} + P_{ci_1j_1}$ .

2. (Optional: since step 3 which computes the rotation axis already captures this information through its magnitude) Compute  $\theta_{R_{cq}}$ :

$$\theta_{R_{cg}} = 2 \tan^{-1} |P'_{cg}|$$

3. Compute  $P_{cq}$ 

$$P_{cg} = \frac{2P_{cg}^{'}}{\sqrt{1 + |P_{cg}^{'}|^2}}$$

4. Compute  $T_{cg}$ . Given at least two distinct pairs of stations (i,j), set up a linear system of three linear equations with  $T_{cg}$  as unknowns

$$(R_{gij} - I)T_{cg} = R_{cg}T_{cij} - T_{gij}.$$

For at least two pairs of stations, two sets of the above equation are established and can be solved using least squares solutions.