

## **Codes :**

	<b>A</b>	<b>B</b>	<b>C</b>
(a)	4	1	3
(b)	3	2	5
(c)	4	1	5
(d)	3	2	4



## List I

- A. Activity number
  - B. Liquidity index
  - C. Sensitivity

## List II

1. (Liquid limit-water contenty)/ Plasticity index
  2. Plasticity index/Percent finer than 2 microns
  3. (Natural moisture content-plastic limit)/ Plasticity index
  4. Unconfined compressive strength of undisturbed soil sample/Unconfined compressive strength of remoulded soil sample

## **Codes :**

	<b>A</b>	<b>B</b>	<b>C</b>
(a)	1	3	4
(b)	1	2	3
(c)	3	2	1
(d)	2	3	4

- 66.** A soil has a bulk density of  $1.80 \text{ g/cm}^3$  at a water content of 5%. If the void ratio remains constant, then its bulk density for a water content of 10% will be  
 (a)  $1.98 \text{ g/cm}^3$       (b)  $1.88 \text{ g/cm}^3$   
 (c)  $1.80 \text{ g/cm}^3$       (d)  $1.70 \text{ g/cm}^3$

**67.** Consider the following statements.  
 1. Hydraulic gradient required to initiate "quick" condition is independent of the ratio of volume of voids to volume of solids in a soil mass.  
 2. Initiation of piping under hydraulic structures can be prevented by increasing the length of flow path of water.  
 3. Seepage pressure is independent of the coefficient of permeability.

**Of these statements**  
 (a) 1, 2 and 3 are correct (b) 1 and 2 are correct  
 (c) 1 and 3 are correct (d) 2 and 3 are correct

**68.** The appropriate triaxial test to assess the long-term stability of an unloading problem, such as excavation of a clay slope, would be the  
 (a) unconsolidated-undrained test  
 (b) consolidated-undrained test  
 (c) consolidated-drained test  
 (d) unconsolidated-drained test

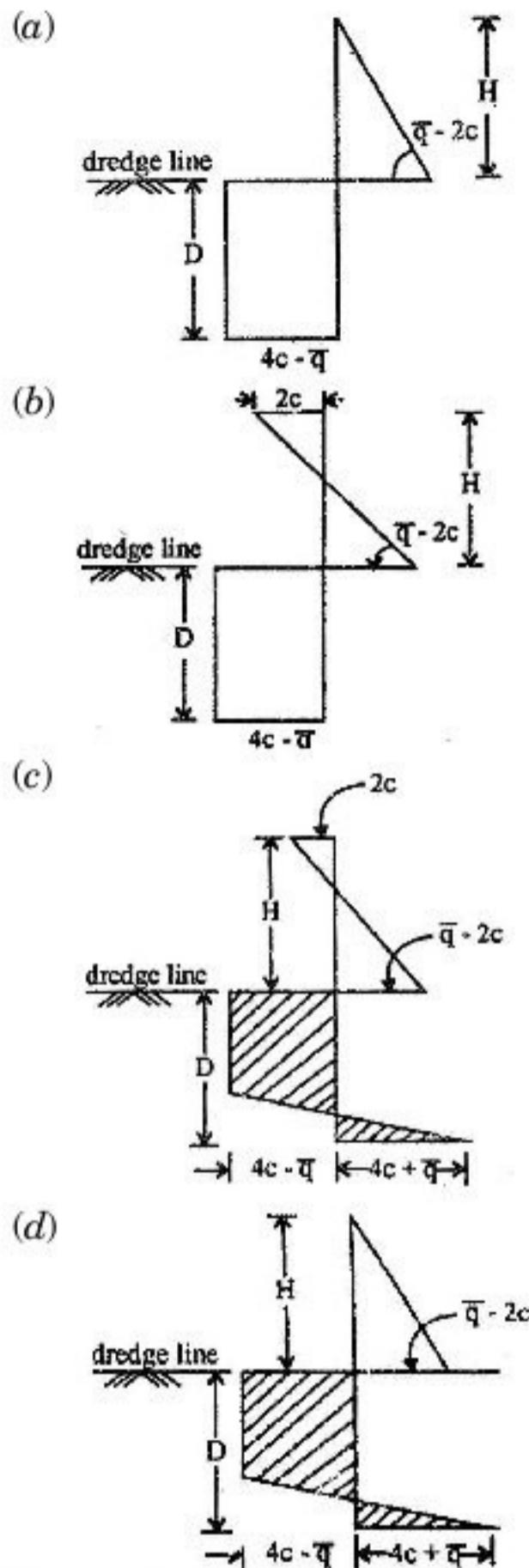
**69.** If a sample of dry sand tested in direct shear test gives failure shear stress  $\tau_f$  as  $1 \text{ kg/cm}^2$  at a normal stress  $\tau_n$  of  $2 \text{ kg/cm}^2$ , then the angle of internal friction of soil is given by  
 (a)  $\tan^{-1}(2)$       (b)  $\tan^{-1}(1)$   
 (c)  $\tan^{-1}(1/2)$       (d)  $\tan^{-1}(1/4)$

