



Uncertainty Quantification of Thermal Damage in Hyperthermia as a Cancer Therapy

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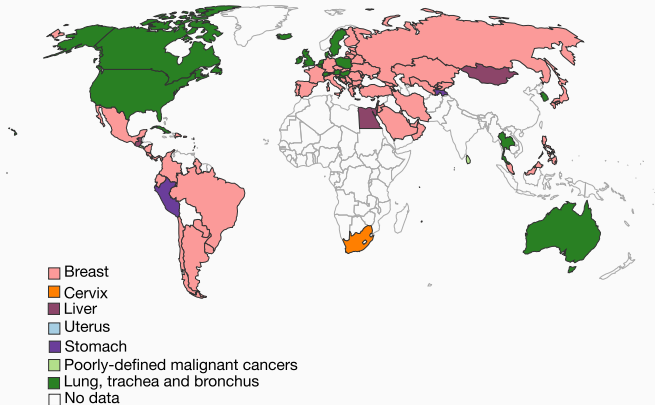
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Introduction

Cancer remains a major global health concern, with breast cancer being the leading cause of cancer-related death among women in many countries.



- Promising non-invasive cancer treatment;
- Heats the tumor region to induce necrosis;
- Hyperthermia is a complementary treatment to chemotherapy and radiotherapy;
- One strategy involves the use of a ferrofluid containing magnetic nanoparticles.

Mathematical Model

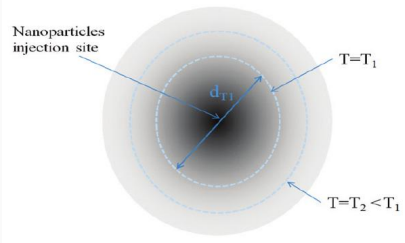
The Pennes equation was considered to simulate bioheat transfer¹.

$$\begin{cases} \rho c \frac{\partial T}{\partial t} = \nabla \cdot k \nabla T + \omega_b \rho_b c_b (T_a - T) + Q_m + Q_r & \text{em } \Omega \times I \\ k \nabla T \cdot \vec{n} = 0 & \text{em } \partial\Omega \times I \\ T(\cdot, 0) = 37, 0 & \text{em } \Omega \end{cases} \quad (1)$$

¹Fatigate, G. R., Lobosco, M., and Reis, R. F. (2023). A 3D Approach Using a Control Algorithm to Minimize the Effects on the Healthy Tissue in the Hyperthermia for Cancer Treatment. *Entropy*, 25(4), 684.

- Possibility of using high energy potential;
- Water-based, biocompatible ferrofluid solution;
- Injection of ferromagnetic fluid, e.g., 0.1, 0.2, or 0.3 cc;
- SAR^2 is responsible for modeling the overheating caused by the injections.

$$Q_r = \sum_{i=1}^{N_p} A e^{-r_i^2/r_{0,i}^2},$$



²Salloum, M., Ma, R., and Zhu, L. (2009). Enhancement in treatment planning for magnetic nanoparticle hyperthermia: optimization of the heat absorption pattern. *International Journal of Hyperthermia*, 25(4), 309–321.



Simplifications adopted in the Pennes' model:

- Heat transfer is assumed to occur only through capillaries;
- Blood flow is considered isotropic;
- Vascular geometry is not taken into account;
- Capillary temperature is assumed to be equal to body temperature;

Numerical Scheme

The solution was approximated using the Finite Difference Method (FDM) in a heterogeneous medium, applying the FTCS scheme.

$$T_{i,j,k}^{n+1} = \frac{h_t}{\rho c} \left[\frac{k_{i+1/2,j,k}(T_{i+1,j,k}^n - T_{i,j,k}^n) - k_{i-1/2,j,k}(T_{i,j,k}^n - T_{i-1,j,k}^n)}{h^2} + \right. \\ \left. \frac{k_{i,j+1/2,k}(T_{i,j+1,k}^n - T_{i,j,k}^n) - k_{i,j-1/2,k}(T_{i,j,k}^n - T_{i,j-1,k}^n)}{h^2} + \right. \\ \left. \frac{k_{i,j,k+1/2}(T_{i,j,k+1}^n - T_{i,j,k}^n) - k_{i,j,k-1/2}(T_{i,j,k}^n - T_{i,j,k-1}^n)}{h^2} + \right. \\ \left. \rho_b c_b \omega_b (T_a - T_{i,j,k}^n) + Q_m + Q_r \right] + T_{i,j,k}^n \quad (2)$$

