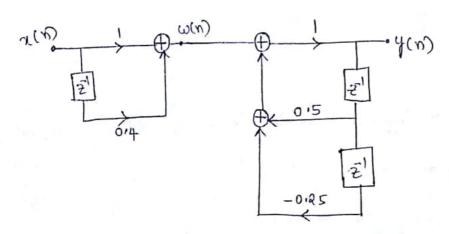
I Realize Direct form I and Direct-form I structures for the System described by the difference equation

du: 1 Direct form I realization:

Given
$$y(n) = 0.5y(n-1) - 0.25y(n-2) + \chi(n) + 0.4\chi(n-1) \longrightarrow 1$$

Let $w(n) = \chi(n) + 0.4\chi(n-1) \longrightarrow 2$
 $y(n) = 0.5y(n-1) - 0.25y(n-2) + w(n) \longrightarrow 3$



(i) Direct form I realization:

Given y(n)= 0.5y(n-1)-0.25y(n-2) + x(n) + 0.14x(n-1)

Apply Z.T.

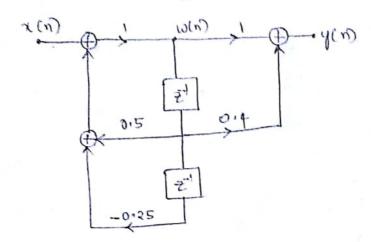
$$H(z) = \frac{y(z)}{x(z)} = \frac{1 + 0.4 \bar{z}^1}{1 - 0.5 \bar{z}^1 + 0.25 \bar{z}^2} = \frac{y(z)}{W(z)} \cdot \frac{W(z)}{X(z)}$$

$$\frac{W(z)}{X(z)} = \frac{1}{1 - 0.5z^{-1} + 0.05z^{-2}}$$

$$\Rightarrow \omega(n) = x(n) + 0.5\omega(n-1) + 0.25\omega(n-2) = x(n)$$

$$\frac{\lambda(5)}{\lambda(5)} = 1 + 0.4 \cdot 1 \Rightarrow \lambda(5) = \lambda(5) \left[1 + 0.4 \cdot 2_1 \right]$$

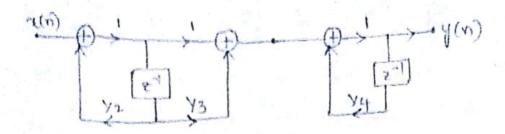
$$\Rightarrow \lambda(5) = \lambda(5) \left[1 + 0.4 \cdot 2_1 \right]$$



2. Realize the system with difference equations in cascade and parallel form.

$$\frac{Y(z)}{X(z)} = \frac{1 + \frac{1}{3}z^{-1}}{1 - \frac{3}{4}z^{-1} + \frac{1}{8}z^{-2}} = \frac{1 + \frac{1}{3}z^{-1}}{(1 - \frac{1}{4}z^{-1})(1 - \frac{1}{4}z^{-1})}$$

$$\frac{Y(2)}{X(2)} = \frac{\left(1 + \frac{1}{3}z^{-1}\right)}{1 - \frac{1}{2}z^{-1}} \times \frac{1}{1 - \frac{1}{4}z^{-1}} = H_1(2)H_2(2)$$



(i) Parallel form realization :

Given
$$y(n) = \frac{3}{4}y(n-1) - \frac{1}{8}y(n-2) + x(n) + \frac{1}{3}x(n-1)$$

$$\Rightarrow Y(z) = \frac{3}{4}z^{-1}y(z) - \frac{1}{8}z^{-2}y(z) + x(z) + \frac{1}{3}z^{-1}x(z)$$

$$Y(2) \left[1 + \frac{3}{4} \vec{\epsilon}^1 + \frac{1}{8} \vec{\epsilon}^2 \right] = X(2) \left[1 + \frac{1}{3} \vec{\epsilon}^1 \right]$$

