

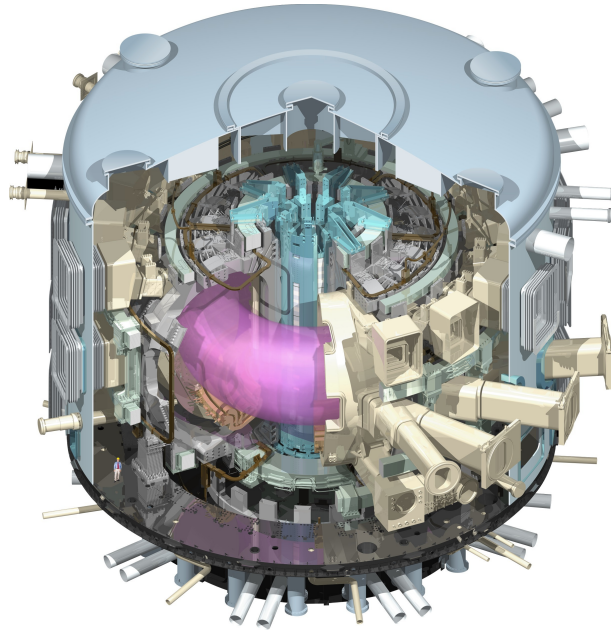
10401

Fusion Energy and Plasma Physics

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Abstract: Abstract



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| Symbol | Quantity |
|----------------------------|---|
| $n_{\text{flux fraction}}$ | n flux in breeder end/n flux in breeder start [] |
| C_F | Fixed cost propotionality constant [\$] |
| C_I | Nuclear island cost propotionality constant [$\$ \cdot \text{W} \cdot \text{m}^{-3}$] |
| P_E | Desired output power [MW] |
| P_W | Maximum wall load [$\text{MW} \cdot \text{m}^{-2}$] |
| B_{max} | Magnetic field at the edge of the coil [T] |
| σ_{max} | Tensile strenght of the magnetic field coils [atm] |
| η_t | Energy conversion efficiency [] |

Table I: Variables in the Freidberg's model

I. INTRO

In recent years a large and quickly growing collaboration between plasma phycisists and engineers have materialised in one of the most ambitious energy producing projects ever seen. The proof-of-concept plasma fusion tokamak reactor ITER¹ in Cadarache is currently taking shape in order to adress the issue of growing energy demands and climate changes.

The mission is simple: Prove that plasma fusion is a viable source of electricity.

Whilst not being the most surmountable task, many researchers and institutions have gathered from across the world, including the Department of Physics at DTU.

In this paper, three assignments are solved as part of the course “10401 Fusion Energy and Fusion Plasma Physics”. Some key aspects of fusion plasma fueled reactors are adressed and discussed in the assignments.

II. PART 1: A SIMPLE REACTOR MODEL

A. Freidberg's simple reactor model

In the 5th chapter of the textbook by Freidberg², he makes a simple model for designing a fusion reactor power plant. The model uses simple geometric and electromagnetic assumptions with little involvement of plasma physics. The variables put into the model are shown in Table I. Table II shows the output quantities from the model. This model

| Symbol | Quantity | Obtained values |
|-------------------------|---|--|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 0.799 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 4.96 m |
| A | Aspect ratio | 2.4670 |
| A_p | Plasma surface | 393 m ² |
| V_p | Plasma volume | 395 m ³ |
| P_{dens} | Power density | $4.97 \times 10^6 \text{ W}\cdot\text{m}^{-1}$ |
| p | Plasma pressure | $7.37 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.53 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 4.57 T |
| β | Normalised plasma pressure | 8.85% |
| $\tau_{E_{\text{min}}}$ | Min confinement time for $(p \times \tau_E)_{\text{min}}$ | 1.14 s |

Table II: Output quantities in the model in Freidberg's² along with the obtained values when inserting the parameters from Eq. (1)

has been implemented in a matlab script provided for the course. The script is shown included in Appendix A. As an example, the model is run with the following parameters:

$$\begin{aligned}
 n_{\text{flux fraction}} &= 0.01 & P_E &= 1000 \text{ MW} \\
 P_W &= 4 \text{ MW}\cdot\text{m}^{-2} & B_{\text{max}} &= 13 \text{ T} \\
 \sigma_{\text{max}} &= 3000 \text{ atm} & \eta_t &= 0.4
 \end{aligned} \tag{1}$$

Note that C_F and C_I has been omitted as these serve no purpose for this assignment. It is not of interest how expensive the plant will be. Rather the geometries and physical quantities are of interest. The results from the model is given in Table II.

B. Model sensitivity

At this point Freidberg has provided a model that produce some reasonable results for a powerplant. It could be interesting to see how this model behaves when some vital parameters are changed. In the last section the model used the parameters shown in

Eq. (1). Now the model will be iterated over variations in the following parameters, while retaining the rest. The variable parameters are the electric power P_E , the maximum wall loading P_W , the maximum magnetic field B_{\max} and the maximum stress σ_{\max} . Appendix B includes the code for iterating the matlab model over various parameters.

1. Change in desired power output.

For the rise in megawatts produced (500-1000 MW) there are a linear rise in aspect ratio, major radius, plasma surface and plasma volume. The rest of the parameters where constant except for the magnetic field strength at the magnetic axis and the normalised plasma pressure. These are shown in ??.

C. Elliptic Cross section

Freidberg's model assumes a circular cross section of the plasma. In reality this is not the case, and as of such we will now make a more realistic, yet still approximate reactor for an elliptic plasma cross section. In describing the geometry one refers to the elongation ratio:

$$\kappa = \frac{a_{\max}}{a_{\min}} \quad (2)$$

With a_{\max} the major radius and a_{\min} the minor radius of the ellipse. This parameter ensures a true elliptic cross section as defined by the equation,

$$\frac{x^2}{a_{\max}^2} + \frac{y^2}{a_{\min}^2} = 1 \quad (3)$$

which can be parameterised as

$$\begin{bmatrix} x_1 \\ y_1 \end{bmatrix} = \begin{bmatrix} a_{\min} \cos \phi \\ \kappa a_{\min} \sin \phi \end{bmatrix} \quad (4)$$

$$(5)$$

Meanwhile the blanket must be implemented as an ellipse or swelled ellipse. The true ellipse results in a difference of thickness in the blanket while the second results in a blanket of equal thickness throughout the structure. To this, the choice of implementing the blanket as a true ellipse has been made, since it simplifies derivations a bit. Note however, that keeping a constant thickness is the preferable option as it will reduce the

engineering volume and hence the cost of the machine.

The outer layer is parameterised

$$\begin{bmatrix} x_2 \\ y_2 \end{bmatrix} = \begin{bmatrix} (b + a_{\min}) \cos \phi \\ \kappa(b + a_{\min}) \sin \phi \end{bmatrix} \quad (6)$$

with b the blanket thickness at the minor ellipse axis. Choosing for now, $a_{\min} = 2$, $\kappa = 2$ and $b = 1.2$, 5 and 6 are plotted on Figure 1 along with the variation in thickness of the blanket.

Given 5 and 6, the engineering volume can easily be derived if $c \cos(\phi)$ and $\kappa c \sin(\phi)$ is added to the x and y-direction in 6 respectively, where c is the minimum thickness of the magnetic coils that provide the torroidal field.

