

Identification of transfer function of a Single Board Heater System through ramp response experiments

AIM:

1. To perform ramp test on a single board heater system
2. To identify system transfer function using ramp response data

Target group:

- Anyone who has basic knowledge of Control Engineering.

About this Experiment

- Figure 1 shows the single board heater system on which this experiment will be performed.
- The setup consists of a heater assembly, fan, temperature sensor, microcontroller and associated circuitry.
- Heater assembly consists of an iron plate placed at a distance of about 3.5 mm from the nichrome coil.
- A 12 V computer fan positioned below this heater assembly is meant for cooling the assembly.
- The temperature sensed by the temperature sensor, AD 590, after suitable processing, is fed to the microcontroller.
- The microcontroller ATmega16 is the heart of the setup. It provides an interface between the process and the computer.



Figure 1: Single board heater system

- The LCD display mounted above the microcontroller displays the heated plate temperature, heater and fan inputs and also the commands communicated via serial port.
- The setup is powered by 12 V, 8 A SMPS.
- We have used Scilab and scicos as an interface for sending and receiving data. This interface is shown in Fig.2.

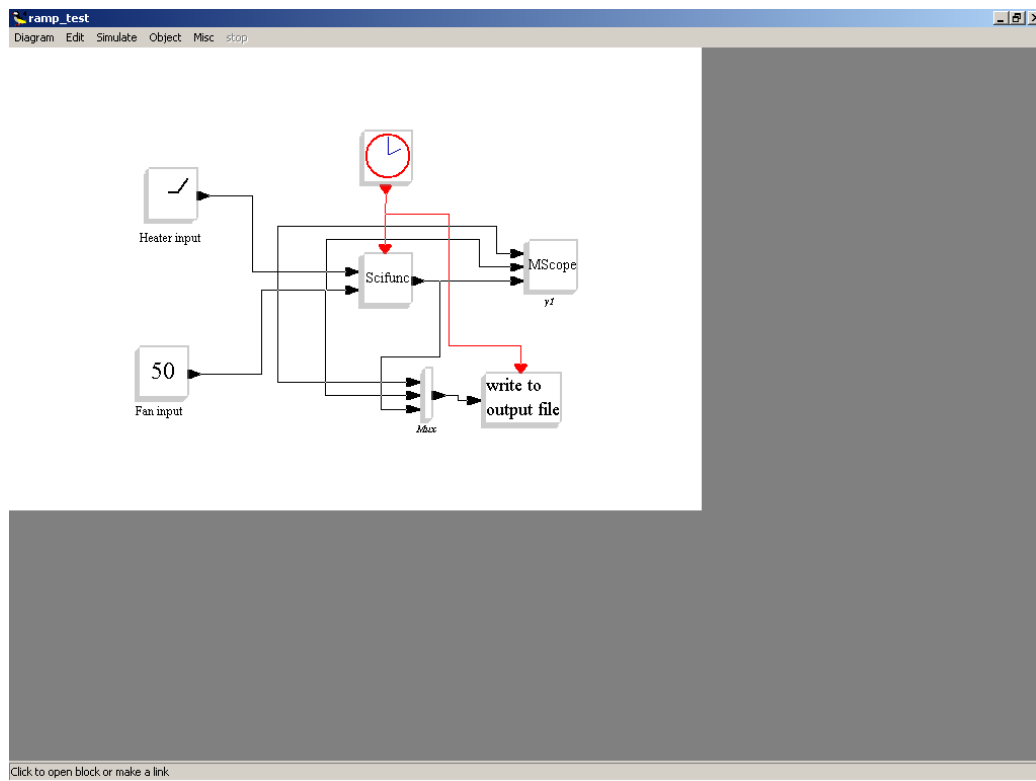


Figure 2: Scicos for this experiment

- Heater current and fan speed are the two inputs for this system. They are given in PWM units.
- These inputs can be varied by the setting the properties of inpput block's properties in scicos. For details of setting of properties please refer "Instruction mannual for temperture controller"
- The plots of their amplitude versus no. of collected samples are also available on the scope windows.
- The output temperature profile, as read by the sensor, is also plotted.
- The data acquired in the process is stored on the local drive and is available to the user for further calculations.