**70.** The Factor of Safety of an infinite slope in a sand deposit is found to be 1.732. The angle of shearing resistance of the sand is  $30^\circ$ . The average slope of the sand deposit is given by  
 (a)  $\sin^{-1}(0.333)$       (b)  $\cos^{-1}(0.252)$   
 (c)  $\tan^{-1}(0.333)$       (d)  $\cot^{-1}(0.621)$

**71.** In the soil sample of a consolidometer test, pore water pressure is  
 (a) minimum at the centre  
 (b) maximum at the top  
 (c) maximum at the bottom  
 (d) maximum at the centre

**4.68 | Soil Mechanics**





99. Lacustrine soils are soils

- (a) transported by rivers and streams
- (b) transported by glaciers
- (c) deposited in sea beds
- (d) deposited in lake beds

100. Consider the following statements in the context of aeolian soils :

1. The soil has low density of low compressibility.
2. The soil is deposited by wind.
3. The soil has large permeability.

**Of these statements**

- (a) 1, 2 and 3 are correct (b) 2 and 3 are correct
- (c) 1 and 3 are correct (d) 1 and 2 are correct

101. A fill having a volume of 1,50,000 cum is to be constructed at a void ratio of 0.8. The borrow pit soil has a void ratio of 1.4. The volume of soil required (in cubic metres) to be excavated from the borrow pit will be

- (a) 1,87,500 (b) 2,00,000
- (c) 2,10,000 (d) 2,50,000

102. Which one of the following equations correctly gives the relationship between the specific gravity of soil grains ( $G$ ) and the hydraulic gradient ( $i$ ) to initiate 'quick' condition in a sand having a void ratio of 0.5 ?

- (a)  $G = 0.5 i + 1$  (b)  $G = i + 0.5$
- (c)  $G = 1.5 i + 1$  (d)  $G = 1.5 i - 1$

103. A clay soil specimen when tested in unconfined condition gave an unconfined compressive strength of 100 kN/m<sup>2</sup>. A specimen of the same clay with the same initial condition is subjected to a UU triaxial test under a cell pressure of 100 kN/m<sup>2</sup>. The axial stress (in kN/m<sup>2</sup>) at failure would be

- (a) 150 (b) 200
- (c) 250 (d) 300

104. If  $s$  is the shear strength,  $c$  and  $\phi$  are shear strength parameters, and  $\sigma_n$  is the normal stress at failure, then Coulomb's equation for shear strength of the soil can be represented by

- (a)  $c = s + \sigma_n \tan \phi$  (b)  $c = s - \sigma_n \tan \phi$
- (c)  $s = \sigma_n + c \tan \phi$  (d)  $s = c - \sigma_n \tan \phi$

105. In a cohesionless soil deposit having a unit weight of 1.5 t/m<sup>3</sup> and an angle of internal friction of 30°, the active and passive lateral earth pressure intensities (in t/m<sup>2</sup>) at a depth of 10 m will, respectively, be

- (a) 15 and 5 (b) 5 and 45
- (c) 10 and 20 (d) 20 and 10

106. Given that for a soil deposit,

$$K_o = \text{earth pressure coefficient at rest},$$

$$K_a = \text{active earth pressure coefficient},$$

$$K_p = \text{passive earth pressure coefficient}$$

and  $\mu$  = Poisson's ratio,

the value of  $\frac{(1-\mu)}{\mu}$  is given by

- |                       |                       |
|-----------------------|-----------------------|
| (a) $\frac{K_a}{K_p}$ | (b) $\frac{K_o}{K_a}$ |
| (c) $\frac{K_p}{K_a}$ | (d) $\frac{1}{K_o}$   |

107. A and B are Skempton's pore pressure coefficients. For saturated normally consolidated soils,

- (a)  $A > 1$  and  $B > 1$  (b)  $A > 1$  and  $B < 1$
- (c)  $A < 1$  and  $B > 1$  (d)  $A < 1$  and  $B = 1$

108. If the actual observed value of standard penetration resistance,  $N$ , is greater than 15 in a fine sand layer below water table, then the equivalent penetration resistance will be

- (a)  $15 + \left[ \frac{(N+15)}{2} \right]$  (b)  $15 - \left[ \frac{(N+15)}{2} \right]$
- (c)  $15 + \left[ \frac{(N-15)}{2} \right]$  (d)  $15 + \left[ \frac{(15-N)}{2} \right]$

- 109.** Match List I (Property) with List II (Slope of the curve) and select the correct answer using the codes given below the Lists :

**List I**

- A. Coefficient of compressibility
- B. Compression index
- C. Coefficient sub-grade modulus

**List II**

- 1. Stress-deformation
- 2. Stress-void ratio
- 3. Volume-pressure
- 4. Log stress-void ratio

**Codes :**

A	B	C
(a) 4	2	2
(b) 4	3	2
(c) 2	4	1
(d) 3	4	1

- 110.** A dry sand specimen is put through a triaxial test. The cell pressure is 50 kPa and the deviator stress at failure is 100 kPa. The angle of internal friction for the sand specimen is