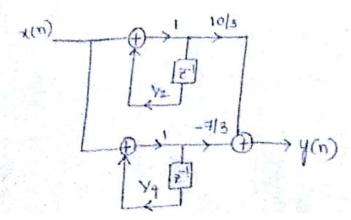
$$H(\bar{z}) = \frac{Y(z)}{X(\bar{z})} = \frac{1 + \frac{1}{3}\bar{z}^{-1}}{1 - \frac{3}{4}\bar{z}^{-1} + \frac{1}{8}\bar{z}^{-2}} = \frac{\frac{1}{3}\bar{z}^{-1} + 1}{\frac{1}{8}\bar{z}^{-2} - \frac{3}{4}\bar{z}^{-1} + 1} = \frac{\frac{1}{3}\bar{z}^{-1} + 1}{(1 - \frac{1}{2}\bar{z}^{-1})(1 - \frac{1}{4}\bar{z}^{-1})}$$

$$\frac{1}{8}e^{\frac{2}{3}}e^{\frac{1}{4}+1} = \frac{A}{1-\frac{1}{2}e^{-1}} + \frac{B}{1-\frac{1}{2}e^{-1}} = \frac{A}{1-\frac{1}{2}e^{-1}} + \frac{B}{1-\frac{1}{4}e^{-1}} = \frac{A}{1-\frac{1}{4}e^{-1}} = \frac{A}{1-\frac{1}{4}e^{$$

Comp courts => A+B=1 Comp. z-coeff=> -1/4 A-1/2 B= 1/3

$$\Rightarrow A = \frac{10}{3} ; B = -\frac{7}{3}$$

$$\Rightarrow H(2) = \frac{10/3}{1 - \frac{1}{2}z^{-1}} + \frac{-7/3}{1 - \frac{1}{4}z^{-1}}$$



elling impulse invariance method. Assume T= 1 second.

Aus:

Given
$$H(3) = \frac{2}{(3+1)(3+2)} = \frac{A}{3+1} + \frac{B}{3+2} = \frac{A(3+2) + B(3+1)}{(3+2)}$$

Compaceff =>
$$2A+B=2$$

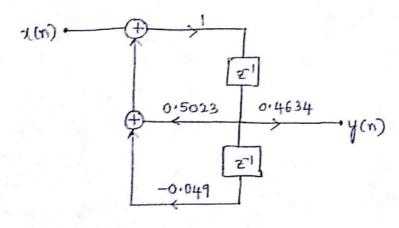
Compaceff => $A+B=0$
 $A=2$, $B=-2$

$$I = \frac{2}{|-\bar{e}|z^{-1}} - \frac{2}{|-\bar{e}^{2}z^{-1}|}$$

..
$$H(z) = \frac{2}{1 - 0.367z^{-1}} - \frac{2}{1 - 0.1353z^{-1}}$$

$$H(t) = \frac{2(1-0.1353t^{-1})-2(1-0.367t^{-1})}{(1-0.367t^{-1})(1-0.1353t^{-1})}$$

$$H(z) = \frac{0.4634z^{1}}{1-0.5023z^{1}+0.049z^{2}}$$



4. Compute the poles of an smalog Butterworth filter TF that satisfies the constraints $0.707 \le |H(j\Omega)| \le 1$; $0 \le \Omega \le 2$ $|H(j\Omega)| \ge 0.1$; $\Omega \ge 4$

and determine Ha(s) and hence obtain H(2) using optimum. transformation.

dur:

$$\frac{1}{\sqrt{1+z^{2}}} = 0.707; \Omega_{p} = 2$$

$$\frac{1}{\sqrt{1+z^{2}}} \Rightarrow \mathcal{E} = 1$$

$$\frac{1}{\sqrt{1+z^{2}}} \Rightarrow \lambda = 9.95$$

$$\frac{1}{\sqrt{1+\lambda^{2}}} \Rightarrow \lambda = \frac{10}{\sqrt{1+\lambda^{2}}} \Rightarrow 3.3147$$

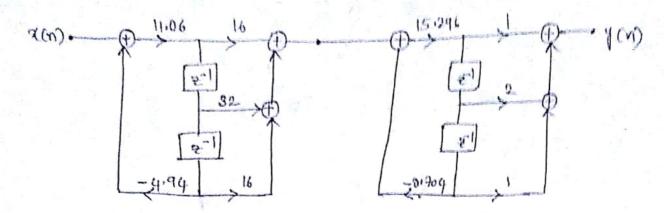
$$\frac{1}{\sqrt{1+z^{2}}} \Rightarrow \lambda = \frac{10}{\sqrt{1+\lambda^{2}}} \Rightarrow 3.3147$$

