

## Notes on rigid body dynamics - algorithms

### Dynamics of a constrained rigid body

Consider a rigid body constrained to move in subspace  $S \subseteq M^6$

Let  $n_c$  be the number of constraints, and  $n_f$  the number of degrees of freedom

$$n_f = \dim(S) \quad (\text{no. of basis vectors in } S)$$

$$n_c = 6 - n_f = \dim(S^\perp)$$

Equation of motion

$$\underbrace{f}_{\substack{\text{applied} \\ \text{force}}} + \underbrace{f_c}_{\substack{\text{constraint} \\ \text{force}}} + \underbrace{f_g}_{\text{gravity}} = I\alpha + v \times^* I v$$

Define bias force  $p = v \times^* I v - f_g$ , so equation is

$$f + f_c = I\alpha + p$$

subject to  $v \in S$ ,  $f_c \in S^\perp$

Method 1:

Define  $6 \times n_f$  matrix  $\underline{S}$  with columns that span  $S$ .

$$v = \underline{S} \dot{q} \quad \text{and} \quad \underline{S}^T f_c = 0$$

Acceleration constraint  $\alpha = \underline{S} \ddot{q} + \dot{\underline{S}} \dot{q}$

Now eliminate  $f_c$  by projecting equations onto  $S$ :

$$\underline{S}^T f + \cancel{\underline{S}^T f_c} = \underline{S}^T I \alpha + \underline{S}^T p \rightarrow \underline{S}^T f = \underline{S}^T I \underline{S} \ddot{q} + \cancel{\underline{S}^T I \dot{\underline{S}} \dot{q}} + \underline{S}^T p$$

$$\therefore \boxed{\ddot{q} = (\underline{S}^T I \underline{S})^{-1} \underline{S}^T (f - I \underline{S} \ddot{q} - p)}$$

(This is approach taken in Eldredge JCP 2008)

$$\text{Then } \dot{\alpha} = \Phi f + b \quad \Phi = \underline{S} (\underline{S}^T I \underline{S})^{-1} \underline{S}^T \quad \text{apparent inverse inertia}$$

$$b = \dot{\underline{S}} \ddot{q} - \Phi (I \underline{S} \ddot{q} + p) \quad \text{bias acceleration}$$

$$\text{range}(\Phi) = S, \text{ null}(\Phi) = S^\perp, \text{rank}(\Phi) = n_f$$

Method 2:

Introduce  $6 \times n_c$  matrix  $\underline{I}$  whose columns span  $S^\perp$

$$\underline{T}^T v = 0, \quad f_c = T\lambda$$

Then acceleration constraint is  $\underline{T}^T a + \dot{\underline{T}}^T v = 0$

$$\text{Substitute: } f + T\lambda = Ia + p \rightarrow \begin{bmatrix} I & T \\ T^T & 0 \end{bmatrix} \begin{bmatrix} a \\ -\lambda \end{bmatrix} = \begin{bmatrix} f - p \\ -\dot{T}^T v \end{bmatrix}$$

Method 3:

Solve in generalized coordinates. Define  $\tau$  as generalized force.

Both  $\tau$  and  $f$  must deliver same power for any velocity in  $S$

$$\tau^T \dot{q} = f^T v = f^T S \dot{q} \rightarrow \tau = S^T f \quad \text{removes } f_c \text{ from } f$$

Then, equation for  $\ddot{q}$  from method 1 is

$$\ddot{q} = (S^T I S)^{-1} (\tau - S^T (I S \dot{q} + p))$$

Write this in standard generalized form

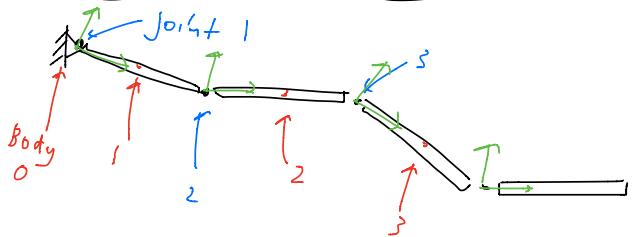
$$H \ddot{q} + C = \tau$$

$S^T I S$        $S^T (I S \dot{q} + p)$

Questions :