The cross sectional area of an ellipse is $A_e = \pi a_{\min} a_{\max}$ so the engineered volume becomes

$$\begin{aligned} V_I &= 2 \pi R_0 (A_{e, \text{outer}} - A_{e, \text{inner}}) \\ &= 2 \pi^2 R_0 ((a_{\min} + b + c)^2 - a_{\min}^2) \kappa \end{aligned} \quad (7)$$

and the plasma volume is similarly calculated as $V_P = 2 \pi^2 R_0 \kappa a_{\min}^2$. The plasma surface area is a bit more tricky, but it can be approximated as

$$S_p = 2 \pi R_0 \pi (3(a_{\min} + \kappa a_{\min}) - \sqrt{(3a_{\min} + \kappa a_{\min})(a_{\min} + 3\kappa a_{\min})}) \quad (8)$$

Using the same arguments as in the book, the B-field in the centre is surprisingly unchanged when going to the elliptical model. Now c is also approximated, or rather overestimated using a slight change to eq. (5.24) in the textbook. Since the force grows with a_{\min} inserting κa_{\min} instead yields an overestimation on the vertical force on the magnet. The tensile forces are the same, so the force balance leads to

$$c = \frac{2\xi}{1-\xi}(\kappa a + b) \quad (9)$$

with $\xi = B_{sic}^2/4\mu_0\sigma_{\max}$. These new equations are inserted in the code. The results are displayed in III. The plasma volume and surface area is of course increased as the plasma was made higher. This of course also results in a decreased power density. Overall, parameters such as B_0 , β and $\tau_{E_{\min}}$ while changing a bit, they were not changed significantly.

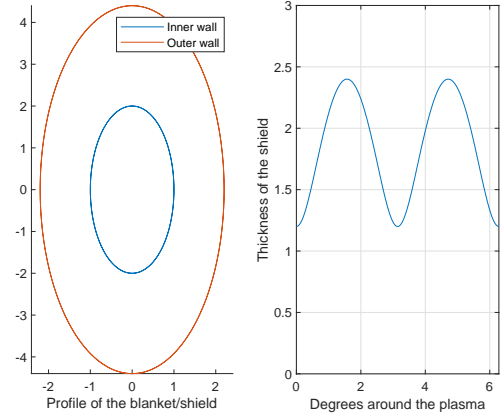


Figure 1: The profile of the blanket-and-shield and the thickness as a function of the angle around origo, ϕ .

| Symbol | Quantity | Obtained values |
|-------------------------|---|--|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 4.96 m |
| A | Aspect ratio | 2.4670 |
| A_p | Plasma surface | 609 m ² |
| V_p | Plasma volume | 793 m ³ |
| P_{dens} | Power density | $2.48 \times 10^6 \text{ W}\cdot\text{m}^{-1}$ |
| p | Plasma pressure | $5.20 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.08 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 4.60 T |
| β | Normalised plasma pressure | 6.17% |
| $\tau_{E_{\text{min}}}$ | Min confinement time for $(p \times \tau_E)_{\text{min}}$ | 1.62 s |

Table III:

Output quantities from the elliptical model

D. Main parameters for DEMO

Setting $P_E = 2000$ in the elliptical model yields the output parameters seen in table IV. Since R_0 is directly proportional to the electric power this of course increases linearly. The other geometric output parameters regarding areas and volumes also increase as a result. β has decreased a lot, so the plasma is not confined effectively in DEMO.

E. Designs for DEMO

With P_E , $\kappa = 2$ and $A = R_0/a_{\text{min}} = 3 \Leftrightarrow R_0 = 3 a_{\text{min}}$. This is implemented in the code and the results are displayed in V. β has increased a bit but only to 4.55%. R_0 has been forced down, so the plasma volume etc. has decreased as well. Overall it seems like a smaller R_0 while keeping a_{min} fixed is an improvement. Or in other words, $A = 3$ is more desirable than $A \approx 5$.

| Symbol | Quantity | Obtained values |
|-------------------------|---|--|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 9.95 m |
| A | Aspect ratio | 4.9512 |
| A_p | Plasma surface | $1.21 \times 10^3 \text{ m}^2$ |
| V_p | Plasma volume | $1.59 \times 10^3 \text{ m}^3$ |
| P_{dens} | Power density | $2.48 \times 10^6 \text{ W}\cdot\text{m}^{-1}$ |
| p | Plasma pressure | $5.20 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.08 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 8.80 T |
| β | Normalised plasma pressure | 1.69% |
| $\tau_{E_{\text{min}}}$ | Min confinement time for $(p \times \tau_E)_{\text{min}}$ | 1.62 s |

Table IV: Output quantities for DEMO using the elliptical model with $P_E = 2\text{GW}$

F. A and κ as free parameters

Designing the tokamak with κ and A as free parameters has led us to try and maximise profitability from V_P/A_P and β . Profitability in this context means that increasing the size of the tokamak leads to an increase in these parameters. However, there is a point when the change vs increase in size becomes constant. This means that we do not profit from increasing the size any longer.

V_P and A_P were calculated earlier so

$$\begin{aligned}
 \frac{V_P}{A_P} &= \frac{2 \pi R_0 \kappa a_{\text{min}}^2}{2 \pi R_0 \pi (3(a + \kappa a_{\text{min}}) - \sqrt{(3a_{\text{min}} + \kappa a_{\text{min}})(a + 3\kappa a_{\text{min}})})} \\
 &= \frac{\kappa a_{\text{min}}}{\pi (3 + 3\kappa - \sqrt{3 + \kappa} \sqrt{1 + 3\kappa})}
 \end{aligned} \tag{10}$$

The expression scales linearly with a_{min} so we set it equal to 1m since it has no effect on the choice of κ . Differentiating with respect to κ and plotting is done, with the results shown in Figure 2a. Considering the figure, $\kappa = 2.5$ is chosen as the change is close enough to zero given this value.

Now work will be done towards choosing a value for A . First for geometric reasons a

| Symbol | Quantity | Obtained values |
|-------------------------|---|--|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 6.03 m |
| A | Aspect ratio | 3 |
| A_p | Plasma surface | 738 m ² |
| V_p | Plasma volume | 962 m ³ |
| P_{dens} | Power density | $4.09 \times 10^6 \text{ W}\cdot\text{m}^{-1}$ |
| p | Plasma pressure | $6.68 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.39 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 6.07 T |
| β | Normalised plasma pressure | 4.55% |
| $\tau_{E_{\text{min}}}$ | Min confinement time for $(p \times \tau_E)_{\text{min}}$ | 1.26 s |

Table V: Output quantities for DEMO using the elliptical model with $P_{siE} = 2$, $\kappa = 2$ and setting $A = 3$

minimum R_0 is calculated. It is simply $R_0 = a_{\text{min}} + b + c$ where a_{min} is to be determined, $b = 1.2\text{m}$ and $c = \frac{2\xi}{1-\xi}(\kappa a_{\text{min}} + b)$. Meanwhile A is chosen to optimize β . Inserting R_0 into B_0 in the textbook yields

$$B_0 = \frac{2\xi(\kappa a_{\text{min}} + b) B_{\text{max}}}{((2\kappa - 1)a_{\text{min}} + a + b)} = \frac{178.75 a_{\text{min}} + 85.8}{55.5 + 36 a_{\text{min}}} \quad (11)$$

Where units has been disregarded and $\xi = 0.11$, $b = 1.2$, $\kappa = 2.5$ and $B_{\text{max}} = 13$ has been inserted. Meanwhile, inserting the textbook's expression for P_{dens} into the expression for p and inserting the input parameters yields

$$p = 1.042\text{E}6 \sqrt{\frac{1}{\kappa a_{\text{min}}}} \quad (12)$$

Thus β becomes

$$\beta = \frac{2148 (a_{\text{min}} + 1.542)^2}{\sqrt{a_{\text{min}}} (178.8 a_{\text{min}} + 85.8)^2} \quad (13)$$