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$$\frac{1}{\sqrt{1+z^{2}}} \Rightarrow \lambda = \frac{10}{\sqrt{1+\lambda^{2}}} \Rightarrow 3.3147$$

$$\frac{1}{\sqrt{1+\lambda^{2}}} \Rightarrow \frac{10}{\sqrt{1+\lambda^{2}}} \Rightarrow$$

$$\begin{aligned} & \frac{\Omega_{c}}{\left(10^{0.11} \text{Kp}_{-1}\right)^{3} 2 \text{N}} &= \frac{\Omega_{p}}{\mathcal{E}^{3} \text{N}} = 2 \\ & \text{H}_{a}(\vec{s}) = \text{H}(\vec{s}) \Big|_{S \to \frac{3}{2c_{c}}} \frac{3}{2} \\ & \text{H}_{a}(\vec{s}) = \frac{1}{\left[\left(\frac{-S}{2}\right)^{2} + 0.7654\left(\frac{1}{2}\right) + 1\right]} \times \frac{3}{\left[\left(\frac{3}{2}\right)^{2} + 1.824\right]\left(\frac{3}{2}\right) + 1} \\ &= \frac{4}{\left(\frac{S^{2}}{2} + 1.53 \cdot S + \frac{1}{4}\right)} \times \frac{4}{\left(\frac{S^{2}}{2} + 3.648 \cdot S + \frac{1}{4}\right)} \\ & \text{H}(\vec{s}) = \frac{16}{\left[\left(\frac{S^{2}}{2} + 1.53 \cdot S + \frac{1}{4}\right)\left(\frac{S^{2}}{2} + 3.648 \cdot S + \frac{1}{4}\right)\right]} \times \frac{1}{\left[\left(\frac{S^{2}}{2} + 1.53 \cdot S + \frac{1}{4}\right)\left(\frac{S^{2}}{2} + 3.648 \cdot S + \frac{1}{4}\right)\right]} \\ & \text{H}(\vec{s}) = \frac{16}{\left[\left(\frac{S^{2}}{1 + z^{-1}}\right)^{2} + 3.06\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right) + 4\right]} \times \frac{1}{\left[\left(\frac{S^{2}}{1 + z^{-1}}\right)^{2} + 7.296\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right) + 4\right]} \\ &= \frac{16\left(1 + z^{-1}\right)^{2}}{\left(4 + 4z^{-2} - 8z^{-1} + 3.06 - 3.06z^{2}} \times \frac{\left(1 + z^{-1}\right)^{2}}{\left(4 + 4z^{-2} - 8z^{-1} + 7.296 - 7.296z^{2} + 4z^{-2} + 8z^{-1} + 4\right)} \\ &+ 4z^{-2} + 8z^{-1} + 4\right) \\ &+ 4z^{-2} + 8z^{-1} + 4\right) \\ &+ 4z^{-2} + 8z^{-1} + 4\right) \\ &= \frac{16\left(1 + 2z^{-1} + 2z^{-2}\right)}{2\left(\frac{S^{2}}{4} + 94 + 11.06\right)} \times \frac{\left(1 + 2z^{-1} + 2z^{-2}\right)}{\left(0 \cdot 704 + z^{-2} + 15.296\right)} \end{aligned}$$



5. Design a digital low pass chebysher filter with 2 dB Cutoff frequency at 100 radiscs. The attenuation should be atteast 15 dB for frequencies larger than 200 radiscs. The sampling frequency is 10 kHz. Use bilinear transformation.

Ans: Given dp = 2dB; ds = 15dBDistribution of the period of the p

PK = T+ EKEDTT -SK = a Cospk+jbsingk

$$\varphi_{1} = \frac{\pi}{2} + \frac{\pi}{q} = \frac{2\pi}{q} ; \quad \varphi_{2} = \frac{\pi}{3} + \frac{2\pi}{q} = \frac{5\pi}{q}$$

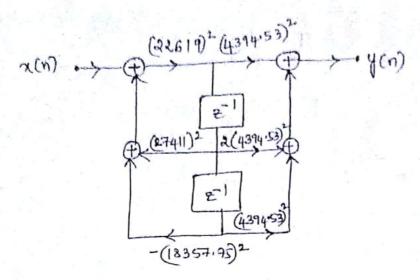
$$\varphi_{1} = \frac{\pi}{2} + \frac{\pi}{q} = \frac{2\pi}{q} ; \quad \varphi_{2} = -2|82.8\mu + \frac{1}{2}442|.54$$

$$\varphi_{2} = \frac{3054}{9} \cos \frac{2\pi}{q} + \frac{1}{9} \cos \frac{2535}{4} \sin \frac{2\pi}{q} = -2|82.8\mu + \frac{1}{9} 442|.54$$

$$\varphi_{3} = \frac{3054}{9} \cos \frac{2\pi}{q} + \frac{1}{9} \cos \frac{2535}{4} \sin \frac{2\pi}{q} = -2|82.8\mu + \frac{1}{9} 442|.54$$

$$\varphi_{3} = \frac{(4-5)}{9} (.5-52)$$

$$= \frac{(4-5)}{5} (.5$$



6. Discuss in detail the procedure of designing an analog filter using Butterworth approximation technique.

Aus: steps in designing an analog tiller using Butterworth approximation:

1) For the given specifications, find the order of filter N

$$\frac{\log_{10} \left(\frac{\lambda}{10^{10}}\right)}{\log_{10} \left(\frac{\lambda}{10^{10}}\right)} = \log_{10} \left(\frac{\lambda}{10^{10}}\right)$$

$$\log_{10} \left(\frac{\lambda}{10^{10}}\right)$$

$$\log_{10} \left(\frac{\lambda}{10^{10}}\right)$$

where Ω_s = analog stop band frequency $\Omega_p = \text{analog pers band Cut-off-frequency}.$ $\Omega_s = \text{attenuation in stop band}$ $\Omega_p = \text{attenuation in pass band}$

- 2) Round off to the nearest higher integer value.
- 3) Find the transfer function H(s) for -2c = 1 rad/sec-for the value of N.
 - a) First Calculate the 'N' no, of poles using the formula $g_k = e^{\int \Phi k}$ where $\Phi_k = \frac{\pi}{2} + \frac{(E_k 1)\pi}{2N}$ in order to obtain only stable poles and for all N.

where
$$\mathcal{E} = \frac{\Omega p}{\Omega}$$
 (d) $\Omega_c = \frac{\Omega c}{2 NN}$
where $\mathcal{E} = \sqrt{\frac{10^{0.1} dp}{10^{0.1} ds}} = \sqrt{\frac{10^{0.1} ds}{10^{0.1} ds}} = \sqrt$

Find the Transfer function
$$H_a(s)$$
 for the above value of $-2c$
a) by substituting $s \rightarrow \frac{s}{-2c}$ in $H(s)$. (for LP)

1.e., $H_a(s) = H(s)$
 $s \rightarrow \frac{s}{-2c}$

c) for designing BP with cutoff frequencies
$$\Omega_{L}$$
, Ω_{L} can be accomplished by $s \rightarrow \frac{s^2 + \Omega_{L}\Omega_{U}}{-s(\Omega_{U} - \Omega_{L})}$; $A = \frac{-\Omega_{1}^{2} + \Omega_{2}\Omega_{U}}{-\Omega_{1}(-\Omega_{U} - \Omega_{L})}$ and $\Omega_{r} = \min \{|A|, |B|\}$; $B = \frac{-\Omega_{2}^{2} - \Omega_{L}\Omega_{U}}{-\Omega_{2}(\Omega_{U} - \Omega_{L})}$

d) for designing Band Stop filter with Cutoff frequencies
$$\Omega_{L}$$
, Ω_{u}

$$S \rightarrow \frac{S(\Omega_{u} - \Omega_{z})}{S^{2} + \Omega_{L}\Omega_{u}}, \quad A = \frac{\Omega_{1}(\Omega_{u} - \Omega_{z})}{-\Omega_{1}^{2} + \Omega_{L}\Omega_{u}}$$

$$\Omega_{r} = \min \left\{ |A|, |B| \right\}; \quad B = \frac{\Omega_{2}(-\Omega_{u} - \Omega_{z})}{-\Omega_{2}^{2} + \Omega_{L}\Omega_{u}}$$

F. Explain how to convert an analog Silter transfer function into digital letter transfer function using Bilenear transformation.

idne! I. From the given specifications, find pre warping analog frequencies using analog $\Omega = \frac{2}{T} tom(\frac{\omega}{2})$ where $\omega = digital frequency (given)$

either butterworth on chebysher approximation.