Theory

Identification of the transfer function of a system is quite important since it helps us to represent the physical system, mathematically. Once the transfer function is obtained one can acquire the response of the system for various inputs without actually applying them to the system.

Consider the standard first order transfer function given below

$$G(s) = \frac{C(s)}{R(s)} \quad (1)$$

$$G(s) = \frac{K}{\tau s + 1} \quad (2)$$

Rewriting the Equation, we get

$$C(s) = K \left\{ \frac{R(s)}{\tau s + 1} \right\} \quad (3)$$

A ramp is given as an input to the first order system. The Laplace Transform of a ramp function with slope 1 is $\frac{1}{s^2}$. Therefore Laplace Transform of a ramp function with slope = v is $\frac{v}{s^2}$. Hence, substituting $R(s) = \frac{v}{s^2}$ in equation 3, we obtain

$$C(s) = \frac{K}{\tau s + 1} \frac{v}{s^2} \quad (4)$$

$$= \frac{A}{s} + \frac{B}{s^2} + \frac{C}{\tau s + 1} \quad (5)$$

Solving $C(s)$ using Heaviside expansion approach, we get

$$C(s) = Kv \left\{ \frac{1}{s^2} - \frac{\tau}{s} + \frac{\tau^2}{\tau s + 1} \right\} \quad (6)$$

Taking the Inverse Laplace transform of the above equation, we get

$$c(t) = Kv \left\{ t - \tau + \tau e^{-\frac{t}{\tau}} \right\} \quad (7)$$

The difference between the reference and output signal is the error signal $e(t)$

$$e(t) = r(t) - c(t) \quad (8)$$

$$e(t) = Kvt - Kvt + Kv\tau - Kv\tau e^{-\frac{t}{\tau}} \quad (9)$$

$$e(t) = Kv\tau(1 - e^{-\frac{t}{\tau}}) \quad (10)$$

normalizing equation 10 for $t \gg \tau$, we get

$$e(t) = \tau \quad (11)$$

This means that the error in following the ramp signal is equal to τ for large value of t [2]. Hence, the smaller the time constant τ , the smaller is the steady state error.

Step by step procedure to perform Ramp Test

- Initiate a ramp input to the system with some value of the slope. For this experiment we have chosen $slope = 0.2$ Note that the value of heater current will not exceed 40 PWM units.

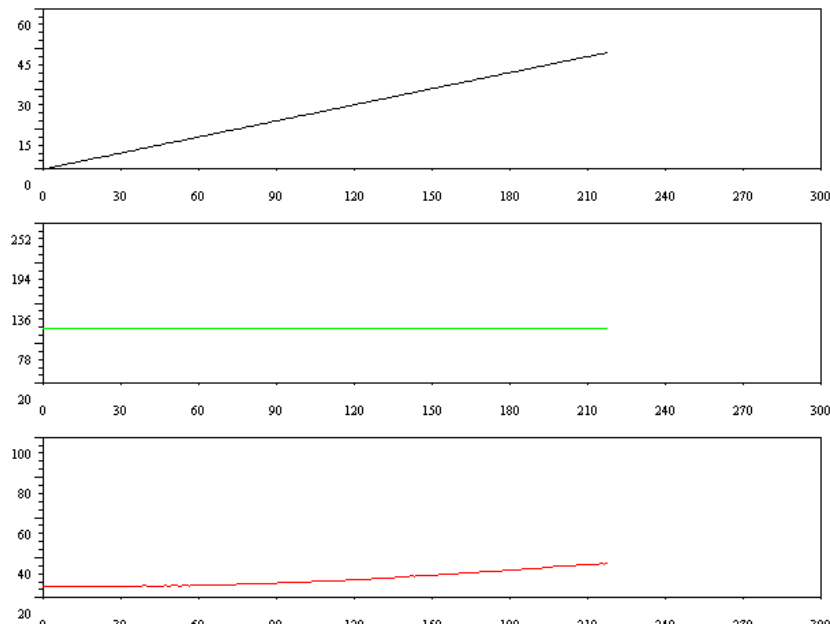


Figure 3: Screen shot of Ramp Test Experiment

The data thus obtained is stored using "Write to output file" Scicos block as shown in Fig.2

```
data7 = [
0.100E+00 0.200E-01 0.100E+03 0.258E+02
0.110E+01 0.220E+00 0.100E+03 0.258E+02
0.210E+01 0.420E+00 0.100E+03 0.257E+02
.
.
0.198E+03 0.396E+02 0.100E+03 0.358E+02
0.199E+03 0.398E+02 0.100E+03 0.359E+02
```