This function is plotted in Fig. 2b and for $(\beta = 10\% \ a = 1.938\text{m})$ is achieved. Therefore $R_0 = 1.9378\text{m} + 1.2\text{m} + 2 \cdot 0.11/(1 - 0.11) \cdot 2.5 \cdot 1.938\text{m} + 1.2\text{m} = 4.632\text{m}$ which means $A = 4.632\text{m}/1.938\text{m} = 2.390$

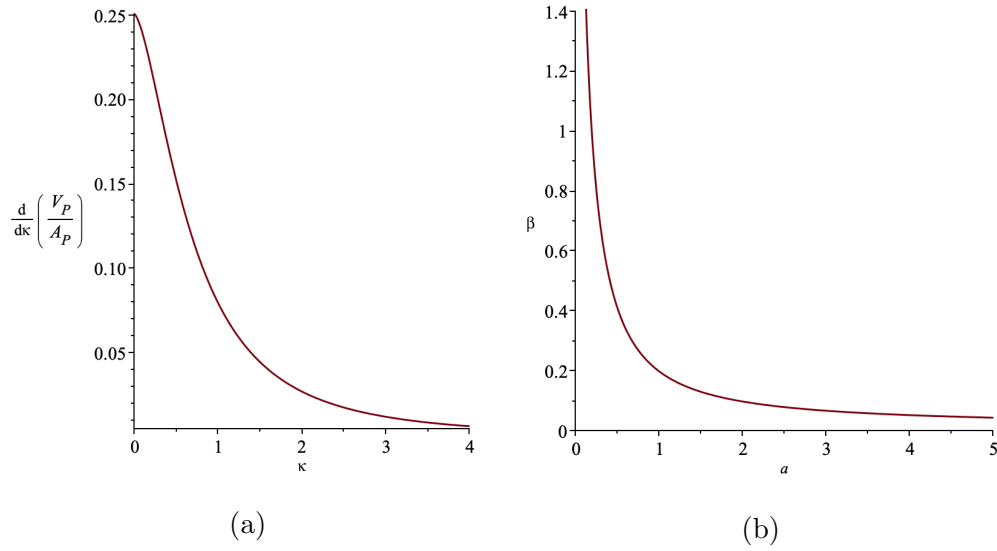


Figure 2

| Symbol | Quantity | Obtained values |
|-------------------------|---|--|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 2.60 m |
| A | Aspect ratio | 1.29 |
| A_p | Plasma surface | 630 m ² |
| V_p | Plasma volume | 414 m ³ |
| P_{dens} | Power density | $9.49 \times 10^6 \text{ W} \cdot \text{m}^{-1}$ |
| p | Plasma pressure | $1.02 \times 10^5 \text{ Pa}$ |
| n | Particle density | $2.12 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | -3.09 T |
| β | Normalised plasma pressure | 26.9% |
| $\tau_{E_{\text{min}}}$ | Min confinement time for $(p \times \tau_E)_{\text{min}}$ | 1.26 s |

Table VI: Output quantities for the elliptical model after β and A has been optimised

III. PART 2: DIAGNOSTICS VIA INTERFEROMETRY

When operating a fusion reactor a continous process of diagnostics is necessary in order to optimise the plasma for the fusion process. One of the active diagnostic methods are

interferometry. The goal here for this part of the paper is to measure the plasma electron density in the Danish Tokamak Undertaking reactor.

A. Cutt-off and Source frequency

Using a interferometer one can measure the electron density n_e of the plasma. The refractive index of electromagnetic waves depend on the electron density and plasma frequency ω_p proportionally:

$$\omega_p^2 \propto n_e \quad (14)$$

For O-mode plasma waves the refractive index is:

$$N_O = \sqrt{1 - \frac{\omega_p^2}{\omega^2}} \quad (15)$$

with ω being the probing wave frequency. The plasma will reflect the beam if the plasma frequency is larger than the beam frequency so

$$\omega > \omega_p = \sqrt{n_e \frac{e^2}{\epsilon_0 m_{e0}}} \quad (16)$$

So for a given frequency, the plasma must not exceed a critical cut off electron density:

$$n_e < n_c = \omega^2 \frac{\epsilon_0 \cdot m_{e0}}{e^2} \quad (17)$$

which gives

$$N_O = \sqrt{1 - \frac{n_e}{n_c}} \quad (18)$$

With a probing frequency much higher than the plasma frequency and the critical density much higher than the electron density Eq. (18) can be approximated by:

$$N_O = \sqrt{1 - \frac{n_e}{n_c}} \approx 1 - \frac{1}{2} \frac{n_e}{n_c} - \frac{\omega_p^2}{2\omega^2} \quad (19)$$

With sufficient accuracy, the linear dependence of the O-mode refractive index on the electron density is obtained if the normalised quantities obey:

$$\frac{n_e}{n_c} \leq 0.4 \quad \frac{\omega_p}{\omega} \leq 0.6 \quad (20)$$

We must calculate the phase shift as one beam travels in vacuum by the length L_V and one wave travels in the plasma by the length L_P . The phase shift in terms of 2π is equal

to the optical difference divided by the wavelength. With the refractive index in vacuum, $N_V = 1$, this yields:

$$\begin{aligned}\frac{\Phi}{2\pi} &= \frac{\Delta L_{opt}}{\lambda} = \frac{\int_{x_1}^{x_2} (N_V - N_O(x')) dx'}{\lambda} \approx \frac{1}{2\lambda n_c} \int_0^x n_e(x') dx' \\ &= 4.48 \times 10^{-16} \left(\frac{\lambda}{\text{m}}\right) \int_0^x \left(\frac{n_e(x')}{\text{m}^{-3}}\right) \left(\frac{dx'}{\text{m}}\right)\end{aligned}\quad (21)$$

Assuming a Gaussian distribution, the electron density at $\pm\infty$ is approximately equal to the densities just inside the reactor walls. Therefore

$$\int_{-\infty}^{\infty} n_e \exp\left(-\frac{(y-b)^2}{2c^2}\right) dy \approx n_e c \sqrt{2\pi} \quad (22)$$

With the density at the centre given as:

$$10^{16} \text{ m}^{-3} \leq n_e \leq 10^{18} \text{ m}^{-3}, \quad (23)$$

The c in Eq. (22) is the width of the Gaussian distribution and must fit inside the reactor. The DTU tokamak has a minor diameter of 0.250 m. Thus

$$\begin{aligned}\frac{\Phi}{2\pi} &\approx 4.48 \times 10^{-16} \left(\frac{\lambda}{\text{m}}\right) n_e 0.250 \text{ m} \sqrt{2\pi} = 1.12 \times 10^{-16} n_e \left(\frac{\sqrt{2\pi} c}{\omega \text{m}}\right) \\ &= 8.416 \times 10^{-8} \left(\frac{n_e}{\omega \text{S}}\right)\end{aligned}\quad (24)$$

Remembering Eq. (17)

$$\omega^2 \frac{\epsilon_0 m_{e0}}{e^2} = \omega^2 \frac{8.85 \times 10^{-12} \text{ F}\cdot\text{m}^{-1} \cdot 9.11 \times 10^{-31} \text{ kg}}{1.60 \times 10^{-19} \text{ C}} \quad (25)$$

\Downarrow

$$n_e < 0.000314 \omega^2 \quad (26)$$

Where any units has been disregarded. We want the largest possible phase shift which means that the lower the frequency the better. However cutoff must first be taken into account. Since the cutoff is given by Eq. (26) and since we want to measure densities up to 10^{18} m^{-3} the minimum frequency of the wave is

$$\frac{\omega}{2\pi} > \frac{\sqrt{\frac{10^{18} \text{ m}^{-3}}{0.000314}}}{2\pi} \quad (27)$$

\Downarrow

$$f \approx 9 \text{ GHz} \quad (28)$$

Given the available emitters, the best emitter is therefore the one with $f = 60\text{GHz}$.