3. Select the sampling rate T of the digital filter.

4. Substitute s= 2 [1-2] into the Transfer-function

H(2) = H(3) $\rightarrow \frac{2}{7} \left[\frac{1-2^{-1}}{1+2^{-1}} \right]$

5. Realize the obtained H(2) using any one of the forms.

8. Design an ideal HPF with Frequency response $H_d(e^{j\omega}) = \{1 \text{ for } \frac{T}{4} \leq \omega \leq T \}$ Using Hamming window for N = 9.

ahu

$$h_{d}(n) = \frac{1}{2\pi j n} \left[\frac{j \omega \eta}{e} \right]^{\frac{1}{1}/4} + e^{j \omega \eta} \right]^{\frac{1}{1}}$$

$$= \frac{1}{\pi n (2j)} \left[e^{j \frac{1}{1} \frac{\eta}{4}} - e^{j \frac{1}{1} \frac{\eta}{4}} + e^{j \frac{1}{1} \frac{\eta}{4}} \right]$$

$$= \frac{1}{\pi n} \left[\frac{e^{j \frac{1}{1} \frac{\eta}{4}} - e^{j \frac{1}{1} \frac{\eta}{4}}}{2j} + -\frac{e^{j \frac{1}{1} \frac{\eta}{4}}}{2j} + e^{j \frac{1}{1} \frac{\eta}{4}} \right]$$

$$h_{d}(n) = \frac{1}{\pi n} \left(\frac{\sin \pi n - \sin \pi}{4} \right) \text{ for all } m \text{ except } n = 0 \right]$$

$$N = 9 \implies h(n) = \begin{cases} h_{d}(n) \omega_{j}(n) \text{ for } |n| \leq t_{f} \\ e \text{ otherwise} \end{cases}$$

Using Hamming window:

$$W_{H}(n) = \begin{cases} 0.54 + 0.46 \cos \frac{2\pi n}{N-1}; & -\frac{(N-1)}{2} \leq n \leq \frac{N-1}{2} \\ 0; & \text{otherwise.} \end{cases}$$

$$\omega_{H}(n) = 0.54 + 0.46 \cos \frac{\pi n}{4}$$
 $\omega_{H}(0) = 1$
 $\omega_{H}(0) = 1$
 $\omega_{H}(-1) = \omega_{H}(1) = 0.912$
 $\omega_{H}(-2) = \omega_{H}(2) = 0.682$
 $\omega_{H}(-3) = \omega_{H}(3) = 0.398$
 $\omega_{H}(-4) = \omega_{H}(4) = 0.1678$
 $\omega_{H}(-4) = \omega_{H}(4) = 0.1678$
 $\omega_{H}(-4) = \omega_{H}(4) = 0.1678$
 $\omega_{H}(1) = \omega_{H}(-1) = -0.1678$
 $\omega_{H}(2) = \omega_{H}(-2) = -0.159$
 $\omega_{H}(3) = \omega_{H}(-3) = -0.075$
 $\omega_{H}(-4) = \omega_{H}(4) = 0.1678$
 $\omega_{H}(4) = \omega_{H}(4) = 0.1679$
 $\omega_{H}(4) = \omega_{H}(4) =$

$$hd(0) = Lt \frac{Sin \pi n}{\pi n} - Lt \frac{Sin \frac{\pi}{4}n}{\pi n}$$

$$hd(0) = 1 - \frac{1}{4} = 3/4 = 0.75$$

,'. Filter Co-efficients using Hamming window
$$h(0) = hd(0) \omega_{H}(0) = 0.75$$

 $h(1) = hd(1) \omega_{H}(1) = -0.2052 = h(-1)$

$$h(2) = h(-2) = h_{1}(2) \text{ id}_{1}(2) = -0.1084$$

$$h(3) = h(-3) = h_{2}(3) \text{ id}_{1}(3) = -0.03$$

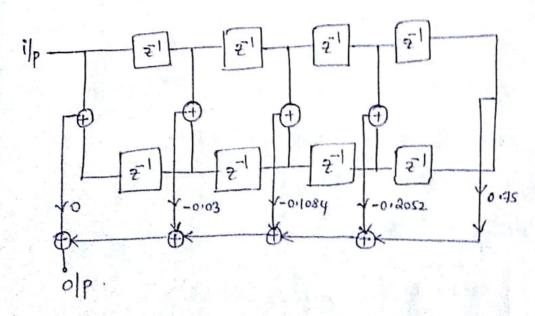
$$h(4) = h(-4) = h_{2}(4) \text{ id}_{1}(4) = 0$$

$$\therefore H(2) = h(0) + \frac{1}{2} h(n) \left[\frac{1}{2} n + \frac{1}{2} n \right]$$

$$H(2) = 0.75 = 0.2052 \left(\frac{1}{2} + 2 \right) -0.1084 \left(\frac{1}{2} + 2^{9} \right) -0.03 \left(\frac{1}{2} + 1^{1/3} \right)$$
Transfer function of a realizable filter

