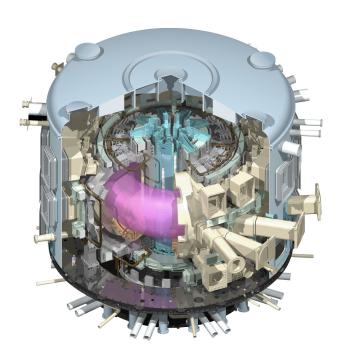
10401

Fusion Energy and Plasma Physics

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Abstract: Plasma fusion for energy production is a growing scientific field with interests all over the globe as clean and sustainable energy as well as growing energy demands needs to be addressed. In the course 10401: Fusion energy and plasma physics we deal with some of the fundamental engineering aspects of a commercial fusion energy power plant, as well as the research towards this goal. In this paper we first address a simple model for such a plant and how the model can be improved upon. Secondly we investigate how to diagnose plasma density with simple interferometry in the DTU tokamak reactor. Lastly we made measurements in the DTU fusor, and investigated some energy production aspects with such a device.



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Course 10401 Fusion Energy and Plasma Physics

 $\begin{array}{c} \rm January~24^{th} \\ 2019 \end{array}$

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A. Intro

In recent years a large and quickly growing collaboration between plasma physicists and engineers have materialised into one of the most ambitious energy producing projects ever seen. The proof-of-concept plasma fusion tokamak reactor ITER¹ in Cadarache is currently taking shape in order to address the issue of growing energy demands and climate changes.

The mission is simple: Prove that plasma fusion is a viable source of electricity.

Whilst not being the most surmountable task, many researchers and institutions have gathered from across the world, including the Department of Physics at DTU.

In this paper, three assignments are solved as part of the course "10401 Fusion Energy and Fusion Plasma Physics". Some key aspects of fusion plasma fuelled reactors are addressed and discussed in the assignments.

I. A SIMPLE REACTOR MODEL

A. Freidberg's simple reactor model

In the 5th chapter of the textbook by Freidberg², he makes a simple model for designing a fusion reactor power plant. The model uses simple geometric and electromagnetic assumptions with little involvement of plasma physics. The variables put into the model are shown in Table I.

| Symbol | Quantity |
|--------------------------|---|
| $n_{\rm flux\ fraction}$ | n flux in breeder end/n flux in breeder start [1] |
| C_F | Fixed cost proportionality constant [\$] |
| C_I | Nuclear island cost proportionality constant $\left[\$\cdot\mathbf{W}\cdot\mathbf{m}^{-3}\right]$ |
| P_E | Desired output power [MW] |
| P_W | Maximum wall load $[MW \cdot m^{-2}]$ |
| B_{\max} | Magnetic field at the edge of the coil [T] |
| $\sigma_{ m max}$ | Tensile strength of the magnetic field coils [atm] |
| η_t | Energy conversion efficiency [1] |

Table I: Variables in the Freidberg's model

Table II shows the output quantities from the model.

| Symbol | Quantity | Obtained values |
|------------------|---|---|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | $0.799~\mathrm{m}$ |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 4.96 m |
| A | Aspect ratio | 2.4670 |
| A_p | Plasma surface | 393 m^2 |
| V_p | Plasma volume | 395 m^3 |
| $P_{\rm dens}$ | Power density | $4.97\times10^6~\mathrm{W}\cdot\mathrm{m}^{-1}$ |
| p | Plasma pressure | $7.37 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.53 \times 10^{20}~{\rm m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 4.57 T |
| β | Normalised plasma pressure | 8.85% |
| $	au_{E_{\min}}$ | Min confinement time for $(p \times \tau_E)_{\min}$ | 1.14 s |

Table II: Output quantities in the model in Freidberg's along with the obtained values when inserting the parameters from Eq. (1)

This model has been implemented in a Matlab script provided for the course. The script

is shown included in Appendix A. As an example, the model is run with the following parameters:

$$n_{\text{flux fraction}} = 0.01$$
 $P_E = 1000 \text{ MW}$
$$P_W = 4 \text{ MW} \cdot \text{m}^{-2} \quad B_{\text{max}} = 13 \text{ T}$$
 (1)
$$\sigma_{\text{max}} = 3000 \text{ atm} \qquad \eta_t = 0.4$$

Note that C_F and C_I has been omitted as these serve no purpose for this assignment. It is not of interest how expensive the plant will be. Rather the geometries and physical quantities are of interest. The results from the model is given in Table II.

B. Model sensitivity

At this point Freidberg has provided a model that produce some reasonable results for a power plant. It could be interesting to see how this model behaves when some vital parameters are changed. In the last section the model used the parameters shown in Eq. (1). In Eq. (2) are listed some parameter ranges.

$$P_E : 500 - 1000 \text{ MW}$$
 $P_W : 0 - 10 \text{ MW} \cdot \text{m}^{-2}$ $B_{\text{max}} : 0 - 20 \text{ T}$ $\sigma_{\text{max}} : 2000 - 5000 \text{ atm}$ (2)

Appendix B includes Matlab code that does the following:

- 1. Take a variable range from Eq. (2).
- 2. Set all other input parameters as in Eq. (1).
- 3. Plot the model outputs as functions of the variable range.
- 4. Repeat with another range from Eq. (2).

The iteration showed some interesting breakdowns in the model. When varying the desired power output there was a breakdown in magnetic field strength at the magnetic axis as well as in the normalised plasma pressure. This is shown in Fig. 1. In this case, limits for what is physically possible broke and in these cases the model is unusable. The full gallery of model output is found in Appendix C.

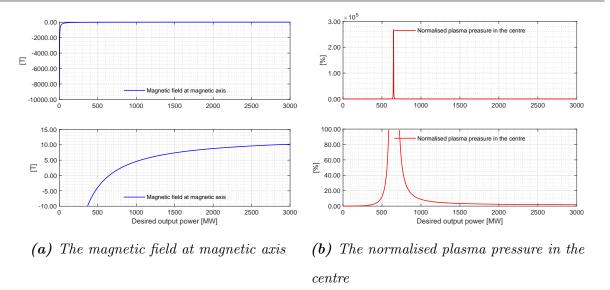


Figure 1: Model breakdown when iterating over desired power output.

C. Elliptic Cross section

Freidberg's model assume a circular cross section of the plasma. In reality this is not the case. We will now make a more realistic, yet still approximate reactor for an elliptic plasma cross section. In describing the geometry one refers to the elongation ratio:

$$\kappa = \frac{a_{\text{max}}}{a_{\text{min}}} \tag{3}$$

With a_{max} the major radius and a_{min} the minor radius of the ellipse. This parameter ensures a true elliptic cross section as defined by the equation,

$$\frac{x^2}{a_{\text{max}}} + \frac{y^2}{a_{\text{min}}} = 1 \tag{4}$$

which can be parameterised as

$$\begin{bmatrix} x_1 \\ y_1 \end{bmatrix} = \begin{bmatrix} a_{\min} \cos \phi \\ \kappa a_{\min} \sin \phi \end{bmatrix}$$
 (5)

Meanwhile the blanket must be implemented as an ellipse or swelled ellipse. The true ellipse results in a thickness difference throughout the blanket, while the second model results in a blanket of equal thickness throughout. To this, the choice of implementing the blanket as a true ellipse has been made, since it simplifies derivations a bit. Note however, that keeping a constant thickness is the preferable option as it will reduce the engineering

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volume and hence the cost of the machine.

The outer layer is parameterised

$$\begin{bmatrix} x_2 \\ y_2 \end{bmatrix} = \begin{bmatrix} (b + a_{\min})\cos\phi \\ \kappa(b + a_{\min})\sin\phi \end{bmatrix}$$
 (6)

with b the blanket thickness at the minor ellipse axis. Choosing for now, $a_{\min} = 2$, $\kappa = 2$ and b = 1.2, Eq. (5) and Eq. (6) are plotted on Figure Fig. 2 along with the variation in thickness of the blanket.

Given Eq. (5) and Eq. (6), the engineering volume can easily be derived if $c\cos(\phi)$ and $\kappa c\sin(\phi)$ is added to the x and y-direction in Eq. (6) respectively, where c is the minimum thickness of the magnetic coils that provide the toroidal field.

The cross sectional area of an ellipse is $A_{\rm e}$ = $\pi a_{\min} a_{\max}$ so the engineered volume becomes

$$V_{\rm I} = 2 \pi R_0 \left(A_{\rm e, outer} - A_{\rm e, inner} \right)$$
$$= 2 \pi^2 R_0 \left(\left(a_{\rm min} + b + c \right)^2 - a_{\rm min}^2 \right) \kappa \qquad (7)$$

and the plasma volume is similarly calculated as $V_{\rm P} = 2 \pi^2 R_0 \kappa a_{\rm min}^2$. The plasma surface area is a bit more tricky, but it can be approximated as

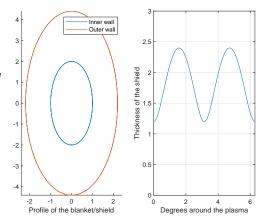


Figure 2: The profile of the blanket-and-shield and the thickness as a function of the angle around origin, ϕ .

$$S_{\rm p} = 2 \pi R_0 \pi \left(3 \left(a_{\rm min} + \kappa a_{\rm min} \right) - \sqrt{\left(3 a_{\rm min} + \kappa a_{\rm min} \right) \left(a_{\rm min} + 3 \kappa a_{\rm min} \right)} \right) \tag{8}$$

Using the same arguments as in the book, the B-field in the centre is surprisingly unchanged when going to the elliptical model. Now c is also approximated, or rather overestimated using a slight change to Eq. (5.24) in the textbook. Since the force grows with a_{\min} , inserting κa_{\min} instead yields an overestimation on the vertical force on the magnet. The tensile forces are the same, so the force balance leads to

$$c = \frac{2\xi}{1-\xi}(\kappa a + b) \tag{9}$$

with $\xi = B_{sic}^2/4\,\mu_0\,\sigma_{\rm max}$. These new equations are inserted in the code. The results are displayed in III. The plasma volume and surface area is of course increased as the plasma was made higher. This of course also results in a decreased power density. Overall, parameters such as B_0 , β and $\tau_{\rm E_{min}}$ while changing a bit, they were not changed significantly.

| Symbol | Quantity | Obtained values |
|------------------|---|---|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 4.96 m |
| A | Aspect ratio | 2.4670 |
| A_p | Plasma surface | 609 m^2 |
| V_p | Plasma volume | 793 m^3 |
| $P_{\rm dens}$ | Power density | $2.48\times10^6~\mathrm{W}\cdot\mathrm{m}^{-1}$ |
| p | Plasma pressure | $5.20 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.08 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 4.60 T |
| β | Normalised plasma pressure | 6.17% |
| $	au_{E_{\min}}$ | Min confinement time for $(p \times \tau_E)_{\min}$ | $1.62 \mathrm{\ s}$ |

Table III:

Output quantities from the elliptical model

D. Main parameters for DEMO

Setting $P_{\rm E}=2000$ in the elliptical model yields the output parameters seen in Table IV. Since R_0 is directly proportional to the electric power, it increases linearly. The other geometric output parameters regarding areas and volumes also increase as a result. β has decreased a lot, so the plasma is not confined effectively in DEMO.