Thermal Damage

Thermal damage was evaluated using the Arrhenius model in both tumor and healthy tissue regions.

$$\Omega(x, y, z, t) = \ln \left(\frac{C(0)}{C(t)} \right) = \int_0^t A e^{\frac{-E_a}{R_u T(x, y, z, \tau)}} d\tau, \quad (3)$$

- If the computed damage parameter $\Omega(x, y, z, t)$ reaches 1.0, approximately 63.2% of the cells are considered to be dead;
- An Arrhenius damage parameter of 4 indicates nearly 98.2% cellular death;
- Omega values in the range $4 \leq \Omega \leq 10$ are considered indicative of complete tumor ablation.

Uncertainty Quantification

Monte Carlo simulations with 1,000 samples were performed to quantify the uncertainties associated with two correlated parameters in the Arrhenius model: the frequency factor A and the activation energy E_a .

$$E_a \approx 2.63 \times 10^3 \ln(A) + 2.46 \times 10^4 \begin{cases} E_{a_u} & = W \sim U(E_{a_{\min}}, E_{a_{\max}}), \\ A & = e^{3.832 \times 10^{-4} E_a - 10.042}, \end{cases}$$

$$\ln(A) = 3.832 \times 10^{-4} E_a - 10.042 \begin{cases} A_u & = W \sim U(A_{\min}, A_{\max}), \\ E_a & = 2.63 \times 10^3 \ln(A_u) + 2.46 \times 10^4 \end{cases}$$

Results

- Implemented in C;
- AMD® EPYC™ 7713 CPU;
- NVIDIA A100 GPU (for CUDA parallelization);
- Single-core execution;
- Results visualized using ParaView;
- Execution parameters and domain taken from the literature.

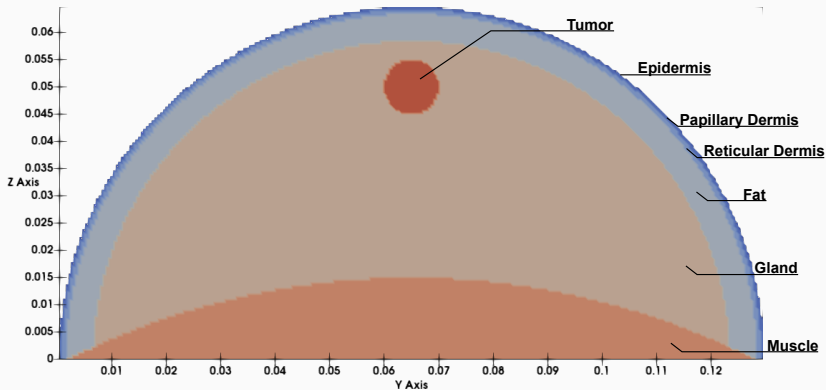


Figure 1: Simulated breast tumor

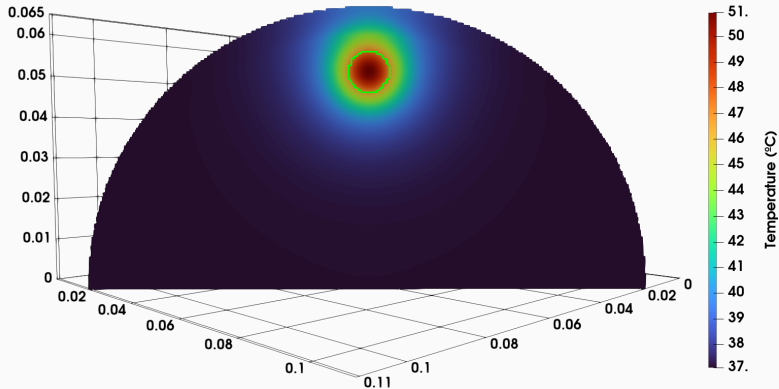


Figure 2: Temperature distribution computed from the bioheat equation at $t = 50$ min.