- (1) How do we classify the nullspace method in this list?  
Can we identify the nullspace matrix  $Z$  with matrices presented here?
- (2) Relate link assembly and equations in Eldredge JCP 2008 to these (Meth 1)
- (3) Develop free swimming linkage methods with specific details
- (4) Relate linkage construction in DynPlate to these methods

## Assembly of linked rigid bodies



Given  $v_{0j}, \alpha_{0j}$

$$I_j = {}^j X_c^* I_{c,j} {}^c X_j$$

$$v_{rj} = S \dot{\theta}_j \rightarrow v_j = {}^j X_{j-1} v_{j-1} + S \dot{\theta}_j$$

$$c_j = v_j \times S \dot{\theta}_j \leftarrow \alpha_j = S \ddot{\theta}_j + \underbrace{{}^j X_{j-1} \alpha_{j-1}}_{\alpha'} + \underbrace{c_j}_{\alpha'}$$

$$\begin{aligned} p_j &= v_j \times {}^j I_j v_j - {}^j X_c^* f_{ex,j} \\ {}^{j+1} X_c &= {}^j X_c {}^j X_c \end{aligned}$$

for  $j = N_b, \dots, 1$

$$U_j = {}^j I_j^A \Sigma$$

$$D_j = \Sigma^T {}^j I_j^A \Sigma$$

$$\tau_j = -R_j \dot{\theta}_j - K_j \theta_j$$

$$u_j = \tau_j - \Sigma^T p_j^A$$

if  $j > 1$

$$I^A = {}^j I_j^A - U_j D_j^{-1} U_j^T = {}^j I_j^A - {}^j I_j^A \Sigma (\Sigma^T {}^j I_j^A \Sigma)^{-1} \Sigma^T ({}^j I_j^A)$$

$$p^A = p_j^A + I^A c_j + U_j D_j^{-1} u_j = p_j^A + I^A c_j + {}^j I_j^A \Sigma (\Sigma^T {}^j I_j^A \Sigma)^{-1} (\tau_j - \Sigma^T p_j^A)$$

$$I_{j-1}^A = {}^j I_{j-1}^A + {}^{j-1} X_j^* I^A {}^j X_{j-1}$$

$$p_{j-1}^A = p_{j-1} + {}^{j-1} X_j^* p^A$$

end

for  $j = 1, \dots, N_b$

$$\alpha^A = {}^j X_{j-1} \alpha_{j-1} + c_j$$

$$\ddot{\theta}_j = D_j^{-1} (u_j - U_j^T \alpha^A)$$

$$\alpha_j = \alpha^A + S \ddot{\theta}_j$$

end

$$j = N_b$$

$$f_j = I_j \alpha_j + p_j$$

$\alpha' + S\theta_j$

$$= I_j S\theta_j + I_j \alpha' + p_j$$

Project onto  $\alpha'$ :  $0 = \underbrace{S^T I_j S\theta_j}_{D_j} + \underbrace{S^T I_j \alpha'}_{U_j^\top} + \underbrace{S^T p_j - f_j}_{-u_j} \rightarrow \begin{cases} D_j \theta_j = u_j - U_j^\top \alpha' \\ \theta_j = D_j^{-1} (u_j - U_j^\top \alpha') \end{cases}$

Solve for  $f_j$ :

$$\rightarrow f_j = I_j S\theta_j + I_j \alpha' + p_j$$

$$= I_j S D_j^{-1} (u_j - U_j^\top \alpha') + I_j \alpha' + p_j$$

$$= \underbrace{(I_j - I_j S D_j^{-1} U_j^\top)}_{I_j^\alpha} \alpha' + I_j S D_j^{-1} u_j + p_j$$

$$\rightarrow f_j = I_j^\alpha \alpha_{j-1} + \underbrace{p_j + I_j^\alpha c_j}_{p_j^\alpha} + I_j S D_j^{-1} u_j \rightarrow \boxed{I_j^\alpha f_j = I_j^\alpha \alpha_{j-1} + I_j^\alpha p_j^\alpha}$$