E. Designs for DEMO

With $P_{\rm E}$, $\kappa=2$ and $A=R_0/a_{\rm min}=3 \Leftrightarrow R_0=3\,a_{\rm min}$. This is implemented in the code and the results are displayed in Table V. β has increased a bit but only to 4.55%. R_0 has been forced down, so the plasma volume etc. has decreased as well. Overall it seems like a smaller R_0 while keeping a_{min} fixed is an improvement. Or in other words, A=3 is more desirable than $A\approx 5$.

| Symbo | l Quantity | Obtained values |
|------------------|---|---|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | $9.95~\mathrm{m}$ |
| A | Aspect ratio | 4.9512 |
| A_p | Plasma surface | $1.21\times10^3~\mathrm{m}^2$ |
| V_p | Plasma volume | $1.59\times10^3~\mathrm{m}^3$ |
| $P_{\rm dens}$ | Power density | $2.48\times10^6~\mathrm{W}\cdot\mathrm{m}^{-1}$ |
| p | Plasma pressure | $5.20 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.08 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 8.80 T |
| β | Normalised plasma pressure | 1.69% |
| $	au_{E_{\min}}$ | Min confinement time for $(p \times \tau_E)_{\min}$ | $1.62 \mathrm{\ s}$ |

Table IV: Output quantities for DEMO using the elliptical model with $P_{\rm E}=2{\rm GW}$

F. A and κ as free parameters

Designing the tokamak with κ and A as free parameters has led us to try and maximise profitability from V_P/A_P and β . Profitability in this context means that increasing the size of the tokamak leads to an increase in these parameters. However, there is a point when the change vs increase in size becomes constant. This means that we do not profit from increasing the size any longer.

 $V_{\rm P}$ and $A_{\rm P}$ were calculated earlier so

$$\frac{V_{\rm P}}{A_{\rm P}} = \frac{2\pi R_0 \kappa a_{\rm min}^2}{2\pi R_0 \pi (3 (a + \kappa a_{\rm min}) - \sqrt{(3 a_{\rm min} + \kappa a_{\rm min}) (a + 3 \kappa a_{\rm min})})}$$

$$= \frac{\kappa a_{\rm min}}{\pi (3 + 3 \kappa - \sqrt{3 + \kappa} \sqrt{1 + 3 \kappa})} \tag{10}$$

The expression scales linearly with a_{min} so we set it equal to 1 m since it has no effect on the choice of κ . Differentiating with respect to κ and plotting is done, with the results shown in Fig. 3a. Considering the figure, $\kappa = 2.5$ is chosen as the change is close enough to zero given this value.

Now work will be done towards choosing a value for A. First, for geometric reasons, a

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| Symbol | Quantity | Obtained values |
|------------------|---|---|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | $6.03~\mathrm{m}$ |
| A | Aspect ratio | 3 |
| A_p | Plasma surface | 738 m^2 |
| V_p | Plasma volume | $962~\mathrm{m}^3$ |
| $P_{\rm dens}$ | Power density | $4.09\times10^6~\mathrm{W}{\cdot}\mathrm{m}^{-1}$ |
| p | Plasma pressure | $6.68 \times 10^5 \text{ Pa}$ |
| n | Particle density | $1.39 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | 6.07 T |
| β | Normalised plasma pressure | 4.55% |
| $	au_{E_{\min}}$ | Min confinement time for $(p \times \tau_E)_{\min}$ | 1.26 s |

Table V: Output quantities for DEMO using the elliptical model with $P_E = 2$, $\kappa = 2$ and A = 3.

minimum R_0 is calculated. It is simply $R_0 = a_{\min} + b + c$ where a_{\min} is to be determined, b = 1.2m and $c = \frac{2\xi}{1-\xi}(\kappa a_{\min} + b)$. Meanwhile A is chosen to optimise β . Inserting R_0 into B_0 in the textbook yields

$$B_0 = \frac{2\xi (\kappa a_{\min} + b) B_{max}}{((2\kappa - 1) a_{\min} + a + b)} = \frac{178.75 a_{\min} + 85.8}{55.5 + 36 a_{\min}}$$
(11)

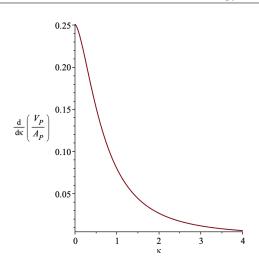
Where units has been disregarded and $\xi = 0.11$, b = 1.2, $\kappa = 2.5$ and $B_{\text{max}} = 13$ has been inserted. Meanwhile, inserting the textbook's expression for P_{dens} into the expression for p and inserting the input parameters yields

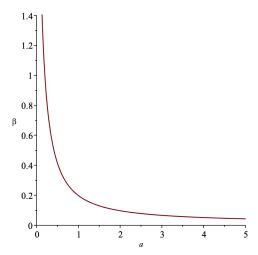
$$p = 1.04 \times 10^6 \sqrt{\frac{1}{\kappa \, a_{\min}}} \tag{12}$$

Thus β becomes

$$\beta = \frac{2148 \left(a_{\min} + 1.542 \right)^2}{\sqrt{a_{\min}} \left(178.8 \, a_{\min} + 85.8 \right)^2} \tag{13}$$

This function is plotted in Fig. 3b, and for $\beta = 10\%$ a = 1.94 m) is achieved. Therefore $(R_0 = 1.94 \text{ m} + 1.20 \text{ m} + 2 \cdot 0.11/(1 - 0.11) \cdot 2.5 \cdot 1.94 \text{ m} + 1.20 \text{ m} = 4.63 \text{ m})$ which means A = 4.63 m/1.94 m = 2.39 m





- (a) The change in the ratio between plasma volume per plasma surface area.
- (b) The normalised plasma pressure as a function of the minor radius.

Figure 3

| Symbol | Quantity | Obtained values |
|------------------|---|---|
| b | Blanket-and-shield thickness | 1.20 m |
| c | Magnet coil thickness | 1.30 m |
| a | Minor radius | 2.01 m |
| R_0 | Major radius | 4.63 m |
| A | Aspect ratio | 2.390 |
| A_p | Plasma surface | 630 m^2 |
| V_p | Plasma volume | 414 m^3 |
| $P_{\rm dens}$ | Power density | $9.49\times10^6~\mathrm{W}\cdot\mathrm{m}^{-1}$ |
| p | Plasma pressure | $1.02 \times 10^5 \text{ Pa}$ |
| n | Particle density | $2.12 \times 10^{20} \text{ m}^{-3}$ |
| B_0 | Magnetic field at magnetic axis | -3.09 T |
| β | Normalised plasma pressure | 26.9% |
| $	au_{E_{\min}}$ | Min confinement time for $(p \times \tau_E)_{\min}$ | $1.26 \mathrm{\ s}$ |

Table VI: Output quantities for the elliptical model after β and A has been optimised

DIAGNOSTICS VIA INTERFEROMETRY II.

When operating a fusion reactor a continuous process of diagnostics is necessary in order to optimise the plasma for the fusion process. One of the active diagnostic methods are interferometry. The goal here for this part of the paper is to measure the plasma electron density in the Danish Tokamak Undertaking reactor.

Cut-off and Source frequency

Using a interferometer one can measure the electron density n_e of the plasma. The refractive index of electromagnetic waves depend on the electron density and plasma frequency ω_p proportionally:

$$\omega_p^2 \propto n_e \tag{14}$$

For O-mode plasma waves, the refractive index is:

$$N_{\rm O} = \sqrt{1 - \frac{\omega_p^2}{\omega^2}} \tag{15}$$

with ω being the probing wave frequency. The plasma will reflect the beam if the plasma frequency is larger than the beam frequency so

$$\omega > \omega_p = \sqrt{n_e \frac{e^2}{\epsilon_0 m_{e0}}} \tag{16}$$

So for a given frequency, the plasma must not exceed a critical cut off electron density:

$$n_e < n_c = \omega^2 \frac{\epsilon_0 \cdot m_{e0}}{e^2} \tag{17}$$

which gives

$$N_{\rm O} = \sqrt{1 - \frac{n_e}{n_c}} \tag{18}$$

With a probing frequency much higher than the plasma frequency and the critical density much higher than the electron density Eq. (18) can be approximated by:

$$N_{\rm O} = \sqrt{1 - \frac{n_e}{n_c}} \approx 1 - \frac{1}{2} \frac{n_e}{n_c} - \frac{\omega_p^2}{2\omega^2}$$
 (19)

With sufficient accuracy, the linear dependence of the O-mode refractive index on the electron density is obtained if the normalised quantities obey:

$$\frac{n_e}{n_c} \le 0.4 \quad \frac{\omega_p}{\omega} \le 0.6 \tag{20}$$

We must calculate the phase shift as one beam travels in vacuum by the length L_V and one wave travels in the plasma by the length L_P . The phase shift in terms of 2π is equal to the optical difference divided by the wavelength. With the refractive index in vacuum, $N_V = 1$, this yields:

$$\frac{\Phi}{2\pi} = \frac{\Delta L_{opt}}{\lambda} = \frac{\int_{x_1}^{x_2} (N_V - N_O(x')) dx'}{\lambda} \approx \frac{1}{2\lambda n_c} \int_0^x n_e(x') dx'$$

$$= 4.48 \times 10^{-16} \left(\frac{\lambda}{m}\right) \int_0^x \left(\frac{n_e(x')}{m^{-3}}\right) \left(\frac{dx'}{m}\right) \tag{21}$$