- (a) 15°
- (b) 30°
- (c) 37°
- (d) 45°

- 111.** The initial and final void ratios of a clay sample in a consolidation test are 1 and 0.5, respectively. If the initial thickness of the sample is 2.4 cm, then its final thickness will be

- (a) 1.3 cm
- (b) 1.8 cm
- (c) 1.9 cm
- (d) 2.2 cm

- 112.** In standard penetration test, the split-spoon sampler is penetrated into the soil stratum by giving blows from a drop weight whose weight (in kg) and free fall (in cm) are, respectively,

- (a) 30 and 60
- (b) 60 and 30
- (c) 65 and 75
- (d) 75 and 65

- 113.** Given that Plasticity Index (PI) of local soil = 15 and PI and sand = zero, for a desired PI of 6, the percentage of sand in the mix should be

- (a) 70
- (b) 60
- (c) 40
- (d) 30

- 114.** Consider the following statements :

A well-graded sand should have

- 1. uniformity coefficient grater than 6.
- 2. coefficient of curvature between 1 and 3
- 3. effective size greater than 1 mm.

**Of these statements**

- (a) 1, 2 and 3 are correct
- (b) 1 and 2 are correct
- (c) 2 and 3 are correct
- (d) 1 and 3 are correct

- 115.** Consider the following statements:

- 1. Increase in volume of a soil sample without external constraints on submergence in water is termed as the 'free swell of soil'.
- 2. Clay soil rich in montmorillonite exhibits very low swelling characteristic.
- 3. Generally, free swell of soil sample ceases when its water content reaches the plastic limit.

**Of these statements**

- (a) 1 and 2 are correct
- (b) 1 and 3 are correct
- (c) 2 and 3 are correct
- (d) 1, 2 and 3 are correct

- 116.** The configuration of flow nets depend upon

- (a) the permeability of the soil
- (b) the difference in the head between upstream and downstream sides
- (c) the boundary conditions of flow
- (d) the amount of seepage that takes place

- 117.** A soil has mass unit weight  $\gamma$ , water content  $w$  (as ratio). The specific gravity of soil solids = G, unit weight of water =  $\gamma_w$ , 'S', the degree of saturation of the soil is given by

$$(a) S = \frac{1+w}{\frac{\gamma_w}{\gamma}(1+w) - \frac{1}{G}} \quad (b) S = \frac{w}{\frac{\gamma_w}{\gamma}(1+w) - \frac{1}{G}}$$

$$(c) S = \frac{(1+w)}{\frac{\gamma_w}{\gamma}(1+w) - \frac{1}{wG}} \quad (d) S = \frac{w}{\frac{\gamma_w}{\gamma}(1+w) - \frac{1}{wG}}$$

- 118.** Shear failure of soils takes place when

- (a) the angle of obliquity is maximum
- (b) maximum cohesion is reached in cohesive soils
- (c)  $\phi$  reaches its maximum value in cohesionless soils
- (d) residual strength of the soil is exhausted.

- 119.** In a Mohr's diagram, a point above Mohr's envelope indicates

- (a) imaginary condition
- (b) safe condition
- (c) imminent failure condition
- (d) condition of maximum obliquity

- 120.** Minimum centre to centre spacing of friction piles of diameter (D) as per BIS code is

- (a) 1.5 D
- (b) 2 D
- (c) 2.5 D
- (d) 3 D

- 121.** A good quality undisturbed soil sample is one which is obtained using a sampling tube having an area ratio of

- (a) 8%
- (b) 16%
- (c) 24%
- (d) 32%

#### 4.72 Soil Mechanics

- 122.** Which one of the following tests cannot be done without undisturbed sampling?
- shear strength of sand
  - shear strength of clay
  - determination of compaction parameters
  - Atterberg limits
- 123.** If an unconfined compressive strength of  $4 \text{ kg/cm}^2$  in the natural state of clay reduces by four times in the remoulded state, then its sensitivity will be
- 1
  - 2
  - 4
  - 8
- 124.** In a direct shear test, the shear stress and normal stress on a dry sand sample at failure are  $0.6 \text{ kg/cm}^3$  and  $1 \text{ kg/cm}^2$  respectively. The angle of internal friction of the sand will be nearly
- $25^\circ$
  - $31^\circ$
  - $37^\circ$
  - $43^\circ$
- 125.** If an infinite slope of clay at a depth 5 m has cohesion of  $1 \text{ t/m}^2$  and unit wt. of  $2 \text{ t/m}^3$ , then the stability number will be
- 0.1
  - 0.2
  - 0.3
  - 0.4
- 126.** Given that  $c = 2 \text{ t/m}^2$ ,  $\phi = 0^\circ$  and  $\gamma = 2 \text{ t/m}^3$ , the depth of tension crack developing in a cohesive soil backfill would be
- 1 m
  - 2 m
  - 3 m
  - 4 m
- 127.** Which one of the following pairs of parameters and expressions is not correctly matched?
- Coefficient of consolidation ...  $\frac{T_v H^2}{t}$
  - Coeff. of volume compressibility ...  $\frac{e_0 - e}{(1 + e_0)(p - p_0)}$