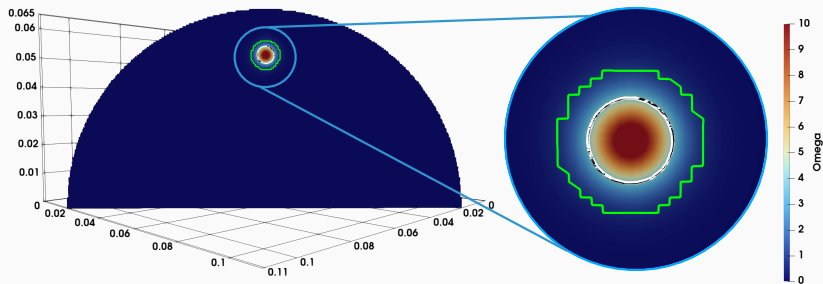


Figure 3: Simulation results for the scenario with uncertainty in the frequency factor A at $t = 5$ min.

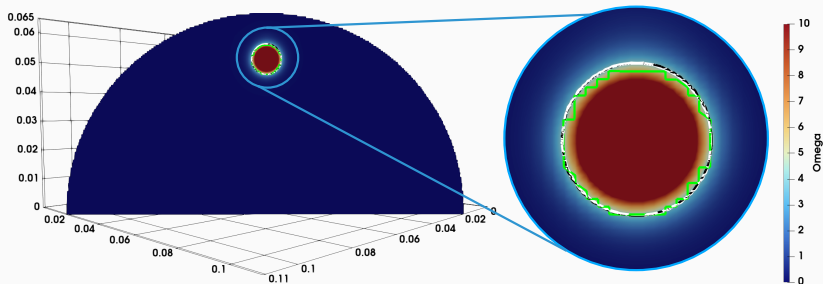


Figure 4: Simulation results for the scenario with uncertainty in the frequency factor A at $t = 10$ min.

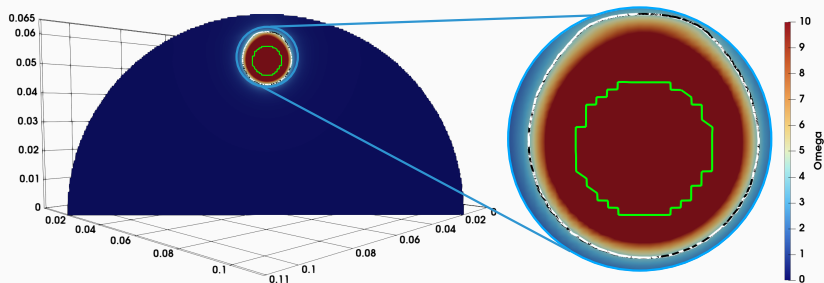


Figure 5: Simulation results for the scenario with uncertainty in the frequency factor A at $t = 50$ min.

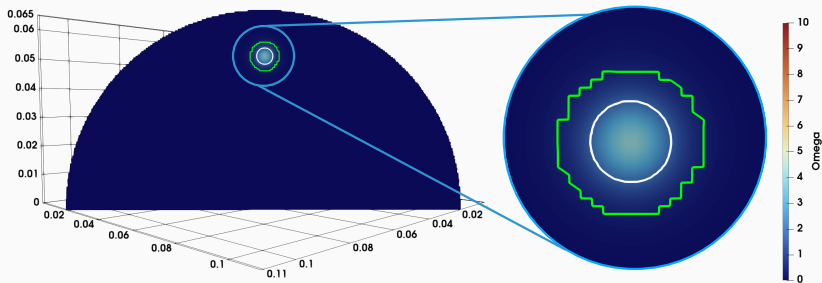


Figure 6: Simulation results for the scenario with uncertainty in the activation energy E_a at $t = 5$ min.