Assuming a Gaussian distribution, the electron density at $\pm \infty$ is approximately equal to the densities just inside the reactor walls. Therefore

$$\int_{-\infty}^{\infty} n_e \exp\left(-\frac{(y-b)^2}{2c^2}\right) dy \approx n_e \ c \ \sqrt{2\pi}$$
 (22)

With the density at the centre given as:

$$10^{16} \text{ m}^{-3} \le n_e \le 10^{18} \text{ m}^{-3},$$
 (23)

The c in Eq. (22) is the width of the Gaussian distribution and must fit inside the reactor. The DTU tokamak has a minor diameter of 0.250 m. Thus

$$\frac{\Phi}{2\pi} \approx 4.48 \times 10^{-16} \left(\frac{\lambda}{\text{m}}\right) n_e 0.250 \text{ m} \sqrt{2\pi} = 1.12 \times 10^{-16} n_e \left(\frac{\sqrt{2\pi}c}{\omega \text{m}}\right) \\
= 8.416 \times 10^{-8} \left(\frac{n_e}{\omega \text{S}}\right) \tag{24}$$

Remembering Eq. (17)

$$\omega^2 \frac{\epsilon_0 \ m_{e0}}{e^2} = \omega^2 \frac{8.85 \times 10^{-12} \ \text{F} \cdot \text{m}^{-1} \ 9.11 \times 10^{-31} \ \text{kg}}{1.60 \times 10^{-19} \ \text{C}}$$
(25)

$$n_e < 0.000314\omega^2 (26)$$

Where any units has been disregarded. We want the largest possible phase shift which means that the lower the frequency the better. However cutoff must first be taken into account. Since the cutoff is given by Eq. (26) and since we want to measure densities up to 10^{18} m⁻³ the minimum frequency of the wave is

$$\frac{\omega}{2\pi} > \frac{\sqrt{\frac{10^{18} \text{ m}^{-3}}{0.000314}}}{2\pi}$$

$$\downarrow \downarrow$$
(27)

$$f \approx 9 \text{ GHz}$$
 (28)

Given the available emitters, the best emitter is therefore the one with f = 60 GHz.

В. Beam Phase shifts

The goal of the interferometer is to find the phase shift between the microwave beam in vacuum and in plasma. Our suggestion is a setup involving a interferometer emitting a beam through the centre of the reactor. The first measurement would be through vacuum to find the source phase. Afterwards phase measurements can be conducted with an active plasma in the reactor. So by first measuring the phase of the probing beam in vacuum, one can simply measure the phase shift.

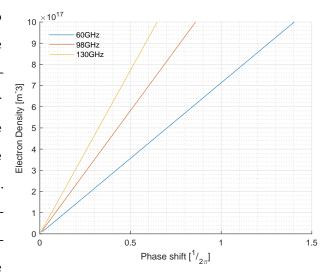


Figure 4: Electron densities for different wavelengths and phase shifts

We know from Eqs. (21), (22) and (24) that:

$$\frac{\Phi}{2\pi} = 8.416 \times 10^{-8} \left(\frac{n_e}{\omega_S}\right) \tag{29}$$

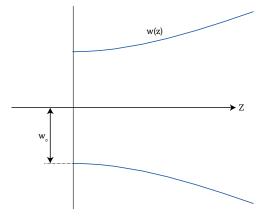
So for different average electron densities through the plasma, one can plot the resulting phase shifts. Using the code in Appendix E the plot in Fig. 4 is generated. The measured phase shift is then correlated to an electron density using Fig. 4.

Evolving beam width

In our case we want to use a Gaussian microwave. Such beam propagates spatially as shown in Fig. 5. w_0 is the initial beam waist determined by the source, and w(z) is the function describing the waist. This equation is:

$$w(z) = w_0(z)\sqrt{1 + \left(\frac{\lambda z}{\pi w_0^2}\right)^2}$$
 (30)

From this equation one can track the spatial propa- Figure 5: Sketch of Gaussian beam gation of the wave. In this project three sources are propagation with indication of w_0 given. The initial beam waist is set to $w_0 = 0.0275 \,\mathrm{m}$ and w(z).



corresponding to half a reactor port. With

$$\frac{\lambda z}{\pi w_0^2} = \frac{9.543 \times 10^7 z}{w_0^2 f} \tag{31}$$

, and f the frequency of the emitter, the sources' beam waists are given as such:

60 GHz:
$$w(z) = 0.0275\sqrt{\left(1 + \frac{9.543 \times 10^7 z}{0.0275^2 60 \times 10^9}\right)^2}$$
 (32)

98 GHz:
$$w(z) = 0.0275\sqrt{\left(1 + \frac{9.543 \times 10^7 z}{0.0275^2 \ 98 \times 10^9}\right)^2}$$
 (33)

130 GHz:
$$w(z) = 0.0275\sqrt{\left(1 + \frac{9.543 \times 10^7 z}{0.0275^2 \ 130 \times 10^9}\right)^2}$$
 (34)

For the three given sources in this project, the beam waist has been plotted on Fig. 6

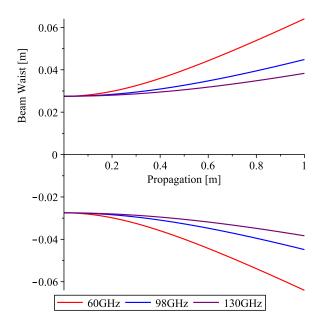


Figure 6: Beam Waist for the three microwave sources. The functions are Eqs. (32), (33) and (34).

It is undesirable for some of the beam to not reach the output port and instead propagate into the reactor wall, as this will result in a lesser signal strength. Therefore it can be necessary to deploy a Gaussian telescope.

D. Gaussian beam telescope interferometer

In order to control the beam waist, one can use a Gaussian beam telescope arrangement around the reactor. A lens is placed between the source and the reactor input port and R. K. F. Wiuff

again between the output port and the receiver. From chapter 5 in "Fusion Plasma Diagnostics with mm-Waves" the authors explains how such an arrangement can be obtained. Starting with the focal lengths of the lenses,

$$d = f_0 + f_1 (35)$$

, where f_0 and f_1 are focal lengths, and d are the distance between the lenses. The resulting narrowest beam waist after the second lens are given as:

$$w_2 = \frac{f_1}{f_0} w_0 \tag{36}$$

The use of two lenses make the transformation wavelength independent (Eq 5.118)³, thus the only interaction with the wavelength of the probing beam will be that of the plasma itself. The distance to the minimum waist after the second lens is given as:

$$d_3 = \frac{f_1}{f_0} \left(f_0 + f_1 - \frac{f_1}{f_0} d_0 \right) \tag{37}$$

The waist in between the lenses is given as:

$$w_1 = \frac{\lambda f_0}{\pi w_0} \tag{38}$$

And the distance from the first lens to this waist is:

$$d_1 = \left(\frac{\frac{d_0}{f_0} - 1}{\frac{w_0^2 \pi}{f_0 \lambda} + \left(\frac{d_0}{f_0} - 1\right)^2} + 1\right) f_0 \tag{39}$$

Thus the distance from w_1 to the second lens is:

$$d_2 = d - d_1 \tag{40}$$

Knowing these variables and utilising Eq. (30) we can model a complete setup. Using the Matlab code in Appendix D, the following parameters are used:

$$r_p = 0.0550 \text{ m}$$
 $r = 0.125 \text{ m}$ $w_0 = 0.0275 \text{ m}$ $freq = 60 \text{ GHz}$
 $d_0 = 0.200 \text{ m}$ $d_r = 0.100 \text{ m}$ $f_0 = 0.250 \text{ m}$ 0.200 m (41)

With r_p being the tokamak port radius, r the tokamak minor radius and d_r the distance between the first lens and the reactor wall. In the case of the Danish Tokamak Undertaking, two ports opposing each other is ideal for use with interferometry. In this example, the port radius, r_p , and the minor radius r are based on the ST-25 in the basement of building 309 at DTU. The script gave the results:

$$w_1 = 0.0145 \text{ m}$$
 $w_2 = 0.0220 \text{ m}$ $d_1 = 0.224 \text{ m}$ $d_2 = 0.226 \text{ m}$ $d_3 = 0.232 \text{ m}$ (42)

Beam Waist In A Gaussian Beam Interferometer

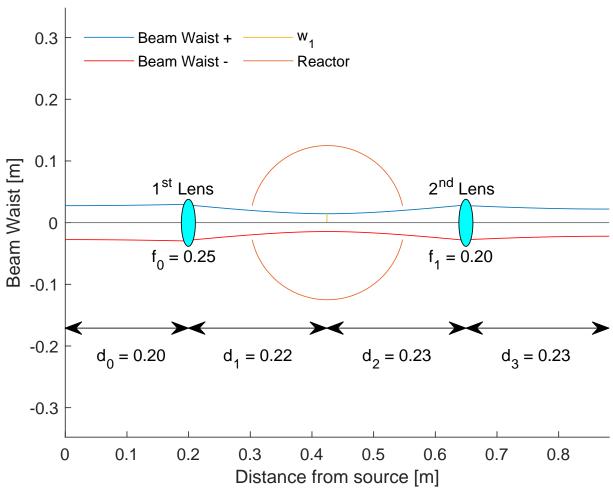


Figure 7: Gaussian beam telescope interferometer setup with input parameters shown in Eq. (41) and output parameters shown in Eq. (42)

Furthermore the code plots a sketch of the desired interferometer setup. The sketch can be seen in Fig. 7.

Lastly it should be mentioned that the beam waist confinement does not matter if the wave is refracted into the side of the reactor. As the plasma density varies from the centre and out, the plasma itself act as a variable lens with variable refractive indices. If the beam is emitted straight through the centre, the refractive indices will only shorten and lengthen the wavelength back to normal, however if the beam is emitted off centre, it will be refracted away from the centre. In such a setup, further calculations need to be conducted to determine variation in signal strength, phase and wavelength. The two described setups are depicted on Fig. 8.

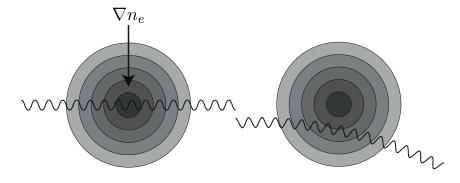


Figure 8: Refraction of the probing beam at centre (left) and off centre (right).