(c) Over consolidation ratio ...

$$\sqrt{\frac{\text{Maximum previous effective pressure}}{\text{Existing effective pressure}}}$$

(d) Modulus of volume change ....  $\frac{a_v}{1 + e_0}$

**128.** Consider the following

- Initial consolidation
- Primary consolidation
- Secondary consolidation
- Final consolidation

The three stages which would be relevant to consolidation of a solid deposit includes

- 1, 2 and 3
- 2, 3 and 4
- 1, 3 and 4
- 1, 2 and 4

**129.** As per Terzaghi's equation, the bearing capacity of strip footing resting on cohesive soil ( $c = 10 \text{ kN/m}^2$ ) for unit depth and unit width (assume  $N_c$  as 5.7) is

- $47 \text{ kN/m}^2$
- $57 \text{ kN/m}^2$
- $67 \text{ kN/m}^2$
- $77 \text{ kN/m}^2$

**130.** With a vertical point load on the surface when considering the vertical plane passing through the load, the stress gets reduced by 52.3% at a depth of

- 0.25 of unit length
- 0.5 of unit length
- 0.75 of unit length
- 1 of unit length

**131.** Ratio of bearing capacity of double Under Reamed (U.R.) pile to that of single U.R. pile is nearly

- 2
- 1.5
- 1.2
- 1.7

**132.** A raft of  $6 \text{ m} \times 9 \text{ m}$  is founded at a depth of 3 m in a cohesive soil having  $c = 120 \text{ kN/m}^2$ . The ultimate net bearing capacity of the soil using Terzaghi's theory will be nearly

- $820 \text{ kN/m}^2$
- $920 \text{ kN/m}^2$
- $1036 \text{ kN/m}^2$
- $1067 \text{ kN/m}^2$

## EXERCISE - II

### (Questions From Previous SSC CPWD Exams)

#### 2008

1. A footing is resting on fully saturated clayey strata for checking the initial stability shear parameter are used from
- Consolidated undrained test
  - Unconsolidated drained test
  - Unconsolidated undrained test
  - Unconsolidated undrained test with pore pressure measurement

2. Coefficient of active earth pressure for cohesion less soil is given by

- $\frac{1 + \sin \theta}{1 - \sin \theta}$
- $\frac{1 - \sin \theta}{1 + \sin \theta}$
- $\frac{1 + \tan \theta}{1 - \tan \theta}$
- $\frac{1 + \cos \theta}{1 - \cos \theta}$

3. For routine consolidation test in laboratory, the thickness of the specimen is

- 10 mm
- 20 mm
- 40 mm
- 60 mm

2009

- 8.** The rate of consolidation.

  - (a) Increases with decrease in temperature.
  - (b) Increases with increase in temperature.
  - (c) Is independent of temperature.
  - (d) All the above.

**9.** Cohesionless soil is

  - (a) Silt
  - (b) Sand
  - (c) Clay
  - (d) None of the above

**10.** Physical properties which influence permeability are

  - (a) Viscosity only
  - (b) Unit weight only
  - (c) Both viscosity and unit weight
  - (d) None of the above

11. If the voids of a soil mass are full of air only, the soil is termed as

  - (a) Air entrained soil
  - (b) Partially saturated soil
  - (c) Dry soil
  - (d) None of the above

12. The ratio of volume of voids to the total volume of the soil mass is called

  - (a) Air content
  - (b) Porosity
  - (c) Voids ratio
  - (d) All the above

13. Pycnometer is used to determine

  - (a) Water content and voids ratio
  - (b) Specific gravity and dry density
  - (c) Water content and specific gravity
  - (d) None of the above

2011



$$(a) \gamma_d = \frac{(1+n_a)G\gamma_w}{1+wG} \quad (b) \gamma_d = \frac{(1+n_a)G\gamma_w}{1-wG}$$

$$(c) \gamma_d = \frac{(1-n_a)G\gamma_w}{1+wG} \quad (d) \gamma_d = \frac{(1-n_a)G\gamma_w}{1-wG}$$

28. A shallow foundation is defined as a foundation which

  - (a) has low bearing capacity
  - (b) has a depth of embedment less than its width
  - (c) is resting on the ground surface
  - (d) causes less settlement

2012

29. Water content of soil can

  - (a) Be less than 0%
  - (b) Be greater than 100%
  - (c) Never be greater than 100%
  - (d) Take values only from 0% to 100%

30. The coefficient of active earth pressure for a loose sand having an angle of internal friction ' $\phi$ ' is

(a)  $\frac{1 - \sin \frac{\phi}{2}}{1 + \sin \frac{\phi}{2}}$       (b)  $\frac{1 + \sin \frac{\phi}{2}}{1 - \sin \frac{\phi}{2}}$   
 (c)  $\frac{1 - \sin \phi}{1 + \sin \phi}$       (d)  $\frac{1 + \sin \phi}{1 - \sin \phi}$