0.200E+03 0.400E+02 0.100E+03 0.358E+02
];

The first column denotes time in seconds. The second column in this table denotes heater current. It is zero to start with and increases with constant slope from the second row onwards. The third column denotes the fan speed. It has been held constant at 100 units. Only one point is retained for zero current value and all other points are deleted. The last column denotes the plate temperature.

- Plot the graph of the data thus acquired using Scilab code 'first.sce'

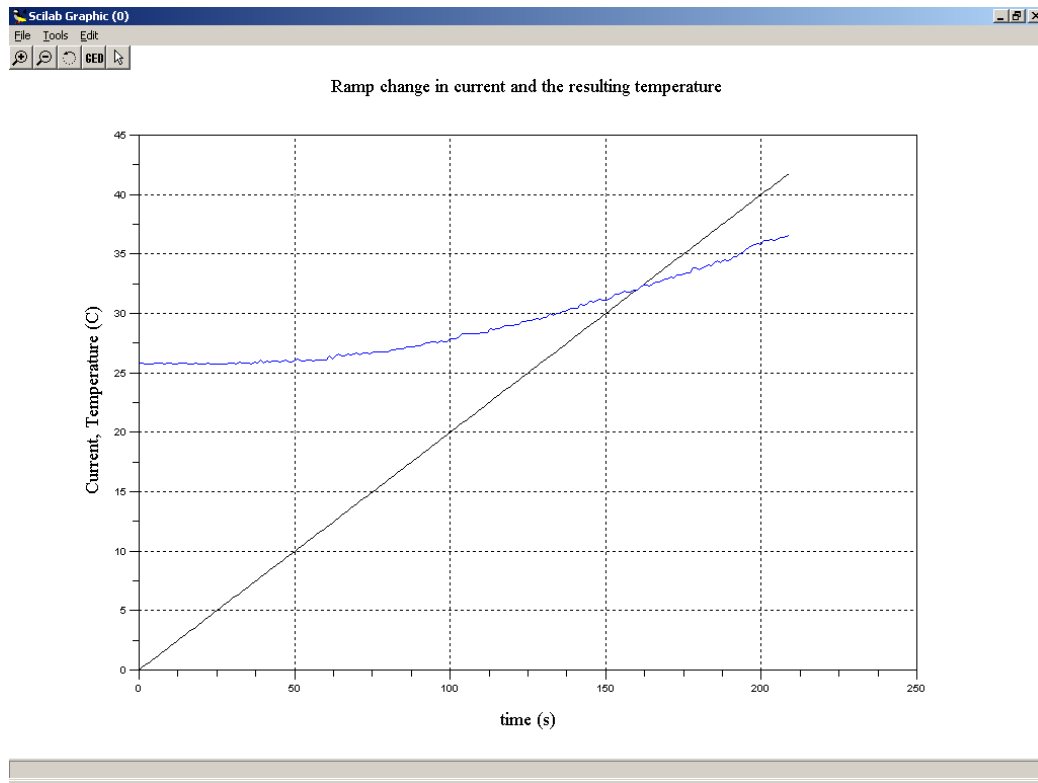


Figure 4: Plot obtained using Scilab code 'first.sce'

Note:- The associated Scilab codes are given at the end of this Document.

Consider the system to be first order. We try to fit a first order transfer function of the form

$$G(s) = \frac{K}{\tau s + 1} \quad (12)$$

to the single board heater system. Because the transfer function approach uses deviational variables, $G(s)$ denotes the Laplace transform, of the gain of the system between the change in heater current and the change in the system temperature. We denote both the time domain and the Laplace transform variable by the same lower case variable. Let the change in temperature be denoted by y . Suppose that the heater current changes as a ramp with slope = v , then we obtain the following relation between the current and the temperature.