III. FUSOR EXERCISE

Studying the Inertial electrostatic confinement fusor at DTU. Measurements of neutron counts and the spectral line width are made as a function of the voltage and current. To this, the emission spectrum of the gas are also measured.

A. Plasma light emission and spectral line

When doing spectroscopy on a plasma of an unknown gas. Optical dispersion splits up the spectrum of light into lines which are then recorded using a detector. This detector measures the frequency/wavelength of the light and the intensity of the light. Thus a plot with the wavelength along the x-axis vs the intensity along the y-axis are produced. For our recordings a typical spectrum looked like that of Fig. 9.

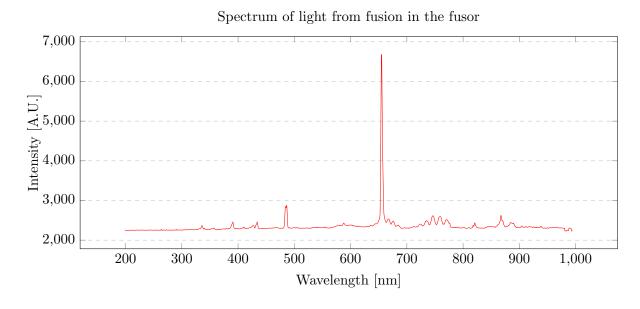


Figure 9: Spectrum of light from fusion in the fusor

Each peak correspond with a constituent gas in the fusor. The peaks present on the spectrum are subject to broadening effects. Considering the Doppler effect, each photon's frequency will be shifted since the particles (which are the emitters) are moving at fast speeds (the Doppler shift increases with speed). Therefore if each particle where moving in the same direction, the entire intensity peak would be shifted. But since the particles are moving more or less isotropic around the centre of the device, the peaks are not shifted but rather broadened around the normal emission wavelength. To this, it is also noted that the Doppler broadening increases if particles are moving faster.

Considering Fig. 9, a spectrum is shown with central wavelengths around 656 nm, 486 nm and 433 nm which correspond to accepted values of hydrogen light emission wavelengths⁴. Meanwhile the spectral lines of Deuterium only differs by a factor of 1.000272⁵, which will not be detected using our methods. There are other peaks but those peaks are due to noise from impurities etc.

Since the speed of the particles increases with the voltage we expect the line broadening to do the same since $\sigma = \lambda_0/c v_{1D}$. While there seems to be enormous uncertainties on the hydrogen measurements, Fig. 10 shows a tendency to increase for both hydrogen and deuterium. Disregarding outliers, the hydrogen also seems to have a wider spectral line than deuterium which makes sense, due to the mass difference between the species. Meanwhile the uncertainties seen might be due to differences in pressure, which leads to differences in kinetic energy lost per time. Other uncertainties are most likely also present. For the width of a spectral line, it is known that:

$$\sigma = \Delta \lambda = \frac{\lambda_0}{c} v_{1D} \tag{43}$$

So for the obtained widths, the velocities can be estimated via Eq. (43). Once these points are obtained a curve is fitted to it. The fit is assumed to be linear, as velocity is proportional to voltage applied. The kinetic energies are also estimated via:

$$KE = \frac{1}{2}mv^2 \tag{44}$$

These points are also estimated and plotted along with a fit. The fit is assumed to be some constant, times the square root of the voltage as isolated from Eq. (44). This is done for both hydrogen and deuterium. The plot can be seen in Fig. 11.

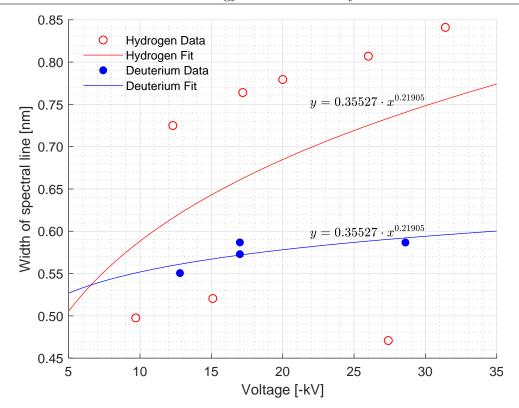


Figure 10: The spectral line width as a function of applied voltage

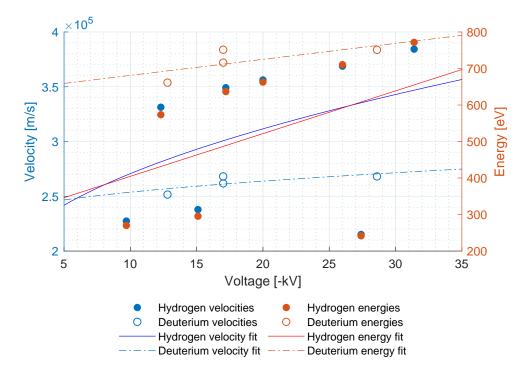


Figure 11: The estimated velocities and kinetic energies for hydrogen and deuterium as
functions of applied voltage

The four fits were computed to be:

Velocity for hydrogen:
$$v = 3.12 \times 10^4 \sqrt{x} + 1.72 \times 10^5$$
 (45)

Velocity for deuterium:
$$v = 0.7666 \times 10^4 \sqrt{x} + 2.295 \times 10^5$$
 (46)

Kinetic energy for hydrogen:
$$KE = 11.7x + 287.7$$
 (47)

Kinetic energy for deuterium:
$$KE = 4.387x + 637.3$$
 (48)

with x being the applied voltage. Of course the uncertainties from Fig. 10 carries over which is unfortunate. We expected the deuterium and hydrogen energies to be equal which was not the case, but the velocity of hydrogen seems to be larger than the deuterium atoms which is to be expected.

B. Neutron production rate

The fusion reaction rate should increase with voltage and current where approximately every second reaction produce a neutron. Measurements of the neutron production rate are made and seen in Table VII. It is important to note that only 5 measurements are made, so the sample size is very small. There are 3 parameters that varies throughout the measurements which makes it hard to say anything about the data. There is an unknown dependency on the pressure(and on the voltage and current) since an increasing pressure will decelerate the particles overall, but it will also increase the amount of fuel available. The pressure varies from 1.40 μ bar to 2 μ bar. This should have an effect on the neutron rate, but let us disregard that fact for now. The data suggests that a current of 6 mA is needed to get decent reaction rates when the voltage is in the ranges measured. On top of that, the data also suggests that the voltage needed is between 24 V and 28 V. Note that the last suggestion is made at an approximately constant pressure.

Calculating the total neutron flux at the detector and the total neutron production rate is trivial given Cts./s, $\eta_{\rm eff.}=15\%$, $A_{\rm det}=6\times10^{-5}~{\rm m}^2$ and $R_{\rm det}=0.500~{\rm m}$.

$$\Gamma_{\rm n} = \frac{\rm Cts.}{\rm s} \frac{1}{\eta_{\rm det}} \frac{1}{A_{\rm det}} \tag{49}$$

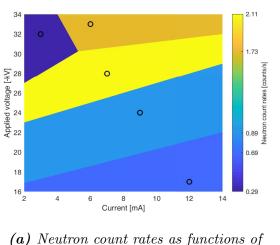
And $n/s = 4 \pi R_{det} \Gamma_n$. Now the power is equal to the product of the current and voltage, but there is a voltage drop across the resistor bank which must be taken into account. Meanwhile the fusion power $P_{fusion} = n/s (E_n + E_\alpha)$ with E_n , E_T being the energy release of the reaction that results in a neutron and a tritium particle respectively (disregarding the other resulting particles). For the remaining problems Table VII displays the data that are

fitted in Fig. 12. On the Q-value; the tokamak reactor JET for example displays a Q-value of around 0.67⁶. This is approximately 10⁵ times higher than the DTU fusor, so the inertial electrostatic confinement technology is way behind the magnetostatic confinement technology. Calculating the neutron production rates etc. is easy enough, however due to a very small amount of data points, it is hard to say anything meaningful about the fits. We do see an increase in rates when increasing the current and voltage. But the size of the contours should tell us that this conclusion is laughably optimistic. On top of that, the pressure is varying which is not taken into account. Thus our conclusion is that this data is close to, if not completely unusable.

| p [µbar] | I [mA] | V[-kV] | P[W] | [Cts./s] | $\Gamma_n \big[s^{-1} {\cdot} m^{-2} \big]$ | [n/s] | $Q[10^{-6}]$ |
|----------|--------|--------|------|----------|--|------------------|--------------|
| 2 | 12 | 17 | 194 | 0.689 | 0.766×10^5 | 2.41×10^5 | 1.45 |
| 1.7 | 9 | 24 | 210 | 0.891 | 0.990×10^5 | 3.11×10^5 | 1.73 |
| 1.6 | 7 | 28 | 193 | 2.106 | 2.34×10^5 | 7.35×10^5 | 4.45 |
| 1.4 | 3 | 32 | 95.4 | 0.295 | 0.328×10^5 | 1.03×10^5 | 1.26 |
| 1.4 | 6 | 33 | 195 | 1.725 | 1.92×10^5 | 6.02×10^5 | 3.61 |

Table VII: Table containing the measured parameters for deuterium.

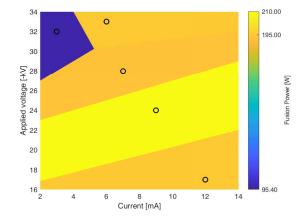
32

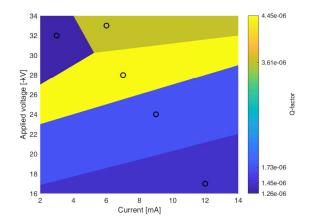


1.92e+05 30 Applied voltage [-kV] 0 20 18 8 Current [mA]

(a) Neutron count rates as functions of current and voltage

(b) The neutron flux at the detector as functions of current and voltage





and voltage

(c) The fusion power as functions of current (d) The Q-factor as functions of current and voltage

Figure 12: Fusor neutron count, flux, power and q-factor as functions of current and voltage

IV. CONCLUSIONS

A. Assignment 1: A simple reactor model

Freidberg's model produced some reasonable results for a simple tokamak design. The model would however break down when certain parameters would lie in certain regions. For example β would go to infinity when $P_{\rm E}$ would lie approximately between 500 MW and 1000 MW. Meanwhile after implementing the elliptical model and solving it for $P_{\rm E}=2$ GW β would go to 1.69% which we deemed to low. Setting $\kappa=2$ and A=3 would increase β to 4.55%. Further optimising β and $V_{\rm P}/A_{\rm P}$ would lead to $\kappa=2.5$ and A=2.39 using a desired $\beta=10\%$.