- 31.** A plate load test is useful to estimate

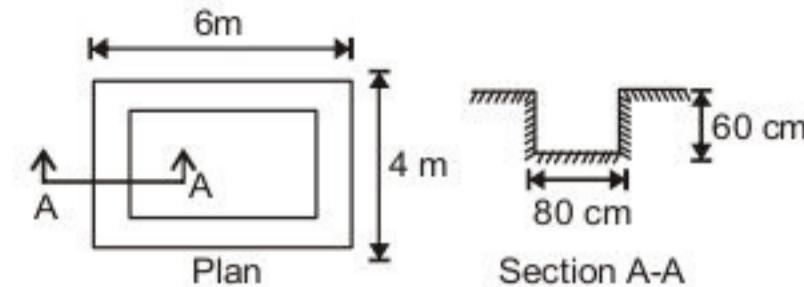
  - (a) Both bearing capacity and settlement of foundation
  - (b) Consolidation of soil
  - (c) Bearing capacity of foundation
  - (d) Settlement of foundation

**32.** The unit of the coefficient of consolidation is

  - (a) gm/cm<sup>2</sup>/sec
  - (b) gm–cm/sec
  - (c) cm<sup>2</sup>/sec
  - (d) cm<sup>3</sup>/sec

2013

- 33.** Anti-siphonage pipe is connected to  
(a) Main soil pipe      (b) Bottom of P trap W.C.  
(c) Top of P trap W.C. (d) Side of Water Closet



The above figure represents plan and section of an excavation layout. The volume of earthwork in excavation of foundation trench is

- (a) 6.528 cu.m.      (b) 8.064 cu.m.  
(c) 8.832 cu. m.      (d) 9.600 cu. m.

**35.** A shallow foundation is defined as a foundation which

  - (a) has low bearing capacity
  - (b) has a depth of embedment less than its width
  - (c) is resting on the ground surface
  - (d) causes less settlement

- 36.** If the volume of voids is equal to the volume of solids in a soil mass, than the values of porosity and voids ratio respectively are

(a) 1.0 and 0.0      (b) 0.0 and 1.0  
(c) 1.5 and 1.0      (d) 1.0 and 0.5

- 37.** The lime stabilization is very effective in treating  
(a) Sandy soils                    (b) Silty soils  
(c) Non-plastic soils              (d) Plastic clayey soils






(a)  $n = \frac{1+e}{1-e}$       (b)  $e = n(1+n)$   
 (c)  $n = \frac{e}{1-e}$       (d)  $e = \frac{1+n}{1-n}$

- 41.** When the plastic limit of a soil is greater than the liquid limit, then the plasticity index is reported as :  
 (a) 1 (b) Negative  
 (c) Zero (d) Non-Plastic(NP)
- 42.** Compression members always tend to buckle in the direction of the :  
 (a) Least radius of gyration  
 (b) Axis of load  
 (c) Perpendicular to the axis of load  
 (d) Minimum cross-section
- 2015**
- 43.** Black cotton soil is not suitable for foundation because of its  
 (a) low bearing capacity  
 (b) cohesive particles  
 (c) swelling and shrinkage  
 (d) black colour
- 44.** Optimum moisture content is obtained from  
 (a) triaxial test (b) standard proctor test  
 (c) consolidation test (d) hydrometer test
- 45.** The effective size of particles of soil is denoted by  
 (a)  $D_{10}$  (b)  $D_{20}$   
 (c)  $D_{30}$  (d)  $D_{60}$
- 46.** When the plasticity index of a soil is zero, the soil is  
 (a) Clay (b) Silt  
 (c) Sand (d) Silty sand
- 47.** The depth of foundation is usually calculated from  
 (a) Rankine's formula  
 (b) Newton's formula  
 (c) De Almbert's formula  
 (d) Gutter's formula
- 48.** Pollution potential of domestic sewage generated in a town and its industrial sewage can be compared with reference to  
 (a) their BOD value  
 (b) population equivalent  
 (c) their volume  
 (d) the relative density