$$y(s) = G(s)u(s) \quad (13)$$

$$y(s) = \frac{K}{s + 1} \frac{v}{s^2} \quad (14)$$

solving the above equation we get,

$$y(t) = Kv[t - \tau + \tau e^{\frac{-t}{\tau}}] \quad (15)$$

for $t \gg \tau$,

$$y(t) = Kv[t - \tau] \quad (16)$$

from equation 6

$$B = -Kv\tau \quad (17)$$

therefore

$$y(t) = Kvt + B \quad (18)$$

The calculation of τ and K is done for the range of time over which the slope of the temperature profile becomes almost constant. Hence, the calculations are done for data obtained for last 50 seconds. $y(t)$ is taken as change in temperature.

$$5.8 = 154Kv + B$$

$$5.9 = 155Kv + B$$

.

.

.

$$10.3 = 204Kv + B$$

These equations are in the form $Ax = b$, with

$$A = \begin{bmatrix} 154 & 1 \\ 155 & 1 \\ . & . \\ . & . \\ 204 & 1 \end{bmatrix}, x = \begin{bmatrix} Kv \\ B \end{bmatrix}, b = \begin{bmatrix} 5.8 \\ 5.9 \\ . \\ . \\ 10.3 \end{bmatrix}$$

The Least Square solution is given by,

$$\begin{aligned} x &= (A^T A)^{-1} A^T b \\ &= \begin{bmatrix} 0.084 \\ -6.959 \end{bmatrix} \end{aligned}$$

therefore, for $v = 0.2$

$$Kv = 0.084$$

$$K = 0.418$$

Also,

$$B = -Kv\tau = -6.95$$

Hence

$$\tau = 83.14$$

- The scilab code 'approx_ramp.sce' does these calculations. This code uses the routines 'label.sci' and 'approx_ramp.sci'. Assign a value to the argument 'N' used on the sixth line of the scilab code 'approx_ramp.sce' indicating the number of sampled data should be used for calculation. Also put the value of 'input_slope'. The plot thus obtained is as shown in the figure.

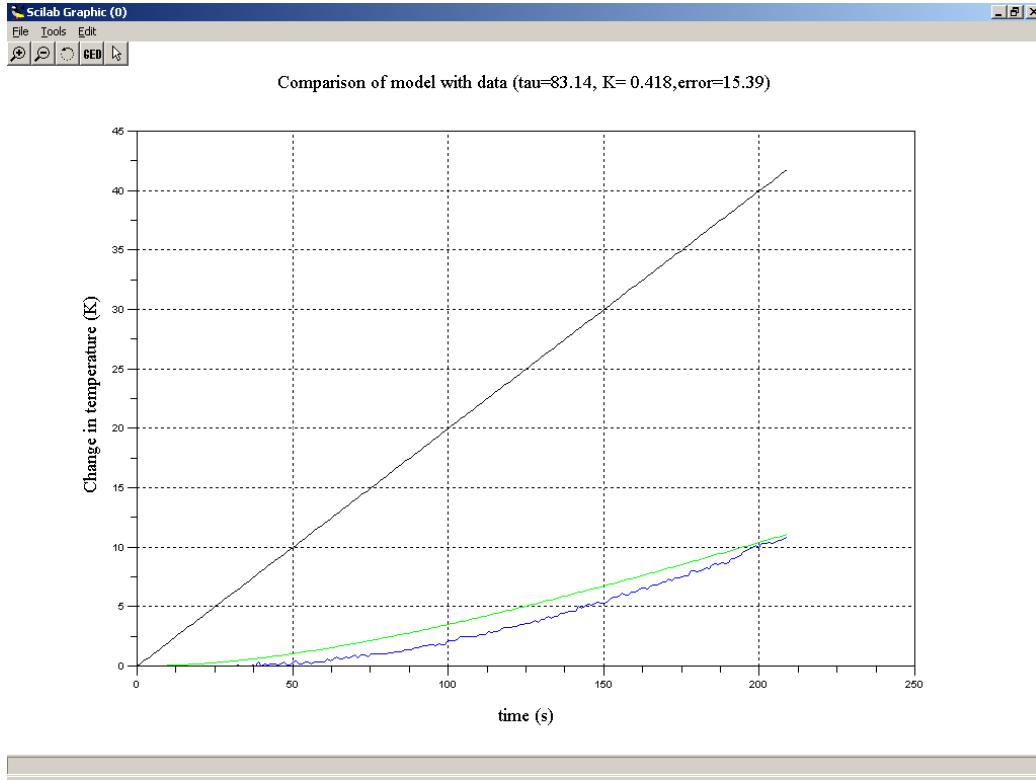


Figure 5: Plot obtained using Scilab code 'approx_ramp.sce'

The plot thus obtained is reasonably good. We obtain $\tau = 83.14$, $K = 0.418$ and the least square error to be 15.39.