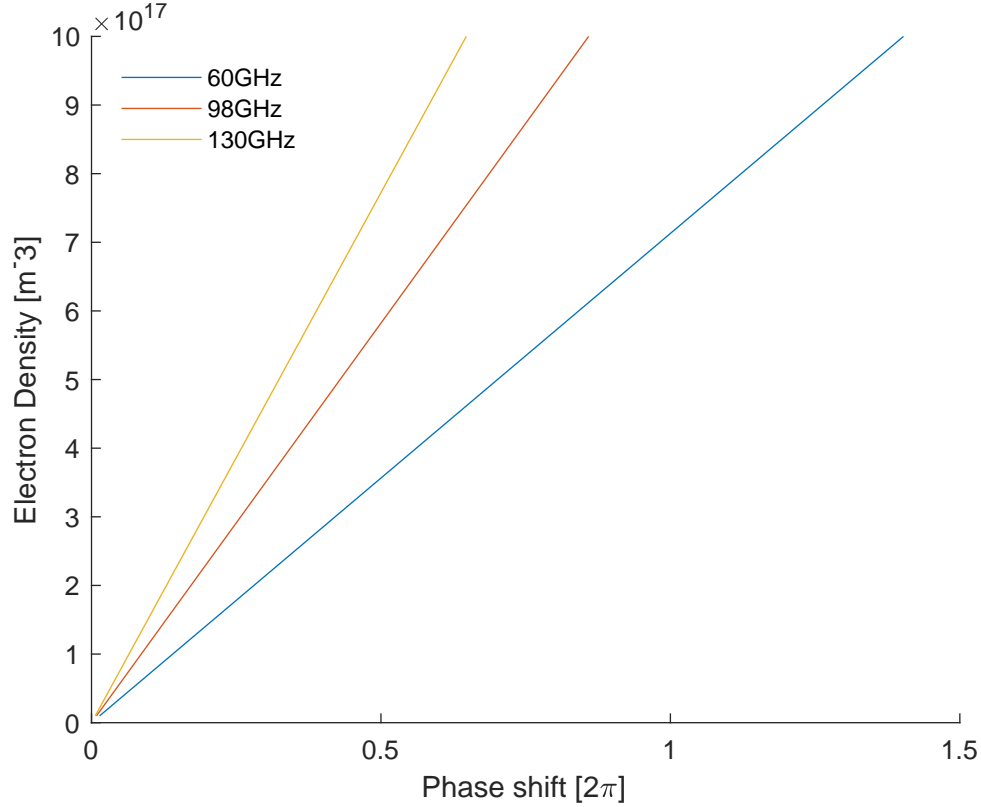


Figure 3: Electron densities for different wavelengths and phaseshifts

B. Beam Phaseshifts

The goal of the interferometer is to find the phaseshift between the microwave beam in vacuum and in plasma. Our suggestion is a setup involving a interferometer emitting a beam through the center of the reactor. The first measurement would be through vacuum to find the source phase. Afterwards phase measurements can be conducted with an active plasma in the reactor. So by first measuring the phase of the probing beam in vacuum, one can simply measure the phase shift.

We know from Eqs. (21), (22) and (24) that:

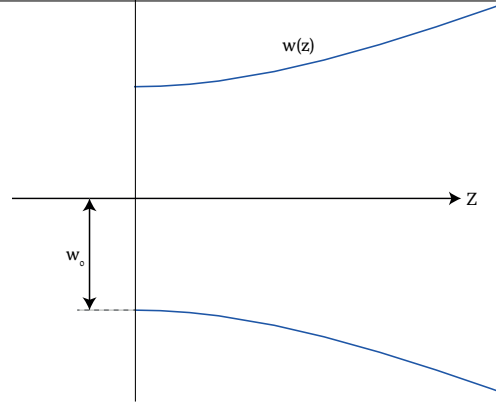
$$\frac{\Phi}{2\pi} = 8.416 \times 10^{-8} \left(\frac{n_e}{\omega s} \right) \quad (29)$$

So for different average electron densities through the plasma one can plot the resulting phaseshifts. This plot is shown in Fig. 3.

C. Evolving beam width

In our case we want to use a Gaussian microwave. Such beam propagates spatially as shown in Fig. 4. w_0 is the beam initial beam waist determined by the source and $w(z)$ is the function describing the waist. This equation is:

$$w(z) = w_0 \sqrt{1 + \left(\frac{\lambda z}{\pi w_0^2} \right)^2} \quad (30)$$



From this equation one can track the spatial propagation of the wave. In this project three sources are given. The initial beam waist is set to $w_0 = 0.0275\text{m}$ corresponding with half a reactor port. With

$$\frac{\lambda z}{\pi w_0^2} = \frac{9.542690316 \times 10^7 z}{w_0^2 f} \quad (31)$$

, and f being the frequency, the sources' beam waists are given as such:

$$60 \text{ GHz} : \quad w(z) = 0.0275 \sqrt{\left(1 + \frac{9.542690316 \times 10^7 z}{0.0275^2 \cdot 60 \times 10^9} \right)^2} \quad (32)$$

$$98 \text{ GHz} : \quad w(z) = 0.0275 \sqrt{\left(1 + \frac{9.542690316 \times 10^7 z}{0.0275^2 \cdot 98 \times 10^9} \right)^2} \quad (33)$$

$$130 \text{ GHz} : \quad w(z) = 0.0275 \sqrt{\left(1 + \frac{9.542690316 \times 10^7 z}{0.0275^2 \cdot 130 \times 10^9} \right)^2} \quad (34)$$

For the three given sources in this project, the beam waist has been plotted on Fig. 5. It is undesirable for some of the beam to not reach the output port and instead propagate into the reactor wall, as this will result in a lesser signal strength. Therefore it can be necessary to deploy a gaussian telescope.

D. Gaussian beam telescope interferometer

In order to control the beam waist, one can use a Gaussian beam telescope arrangement around the reactor. A lens is placed between the source and the reactor input port and again between the output port and the receiver. From chapter 5 in "Fusion Plasma Diagnostics with mm-Waves"³ the authors explain how such an arrangement can be obtained. Starting with the focal lengths of the lenses,

$$d = f_0 + f_1 \quad (35)$$

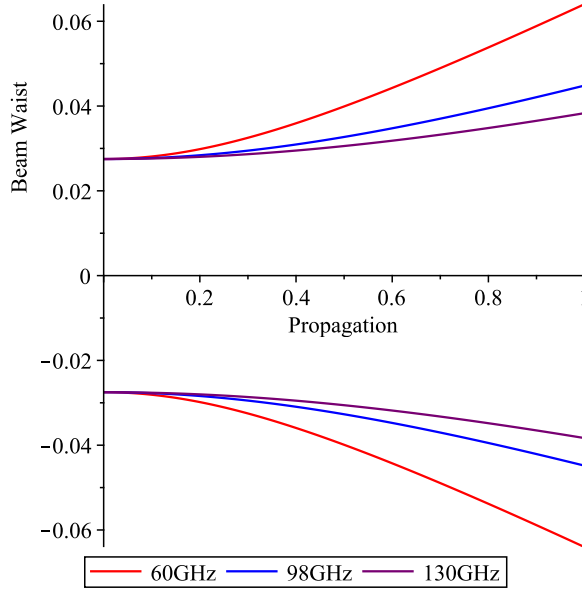


Figure 5: Beam Waist for the three microwave sources. The functions are Eqs. (32), (33) and (34).