Each body  $j < N_b \rightarrow$

$$\begin{aligned} f_{j-1} &= I_{j-1} \alpha_{j-1} + p_{j-1} + I_{j-1}^\alpha f_j \\ &= \underbrace{(I_{j-1} + I_j^\alpha + I_j^\alpha I_{j-1})}_{I_{j-1}^\alpha} \alpha_{j-1} + \underbrace{p_{j-1} + I_j^\alpha p_j^\alpha}_{p_{j-1}^\alpha} \end{aligned}$$

$$\left. \right\} \boxed{f_{j-1} = I_{j-1}^\alpha \alpha_{j-1} + p_{j-1}^\alpha}$$

Multiply by  $Z_p^T = P_{v_p}^T D^{-T}$

$$\underbrace{Z_p^T H Z_p}_{\tilde{H}_p} \quad \ddot{\tilde{q}} = Z_p \ddot{\tilde{q}}_p + Z_A \ddot{\tilde{q}}_A + D^{-1} c$$

$$(Z_p = D^{-1} P_{v_p}, Z_A = D^{-1} P_{v_A})$$

$$\boxed{\tilde{H}_p \ddot{\tilde{q}}_p = Z_p^T (\tau - H D^{-1} c - H Z_A \ddot{\tilde{q}}_A) + \tau_p}$$

Note that  $D^{-1} = \begin{pmatrix} I & X_{J_1} \\ X_{J_1}^T & X_{J_2} \\ \vdots & \ddots \\ X_{J_n}^T & \dots & \dots & X_{J_m} \end{pmatrix}$

$$\underbrace{H \ddot{\tilde{q}} - K^T \lambda}_{\tau} = \tau + D^T P_{v_p} \tau_p + D^T P_{v_A} \tau_A$$

The articulated body inertia  $I_j^A$  and the bias force  $p_j^A$  allow us to write

$$f_j = I_j^A \dot{q}_j + p_j^A$$

where  $f_j$  is force transmitted across joint  $j$  (the parent joint)

Also,  $P_{v_p}^T f_j = \tau_{pj}$  (passive force)

so  $\tau_{pj} = P_{v_p}^T I_j^A \dot{q}_j + P_{v_p}^T p_j^A$

If  $j=1$ , then we have

$$\tau_{p1} = P_{v_p1}^T I_1^A \dot{q}_1 + P_{v_p1}^T p_1^A \rightarrow P_{v_p1}^T I_1^A P_{v_p1} \ddot{\tilde{q}}_{1p} = \tau_{p1} - \underbrace{P_{v_p1}^T J_1^A (P_{v_A} \ddot{\tilde{q}}_{1A} + P_{v_p1} \dot{q}_{1p})}_{-P_{v_p1}^T p_1^A}$$

$$\text{Thus } \ddot{\tilde{q}}_{1p} = (P_{v_p1}^T I_1^A P_{v_p1})^{-1} \left[ \tau_{p1} - P_{v_p1}^T (p_1^A + J_1^A (c_1 + P_{v_A} \ddot{\tilde{q}}_{1A})) \right]$$

In general,

$$\boxed{\ddot{\tilde{q}}_{j1p} = (P_{v_pj}^T I_j^A P_{v_pj})^{-1} \left[ \tau_{pj} - P_{v_pj}^T (p_j^A + I_j^A (a_{xj1} + c_j + P_{v_A} \ddot{\tilde{q}}_{j1A})) \right]}$$

$$\boxed{a_j = a_{xj1} + c_j + P_{v_pj} \ddot{\tilde{q}}_{j1p}}$$

Define  $U_j = I_j^A P_{up_j}$   $\Phi_j = (P_{up_j}^\top U_j) \bar{U}_j^{-1}$   $u_j = \tau_{pj} - P_{up_j}^\top p_j^A$   $a_j' = a_{pj} + c_j'$

$$\boxed{\begin{aligned}\dot{\tilde{q}}_{pj} &= \Phi_j (u_j - U_j^\top a_j') \\ a_j &= a_j' + P_{up_j} \dot{\tilde{q}}_{pj}\end{aligned}}$$

Also, note that

$$\begin{aligned}I_j^A &= I_j + \sum_{i \in \mu(j)} I_i^A & I_j^A &= I_j - U_j \Phi_j U_j^\top \\ p_j^A &= p_j + \sum_{i \in \mu(j)} p_i^A & p_j^A &= p_j + I_j^\top c_j + U_j \Phi_j u_j\end{aligned}$$

Check this...