B. Assignment 2: Diagnostics via interferometry

Wanting to keep the emitter frequency above the plasma frequency resulted in a minimum frequency of 9 GHz given the calculations, this is the optimum frequency however the best emitter available is emitting at a frequency of 60 GHz so this emitter should be chosen. In order to make sure that the beam is controlled and that most of the beam is transmitted, a Gaussian telescope with a focal length of 0.250 m is implemented. It is also important that the beam hits the plasma surface perpendicular so refraction is avoided.

C. Assignment 3: Fusor exercise

While it is hard to conclude anything based on the very poor measurements, minor conclusions are somewhat possible. Barring the trivial measurement of the plasma constituents and focusing on the information the spectral line width should provide. While(again) measurements are very uncertain it does seem, as expected, that it measures that the velocity of the deuterium is smaller than for the hydrogen at a given voltage. This points towards the measurement being correct and the average ion energy as a function of voltage can then be calculated. While an increasing energy was derived with increasing voltage, the result did not correspond with expectations as the energies for the two species were not equal. On the neutron rates. A very optimistic conclusion of increasing neutron rates with voltage and current was achieved. The more important conclusion for now seems to be that an automatic pressure regulator must be implemented if an experiment is to be

precise. Furthermore, a much larger amount of data points must also be gathered.

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[†] E-mail at spacrone@live.dk

[‡] Homepage of the Technical University of Denmark http://www.dtu.dk/english/;

[•] Project Repository: https://github.com/rwiuff/10401

¹ https://www.iter.org/.

² Jeffrey P. Freidberg, *Plasma physics and fusion energy* (Cambridge University Press, 2007).

 $^{^3}$ Hans-Jürgen Hartfuß and Thomas Geist, Fusion Plasma Diagnostics with mm-Waves (Wiley-VCH, 2013).

⁴ "Hydrogen spectral series" - Wikipedia (Visited January 22nd).

 $^{^5}$ "Deuterium#Spectroscopy" - Wikipedia (Visited January $22^{\rm nd}).$

⁶ "Fusion energy gain factor" - Wikipedia (Visited January 24th).

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| | | |

LISTINGS

Appendices

Appendix A: tokamakDTU_asign_1

```
% Name:
                    tokamakDTU
3
     Version:
4
5
                    Contains the function 'tokamakDTU' which gives parameters
     Purpose:
6
                    for a tokamak fusion power plant as output based on a
7
                    simplified model. The equations used are derived in
8
                    chapter 5 in Friedberg, Plasma physics and Fusion
9
                    Energy, 2007 (all references are referring thereto).
10
11
    % To do (NOT for 10401 - Fusion Energi students):
12
                 1. Rewrite the code to a class (this is not done on purpose so
13
14
15
                    R_0/a and/or the ellipticity as an input into one file.
16
17
18
                 1. December 2014:
19
                    Written by Michael Løiten based on a similar code written
20
                    as a bachelor project by Elias Pagh Sentius
21
                    mailto: mmag@fysik.dtu.dk
22
                           ********************
23
24
    function [b, c, a, R_0, A, A_p, V_p, P_dens, p, n, B_0, beta, tau_E_min,...
25
              C_per_watt] = ...
26
        tokamakDTU_asign_1(...
27
            n_flux_fraction, C_F, C_I, P_E, P_W, B_max, sigma_max, eta_t)
28
```

January 24th

R. K. F. Wiuff

```
%TOKAMAK_DTU Function which returns the parameters of a power plant
29
30
    % Output parameters
31
32
33
                 - Magnet coil thickness [m]
34
35
    % R_0
                 - Major radius [m]
36
    % A
                 - Aspect ratio []
37
    % A_p
38
   % V_p
39
   % P_dens
40
                 - Plasma pressure [Pa]
41
    % n
42
                 - Magnetic field at magnetic axis [T]
    % B_0
43
                 - Plasma beta in the centre []
    % beta
44
    % tau_E_min - Min confinement time for satisfaction of (p*tau_E)_min [s]
45
    % C_per_watt - The cost of the powerplant [$]
46
47
    % Input parameters
48
49
    % n_flux_fraction - n flux in breeder end/n flux in breeder start []
50
                       - Fixed cost propotionality constant [$]
51
                       - Nuclear island cost propotionality constant [$W/m^3]
   % C_I
52
                       - Desired output power [MW]
   % P_E
53
   % P_W
                       - Maximum wall load [MW/m^2]
54
                       - Magnetic field at the edge of the coil [T]
   % B_max
55
    % sigma_max
56
    % eta_t
                       - Energy conversion efficiency []
57
58
59
    % The function starts by defining fixed constants
60
```

```
61
   % makes the code easier to use, as these are not needed as input parameters
62
63
64
   65
   % Nuclear
66
67
68
              = 2.5e-8; % [MeV] Energy of slow (thermal) neutron (eq 5.6)
   E_t
69
              = 14.1; % [MeV] Neutron energy after fusion (eq 2.17)
70
              = 3.5;
                       % [MeV] alpha energy after fusion (eq 2.17)
   E_a
71
              = 4.8;
                       % [MeV] Heat produced by breeding Li (under eq 4.31)
   E_Li
72
73
   sigma_v_avg = 3.0e-22;% [m^3/s] DT fusion cross section @ 15keV (table 5.2)
74
              = 0.0031; % [m] Breeding mean free path (under eq 5.7)
   lambda_br
75
   lambda_sd
              = 0.055; % [m] Mean free path from sigma_sd (eq 5.3)
76
77
   % Plamsa physics
78
79
   % Parameters for infinity gain at the minimum of p tau_E (eq 4.20)
80
               = 15.0; % [keV] Temparature for obtaining min tripple product
81
   tripple_min = 8.3; % [atm s] Min tripple prod to obtain Q=inf @ T=15 keV
82
83
   % Natural constants
84
85
   mu_0 = 4.0*pi*1e-7;
                     % Vacuum permeability [T*m/A]
86
       = 1.602176565e-19; % Elementary charge [C]
87
   88
89
90
   % Secondly we convert everything to SI units, so that the variables are
91
92
```

```
% Again, this is computationally inefficient, but it suffices for our use
93
    % Conversion to SI-units
94
    95
    % Conversion factors
96
   W_per_MW
               = 1.0e6;
97
   Pa_per_atm
               = 1.01325e5;
98
   eV_per_keV
               = 1.0e3;
99
   eV_per_MeV
               = 1.0e6;
100
   J_per_eV
               = e;
101
   J_per_keV
               = J_per_eV * eV_per_keV;
102
   J_per_MeV
103
               = J_per_eV * eV_per_MeV;
   % Conversions
104
   P_E
                                       % Desired output power
               = P_E * W_per_MW;
105
   P_W
               = P_W * W_per_MW;
106
   E_t
               = E_t * J_per_MeV;
107
   E_n
               = E_n * J_per_MeV;
108
   E_a
               = E_a * J_per_MeV;
109
   E_Li
               = E_Li * J_per_MeV;
110
    sigma_max
               = sigma_max * Pa_per_atm; % Max allowable structural stress
111
               = T * J_per_keV;
                                       % Temparature for minimum p*tau_E
112
    tripple_min = tripple_min * Pa_per_atm; % The Lawson parameter (p*tau_E)
113
    114
115
116
117
118
   % Find the breeder thickness
119
    b = get_b(lambda_sd, E_n, E_t, lambda_br, n_flux_fraction);
120
121
    [a, c] = get_a_and_c(B_max, mu_0, sigma_max, b);
122
123
   R_0 = get_R_0(a, eta_t, E_n, E_a, E_Li, P_E, P_W);
```

```
% Find the resulting geometrical factors
125
        = R_0/a;
                                         % Aspect Ratio
126
    A_p = (2.0*pi*a)*(2.0*pi*R_0); % Plasma surface area
    V_p = (pi*a (2.0))*(2.0*pi*R_0); % Plasma volume
128
129
130
    % Calculate the plasma physics parameters
131
132
    % Find the power density in the plasma
133
    P_dens = get_P_dens(E_a, E_n, E_Li, P_E, eta_t, V_p);
134
135
    p = get_p(E_a, E_n, P_dens, T, sigma_v_avg);
136
137
    n = p/(2.0*T);
138
139
    B_0 = get_B_0(R_0,a,b,B_max);
140
141
    beta = get_beta(p, B_0, mu_0);
142
    % Find the minimum required confinement time from the definition of the
143
    % minimum tripple product.
144
    \% NOTE: A higher confinement time is advantegous, and could in principle
145
    % yield a smaller (and cheaper) reactor. However, the effect is not
146
147
    tau_E_min = tripple_min/p;
148
149
150
151
    % (details about the cost can be found in the function get_a_and_c)
152
153
154
155
    V_I = get_V_I(R_0,a,b,c);
156
```

```
% Find the reactor volume per power out
157
    % In the current model, this is the only non-constant in the expression for
158
    % cost per watt
159
    V_I_per_P_E = V_I/P_E;
160
    C_per_watt = get_C_per_watt(C_F, C_I, V_I_per_P_E);
161
    end
162
164
165
                                                                              )
    function
                  = get_b(
166
    %GET_B Calculates b from the need of slowing down and breeding neutrons
167
168
    % Thickness of the moderator-breeding region so that 1 - n_flux_fraction
169
171
172
    delta_x = 2.0*lambda_sd*...
173
               log(1.0-(1.0/2.0)*(E_n/E_t) (1.0/2.0)*...
                     (lambda_br/lambda_sd)*log( n_flux_fraction )...
175
                   );
176
    % Set b from delta_x
178
    \% Friedberg argues above equation 5.11 that b should be between 1 and 1.5 m
179
180
    self_chosen_constant = 0.32;
181
    b = delta_x + self_chosen_constant;
182
    end
183
184
185
186
187
                                                               )
    function
                     = get_a_and_c(
188
```

```
%GET_A_AND_C Calculates a and c
189
190
    \% c is obtained from requiring that the magnets are so thin that they are
191
192
193
194
    \% xi defined when making the magnetic coil c as thin as possible
195
    % Under equation 5.27
196
    xi = B_{max} (2.0) / (4.0*mu_0*sigma_max);
197
198
    % a is found from optimization of the cost, where
199
200
201
    % Fixed cost
202
     %.....
203
    % K_F = Fixed cost for building, turbines, generators etc (also applies to
204
205
    % Assumption: The fixed cost is proportional to power output:
206
207
    % K_F = C_F*P_E;
208
209
210
211
    % Assumption: The proportional to reactor volume:
212
213
    % K_I = C_I*V_I;
214
215
    V_I = 2.0*pi^(2.0) * R_0 * ((a+b+c)^(2.0) - a^(2.0)); % Reactor volume
216
    %.....
217
    % Cost per watt:
218
219
    % Defined as C_p_watt = (K_F + K_I)/P_E, rewritten to
```

```
% C_p_{watt} = C_F + C_I*(V_I/P_E);
221
    % Since the cost per watt contains two constants, we can minimize the
222
    % V_I/P_E in order to optimize the cost
223
    % Given by equation 5.20 inserted in 5.17
224
225
    % V_I_per_P_E = V_I/P_E; % Reactor volume per power out
226
    \% a is found by setting the derivative of V_I_per_P_E = 0
228
    a = ((1.0 + xi)/(2.0*xi (1.0/2.0))) * b;
229
230
    % Knowing xi, a, and, b, we can calculate c
231
    % c found by comparing tensile force and magnetic force working on the coil
232
233
    c = 2*xi/(1-xi)*(a+b);
    end
235
236
237
238
    function
                    = get_R_0(
239
    %GET_R_O Calculate the major radius
240
242
    \% eq 5.19 (wall loading * area = total neutron production) and solve for RO
243
244
    R_0 = (1.0/(4.0*pi (2.0)*eta_t))*(E_n/(E_n + E_a + E_Li))*(P_E/(a*P_W));
245
    end
246
247
248
249
                       = get_P_dens(
                                                                       )
    function
250
     %GET_P_DENS Calculate the power density
251
252
```

```
253
254
255
     P_{dens} = (E_a + E_n)/(E_a + E_n + E_Li)*P_E/(eta_t*V_p);
256
257
258
260
                                                  )
    function
                     = get_B_0(
261
     %GET_B_O Calculte the magnetic field strength on the magnetic axis
262
263
    % B_{max} is found in the edge of the magnet (at R = R_0-a-b)
264
265
     % As B propto 1/R. we have that B_0/B_max = (R_0-a-b)/R_0, which leads to
266
267
    B_0 = ((R_0-a-b)/R_0)*B_max;
268
     end
269
270
271
272
                      = get_beta(
    function
273
     %GET_beta Calculte the magnetic field strength on the magnetic axis
274
275
276
    beta = p / (B_0 2/(2.0*mu_0));
278
279
280
281
282
                                                               )
    function
                   = get_p(
283
     %GET_P Calculate the plasma pressure
```

```
285
286
287
288
    p = ((16.0/(E_a + E_n)) * P_dens) (1.0/2.0)*...
289
          (T (2.0)/sigma_v_avg) (1.0/2.0);
290
     end
291
292
293
294
     function
                     = get_V_I(
295
     %GET_V_I Calculate the volume of the material surrounding the plasma
296
297
298
    V_I = 2.0*pi (2.0) * R_0 * ( (a+b+c) (2.0) - a (2.0) );
299
     end
300
301
302
303
                             = get_C_per_watt(
     function
304
     %GET_C_PER_WATT Calculates the cost for one watt out from the power plant
305
306
     % For details in how the cost is derived, see comments in the function
307
     % get_a_and_c
309
     C_{per_watt} = C_F + C_I*(V_I_{per_P_E});
310
311
```