, where f_0 and f_1 are focal lengths, and d are the distance between the lenses. The resulting narrowest beam waist after the second lens are given as:

$$w_2 = \frac{f_1}{f_0} w_0 \quad (36)$$

This making the transformation wavelength independent³ (Eq 5.118). The distance to this waist is given as:

$$d_3 = \frac{f_1}{f_0} \left(f_0 + f_1 - \frac{f_1}{f_0} d_0 \right) \quad (37)$$

The waist in between the lenses is given as:

$$w_1 = \frac{\lambda f_0}{\pi w_0} \quad (38)$$

And the distance from the first lens to this waist is:

$$d_1 = \left(\frac{\frac{d_0}{f_0} - 1}{\frac{w_0^2 \pi}{f_0 \lambda} + \left(\frac{d_0}{f_0} - 1 \right)^2} + 1 \right) f_0 \quad (39)$$

Thus the distance from w_1 to the second lens is:

$$d_2 = d - d_1 \quad (40)$$

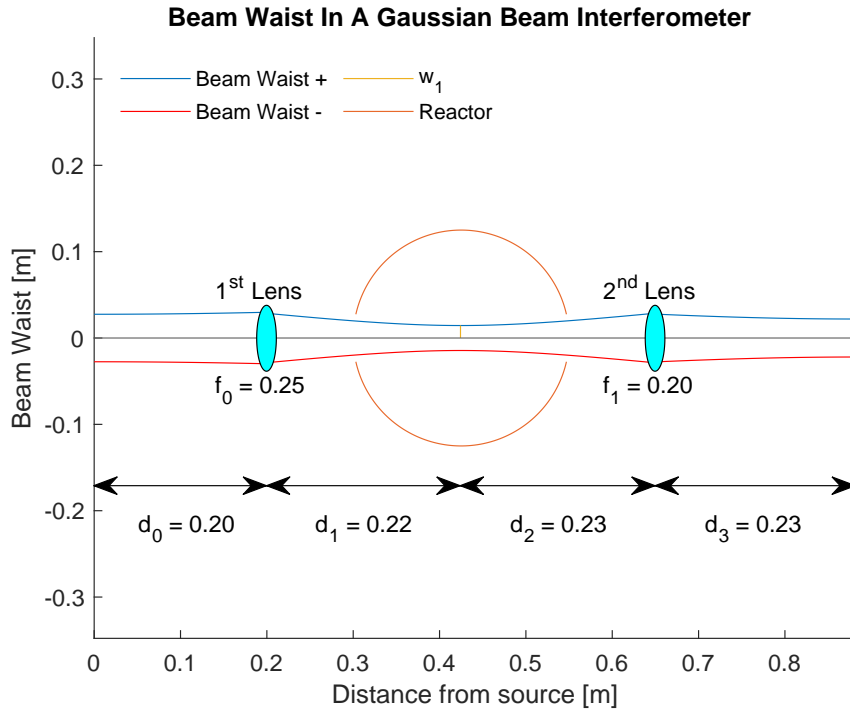


Figure 6: Gaussian beam telescope interferometer setup with input parameters shown in Eq. (41) and output parameters shown in Eq. (42)

Knowing these variables and utilising Eq. (30) we can model a complete setup. Using the matlab code in Appendix C, the following parameters were input:

$$\begin{aligned} r_p &= 0.0550 \text{ m} & r &= 0.125 \text{ m} & w_0 &= 0.0275 \text{ m} & freq &= 60 \text{ GHz} \\ d_0 &= 0.200 \text{ m} & d_r &= 0.100 \text{ m} & f_0 &= 0.250 \text{ m} & & 0.200 \text{ m} \end{aligned} \quad (41)$$

With r_p being the tokamak port radius, r the tokamak minor radius and d_r the distance between the first lens and the reactor wall. The script gave the results:

$$\begin{aligned} w_1 &= 0.0145 \text{ m} & w_2 &= 0.0220 \text{ m} \\ d_1 &= 0.224 \text{ m} & d_2 &= 0.226 \text{ m} & d_3 &= 0.232 \text{ m} \end{aligned} \quad (42)$$

Furtermore it plots a sketch of the desired interferometer setup. The sketch can be seen in Fig. 6.

Write section about interferometer considerations

ACKNOWLEDGMENTS

The authors would like to thank...

TODO LIST

| | |
|---|----|
|  Write section about interferometer considerations | 15 |
|---|----|

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‡ Homepage of the Technical University of Denmark <http://www.dtu.dk/english/>;

🔗 Project Repository: <https://github.com/rwiuff/10401>

¹ <https://www.iter.org/>.

² Jeffrey P. Freidberg, *Plasma physics and fusion energy* (Cambridge University Press, 2007).

³ Hans-Jürgen Hartfuß and Thomas Geist, *Fusion Plasma Diagnostics with mm-Waves* (Wiley-VCH, 2013).

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LISTINGS

Appendices

Appendix A: tokamakDTU_asign_1

```
1  %*****
2  % Name:          tokamakDTU
3  %
4  % Version:       1.0
5  %
6  % Purpose:       Contains the function 'tokamakDTU' which gives parameters
7  %                for a tokamak fusion power plant as output based on a
8  %                simplified model. The equations used are derived in
9  %                chapter 5 in Friedberg, Plasma physics and Fusion
10 %                Energy, 2007 (all references are referring thereto).
11 %
12 % To do (NOT for 10401 - Fusion Energi students):
13 %                1. Rewrite the code to a class (this is not done on purpose so
14 %                that the code is more readable for students not familiar
15 %                with classes). Can from that merge the files which takes
16 %                R_0/a and/or the ellipticity as an input into one file.
17 %
18 % Changelog:
19 %                1. December 2014:
20 %                Written by Michael Løiten based on a similar code written
21 %                as a bachelor project by Elias Pagh Sentius
22 %                mailto: mmag@fysik.dtu.dk
23 %*****
24
25 function [b, c, a, R_0, A, A_p, V_p, P_dens, p, n, B_0, beta, tau_E_min,...
26          C_per_watt] =...
27          tokamakDTU_asign_1(...
28          n_flux_fraction, C_F, C_I, P_E, P_W, B_max, sigma_max, eta_t)
```

```
29 %TOKAMAK_DTU Function which returns the parameters of a power plant
30 %
31 % Output parameters
32 %-----
33 % b          - Blanket/shield thickness [m]
34 % c          - Magnet coil thickness [m]
35 % a          - Minor radius [m]
36 % R_0        - Major radius [m]
37 % A          - Aspect ratio []
38 % A_p        - Plasma surface [m^2]
39 % V_p        - Plasma volume [m^3]
40 % P_dens     - Power density [W/m]
41 % p          - Plasma pressure [Pa]
42 % n          - Particle density [m^-3]
43 % B_0        - Magnetic field at magnetic axis [T]
44 % beta       - Plasma beta in the centre []
45 % tau_E_min  - Min confinement time for satisfaction of (p*tau_E)_min [s]
46 % C_per_watt - The cost of the powerplant [$]
47 %
48 % Input parameters
49 %-----
50 % n_flux_fraction - n flux in breeder end/n flux in breeder start []
51 % C_F          - Fixed cost propotionality constant [$]
52 % C_I          - Nuclear island cost propotionality constant [$W/m^3]
53 % P_E          - Desired output power [MW]
54 % P_W          - Maximum wall load [MW/m^2]
55 % B_max        - Magnetic field at the edge of the coil [T]
56 % sigma_max    - Tensile strenght of the magnetic field coils [atm]
57 % eta_t        - Energy conversion efficiency []
58
59
60 % The function starts by defining fixed constants
```

```

61 % Note that this is inefficient if we are looping over the function, but it
62 % makes the code easier to use, as these are not needed as input parameters
63
64 % Fixed constants
65 %#####
66 % Nuclear
67 %-----
68 % Energies
69 E_t      = 2.5e-8; % [MeV] Energy of slow (thermal) neutron (eq 5.6)
70 E_n      = 14.1;  % [MeV] Neutron energy after fusion (eq 2.17)
71 E_a      = 3.5;   % [MeV] alpha energy after fusion (eq 2.17)
72 E_Li     = 4.8;   % [MeV] Heat produced by breeding Li (under eq 4.31)
73 % Cross section and main free paths
74 sigma_v_avg = 3.0e-22; % [m^3/s] DT fusion cross section @ 15keV (table 5.2)
75 lambda_br   = 0.0031; % [m] Breeding mean free path (under eq 5.7)
76 lambda_sd   = 0.055;  % [m] Mean free path from sigma_sd (eq 5.3)
77
78 % Plasma physics
79 %-----
80 % Parameters for infinity gain at the minimum of p tau_E (eq 4.20)
81 T          = 15.0;  % [keV] Temperature for obtaining min tripple product
82 tripple_min = 8.3;  % [atm s] Min tripple prod to obtain Q=inf @ T=15 keV
83
84 % Natural constants
85 %-----
86 mu_0 = 4.0*pi*1e-7; % Vacuum permeability [T*m/A]
87 e    = 1.602176565e-19; % Elementary charge [C]
88 %#####
89
90
91 % Secondly we convert everything to SI units, so that the variables are
92 % easier to handle