H(2) =
$$H(2) = H(2) = 0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23) -0.03 (23 + 23)$$

:. Filter Co-efficients are
$$h(0) = h(8) = 0$$
.
 $h(1) = h(7) = -0.03$
 $h(2) = h(6) = -0.1084$
 $h(3) = h(5) = -0.2052$
 $h(4) = +0.75$

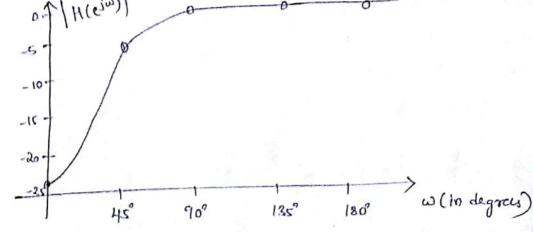


H(e/w) =
$$\sum_{n=0}^{(N-1)/2} a(n) \cos \omega n$$

where $a(0) = h(\frac{N-1}{2}) = h(4) = 0.45$
 $a(n) = 2h(\frac{N-1}{2}-n)$
 $a(1) = 2h(4-1) = 2h(3) = -0.8052x2 = -0.4104$
 $a(2) = 2h(4-2) = 2h(2) = -0.1084x2 = -0.2168$
 $a(3) = 2h(4-3) = 2h(1) = -0.03x2 = -0.06$
 $a(4) = 2h(4-4) = 2h(0) = 0$

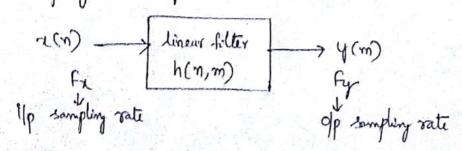
H(elw) = 0.75 - 0.4104 Cosw - 0.2168 Cos2w - 0.06 Cos3w

W(in degree) 0' 45° 60° 90' 120° 135' 120° $H(e^{jw})$ 0.0628 0.50 0.7132 0.9668 1.0036 0.99 1.0036 $H(e^{jw})$ dB -24.04 -6.02 -2.935 -0.293 0.031 -0.087 0.031



9. Derive the expression for decimation by factor D.

Sol. Decimation is a process of down sampling, reducing the sampling rate by a factor D.



To avoid almosing, for Band limited IWI 4 TD. x(n) Sante abusing v(n) Down Sampler Sampler Fy shite-always felter is perfect LPF with impulse h(n). $\vartheta(n) = \chi(n) * h(n)$ $v(n) = \sum_{k=0}^{\infty} h(k) x(n-k)$ $y(m) = y(mD) = \sum_{k=0}^{\infty} h(k) z(mD-k) \rightarrow 0$ Down sampling operation is observed as multiplication of two sequences. าช(n) = าช(n) รู(n) y(m)= 7 (m0) Take Apply ZT. to eq(s) Y(z)= = y(m) = m 1(3)= \(\frac{1}{\infty}\) \(\frac{1}{\infty}\) = \(\frac{1}{\infty}\) \(\frac{1}{\infty}\) \(\frac{1}{\infty}\) D(m) = 0 except at multiples of D. .'. $Y(z) = \sum_{n=0}^{\infty} \overline{y}(m) z^{-\frac{m}{D}} \longrightarrow \emptyset$ v (m)= v(m) f(m) Y(2) = 2 x(m) f(m) = D ->3 S(m) Can be represented by DFS as S(m)= 1 5 e 1 2 TKm ⇒ y(2)2 \(\frac{1}{D}\)\[\frac{1}{D}\]\[\frac{1}{D}\]\[\frac{1}{2}\]\[\frac{1}{D}\]\[\frac{1}{D}\]\[\frac{1}{2}\]\[\frac{1}{D}\]\[\fr

$$Y(2) = \frac{1}{D} \sum_{k=0}^{D-1} \left[\sum_{m=-\infty}^{\infty} v(m) \left(e^{-j \frac{2\pi r}{D}} \frac{y_D}{z} \right)^{-m} \right]$$

$$Y(2) = \frac{1}{D} \sum_{k=0}^{D-1} V\left(e^{-j \frac{2\pi r}{D}} \frac{y_D}{z} \right)$$