## ANSWERS

### EXERCISE - I

- |                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| <b>1.</b> (c)   | <b>2.</b> (b)   | <b>3.</b> (b)   | <b>4.</b> (d)   | <b>5.</b> (d)   | <b>6.</b> (b)   | <b>7.</b> (b)   | <b>8.</b> (c)   | <b>9.</b> (c)   | <b>10.</b> (a)  |
| <b>11.</b> (d)  | <b>12.</b> (c)  | <b>13.</b> (c)  | <b>14.</b> (c)  | <b>15.</b> (c)  | <b>16.</b> (d)  | <b>17.</b> (c)  | <b>18.</b> (a)  | <b>19.</b> (b)  | <b>20.</b> (d)  |
| <b>21.</b> (d)  | <b>22.</b> (a)  | <b>23.</b> (b)  | <b>24.</b> (a)  | <b>25.</b> (c)  | <b>26.</b> (a)  | <b>27.</b> (c)  | <b>28.</b> (c)  | <b>29.</b> (a)  | <b>30.</b> (b)  |
| <b>31.</b> (c)  | <b>32.</b> (b)  | <b>33.</b> (c)  | <b>34.</b> (c)  | <b>35.</b> (d)  | <b>36.</b> (b)  | <b>37.</b> (b)  | <b>38.</b> (c)  | <b>39.</b> (b)  | <b>40.</b> (b)  |
| <b>41.</b> (b)  | <b>42.</b> (b)  | <b>43.</b> (d)  | <b>44.</b> (d)  | <b>45.</b> (b)  | <b>46.</b> (c)  | <b>47.</b> (c)  | <b>48.</b> (d)  | <b>49.</b> (d)  | <b>50.</b> (d)  |
| <b>51.</b> (d)  | <b>52.</b> (a)  | <b>53.</b> (a)  | <b>54.</b> (b)  | <b>55.</b> (c)  | <b>56.</b> (c)  | <b>57.</b> (c)  | <b>58.</b> (a)  | <b>59.</b> (b)  | <b>60.</b> (b)  |
| <b>61.</b> (b)  | <b>62.</b> (c)  | <b>63.</b> (a)  | <b>64.</b> (d)  | <b>65.</b> (d)  | <b>66.</b> (b)  | <b>67.</b> (c)  | <b>68.</b> (c)  | <b>69.</b> (c)  | <b>70.</b> (c)  |
| <b>71.</b> (d)  | <b>72.</b> (c)  | <b>73.</b> (c)  | <b>74.</b> (c)  | <b>75.</b> (b)  | <b>76.</b> (b)  | <b>77.</b> (b)  | <b>78.</b> (d)  | <b>79.</b> (c)  | <b>80.</b> (a)  |
| <b>81.</b> (b)  | <b>82.</b> (a)  | <b>83.</b> (a)  | <b>84.</b> (b)  | <b>85.</b> (c)  | <b>86.</b> (b)  | <b>87.</b> (d)  | <b>88.</b> (d)  | <b>89.</b> (d)  | <b>90.</b> (b)  |
| <b>91.</b> (c)  | <b>92.</b> (b)  | <b>93.</b> (b)  | <b>94.</b> (d)  | <b>95.</b> (d)  | <b>96.</b> (c)  | <b>97.</b> (d)  | <b>98.</b> (c)  | <b>99.</b> (d)  | <b>100.</b> (b) |
| <b>101.</b> (b) | <b>102.</b> (c) | <b>103.</b> (b) | <b>104.</b> (c) | <b>105.</b> (b) | <b>106.</b> (d) | <b>107.</b> (c) | <b>108.</b> (c) | <b>109.</b> (c) | <b>110.</b> (b) |
| <b>111.</b> (b) | <b>112.</b> (c) | <b>113.</b> (b) | <b>114.</b> (b) | <b>115.</b> (b) | <b>116.</b> (c) | <b>117.</b> (a) | <b>118.</b> (a) | <b>119.</b> (a) | <b>120.</b> (d) |
| <b>121.</b> (a) | <b>122.</b> (b) | <b>123.</b> (c) | <b>124.</b> (b) | <b>125.</b> (a) | <b>126.</b> (b) | <b>127.</b> (c) | <b>128.</b> (a) | <b>129.</b> (b) | <b>130.</b> (d) |
| <b>131.</b> (b) | <b>132.</b> (a) |                 |                 |                 |                 |                 |                 |                 |                 |

### EXERCISE - II

- |                |                |                |                |                |                |                |                |                |                |
|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| <b>1.</b> (c)  | <b>2.</b> (b)  | <b>3.</b> (d)  | <b>4.</b> (a)  | <b>5.</b> (a)  | <b>6.</b> (b)  | <b>7.</b> (a)  | <b>8.</b> (b)  | <b>9.</b> (b)  | <b>10.</b> (c) |
| <b>11.</b> (c) | <b>12.</b> (b) | <b>13.</b> (c) | <b>14.</b> (b) | <b>15.</b> (b) | <b>16.</b> (c) | <b>17.</b> (a) | <b>18.</b> (c) | <b>19.</b> (b) | <b>20.</b> (d) |
| <b>21.</b> (a) | <b>22.</b> (d) | <b>23.</b> (d) | <b>24.</b> (b) | <b>25.</b> (b) | <b>26.</b> (c) | <b>27.</b> (c) | <b>28.</b> (b) | <b>29.</b> (b) | <b>30.</b> (c) |
| <b>31.</b> (a) | <b>32.</b> (c) | <b>33.</b> (c) | <b>34.</b> (b) | <b>35.</b> (b) | <b>36.</b> (d) | <b>37.</b> (d) | <b>38.</b> (c) | <b>39.</b> (d) | <b>40.</b> (b) |
| <b>41.</b> (c) | <b>42.</b> (a) | <b>43.</b> (c) | <b>44.</b> (c) | <b>45.</b> (a) | <b>46.</b> (c) | <b>47.</b> (a) | <b>48.</b> (b) |                |                |

## EXPLANATIONS

### **EXERCISE-II**

1. A footing is resting on fully saturated clayey strata for checking the initial stability, shear parameter are used from Unconsolidated undrained test.