```

```

93 % Again, this is computationally inefficient, but it suffices for our use
94 % Conversion to SI-units
95 %#####
96 % Conversion factors
97 W_per_MW      = 1.0e6;
98 Pa_per_atm    = 1.01325e5;
99 eV_per_keV    = 1.0e3;
100 eV_per_MeV    = 1.0e6;
101 J_per_eV      = e;
102 J_per_keV     = J_per_eV * eV_per_keV;
103 J_per_MeV     = J_per_eV * eV_per_MeV;
104 % Conversions
105 P_E           = P_E * W_per_MW;           % Desired output power
106 P_W           = P_W * W_per_MW;           % Wall Loading limit on first wall
107 E_t           = E_t * J_per_MeV;           % Energy of slow (thermal) neutron
108 E_n           = E_n * J_per_MeV;           % Neutron energy after fusion
109 E_a           = E_a * J_per_MeV;           % alpha energy after fusion
110 E_Li          = E_Li * J_per_MeV;           % Heat produced by breeding Li
111 sigma_max     = sigma_max * Pa_per_atm;    % Max allowable structural stress
112 T             = T * J_per_keV;             % Temperature for minimum p*tau_E
113 tripple_min   = tripple_min * Pa_per_atm;  % The Lawson parameter (p*tau_E)
114 %#####
115
116
117 % Calculate the geometrical factors
118 %-----
119 % Find the breeder thickness
120 b = get_b(lambda_sd, E_n, E_t, lambda_br, n_flux_fraction);
121 % Find the minor plasma radius and the coil thickness
122 [a, c] = get_a_and_c(B_max, mu_0, sigma_max, b);
123 % Find the major radius
124 R_0 = get_R_0(a, eta_t, E_n, E_a, E_Li, P_E, P_W);

```

```

125 % Find the resulting geometrical factors
126 A = R_0/a; % Aspect Ratio
127 A_p = (2.0*pi*a)*(2.0*pi*R_0); % Plasma surface area
128 V_p = (pi*a (2.0))*(2.0*pi*R_0); % Plasma volume
129
130
131 % Calculate the plasma physics parameters
132 %-----
133 % Find the power density in the plasma
134 P_dens = get_P_dens(E_a, E_n, E_Li, P_E, eta_t, V_p);
135 % Find the plasma pressure
136 p = get_p(E_a, E_n, P_dens, T, sigma_v_avg);
137 % Calculate the density from the definition of p under eq 5.36
138 n = p/(2.0*T);
139 % Find the magnetic field strength on the magnetic axis
140 B_0 = get_B_0(R_0,a,b,B_max);
141 % Find the plasma beta on the magnetic axis
142 beta = get_beta(p, B_0, mu_0);
143 % Find the minimum required confinement time from the definition of the
144 % minimum tripple product.
145 % NOTE: A higher confinement time is advantegous, and could in principle
146 % yield a smaller (and cheaper) reactor. However, the effect is not
147 % included in this model
148 tau_E_min = tripple_min/p;
149
150
151 % Calculate the cost
152 % (details about the cost can be found in the function get_a_and_c)
153 %-----
154 % Find the volume of the nuclear island
155 % (the material surrounding the plasma)
156 V_I = get_V_I(R_0,a,b,c);

```



```
157 % Find the reactor volume per power out
158 % In the current model, this is the only non-constant in the expression for
159 % cost per watt
160 V_I_per_P_E = V_I/P_E;
161 C_per_watt = get_C_per_watt(C_F, C_I, V_I_per_P_E);
162 end
163
164
165
166 function      = get_b(
167 %GET_B Calculates b from the need of slowing down and breeding neutrons
168
169 % Thickness of the moderator-breeding region so that 1 - n_flux_fraction
170 % have slowed down and undergone a breeding reaction
171 % [m]
172 % Equation 5.10
173 delta_x = 2.0*lambda_sd*...
174           log( 1.0-(1.0/2.0)*(E_n/E_t) (1.0/2.0)*...
175               (lambda_br/lambda_sd)*log( n_flux_fraction )...
176           );
177
178 % Set b from delta_x
179 % Friedberg argues above equation 5.11 that b should be between 1 and 1.5 m
180 % Therefore a self chose constant is set to 0.38
181 self_chosen_constant = 0.32;
182 b = delta_x + self_chosen_constant;
183 end
184
185
186
187
188 function      = get_a_and_c(
```

```
189 %GET_A_AND_C Calculates a and c
190
191 % c is obtained from requiring that the magnets are so thin that they are
192 % on the limit of the tensile strenght
193 % a is obtained from minimizing the costs
194
195 % xi defined when making the magnetic coil c as thin as possible
196 % Under equation 5.27
197 xi = B_max (2.0) / (4.0*mu_0*sigma_max);
198
199 % a is found from optimization of the cost, where
200 % total cost = fixed cost + nuclear island cost
201 %.....
202 % Fixed cost
203 %.....
204 % K_F = Fixed cost for building, turbines, generators etc (also applies to
205 % fusion, fission, fossil)
206 % Assumption: The fixed cost is proportional to power output:
207 % Equation 5.13
208 % K_F = C_F*P_E;
209 %.....
210 % Nuclear island cost (mainly cost of magnets, blanket and shield)
211 %.....
212 % Assumption: The proportional to reactor volume:
213 % Equation 5.14
214 % K_I = C_I*V_I;
215 % Equation 5.15
216 % V_I = 2.0*pi^(2.0) * R_0 * ( (a+b+c)^(2.0) - a^(2.0) ); % Reactor volume
217 %.....
218 % Cost per watt:
219 %.....
220 % Defined as C_p_watt = (K_F + K_I)/P_E, rewritten to
```

```

221 % C_p_watt = C_F + C_I*(V_I/P_E);
222 % Since the cost per watt contains two constants, we can minimize the
223 % V_I/P_E in order to optimize the cost
224 % Given by equation 5.20 inserted in 5.17
225 % Equation 5.21
226 % V_I_per_P_E = V_I/P_E; % Reactor volume per power out
227 % a is found by setting the derivative of V_I_per_P_E = 0
228 % Equation 5.29
229 a = ((1.0 + xi)/(2.0*xi (1.0/2.0))) * b;
230
231 % Knowing xi, a, and, b, we can calculate c
232 % c found by comparing tensile force and magnetic force working on the coil
233 % Equation 5.27
234 c = 2*xi/(1-xi)*(a+b);
235 end
236
237
238
239 function      = get_R_0(
240 %GET_R_0 Calculate the major radius
241
242 % Divide eq 5.18 (electric power out) by
243 % eq 5.19 (wall loading * area = total neutron production) and solve for R0
244 % Equation 5.20
245 R_0 = (1.0/(4.0*pi (2.0)*eta_t))*(E_n/(E_n + E_a + E_Li))*(P_E/(a*P_W));
246 end
247
248
249
250 function      = get_P_dens(
251 %GET_P_DENS Calculate the power density
252