For  $i \in \mu(j)$ ,  $f_i = I_i^A a_i + p_i^A$

But  $a_i = a_{\lambda(i)} + c_i + P_u \dot{\tilde{q}}_i$ , so  $f_i = I_i^A a_{\lambda(i)} + I_i^\top (c_i' + P_{up_j} \dot{\tilde{q}}_{pj}) + p_i^A$

$$\begin{aligned}&\Phi_i (u_i - U_i^\top a_{\lambda(i)} - U_i^\top c_i') \\&= (I_i^A - \underbrace{I_i^A P_{up_i} \Phi_i}_{U_i} U_i^\top) a_{\lambda(i)} \\&\quad + p_i^A + (I_i^A - U_i \Phi_i U_i^\top) c_i' \\&\quad + U_i \Phi_i u_i\end{aligned}$$

$\rightarrow f_i = I_i^A a_{\lambda(i)} + p_i^A$

$f_i = \underbrace{\frac{d}{dt} (I_i^A v_i + m_i^A)}_{v_i} \quad v_i = v_{\lambda(i)} + \underbrace{P_{ua_i} \dot{\tilde{q}}_{ia}}_{v_{\sigma_i}} + \underbrace{P_{up_i} \dot{\tilde{q}}_{ip}}_{v_{\tau_i}}$

$f_i = \frac{d}{dt} (I_i^A v_{\lambda(i)} + m_i^A + I_i^A P_u \dot{\tilde{q}}_i)$

$\downarrow$  (if only one child)

$$f_{\lambda(i)} = \frac{d}{dt} (I_{\lambda(i)} v_{\lambda(i)} + m_{\lambda(i)}) + f_i$$

$$= \frac{d}{dt} \left[ \underbrace{(I_{\lambda(i)} + I_i^A)}_{I_{\lambda(i)}^A} v_{\lambda(i)} + \underbrace{m_{\lambda(i)} + m_i^A}_{m_{\lambda(i)}^A} + I_i^A P_{up_i} \dot{\tilde{q}}_i \right]$$

When  $\lambda(i) = 1$ , then  $P_{up_{j1}}^\top f_{j1} = 0 = \frac{d}{dt} \left[ \underbrace{P_{up_{j1}}^\top I_1^A P_{up_{j1}} \dot{\tilde{q}}_{jp}}_{M_{tot,jp}^A} + \underbrace{P_{up_{j1}}^\top m_1^A}_{M_{tot,jp}} \right]$

To set  $M_{tot,jp}(0) = 0 \rightarrow \boxed{\dot{\tilde{q}}_{jp}(0) = -(P_{up_{j1}}^\top I_1^A P_{up_{j1}})^{-1} P_{up_{j1}}^\top m_1^A M_{tot,jp}}$

So total momentum  $\sum_j^i \dot{X}_j^* I_j v_j = 0$   $\rightarrow \sum_j^i \dot{X}_{c_j}^* I_{c_j} v_{c_j} = 0$

$\dot{X}_{c_j}^* I_{c_j} \sim \dot{X}_j v_j$

$\left[ \begin{array}{c} \dot{X}_{c_j}^* I_{c_j} \\ \dot{X}_j v_j \end{array} \right] = \left[ \begin{array}{c} \bar{I}_{c_j} \omega_j \\ m_j \dot{r}_{c_j} \end{array} \right]$

$$\sum_j^i \dot{X}_{c_j}^* I_{c_j} \sim \dot{X}_j v_j = 0$$

$\dot{X}_{c_j}^* = \frac{d}{dt} \dot{X}_j$

$= \int_{c_j}^i (v_i - v_{c_j}) \times \dot{X}_j^+ + \dot{X}_{c_j}^* v_{c_j} \times \dot{X}_j^+$

$$\rightarrow \frac{d}{dt} \sum_j^i \dot{X}_{c_j}^* I_{c_j} \int_{c_j}^i \frac{\partial \dot{X}_j}{\partial r_{c_j}} = \sum_j^i \dot{X}_{c_j}^* v_{c_j} \times I_{c_j} v_{c_j}$$

center of mass:

$$M \underline{x}_c = \sum_j^i \underline{x} \rho dA$$

$$\frac{dx_c}{dt} = \underline{v}_c = \frac{1}{M} \sum_j^i \underline{v}_j = \frac{1}{M} \sum_j M_j \underline{v}_{c_j}$$