2. Coefficient of active earth pressure ( $K_a$ )

$$K_a = \frac{1 - \sin \theta}{1 + \sin \theta} = \tan^2 \left( 45 - \frac{\theta}{2} \right)$$

Where,  $\theta$  = angle of internal friction

3. For performing consolidation the test, a soil sample of **60 mm dia** is taken as per ISI standards. Samples of 50, 70 and 100 mm dia may also be used in special cases. The sample thickness should not be less than 10 times the maximum dia of the soil grains, and the dia to thickness ratio of the sample should be minimum of 3.

4. Factors affecting permeability (K)-

1. Grain size-  $K \propto D_{10}^2$

2. Properties of water-  $K \propto \frac{\gamma_w}{\mu}$

→ With increases temperature, viscosity ( $\mu$ ) decreases; and hence K increases

3. Void ratio of soil-  $K \propto e^2$

4. Degree of saturation-  $K \propto S$

5. Shape of particles-  $K \propto \frac{1}{s^2}$

(Specific surface area  $s$  = Surface Area/Volume)

6. Temperature-  $K \propto \text{Temp}$

7. Impurities present in water block the voids and hence permeability reduces

8. Adsorbed water hinders the flow under gravity. Hence K is reduces.

5. Critical hydraulic gradient  $i_c = \frac{G-1}{1+e}$

Where,

$G$  = Specific gravity and  $e$  = void ratio

Hence increasing void ratio, the critical hydraulic gradient will decrease.

6. In a compaction test, as the compaction effort is increased, the optimum moisture content decreases.

7. Relationship between void ratio 'e' and porosity 'n' is given by

$$n = \frac{e}{1+e}$$

$$n(1+e) = e$$

$$n + ne = e$$

$$n = e - ne$$

$$n = e(1 - n)$$

$$\therefore e = \frac{n}{1-n} = \frac{0.562}{1-0.562} = 1.283 \text{ (since } n = 0.562\text{)}$$

8. Factors affecting rate of consolidation-

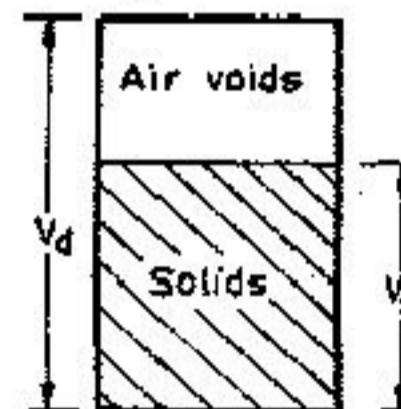
- The rate of consolidation increases with increase in temperature.
- Decreases with increase of liquid limit.
- Changes with increase in effective stress etc.

9. **Cohesionless soil**-Lacking cohesion among particles, such as in the case of sand a Cohesionless soil.

Any free-running type of soil, such as sand or gravel, whose strength depends on friction between particles is called Cohesionless soil. Also called frictional.

**Cohesive soil**-It is hard to break up when dry, and exhibits significant cohesion when submerged. Cohesive soils include clayey silt, sandy clay, silty clay, clay and organic clay. "Dry soil" means soil that does not exhibit visible signs of moisture content.

11. If the voids of a soil mass are full of air only, the soil is termed as Dry soil.



12. **Air content**- The ratio of volume of air voids to

the total volume of the voids, i.e.  $a_c = \frac{V_a}{V_v}$

**Porosity**- The ratio of volume of voids to the

total volume of the soil mass. i.e.  $n = \frac{V_v}{V}$

**Voids ratio**- The ratio of volume of voids to the

volume of the solids, i.e.  $e = \frac{V_v}{V_s}$

13. **Pycnometer**- is a glass jar of about 1 litre capacity and fitted with a brass conical cap by means of a screw-type cover. The cap has a small hole of 6 mm diameter at its apex.

Pycnometer is used to determine water content and specific gravity.

**14. Plasticity index  $I_p = \omega_L - \omega_P$** 

When the plastic limit of a soil is greater than the liquid limit, then the plasticity index is reported as zero soil will be non-plastic.