2019

Appendix B: IterateTokamakDTU

```
close all
1
    clear all
2
3
    titl = [ Desired output power [MW] , Maximum wall load [MW, m -2] , ...
4
         Magnetic field at the edge of the coil [T] , \ldots
5
         Tensile strenght of the magnetic field coils [atm] ];
6
    foldertitl = [ PE , PW , Bmax , sigmamax ];
7
8
    for d = 1:4
9
        1 = d; % Choose iteration: 1 = P_E, 2 = P_W, 3 = B_max, 4 = sigma_max
10
        p0 = [];
11
        x = [];
12
        mkdir('../MatlabFigures', foldertitl(1))
13
        printout = (sprintf('Created folder %s', foldertitl(1)));
14
        disp(printout)
15
        if 1 == 1
16
            x = linspace(1, 3000, 1000);
^{17}
            for i = 1:length(x)
18
                [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
19
                     n, B_O, beta, tau_E_min, C_per_watt] = ...
20
                     tokamakDTU_asign_1(0.01, 1, 2, x(i), 4, 13, 3000, 0.4);
21
                q = [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
22
                    n, B_0, beta, tau_E_min, C_per_watt];
                p0 = cat(1, p0, q);
24
            end
25
        elseif 1 == 2
26
            x = linspace(1, 10, 1000);
27
            for i = 1:length(x)
28
                [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
29
                    n, B_0, beta, tau_E_min, C_per_watt] = ...
30
```

```
tokamakDTU_asign_1(0.01, 1, 2, 1000, x(i), 13, 3000, 0.4);
31
                 q = [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
32
                     n, B_0, beta, tau_E_min, C_per_watt];
33
                p0 = cat(1, p0, q);
            end
35
        elseif 1 == 3
36
            x = linspace(10, 20, 1000);
37
            for i = 1:length(x)
                 [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
39
                     n, B_0, beta, tau_E_min, C_per_watt] = ...
40
                     tokamakDTU_asign_1(0.01, 1, 2, 1000, 4, x(i), 3000, 0.4);
                q = [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
42
                     n, B_0, beta, tau_E_min, C_per_watt];
43
                p0 = cat(1, p0, q);
44
            end
45
        elseif 1 == 4
46
            x = linspace(2000, 5000, 1000);
47
            for i = 1:length(x)
48
                 [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
49
                     n, B_0, beta, tau_E_min, C_per_watt] = ...
50
                     tokamakDTU_asign_1(0.01, 1, 2, 1000, 4, 13, x(i), 0.4);
51
                q = [b, c, a, R_0, A, A_p, V_p, P_dens, p, ...
                     n, B_0, beta, tau_E_min, C_per_watt];
53
                p0 = cat(1, p0, q);
54
            end
55
56
        printout = (sprintf('Iterated tokamakDTU_asign_1.m %d of 4', d));
57
        disp(printout)
58
        b = p0(:, 1);
        c = p0(:, 2);
60
        a = p0(:, 3);
61
        R_0 = p0(:, 4);
62
```

```
A = p0(:, 5);
63
        A_p = p0(:, 6);
64
        V_p = p0(:, 7);
65
        P_{dens} = p0(:, 8);
66
        p = p0(:, 9);
67
        n = p0(:, 10);
68
        B_0 = p0(:, 11);
69
        beta = p0(:, 12);
70
        beta = beta * 100;
71
        tau_E_min = p0(:, 13);
72
        C_{per_watt} = p0(:, 14);
74
        f1 = figure;
75
        ptau = plot(x, tau_E_min, 'color', 'r', 'LineWidth', 1);
76
        xlabel(titl(1));
77
        ylabel('[s]');
78
        ytickformat('%.2f');
79
        grid on
80
        grid minor
81
        lgd = legend([ptau], ...
82
            { Min confinement time for satisfaction of (p tau_E)_{min} }); % Figure legend
83
        legend('boxoff')
        legend('Location', 'north')
85
        figcount = 1;
86
        printout = (sprintf('Created figure %d of 8', figcount));
        disp(printout)
88
89
        f2 = figure;
90
        pb = plot(x, b, 'color', 'r', 'LineWidth', 1);
        hold on
92
        pc = plot(x, c, '--', 'color', 'b', 'LineWidth', 1);
93
        pa = plot(x, a, '-.', 'color', 'm', 'LineWidth', 1);
94
```

```
pcpw = plot(x, C_per_watt, 'color', 'g', 'LineWidth', 1);
95
         hold off
96
         xlabel(titl(1));
97
         ytickformat('%.2f');
98
         lgd = legend([pb, pc, pa, pcpw], ...
99
             { Blanket - shield, thickness, [m], Magnet, coil, thickness, [m], ...
100
              Minor, radius, [m] , ...
101
              Cost, per, watt, [ ] });% Figure legend
102
         legend('boxoff')
103
         if 1 == 3
104
             legend('Location', 'north')
105
         else
106
             legend('Location', 'west')
107
         end
108
         grid on
109
         grid minor
110
         figcount = 2;
111
         printout = (sprintf('Created figure %d of 8', figcount));
112
         disp(printout)
113
114
         f3 = figure;
115
         hold on
         yyaxis left
117
         pA = plot(x, A, 'LineWidth', 1);
118
         ylabel('Aspect ratio')
119
         yyaxis right
120
         pr_0 = plot(x, R_0, '--', 'LineWidth', 2);
121
         ylabel('Major radius [m]')
122
         hold off
123
         xlabel(titl(1));
124
         ytickformat('%.2f');
125
         lgd = legend([pr_0, pA], ...
126
```

```
{ Major, radius , Aspect, ratio, [] }); % Figure legend
127
         legend('boxoff')
128
         legend('Location', 'east')
129
         grid on
130
         grid minor
131
         figcount = 3;
132
         printout = (sprintf('Created figure %d of 8', figcount));
133
         disp(printout)
134
135
         f4 = figure;
136
         pA_p = plot(x, A_p, 'LineWidth', 1);
137
         hold on
138
         pV_p = plot(x, V_p, '--', 'LineWidth', 2);
139
         hold off
140
         xlabel(titl(1));
141
         ytickformat('%.2f');
142
         lgd = legend([pA_p, pV_p], ...
143
             { Plasma, surface, [m 2] , Plasma, volume, [m 3] }); % Figure legend
144
         legend('boxoff')
145
         legend('Location', 'east')
146
         grid on
147
         grid minor
         figcount = 4;
149
         printout = (sprintf('Created figure %d of 8', figcount));
150
         disp(printout)
151
152
         f5 = figure;
153
         pP_dens = plot(x, P_dens, 'color', 'r', 'LineWidth', 1);
154
         xlabel(titl(1));
         ylabel('[W m^-1]');
156
         ytickformat('%.2f');
157
         grid on
158
```

```
grid minor
159
          lgd = legend([pP_dens], ...
160
             { Power density });% Figure legend
161
         legend('boxoff')
162
         legend('Location', 'north')
163
         figcount = 5;
164
         printout = (sprintf('Created figure %d of 8', figcount));
165
         disp(printout)
166
167
         f6 = figure;
168
         yyaxis left
169
         pn = plot(x, n, 'LineWidth', 1);
170
         ylabel('Particle density [m^-3]')
171
         ytickformat('%.2f');
172
         yyaxis right
173
         p = plot(x, p, '--', 'LineWidth', 2);
174
         ylabel('Plasma pressure [Pa]')
175
         ytickformat('%.2f');
176
         xlabel(titl(1));
177
         lgd = legend([pn, p], ...
178
             { Particle, density , Plasma, pressure, [Pa] }); % Figure legend
179
         legend('boxoff')
180
         legend('Location', 'north')
181
         grid on
182
         grid minor
183
         figcount = 6;
184
         printout = (sprintf('Created figure %d of 8', figcount));
185
         disp(printout)
186
187
         if 1 == 1
188
             f7 = figure;
189
             subplot(2, 1, 1);
190
```