```

```

253 % The power density is found by the sum of the power from the alphas plus
254 % the power from the neutrons, divided by the plasma volume
255 % Equation 5.35
256 P_dens = (E_a + E_n)/(E_a + E_n + E_Li)*P_E/(eta_t*V_p);
257 end
258
259
260
261 function      = get_B_0(
262 %GET_B_0 Calculte the magnetic field strength on the magnetic axis
263
264 % B_max is found in the edge of the magnet (at R = R_0-a-b)
265 % B0 is the magnetic field at R0
266 % As B propto 1/R. we have that B_0/B_max = (R_0-a-b)/R_0, which leads to
267 % Equation 5.42
268 B_0 = ((R_0-a-b)/R_0)*B_max;
269 end
270
271
272
273 function      = get_beta(
274 %GET_beta Calculte the magnetic field strength on the magnetic axis
275
276 % Plasma beta in the center (kinetical pressure over magnetical pressure):
277 % Equation 5.43
278 beta = p / (B_0^2/(2.0*mu_0));
279 end
280
281
282
283 function      = get_p(
284 %GET_P Calculate the plasma pressure

```

```
285
286 % Found from solving the sum of neutron and alpha power for n, and multiply
287 % the result with T
288 % Equation 5.37
289 p = ( (16.0/(E_a + E_n)) * P_dens ) (1.0/2.0)*...
290      (T (2.0)/sigma_v_avg) (1.0/2.0);
291 end
292
293
294
295 function      = get_V_I(
296 %GET_V_I Calculate the volume of the material surrounding the plasma
297
298 % Equation 5.15
299 V_I = 2.0*pi (2.0) * R_0 * ( (a+b+c) (2.0) - a (2.0) );
300 end
301
302
303
304 function      = get_C_per_watt(
305 %GET_C_PER_WATT Calculates the cost for one watt out from the power plant
306
307 % For details in how the cost is derived, see comments in the function
308 % get_a_and_c
309
310 C_per_watt = C_F + C_I*(V_I_per_P_E);
311 end
```

Appendix B: IterateTokamakDTU

```
1 close;
2 clear;
3
4 titl = [ Desired output power [MW] , Maximum wall load [MW m-2] ,...
5         Magnetic field at the edge of the coil [T] ,...
6         Tensile strenght of the magnetic field coils [atm] ];
7 foldertitl = [ DesiredOutputPower , MaximumWallLoad ,...
8               MagneticFieldAtTheEdgeOfTheCoil ,...
9               TensileStrenghtOfTheMagneticFieldCoils ];
10 l = 5;
11 p1 = [];
12 x = [];
13 mkdir('../MatlabFigures', foldertitl(1))
14
15 for i = 2000:5000
16     [b, c, a, R_0, A, A_p, V_p, P_dens, p,...
17         n, B_0, beta, tau_E_min, C_per_watt] =...
18         tokamakDTU_asign_1(0.01, 1, 2, 1000, 4, 13, 3000, 0.4);
19     q=[b, c, a, R_0, A, A_p, V_p, P_dens, p,...
20         n, B_0, beta, tau_E_min, C_per_watt];
21     p1=cat(1,p1,q);
22     x=cat(1,x,i);
23 end
24
25 T = [ Blanket-shield thickness [m] , Magnet coil thickness [m] ...
26       Minor radius [m] , Major radius [m] , Aspect ratio [] ...
27       Plasma surface [m2] , Plasma volume [m3] , Power density [W m-1] ...
28       Plasma pressure [Pa] , Particle density [m-3] ,...
29       Magnetic field at magnetic axis [T] , Plasma beta in the centre [] ...
30       Min confinement time for satisfaction of (p tau_E)_min [s] ,...
```

```
31     The cost of the powerplant [ ] ];
32 fileT = [ Blanket-shieldThickness , MagnetCoilThickness ...
33     MinorRadius , MajorRadius , AspectRatio ...
34     PlasmaSurface , PlasmaVolume , PowerDensity ...
35     PlasmaPressure , ParticleDensity ,...
36     MagneticFieldAtMagneticAxis , PlasmaBetaInTheCentre ...
37     MinConfinementTime ,...
38     TheCostOfThePowerplant ];
39 for k = 1:14
40     q = figure;
41     y = p1(:,k);
42     CM = jet(14);
43     plot(x, y,'color', CM(k,:));
44     ylabel(T(k));
45     xlabel(titl(1));
46     ytickformat('%.2f');
47     epsfilename = sprintf('%s.eps',fileT(k));
48     foldername = sprintf('../MatlabFigures/%s', foldertitl(1));
49     fullfilename = fullfile(foldername,epsfilename);
50     saveas(q, fullfilename, 'epsc')
51 end
```

Appendix C: interferometer.m

```

1  close all
2  clear all
3
4  mkdir('../MatlabFigures', 'Interferometer'); % Create save directory
5
6  %-----Input Parameters-----%
7  r_p = 0.055; % Reactor port opening [m]
8  w_0 = 0.0275; % Initial Beam Waist [m]
9  r = 0.125; % Minor tokamak radius [m]
10 freq = 60; % Frequency of probe beam [GHz]
11
12 d_0 = 0.20; % Distance between source and first lens
13 d_r = 0.10; % Distance between first lens and reactor wall
14 f_0 = 0.25; % Focal length of first lens
15 f_1 = 0.20; % Focal length of second lens
16 %-----%
17
18 %-----Distances and Lowest Beam Waists Calculations-----%
19 c = 299792458; % The speed of light [m/s]
20 lambda = c / (freq * 109); % Calculates the wavelength [m]
21 d = f_0 + f_1; % Calculates the distance between lenses
22 w_1 = (lambda * f_0) / ...
23     (pi * w_0); % Calculates the beam waist between lenses
24 d_1 = (((d_0 / f_0) - 1) / ((w_02) * pi) / ...
25     (f_0 * lambda) + ((d_0 / f_0) - 1)2) + 1) * ...
26     f_0; % Distance after 1st lens to lowest beam waist
27 w_2 = (f_1 / f_0) * w_0; % Calculates w_2 after 2nd second lens
28 d_2 = d - d_1; % Distance from w_2 to second lens
29 d_3 = f_1 / f_0 * ...
30     (f_0 + f_1 - ...