WKT
$$V(n) = h(n) + x(n) \Rightarrow V(z) = H(z)x(z)$$

$$\Rightarrow \chi(z) = \frac{1}{D} \sum_{k=0}^{D-1} H\left(e^{-j\frac{2\pi k}{D}} \chi^{VD}\right) \cdot \chi\left(e^{-j\frac{2\pi k}{D}} \chi^{VD}\right)$$

Substitute = rejuy; r=1

$$Y(e^{j\omega_{4}}) = \frac{1}{D} \sum_{k=0}^{D-1} H(e^{-j\frac{2\pi k}{D}} e^{j\frac{\omega_{4}}{D}}) \cdot X(e^{-j\frac{2\pi k}{D}} e^{j\frac{\omega_{4}}{D}})$$

Lety(
$$e^{j\omega y}$$
)= $y(\omega y)$

$$Y(\omega_y) = \frac{1}{D} \sum_{k=0}^{D-1} H\left(\frac{\omega_y - 2\pi k}{D}\right), \chi\left(\frac{\omega_y - 2\pi k}{D}\right)$$

$$X\left(\frac{\omega_y-2\pi x}{D}\right)$$
 indicates replica's of $X\left(\frac{\omega_y}{D}\right)$ at $\omega=0,2\pi,4\pi,...,2\pi(D-1)$

These are due to down sampling operations

···
$$Y(\omega_y) = \frac{1}{D} H(\frac{\omega_y}{D}) \cdot X(\frac{\omega_y}{D})$$

with a properly designed filter HD(w), the aliasing is

climinated

$$Y(\omega_y) = \frac{1}{D} \times (\frac{\omega_y}{D})$$
 for $0 \le |\omega_y| \le \pi$
 $Y(\omega_y) = \frac{1}{D} \times (\omega_x)$ $(:\omega_x = \frac{\omega_y}{D})$

The anti-aliasing filter band limits the signel to TID.

$$H(\omega_x) = \begin{cases} 1 & \text{for } |\omega_x| \leq \frac{\pi}{D} \\ 0 & \text{elsewhere} \end{cases}$$

Two sampling rates are related as $f_y = \frac{f_x}{D}$.

$$\omega_{x} = R\pi \frac{F}{Fx}; \quad \omega_{y} = R\pi \frac{F}{Fy}$$

$$\omega_{y} = R\pi \frac{F}{Fx}; \quad \omega_{x} = \Omega \frac{F}{Fx}; \quad D = \omega_{x} D.$$

$$(\cdot) \quad \omega_{x} = \Omega \frac{F}{Fx}; \quad \omega_{x} = \Omega \frac{F}{Fx}; \quad D = \omega_{x} D.$$

10. Explain Interpolation process with equations and spectrum.

The Interpolation is defined as process of upsampling by a factor I Interpolator is also called as sampling rate alternation device.

Sampling from Fx of ilp signal 1 by I => Fy = I(Fx)

Interpolator simply puts (I-1) zeros blw successive samples of X(n)

Derivation of interpolation equation

V(K) \$0 multiples of I

i.
$$h(m-k) V(k) = \begin{cases} 0 & \text{for } k \neq \text{Integral multiple of } I \\ \text{mon-zero} & \text{else where} \end{cases}$$

Replace k by KI

Relation between expections of
$$X(n)$$
 and $y(n)$

Step 1: $V(m) = \begin{cases} x(\frac{m}{n}) & m=0, \pm T, \pm 2T \\ 0 & \text{otherwise} \end{cases}$

thep 2: $\frac{1}{2} = T_{2} n_{1} s_{p} r_{p} m$
 $V(2) = \sum_{m=-\infty}^{\infty} V(m) \geq m T$
 $V(2) = \sum_{m=-\infty}^{\infty} V(m) \geq m T$
 $V(2) = X(2T)$

Step 4: $V(2) = X(m)$
 $V(2) = X(2T)$

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 $V(2) = X(2T)$

Step 5: $V(2) = X(2T)$
 $V(2) = X(2T$

Wy = Wx (0) Wz = Wy I

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$$\psi(0) = \frac{C}{2\pi} \int_{-1T}^{TT} \times (w_x) \cdot \frac{1}{I} dw_x$$

$$Y(0) = \frac{C}{L} \cdot \frac{1}{2\pi \Gamma} \int_{-\pi}^{\pi} X(\omega_x) d\omega_x$$

