# Isotope analytical uncertainty propagation

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Here I (1) state the uncertainty propagation rules plainly, (2) apply them to our mass-balance model equation and calculate the results, and finally (3) I explore the the derivation of Genereux's (1998) isotopic tracer component uncertainty equations and how they, sadly, differ to my arithmetic propagation in section (2).

# 1 Uncertainty propagation rules

Our uncertainty rules are as follows. Let q be some quantity, and  $u_q$  be its uncertainty, where q is a function of variables x, y and z.

For constants

$$q = Bx$$

$$\frac{u_q}{q} = \frac{u_x}{x}$$

$$(1.1)$$

For sums

$$q = x \pm y \pm z$$

$$u_q = \sqrt{u_x^2 + u_y^2 + u_z^2}$$
(1.2)

And for **products/quotients** 

$$q = xyz$$

$$\frac{u_q}{|q|} = \sqrt{\left(\frac{u_x}{x}\right)^2 + \left(\frac{u_y}{y}\right)^2 + \left(\frac{u_z}{z}\right)^2}$$
(1.3)

### 2 Ruan's propagation

#### Derivation

Let  $p_E$  be the proportion of streamflow derived from rainfall according to an isotope E, where

$$p_E = \frac{E_{streamflow} - E_{baseflow}}{E_{rain} - E_{baseflow}}$$
(2.1)

As such, for our analysis, we propagate the uncertainty as follows, relying on our known uncertainty in measuring isotope values  $u_E$ 

$$\begin{split} p_E &= \frac{E_{streamflow} - E_{baseflow}}{E_{rain} - E_{baseflow}} \\ &\therefore u_{p_E} = |p_E| \sqrt{\left(\frac{u_{[E_{streamflow} - E_{baseflow}]}}{E_{streamflow} - E_{baseflow}}\right)^2 + \left(\frac{u_{[E_{rain} - E_{baseflow}]}}{E_{rain} - E_{baseflow}}\right)^2} \end{split}$$

where

$$u_{[E_{streamflow}-E_{baseflow}]} = u_{[E_{rain}-E_{baseflow}]} = \sqrt{u_E^2 + u_E^2}$$

such that

$$u_{p_E} = |p_E| \sqrt{\left(\frac{\sqrt{u_E^2 + u_E^2}}{E_{streamflow} - E_{baseflow}}\right)^2 + \left(\frac{\sqrt{u_E^2 + u_E^2}}{E_{rain} - E_{baseflow}}\right)^2}$$
 (2.2)

We then average  $p_{\delta^2 H}$  and  $p_{\delta^{18}O}$ , each with their own uncertainty derived above, as follows

$$p = \frac{p_{\delta^{18}O} + p_{\delta^{2}H}}{2}$$

$$\therefore u_{p} = |p| \frac{\sqrt{u_{p_{\delta^{18}O}} + u_{p_{\delta^{2}H}}}}{p_{\delta^{18}O} + p_{\delta^{2}H}}$$
(2.3)

### Application to Liesbeek study

For our study, we combined long term analytical precision and accuracy using Equation 1.2

$$u_{\delta^{18}O} = \sqrt{0.07^2 + 0.13^2}$$

$$= 0.1476482$$

$$u_{\delta^2 H} = \sqrt{0.2^2 + 1.5^2}$$

$$= 1.5132746$$

As such, we calculate our  $p_E$  values using Equation 2.1 as

$$\begin{split} p_{\delta^{18}O} &= \frac{-4.7860375 - -2.2142798}{-4.794164 - -2.2142798} \\ &= 0.99685 \\ p_{\delta^2 H} &= \frac{-20.4562927 - -6.0803734}{-20.092425 - -6.0803734} \\ &= 1.0259682 \end{split}$$

and their uncertainties using Equation 2.2

$$\begin{split} u_{p_{\delta^{18}O}} &= |0.99685| \sqrt{\left(\frac{\sqrt{0.1476482^2 + 0.1476482^2}}{-4.7860375 - -2.2142798}\right)^2 + \left(\frac{\sqrt{0.1476482^2 + 0.1476482^2}}{-4.794164 - -2.2142798}\right)^2} \\ &= 0.114281 \\ u_{p_{\delta^2 H}} &= |1.0259682| \sqrt{\left(\frac{\sqrt{1.5132746^2 + 1.5132746^2}}{-20.4562927 - -6.0803734}\right)^2 + \left(\frac{\sqrt{1.5132746^2 + 1.5132746^2}}{-20.092425 - -6.0803734}\right)^2} \\ &= 0.2188186 \end{split}$$

We then use Equation 2.3 to derive p proper

$$p = \frac{0.99685 + 1.0259682}{2}$$

$$= 1.0114091$$

$$\therefore u_p = |1.0114091| \frac{\sqrt{0.114281 + 0.2188186}}{0.99685 + 1.0259682}$$

$$= 0.1234319$$

Thus, we can conclude that, following this method, the Liesbeek River streamflow during our storm constituted  $101\% \pm 12.3\%$  rain-water.

## 3 Genereux's propagation

Knowing Equations 1–3, applying them to Equation 4 Genereux got

$$u_{p_{E}} = \sqrt{\left(u_{E_{baseflow}} \frac{E_{rain} - E_{streamflow}}{\left(E_{rain} - E_{baseflow}\right)^{2}}\right)^{2} + \left(u_{E_{rain}} \frac{E_{streamflow} - E_{baseflow}}{\left(E_{rain} - E_{baseflow}\right)^{2}}\right)^{2} + \left(u_{E_{streamflow}} \frac{-1}{E_{rain} - E_{baseflow}}\right)^{2}}$$

Since we know that, for our analyses, we have identical analytical uncertainty for any measurement of an isotope E, such that

$$u_{E_{streamflow}} = u_{E_{rain}} = u_{E_{baseflow}} = u_{E}$$

With this approach, I get  $p_{\delta^{18}O} = 0.99685 \pm 0.1594934$  and  $p_{\delta^2H} = 1.0259682 \pm 0.1413952$ , such that following (2.3)  $p = 1.0114091 \pm 0.1065724$ .

Problem:  $u_p$  from  $(2.2) \neq \text{that from } (3.2)$ 

### References

Genereux (1998) Water Resources Research 34(4):915–919