```



```

31     (f_1 / f_0) * d_0);% Distance to lowest beam waist after 2nd lens
32 %-----%
33
34 %-----Beam Waist Datapoints-----%
35 x_0 = linspace(0, d_0, 1000);% Plotpoints till first lens
36 y_0 = [];
37 for i = 1:1000
38     w = w_0 * ...
39         sqrt(1+((lambda * x_0(i)) / ...
40             (pi * w_0 ^ 2)) ^ 2);% Calculates the beam waist from source
41     y_0 = horzcat(y_0, w);
42 end
43
44 x_1 = linspace(0, d_1, 1000); % Plotpoints from first lens to w_1
45 y_1 = [];
46 for i = 1:1000
47     w = w_1 * ...
48         sqrt(1+((lambda * x_1(i)) / ...
49             (pi * w_1 ^ 2)) ^ 2);% Beam waist between w_1 and the 1st lens
50     y_1 = horzcat(y_1, w);
51 end
52 y_1 = fliplr(y_1); % Flips the y-plot points as the beam waist is declining
53 y = horzcat(y_0, y_1);
54
55 x_2 = linspace(0, d_2, 1000); % Plotpoints from w_1 to second lens
56 y_2 = [];
57 for i = 1:1000
58     w = w_1 * ...
59         sqrt(1+((lambda * x_2(i)) / ...
60             (pi * w_1 ^ 2)) ^ 2);% Beam waist between w_1 and the 2nd lens
61     y_2 = horzcat(y_2, w);
62 end

```

```
63
64 y = horzcat(y, y_2);
65
66 x_3 = linspace(0, d_3, 1000); % Plotpoints from 2nd lens to w_2
67 y_3 = [];
68 for i = 1:1000
69     w = w_2 * ...
70         sqrt(1+((lambda * x_3(i)) / ...
71             (pi * w_2^2))^2); % Evolving beam waist after the 2nd lens to w_2
72     y_3 = horzcat(y_3, w);
73 end
74 y_3 = fliplr(y_3); % Flips the y-plot points as the beam waist is declining
75 y = horzcat(y, y_3);
76
77 for i = 1:1000
78     x_1(i) = x_1(i) + d_0; % Creates x-axis data points
79 end
80 for i = 1:1000
81     x_2(i) = x_2(i) + d_0 + d_1; % Creates x-axis data points
82 end
83 for i = 1:1000
84     x_3(i) = x_3(i) + d_0 + d_1 + d_2; % Creates x-axis data points
85 end
86 x = horzcat(x_0, x_1, x_2, x_3);
87
88 Opy = -y; % Flip beam waist to plot 'Beam Waist -'
89 %-----%
90
91 %-----Beam Waist Propagation Plot-----%
92 l = figure; % Creates figure
93 hold on
94 axis equal
```

```

95 p1 = plot(x, y); % Plots Beam Waist+
96 p2 = plot(x, 0py, 'Color', 'red'); % Plots Beam Waist-
97 %p3 = xline(d_0, '--');
98 %xline(d_0+d_1+d_2, '--');
99 axPos = get(gca, 'Position'); % Get normalised axis coordinates
100 xMinMax = xlim; % Get normalised axis coordinates
101 yMinMax = ylim; % Get normalised axis coordinates
102 zAnn = axPos(1) + ((0 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
103     * axPos(3); % Defines points relative to axis in normalised coordinates
104 d0Ann = axPos(1) + ((d_0 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
105     * axPos(3); % Defines points relative to axis in normalised coordinates
106 d1Ann = axPos(1) + ((d_0 + d_1 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
107     * axPos(3); % Defines points relative to axis in normalised coordinates
108 d2Ann = axPos(1) + ((d_0 + d_1 + d_2 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
109     * axPos(3); % Defines points relative to axis in normalised coordinates
110 d3Ann = axPos(1) + ((d_0 + d_1 + d_2 + d_3 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
111     * axPos(3); % Defines points relative to axis in normalised coordinates
112 yAnn = axPos(2) + ((0 - yMinMax(1)) / (yMinMax(2) - yMinMax(1))) ...
113     * axPos(4); % Defines points relative to axis in normalised coordinates
114 annotation('doublearrow', ...
115     [zAnn, d0Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_0
116 annotation('doublearrow', ...
117     [d0Ann, d1Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_1
118 annotation('doublearrow', ...
119     [d1Ann, d2Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_2
120 annotation('doublearrow', ...
121     [d2Ann, d3Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_3
122 annotation('ellipse', ...
123     [d0Ann - 0.01, yAnn - y_0(1000) * 1.5, 0.02, y_0(1000) * 3], ...
124     'FaceColor', 'cyan'); % Draws 1st lens
125 annotation('ellipse', ...
126     [d2Ann - 0.01, yAnn - y_0(1000) * 1.5, 0.02, y_0(1000) * 3], ...

```

```

127     'FaceColor', 'cyan');% Draws 2nd lens
128 text(d_0/4, -0.22, sprintf('d_0 = %0.2f', d_0)) % Distance annotation
129 text(d_0+(d_1 / 4), -0.22, ...
130     sprintf('d_1 = %0.2f', d_1))% Distance annotation
131 text(d_0+d_1+(d_2 / 4), -0.22, ...
132     sprintf('d_2 = %0.2f', d_2))% Distance annotation
133 text(d_0+d_1+d_2+(d_3 / 4), -0.22, ...
134     sprintf('d_3 = %0.2f', d_3))% Distance annotation
135 text(d_0-0.06, 0.06, '1^{st} Lens') % Lens annotation
136 text(d_0-0.06, -0.06, sprintf('f_0 = %0.2f', f_0)) % Lens annotation
137 text(d_0+d_1+d_2-0.06, 0.06, '2^{nd} Lens') % Lens annotation
138 text(d_0+d_1+d_2-0.06, -0.06, ...
139     sprintf('f_1 = %0.2f', f_1))% Lens annotation
140 w1x = (d_0 + d_1); % w_1 coordinate
141 w1x = repelem(w1x, 100); % w_1 x-coordinate array
142 w1y = linspace(0, w_1); % w_1 y-coordinate array
143 p4 = plot(w1x, w1y); % Plots w_1
144 yline(0, '-'); % Plots optical axis
145 xlabel('Distance from source [m]'); % x-axis label
146 ylabel('Beam Waist [m]'); % y-axis label
147 title('Beam Waist In A Gaussian Beam Interferometer'); % Figure title
148
149 topstart = 2 * asin(r_p/(2 * r)) / 2; % Calculates reactor plot coordinates
150 topend = (2 * pi - 2 * topstart) / 2; % Calculates reactor plot coordinates
151 bottomstart = topend + topstart * 2; % Calculates reactor plot coordinates
152 bottomend = 2 * pi - topstart; % Calculates reactor plot coordinates
153
154 top = linspace(topstart, ...
155     topend, 100);% Creates 100 datapoints for the top half reactor cutout
156 x_t = d_0 + d_r + r + r * cos(top); % x-parameter of circle
157 y_t = r * sin(top); % y-parameter of circle
158 bottom = linspace(bottomstart, ...

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```
159     bottomend, 100);% Creates 100 datapoints for the bottom half reactor
160 x_b = d_0 + d_r + r + r * cos(bottom); % x-parameter of circle
161 y_b = r * sin(bottom); % y-parameter of circle
162 p5 = plot(x_t, y_t, 'color', ...
163     [0.911, 0.4100, 0.1700]);% Plot top half reactor
164 plot(x_b, y_b, 'color', ...
165     [0.911, 0.4100, 0.1700]);% Plot bottom half reactor
166 lgd = legend([p1, p2, p4, p5], ...
167     {'Beam Waist +', 'Beam Waist -', 'w_1', 'Reactor'});% Figure legend
168 legend('boxoff')
169 legend('Location', 'northwest')
170 lgd.NumColumns = 2;
171 hold off
172 %-----%
173
174 %-----Saving figure as Encapsulated Postscript-----%
175 epsfilename = 'Interferometer.eps'; % Savename for the figure
176 foldername = sprintf('../MatlabFigures/Interferometer'); % Folder path
177 fullfilename = fullfile(foldername, epsfilename); % Filename path
178 saveas(1, fullfilename, 'eps') % Save the figure as eps
179 %-----%
180
181 %-----Print Outputs-----%
182 w_1
183 w_2
184 d_1
185 d_2
186 d_3
187 %-----%
```