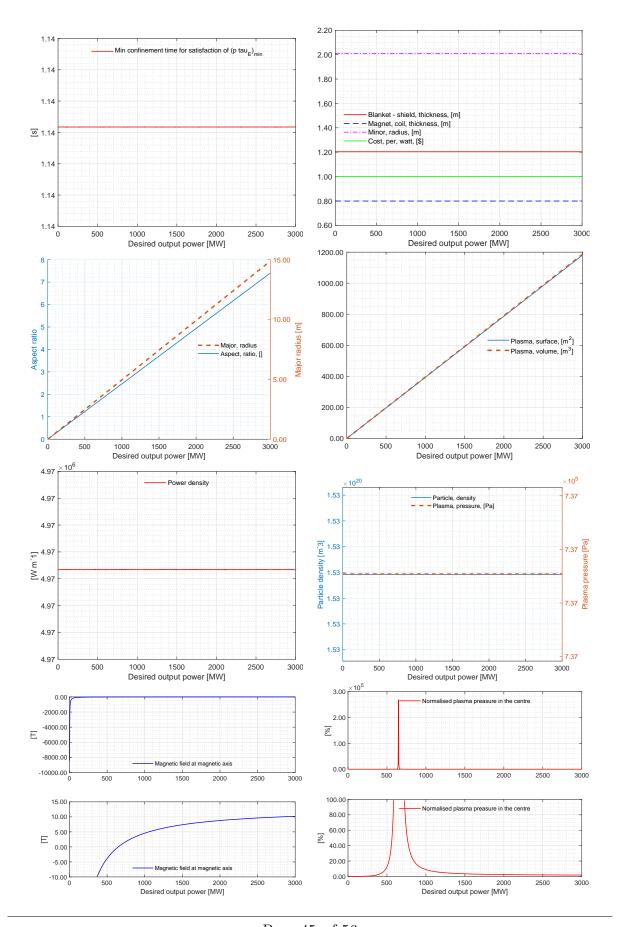
```
pB_0 = plot(x, B_0, 'color', 'b', 'LineWidth', 1);
191
             ylabel('[T]');
192
             ytickformat('%.2f');
193
             grid on
194
             grid minor
195
             lgd = legend([pB_0], ...
196
             { Magnetic field at magnetic axis }); % Figure legend
197
             legend('boxoff')
198
             legend('Location', 'south')
199
             subplot(2, 1, 2);
200
             B_0(B_0 \le -10) = NaN;
201
             pB_0 = plot(x, B_0, 'color', 'b', 'LineWidth', 1);
202
             xlabel(titl(1));
203
             ylabel('[T]');
204
             ytickformat('%.2f');
205
             grid on
206
             grid minor
207
             lgd = legend([pB_0], ...
208
             { Magnetic field at magnetic axis }); % Figure legend
209
             legend('boxoff')
210
             legend('Location', 'south')
         else
             f7 = figure;
213
             pB_0 = plot(x, B_0, 'color', 'b', 'LineWidth', 1);
214
             xlabel(titl(1));
215
             ylabel('[T]');
216
             ytickformat('%.2f');
217
             grid on
218
             grid minor
             lgd = legend([pB_0], ...
220
             { Magnetic field at magnetic axis }); % Figure legend
221
             legend('boxoff')
```

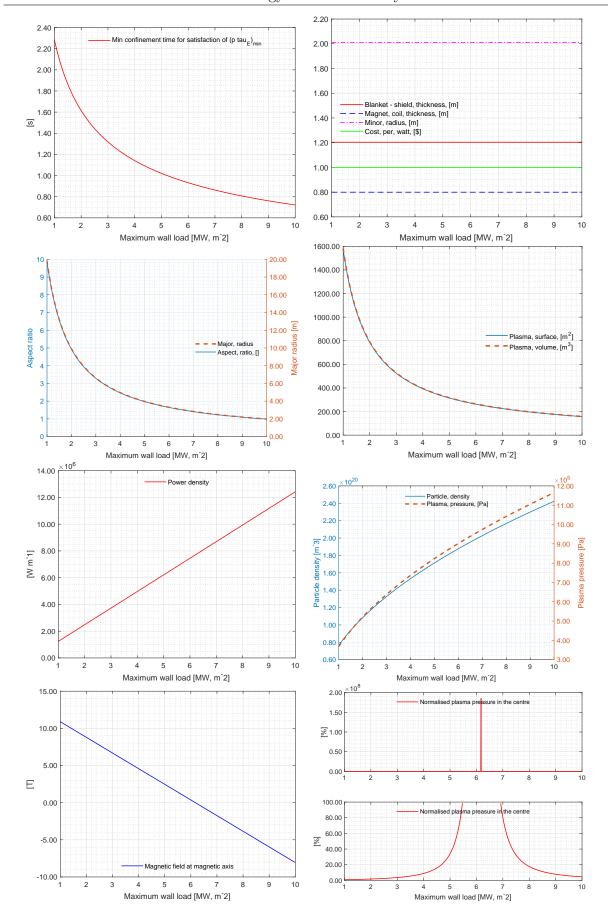
```
legend('Location', 'south')
223
         end
224
         figcount = 7;
225
         printout = (sprintf('Created figure %d of 8', figcount));
226
         disp(printout)
227
         if 1 == 1 || 1 == 2
228
             f8 = figure;
229
             subplot(2, 1, 1);
230
             pbeta = plot(x, beta, 'color', 'r', 'LineWidth', 1);
231
             ylabel('[%]');
232
             ytickformat('%.2f');
233
             grid on
234
             grid minor
235
             lgd = legend([pbeta], ...
236
             { Normalised plasma preasure in the centre }); % Figure legend
237
             legend('boxoff')
238
             legend('Location', 'north')
239
             subplot(2, 1, 2);
240
             beta(beta >= 100) = NaN;
241
             pbeta = plot(x, beta, 'color', 'r', 'LineWidth', 1);
242
             xlabel(titl(1));
243
             ylabel('[%]');
             ytickformat('%.2f');
245
             grid on
246
             grid minor
247
             lgd = legend([pbeta], ...
248
             { Normalised plasma preasure in the centre }); % Figure legend
249
             legend('boxoff')
250
             legend('Location', 'north')
         else
252
             f8 = figure;
253
             pbeta = plot(x, beta, 'color', 'r', 'LineWidth', 1);
254
```

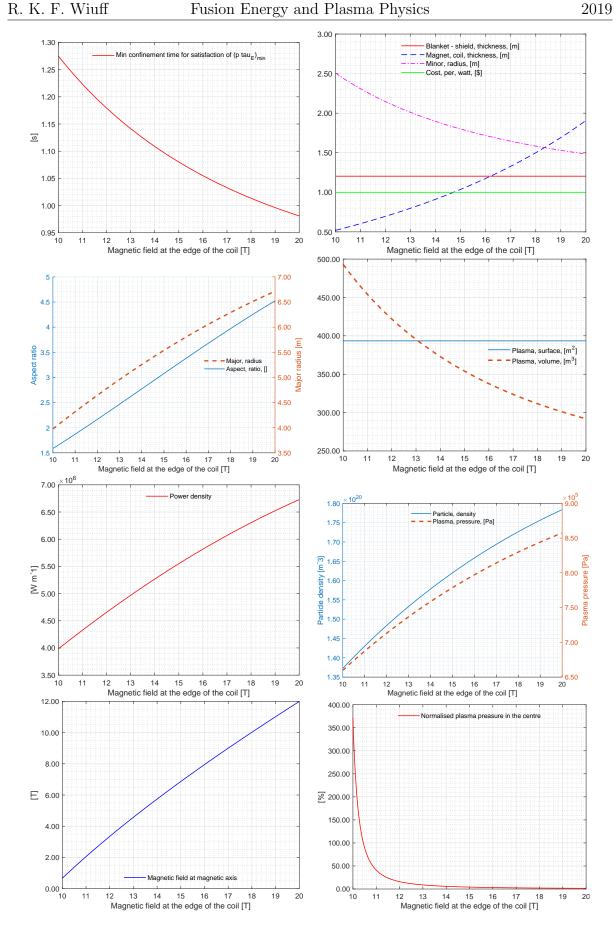
```
xlabel(titl(1));
255
             ylabel('[%]');
256
             ytickformat('%.2f');
257
             grid on
258
             grid minor
259
             lgd = legend([pbeta], ...
260
             { Normalised plasma preasure in the centre }); % Figure legend
261
             legend('boxoff')
262
             legend('Location', 'north')
263
         end
264
        figcount = 8;
265
        printout = (sprintf('Created figure %d of 8', figcount));
266
        disp(printout)
267
        % lgd = legend([pb, pc, pa, pr_0, pA, pA_p, pV_p,...
268
               pP_dens, p, pn, pB_0, pbeta, ptau, pcpw], ...
269
               {"Blanket-shield thickness [m]", "Magnet coil thickness [m]"...
        %
270
               "Minor radius [m]", "Major radius [m]", "Aspect ratio []"...
271
               "Plasma surface [m^2]", "Plasma volume [m^3]", "Power density [W m^-1]"...
273
               "Magnetic field at magnetic axis [T]", "Plasma beta in the centre []"...
274
               "Min confinement time for satisfaction of (p tau_E)_min [s]",...
275
               "The cost of the powerplant [$]"});% Figure legend
277
278
        fignames = [ f1 , f2 , f3 , f4 , f5 , f6 , f7 , f8 ];
279
        figfigs = [f1, f2, f3, f4, f5, f6, f7, f8];
280
281
282
        for i = 1:8
             foldername = sprintf('../MatlabFigures/%s', foldertitl(1));
284
             epsfilename = sprintf('%s.eps', fignames(i));
285
             fullfilename = fullfile(foldername, epsfilename);
286
```

