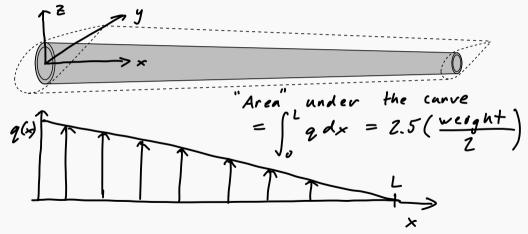
# Project #2 Model

#### Reminder

Objective: minimize spar weight, subject to stress and manufacturing constraints



#### **Euler-Bernoulli Beam Theory**

We will model the spar using Euler-Bernoulli Beam Theory.

Assumptions:

**planar symmetry:** longitudinal axis is straight, and cross section of beam has a longitudinal plane of symmetry

cross-section variation: cross section varies smoothly

**normality:** plan sections that are normal to longitudinal plane before bending remain normal after bending

strain energy: internal strain energy accounts only for bending moment deformations

linearization: deformations are small enough that nonlinear effects are negligible

material: the material is assumed to be elastic and isotropic

The displacement of the beam in the vertical direction, the direction of the load, is governed by the  $4^{th}$ -order PDE

$$\frac{d^2}{dx^2}\left(EI_{yy}\frac{d^2w}{dx^2}\right)=q, \qquad \forall x \in [0, L]$$

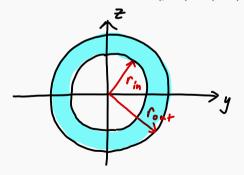
where

- w is the vertical displacement in the z direction; (m)
- q(x) is the applied load; (N/m)
- E is the elastic, or Young's, modulus, and;  $(P_A)$
- $I_{yy}$  is the second-moment of area with respect to the y axis.  $(m^4)$

In particular,

$$I_{yy} = \iint z^2 \ dz dy,$$

with the integral taken over the cross-sectional region. It is assumed that the centroid of the cross section is located at (y, z) = (0, 0).



Tables exist for this shape.

We will treat the spar like a cantilever beam, for which the boundary conditions are

no vertical 
$$\Rightarrow w(x=0)=0$$
,  $\frac{d^2w}{dx^2}(x=L)=0$  at the angular  $\frac{dw}{dx}(x=0)=0$   $\frac{d^3w}{dx^3}(x=L)=0$ . Tup displacement at root

6

Once the Euler-Bernoulli equation is solved for w, these displacements can be used to solve for the normal stress as a function of x:

$$\sigma_{xx}(x) = -z_{\text{max}} E \frac{d^2 w}{dx^2}$$

where  $z_{\text{max}}$  is the maximum height of the cross section (in this case, the outer radius).

• Since we are interested only in the magnitude of  $\sigma_{xx}$ , the negative sign can be ignored.



7

#### **Finite-Element Discretization**

We will discretize the Euler-Bernoulli beam equation using the finite-element method.

- solution is represented using Hermite-cubic shape functions
- finite-element equations result from the minimization of the potential energy functional

#### Matlab Implementation

10

```
This finite-element discretization of the beam equation is implemented by the (top-level)
                  -w, dw in previous slides
 Matlab function
    function [u] = CalcBeamDisplacement(L, E, Iyy, force, Nelem)
    % Estimate beam displacements using Euler-Bernoulli
    % Inputs:
    % L - length of the beam
    % E - longitudinal elastic modulus
    % Iyy - moment of area with respect to the y axis
    % Outputs:
       u - displacements at each node along the beam
11
```

#### Matlab Implementation (cont.)

Once the u displacements are known, they can be passed to CalcBeamSress to obtain the stress:

```
function [sigma] = CalcBeamStress(L, E, zmax, u, Nelem)
    % Compute stress in beam using Euler-Bernoulli
    % Inputs:
    % L - length of the beam
    % E - longitudinal elastic modulus
    % zmax - maximum height of the beam at each node Welem + ( array
    % u - displacements at each node along the beam from previous
8
    % Nelem - number of finite elements to use
    % Outputs:
9
        sigma - stress at each node in the beam 

Nelem + 1
10
11
```

# **High-level Steps For Constraint Function**