$\underline{v}_{c_j} + \underline{\Omega} \times (\underline{x} - \underline{x}_{c_j})$

$$\text{But } \underline{P} = \sum_j M_j \underline{v}_{c_j}$$

$$\frac{d\underline{P}}{dt} = \underline{F} \text{ so if } \underline{F} = 0$$

$$\text{then } \underline{P} = \underline{P}(0) = \underline{P}_0$$

$$\text{Let } \underline{P}_0 = 0, \text{ then}$$

$$\frac{d\underline{x}_c}{dt} = \frac{1}{M} \underline{P} = 0$$

Now return to the spatial vector form

Denote  $\underline{h}$  as momentum ...

$$\underline{h} = \sum_j I_j \underline{v}_j \rightarrow f = \frac{dh}{dt} = \frac{d}{dt} \sum_j I_j \underline{v}_j$$

$$= \sum (v_j \times I_j \underline{v}_j + I_j \alpha_j)$$

$$\text{Note that } v_j \times I_j \underline{v}_j = \begin{bmatrix} \Omega_j^x & v_j^x \\ 0 & \Omega_j^x \end{bmatrix} \begin{bmatrix} \bar{I}_{c_j} & 0 \\ 0 & M_j \end{bmatrix} \begin{bmatrix} \alpha_j \\ v_j \end{bmatrix}$$

$$= \begin{bmatrix} \Omega_j^x & v_j^x \\ 0 & \Omega_j^x \end{bmatrix} \begin{bmatrix} \bar{I}_{c_j} & \alpha_j \\ M_j & v_j \end{bmatrix} = \begin{bmatrix} \Omega_j^x \bar{I}_{c_j} \Omega_j + v_j \times M_j v_j \\ M_j \Omega_j^x v_j \end{bmatrix}$$

$$I_j \alpha_j = \begin{bmatrix} \bar{I}_{c_j} & 0 \\ 0 & M_j \end{bmatrix} \begin{bmatrix} \alpha_j \\ v_j \end{bmatrix} = \begin{bmatrix} \bar{I}_{c_j} \alpha_j \\ M_j \alpha_j - M_j \Omega_j \times v_j \end{bmatrix}$$

$$\therefore f = \sum_j \left( \bar{I}_{c_j} \alpha_j + \Omega_j \times \bar{I}_{c_j} \alpha_j \right) = \frac{d}{dt} \sum_j \left( \bar{I}_{c_j} \alpha_j \right)$$

$$h_j = \dot{I}_{c_j} v_{c_j} = \dot{I}_{c_j} \sim \dot{X}_{c_j} \sim \dot{X}_j v_j$$

$\dot{X}_j v_j$  invariant

$\dot{X}_{c_j} = \dot{X}_j - \dot{r}_{c_j}$  pure rotation from inertial axes to body axes at center of mass

### Equations of motion

The equations of motion for a body are

$$\underline{f} = \frac{d\underline{h}}{dt} = \frac{d(\underline{\underline{I}}\underline{v})}{dt}$$

Note that if we denote  $\underline{o}$  as the origin of some inertial system and  $\underline{c}$  as the center of mass of the body, then

Also, let  $i$  denote a system based at  $c$  but aligned with the inertial axes.

Then  ${}^iX_c$  is a pure rotation and  ${}^cX_i$  is pure translation.  
(by vector  $\underline{c}$ , where  $\underline{c}$  is the vector from  $\underline{o}$  to  $\underline{c}$ )

Note that we can write  $\underline{\underline{I}}$  in coordinates as  $\underline{\underline{I}} = \begin{bmatrix} {}^i\underline{\underline{I}}_c & \underline{0} \\ \underline{0} & M_1 \end{bmatrix}$   
or as  $\underline{\underline{I}} = \begin{bmatrix} \underline{\underline{I}}_c & \underline{0} \\ \underline{0} & M_1 \end{bmatrix}$ , when the coefficients are invariant.