**16. A septic tank combines the function of a sedimentation tank, a sludge digestion tank and a sludge storage tank.****18. The bleaching powder is a white powder and it contains about 30 to 35 per cent of available chlorine****19. Sewage treatment units are normally designed for 15-20 years.****20. Factors Affecting Shear strength of Cohesionless Soil-**

- Shear strength of cohesionless soils is only developed with the presence of effective stress.
- Shear strength increases with increasing effective stress.
- The increase of shear strength of cohesionless soil depends upon the internal friction angle of the soil.
- The type of soil most susceptible to liquefaction is one in which the resistance to deformation is mobilized by friction between particles. If other factors such as grain shape, uniformity coefficient and relative density are equal, the frictional resistance of cohesion less soil decreases as the grain size of soils becomes smaller.

$$21. \text{ Time factor } T_v = \frac{C_v t}{d^2} \Rightarrow C_v = \frac{d^2 T_v}{t}$$

$$22. \text{ Liquidity index } I_L = \frac{w - w_p}{w_L - w_p} = \frac{w - w_p}{I_p}$$

**Shrinkage ratio** - It is defined as the ratio of a given volume change in a soil expressed as a percentage of dry volume to the corresponding change in water content above the shrinkage limit.

$$R = \frac{\frac{V_1 - V_2}{V_d} \times 100}{w_1 - w_2}$$

**Consistency index-**

$$I_c = \frac{w_L - w}{w_L - w_p} = \frac{w_L - w}{I_p}$$

**23. Coefficient of curvature or coefficient of gradation or coefficient of concavity ( $C_c$ )**

$$C_c = \frac{D_{30}^2}{D_{60} \times D_{10}}$$

For well graded soil  $C_c$  should be between 1 to 3.  
i.e.  $1 \leq C_c \leq 3$

**24. Coefficient Of Earth Pressure at Rest ( $K_0$ )-**

$$K_0 = \frac{\mu}{(1 - \mu)}$$

- For a perfectly cohesion-less soil ( $C = 0$ )

$$K_0 = (1 - \sin \phi)$$

- If the soil normally consolidated (N.C. soil)

$$K_0 = 0.19 + 0.2331 \log_{10}(I_p)$$

- For over consolidated soil (OC soil)

$$K_{0(OC)} = K_{0(NC)} \sqrt{O.C.R.}$$

Where,  $\mu$  = poission's ratio

$\phi$  = friction angle

$I_p$  = plasticity index

O.C.R. = over consolidated ratio

**26. Relative density / density index or degree of density ( $I_D$ ) (its range 0 to 1)**

$$I_D = \frac{l_{max} - l}{l_{max} - l_{min}}$$

Where,

$l_{max}$  = maximum void ratio,

$l_{min}$  = minimum void ratio

$l$  = natural void ratio

(when the soil is undisturbed)

In dense condition,

$$l = l_{min}$$

$$\therefore I_D = \frac{l_{max} - l_{min}}{l_{max} - l_{min}} = 1.0$$

But 1.0 is not available in choices, so we take the nearest value of 1.0 i.e. 0.95.

So answer is (c).

**28. A foundation is shallow if its depth is equal to less then its width.****34. Volume of excavation at section A-A**

$$\Rightarrow 80 \text{ cm} \times 60 \text{ cm}$$

$$\Rightarrow 4800 \text{ cm}^2$$

Perimeter of excavation

$$\Rightarrow 4 + 4 + 2 (6 - (2 \times .8 \text{ m}))$$

$$\Rightarrow 4 + 4 + 8.8$$

$$\Rightarrow 16.8 \text{ m}$$

Volume of whole excavation

$$\Rightarrow \frac{4800}{(100)^2} \times 16.8 \text{ m}$$

$$\Rightarrow 8.064 \text{ m}^3$$

$$\text{or} = 8.064 \text{ cu.m}$$

**35. Shallow foundation ( $D < B$ )**

Deep foundation ( $D > B$ )

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36. According to question  $Vv = Vs$

$$(\text{Void Ratio}) e \Rightarrow \frac{Vv}{Vs} \Rightarrow 1.0$$

$$(\text{Porosity}) n = \frac{e}{1+e} \Rightarrow \frac{1}{1+1} \Rightarrow 0.5$$

37. Hydrated lime (or slaked) lime is very effective in treating heavy, plastic clayey soil.

38. For clayey soil (cohesive soil)

$$\rho_p = \rho_f \cdot \frac{B_p}{B}$$

$$\therefore \rho_f = \rho_p \cdot \frac{B}{B_p}$$

$$\rho_f = 15 \times \frac{1000}{300} = 50 \text{ mm}$$

where  $\rho_f$  = Settlement of footing

$\rho_p$  = Settlement of plate

B = Breadth of footing

$B_p$  = Breadth of Plate

40. Relationship between void ratio 'e' and porosity 'n'

$$n = \frac{e}{1+e}$$

$$\therefore n = e(1-n)$$

$$\therefore 1-n = \frac{1}{1+e}$$

42. Compression members always tend to buckle in the direction of the Least radius of gyration. The radius of gyration ( $r$ ) of a section is given by

$$r = \sqrt{I/A}$$

Where I = moment of inertia

A = area of the section

43. Because black soil has high plasticity index.

44. Optimum moisture content is obtained from standrd proctor test because it contains the density of maximum dryness.

45.  $D_{10} \rightarrow 10\%$  of sample finer in weight on Grain Size Distribution Curve.

46. Because clay contains high plasticity index and sand contains zero plasticity index.

47. Depth of foundation is calculated from Ramekin formula.

48. Population equivalent

$$= \frac{\text{B.O.D. Industrial (5 days)}}{\text{B.O.D. domestic sewage/person/day}}$$

■ ■