The Transfer Function thus obtained is

$$G(s) = \frac{0.418}{83.14s + 1} \quad (19)$$

Variation

- It would have been noticed that the experiment is been performed by varying heater current and keeping the fan speed to be constant. However, the user is encouraged to introduce variations in the experiments by choosing different combinations of fan speed and heater current.
- Negative ramp can also be introduced to make the experiment more informative.
- One can even need not keep a particular input constant. By varying both the inputs, one can imagine it to be like a step varying disturbance signal.
- The system can also be treated as a second order system. This consideration is however necessary since it increases the accuracy of the acquired transfer function. [1]

Scilab Codes

- Scilab code ‘label.sci’

```
// Updated (9-12-06), written by Inderpreet Arora  
// Input arguments: title , xlabel , ylabel and their  
font sizes  
  
function label(tname , tfont , labelx , labely , xyfont)  
a = get("current_axes")  
xtitle(tname , labelx , labely)  
xgrid  
t = a.title;  
t.font_size = tfont; // Title font size  
t.font_style = 2; // Title font style  
t.text = tname;  
  
u = a.x_label;  
u.font_size = xyfont; // Label font size  
u.font_style = 2; // Label font style  
  
v = a.y_label;  
v.font_size = xyfont; // Label font size  
v.font_style = 2; // Label font style  
  
// a.label_font_size = 3;  
  
endfunction;
```

- Scilab code ‘approx_ramp.sci’

```

function lsterr = approx_ramp(T,u,y,input_slope ,
    tau ,limits ,no)
t0 = T(1);delta_u = u(2) - u(1);
u = u - u(1); y = y - y(1);
y_prediction = gain*input_slope*((T-t0)-tau+tau*(
    exp(-(T-t0)/tau)));
format('v',6);
lsterr = norm(y-y_prediction,2);
ord = [u y y_prediction]; x = [T T T];
xbasc(); plot2d(x,ord,rect=limits), xgrid();
title = 'Comparison of model with data (tau='
title = title+string(tau)+' , K= '+string(gain)+' ,
    error='+string(lsterr)+' )'
label(title ,4,'time (s)', 'Change in temperature (K
    )',4);

```

- Scilab code ‘first.sce’.

```

clear data7; exec('data02.dat'); getf('label.sci')
;
T = data7(:,1); fan = data7(:,3) //T is time, fan
    is fan speed
u = data7(:,2); y = data7(:,4); // u is current, y
    is temperature
ord = [u y]; x = [T T]; // u and y are plotted vs.
    time and time
xbasc(); plot2d(x,ord); xgrid();
title = 'Ramp change in current and the resulting
    temperature'
label(title,4,'time (s)', 'Current, Temperature (C)
    ',4);

```

- Scilab code ‘approx_ramp.sce’

```

clear data7; exec('ramp30.txt'); getf('label.sci')
;
global N
getf('approx_ramp.sci');
T = data7(:,1); //T is time
u = data7(:,2); y = (data7(:,4) - data7(1,4)); //
    u is current, y is temperature
N = 70; input_slope = 0.5;
e = [T y];
f = e(length(u)-N:length(u),:);
g = f(:,1);
h = (g-g)+1;
i = [g h];
j = f(:,2);
l = inv(i'*i)*i'*j
gain = l(1,1)/(input_slope)
z = -(l(2,1)/(gain*input_slope))
tau = z; limits = [0,0,90,45]; no=4000;
lsterr = approx_ramp(T,u,y,input_slope,tau,limits,
    no);

```

References

- [1] Kannan M. Moudgalya. *Identification of transfer function of a single board heater system through step response experiments*. 2009.
- [2] Katsuhiko Ogata. *Modern Control Engineering*. Prentice-Hall of India, 2005.