Then

$$\begin{aligned} {}^i\underline{\underline{I}} &= {}^iX_c^{-1} \underline{\underline{I}} {}^cX_i \\ {}^iX_c &= {}^iX_b {}^bX_c = \underbrace{\begin{bmatrix} {}^iE_c & \underline{0} \\ \underline{0} & {}^iE_c \end{bmatrix}}_{{}^iX_c} \underbrace{\begin{bmatrix} 1 & \underline{0} \\ \underline{r}^* & 1 \end{bmatrix}}_{{}^cX_{c_i}} \\ {}^cX_i &= {}^cX_b {}^bX_i = \underbrace{\begin{bmatrix} {}^cE_i & \underline{0} \\ \underline{0} & {}^cE_i \end{bmatrix}}_{{}^cX_{c_i}} \underbrace{\begin{bmatrix} 1 & \underline{0} \\ \underline{r}^* & 1 \end{bmatrix}}_{{}^iX_i} \end{aligned}$$

$${}^cV = {}^cX_b {}^bV = {}^cX_c {}^cX_b {}^bV$$

$$\left. \begin{array}{l} I_1^A = I_1 \\ I_2^A = I_2 \\ \\ V_1 = V_{J_1} \\ V_2 = X_1 V_1 + V_{J_2} \\ \\ C_1 = V_1 \times V_{J_1} + P_{V_{A_1}} \\ C_2 = V_2 \times V_{J_2} + P_{V_{A_2}} \\ \\ P_1^A = V_1 \times I_1 V_1 \\ P_2^A = V_2 \times I_2 V_2 \end{array} \right\} \quad \begin{array}{l} I^A = I_2^A \\ p^A = p_2^A + I^A c_2 \\ \\ I_1^A = I_1^A + X_2^A I^A X_1 = I_1 + X_2^A I_2^A X_1 \\ \\ P_1^A = P_1^A + X_2^A p^A = V_1 \times I_1 V_1 \\ \quad \quad \quad + X_2^A (V_2 \times I_2 V_2 + I_2 c_2) \\ \\ U_1 = - P_{V_{A_1}}^T p_1^A \\ \\ \frac{U_1}{P_{V_{A_1}}} = \left( P_{V_{A_1}}^T I_1^A P_{V_{A_1}} \right)^{-1} \\ \\ U_1 = - P_{V_{A_1}}^T p_1^A \end{array}$$

$$a'_1 = c_1$$

$$\hat{\tilde{q}}_{P_1} = \widetilde{H}_{P_1}^{-1} (u_i - U_i^\top q_i) \rightarrow (I_1 + X_2^\top I_2 X_1) \hat{\tilde{q}}_1 = -[v_1 \times I_1 v_1 \\ + X_2^\top (v_2 \times I_2 v_2 + I_2 c_2)]$$

$$a_{J_1} = P_{\nu p_1} \tilde{q}_{r_1},$$

$$a_1 = a'_1 + a_{\overline{J},1}$$

$$g_2 = X_1 a_1 + c_2$$

$$a_2 = a_2'$$

$$\Rightarrow \left( I_1 + X_2^* I_2 X_1 \right) \left( \tilde{q}_1 + V_1 \times V_{J_1} \right)$$

$$+ \quad v_1 \times^* I_1 v_1 + X_2^* (v_2 \times^* I_2 v_2 + I_2 v_2 \times v_{\sigma_2}),$$

$$+ I_2 \alpha_{f_2} ) = 0$$

$$- V_{I_1} \times V_{J_1} \Big) + V_{I_1} \times I_{I_1} V_{I_1}$$

$$X_2 \left[ I_2 - X_1 \left( \frac{\bar{q}_1 + V_1 \times V_{J_1}}{I_2} \right) + V_2 \times I_2 V_2 + I_2 \left( \alpha_{J_2} + V_2 \times V_{J_2} \right) \right] = 0$$

$$\frac{dh_{2i}}{dt}$$

$$(x^+ / (\bar{x}, p_1)) \cup (x^+ / (\bar{x}, p_2))$$

$$\left[ \begin{array}{c} \hat{x}_{1ci} \\ \hat{x}_{2ci} \end{array} \right] = \left[ \begin{array}{c} \frac{\omega_1^2 + \omega_2^2}{M_1} V_{1ci} \\ \frac{\omega_1^2 - \omega_2^2}{M_2} V_{2ci} \end{array} \right]$$