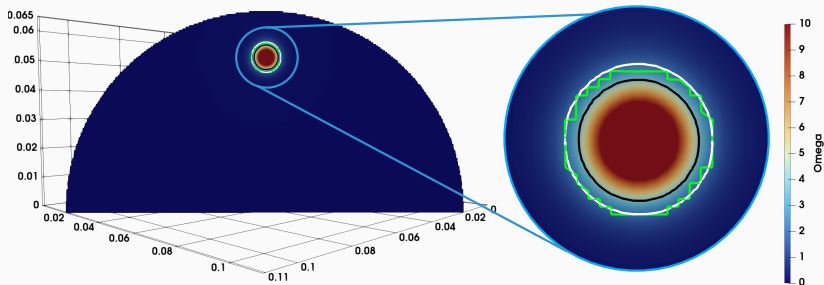


Figure 7: Simulation results for the scenario with uncertainty in the activation energy E_a at $t = 10$ min.

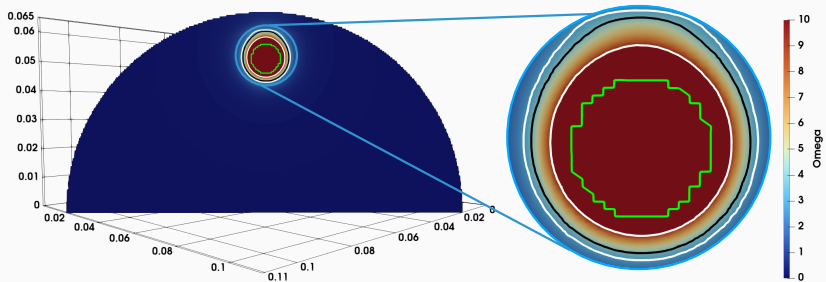


Figure 8: Simulation results for the scenario with uncertainty in the activation energy E_a at $t = 50$ min.

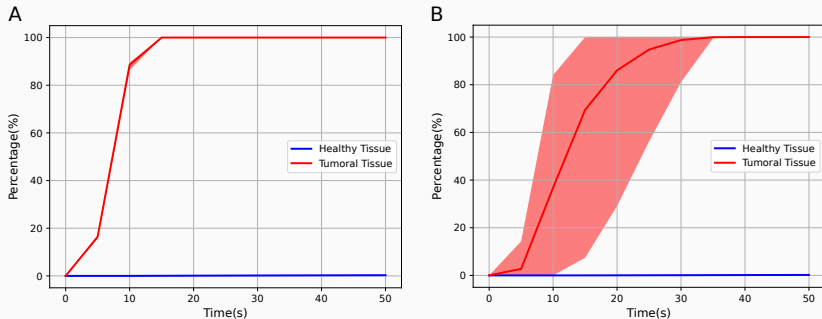


Figure 9: Results of the uncertainty quantification due to variations in A and E_a for assessing tumor damage during hyperthermia treatment.

Conclusion and Future Works

- Variations in the frequency factor A have a minor influence on tissue damage predictions, even when A spans from $A_{\min} = 7.39 \times 10^{39}$ to $A_{\max} = 3.10 \times 10^{98}$.
- In contrast, variations in the activation energy E_a significantly affect the outcomes, with E_a ranging from $E_{a_{\min}} = 2.577 \times 10^5 \text{ J/mol}$ to $E_{a_{\max}} = 6.030 \times 10^5 \text{ J/mol}$.
- The confidence intervals observed in the thermal damage suggest that uncertainty in E_a leads to a critical damage threshold ($\Omega \geq 4$) being reached between 15 and 35 minutes.



- In future work, we plan to study different tissue layers in the human body using realistic tumor and tissue geometries;
- Incorporate Multilevel Monte Carlo (MLMC) methods to accelerate simulations and improve computational efficiency;
- Finally, we intend to validate the model results using clinical or experimental data.

Obrigado!
Thanks!



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⁴APQ-01226-21