, equivalently, after multiplying

by  $x_{ii}$ )

$$X_{1ci}^+ \begin{pmatrix} I_{c_1} & Q_{1i} \\ m_1 & V_{1ci} \end{pmatrix} + X_{2ci}^+ \begin{pmatrix} I_{c_2} & Q_{2i} \\ m_2 & V_{2ci} \end{pmatrix} =$$

$$\frac{d}{dt} \left( h_{ii} + {}^{ii}X_{2i}^* h_{2i} \right) = 0$$

$$i \times \frac{x}{T} \leq v$$

$$\left[ \begin{array}{c} \bar{x}_1 \\ \bar{x}_2 \end{array} \right] = \left( A_2 \right)^{-1} \left[ \begin{array}{c} \bar{y}_1 \\ \bar{y}_2 \end{array} \right]$$

$$\left[ \begin{array}{cc} \frac{1}{c_1} & 0 \\ 0 & m_1 \end{array} \right] \left\{ \begin{array}{l} \downarrow c_1 \\ V_{t c_1} \end{array} \right\} = \left\{ \begin{array}{l} \frac{1}{c_2} \\ 0 \end{array} \right\}$$

$$\longrightarrow \begin{matrix} ii \\ X_{1ci} \end{matrix} + \left\{ \begin{pmatrix} \bar{I}_{1ci} & \Omega_{1i} \\ M_1 & V_{1ci} \end{pmatrix} + \begin{matrix} iii \\ X_{2ci} \end{matrix} + \begin{pmatrix} \bar{I}_{2ci} & \Omega_{2i} \\ M_2 & V_{2ci} \end{pmatrix} \right\} = \text{const}$$

or, equivalently, after multiplying,

$$X_{1c_i} + X_{2c_i} = \text{const}$$

## Free swimming

Now we seek equation for  $a_o$ .

For any body  $j$ ,

$$f_j = I_j \alpha_j + p_j + j X_{j+1}^* f_{j+1}$$

We seek to eliminate the forces  $f_j$ .

Start at body  $j=N_b-1$ ,

$$\begin{aligned} f_j &= I_j \alpha_j + p_j + j X_{j+1}^* (I_{j+1} \alpha_{j+1} + p_{j+1}) \\ &\quad + j X_{j+1}^* \alpha_j + S \ddot{\theta}_{j+1}^* c_{j+1} \\ &= (\underbrace{I_j + j X_{j+1}^* I_{j+1}^* X_{j+1}}_{I_j^A}) \alpha_j + \underbrace{p_j + j X_{j+1}^* p_{j+1}}_{p_j^A} + j X_{j+1}^* c_{j+1} + j X_{j+1}^* S \ddot{\theta}_{j+1}^* \end{aligned}$$

Thus,  $I_j^A = I_j + j X_{j+1}^* I_{j+1}^* X_{j+1}$ ,  $p_j^A = p_j + j X_{j+1}^* p_{j+1}^A + j X_{j+1}^* (c_{j+1} + S \ddot{\theta}_{j+1}^*)$

and

$$f_j = I_j^A \alpha_j + p_j^A$$

But  $f_o = 0$ , so  $\alpha_o = -(\overline{I}_o)^{-1} \overline{p}_o$

$$\begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{pmatrix}$$

If constrained to slide along a rail, then  $v_o = S_x \dot{X}$  and  $f_o \neq 0$ , but  $S_x^T f_o = 0$ . Then

$$\alpha_o = S_x \ddot{X} + \dot{S}_x \dot{X}$$

$$f_o = I_o^A \alpha_o + p_o^A$$

$$\hookrightarrow 0 = \underbrace{S_x^T I_o^A S_x}_{D_o} \ddot{X} + \underbrace{S_x^T p_o^A}_{U_o} \rightarrow \ddot{X} = D_o^{-1} U_o$$