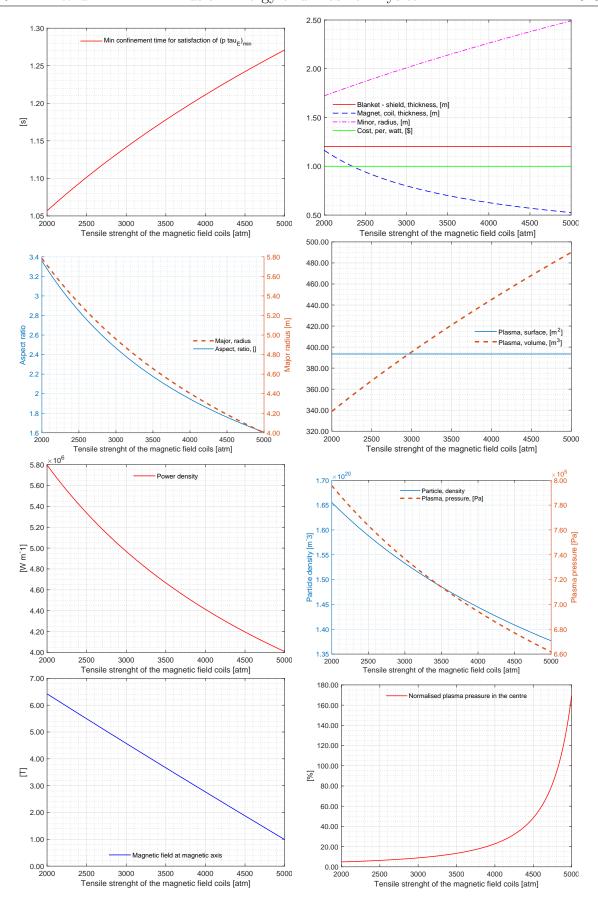
```
saveas(figfigs(i), fullfilename, 'epsc')
287
             printout = (sprintf('Saved figure %d of 8', i));
288
             disp(printout)
289
         end
290
291
         close all
292
        printout = (sprintf('Completed iteration %d of 4', d));
293
        disp(printout)
294
    end
295
```

Appendix C: Iterations over Freidberg's model









Appendix D: interferometer.m

```
close all
1
    clear all
2
3
   mkdir('../MatlabFigures', 'Interferometer'); % Create save directory
4
5
                 -----Input Parameters-----
6
   r_p = 0.055; % Reactor port opening [m]
7
   w_0 = 0.0275; % Initial Beam Waist [m]
8
   r = 0.125; % Minor tokamak radius [m]
9
   freq = 60; % Frequency of probe beam [GHz]
10
   d_0 = 0.20; % Distance between source and first lens
12
   d_r = 0.10; % Distance between first lens and reactor wall
13
   f_0 = 0.25; % Focal length of first lens
14
   f_1 = 0.20; % Focal length of second lens
15
16
17
18
   c = 299792458; % The speec of light [m/s]
19
   lambda = c / (freq * 10 9); % Calculates the wavelength [m]
20
   d = f_0 + f_1; % Calculates the distance between lenses
21
   w_1 = (lambda * f_0) / \dots
22
        (pi * w_0); % Calculates the beam waist between lenses
23
   d_1 = (((d_0 / f_0) - 1) / ((w_0 (2) * pi) / ...
24
        (f_0 * lambda) + ((d_0 / f_0) - 1) (2)) + 1) * ...
        f_0; % Distance after 1st lens to lowest beam waist
26
   w_2 = (f_1 / f_0) * w_0; % Calculates w_2 after 2nd second lens
27
   d_2 = d - d_1; % Distance from w_2 to second lens
28
   d_3 = f_1 / f_0 * \dots
29
        (f_0 + f_1 - \dots
```

```
(f_1 / f_0) * d_0);% Distance to lowest beam waist after 2nd lens
31
32
33
                    -----Beam Waist Datapoints-----
34
    x_0 = linspace(0, d_0, 1000);% Plotpoints till first lens
35
   y_0 = [];
36
    for i = 1:1000
37
        w = w_0 * \dots
38
            sqrt(1+((lambda * x_0(i)) / ...
39
            (pi * w_0 2)) 2); % Calculates the beam waist from source
40
        y_0 = horzcat(y_0, w);
    end
42
43
    x_1 = linspace(0, d_1, 1000); % Plotpoints from first lens to w_1
44
    y_1 = [];
45
    for i = 1:1000
46
        w = w_1 * \dots
47
            sqrt(1+((lambda * x_1(i)) / ...
48
            (pi * w_1 2)) 2); % Beam waist between w_1 and the 1st lens
49
        y_1 = horzcat(y_1, w);
50
    end
51
   y_1 = fliplr(y_1); % Flips the y-plot points as the beam waist is declining
52
   y = horzcat(y_0, y_1);
53
54
    x_2 = linspace(0, d_2, 1000); % Plotpoints from w_1 to second lens
55
   y_2 = [];
56
    for i = 1:1000
57
        w = w_1 * \dots
58
            sqrt(1+((lambda * x_2(i)) / ...
            (pi * w_1 2)) 2); % Beam waist between w_1 and the 2nd lens
60
        y_2 = horzcat(y_2, w);
61
    end
62
```

```
63
   y = horzcat(y, y_2);
64
65
   x_3 = linspace(0, d_3, 1000); % Plotpoints from 2nd lens to <math>w_2
66
   y_3 = [];
67
   for i = 1:1000
68
        w = w_2 * \dots
69
            sqrt(1+((lambda * x_3(i)) / ...
70
            (pi * w_2 2)) 2); % Evolving beam waist after the 2nd lens to w_2
71
        y_3 = horzcat(y_3, w);
72
    end
73
   y_3 = fliplr(y_3); % Flips the y-plot points as the beam waist is declining
74
   y = horzcat(y, y_3);
75
76
    for i = 1:1000
77
        x_1(i) = x_1(i) + d_0; % Creates x-axis data points
78
    end
79
   for i = 1:1000
80
        x_2(i) = x_2(i) + d_0 + d_1; % Creates x-axis data points
81
    end
82
    for i = 1:1000
83
        x_3(i) = x_3(i) + d_0 + d_1 + d_2; % Creates x-axis data points
84
85
    x = horzcat(x_0, x_1, x_2, x_3);
86
87
    Opy = -y; % Flip beam waist to plot 'Beam Waist -'
88
89
90
                 -----Beam Waist Propagation Plot-----
91
   1 = figure; % Creates figure
92
   hold on
93
   axis equal
94
```

```
p1 = plot(x, y); % Plots Beam Waist+
95
    p2 = plot(x, Opy, 'Color', 'red'); % Plots Beam Waist-
96
    %p3 = xline(d_0, '--');
97
    %xline(d_0+d_1+d_2, '--');
98
    axPos = get(gca, 'Position'); % Get normalised axis coordinates
99
    xMinMax = xlim; % Get normalised axis coordinates
100
    yMinMax = ylim; % Get normalised axis coordinates
101
    zAnn = axPos(1) + ((0 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
102
         * axPos(3); % Defines points relative to axis in normalised coordinates
103
    d0Ann = axPos(1) + ((d_0 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
104
        * axPos(3); % Defines points relative to axis in normalised coordinates
105
    d1Ann = axPos(1) + ((d_0 + d_1 - xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
106
        * axPos(3); % Defines points relative to axis in normalised coordinates
107
    d2Ann = axPos(1) + ((d_0 + d_1 + d_2 - ...
108
        xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
109
        * axPos(3); % Defines points relative to axis in normalised coordinates
110
    d3Ann = axPos(1) + ((d_0 + d_1 + d_2 + d_3 - ...
111
        xMinMax(1)) / (xMinMax(2) - xMinMax(1))) ...
112
        * axPos(3); % Defines points relative to axis in normalised coordinates
113
    yAnn = axPos(2) + ((0 - yMinMax(1)) / (yMinMax(2) - yMinMax(1))) ...
114
         * axPos(4); % Defines points relative to axis in normalised coordinates
115
    annotation('doublearrow', ...
116
         [zAnn, dOAnn], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_0
117
    annotation('doublearrow', ...
118
         [dOAnn, d1Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_1
119
    annotation('doublearrow', ...
120
         [d1Ann, d2Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_2
121
    annotation('doublearrow', ...
122
         [d2Ann, d3Ann], [yAnn - 0.2, yAnn - 0.2]); % Annotates d_3
123
    annotation('ellipse', ...
124
         [dOAnn - 0.01, yAnn - y_0(1000) * 1.5, 0.02, y_0(1000) * 3], ...
125
         'FaceColor', 'cyan'); % Draws 1st lens
126
```

```
annotation('ellipse', ...
127
         [d2Ann - 0.01, yAnn - y_0(1000) * 1.5, 0.02, y_0(1000) * 3], \dots
128
         'FaceColor', 'cyan'); % Draws 2nd lens
129
    text(d_0/4, -0.22, sprintf('d_0 = \%0.2f', d_0)) % Distance annotation
130
     text(d_0+(d_1 / 4), -0.22, ...
131
        sprintf('d_1 = %0.2f', d_1))% Distance annotation
132
    text(d_0+d_1+(d_2 / 4), -0.22, \dots)
133
        sprintf('d_2 = \%0.2f', d_2))\% Distance annotation
134
    text(d_0+d_1+d_2+(d_3 / 4), -0.22, ...
135
        sprintf('d_3 = \%0.2f', d_3))\% Distance annotation
136
    text(d_0-0.06, 0.06, '1^{st} Lens') % Lens annotation
137
    text(d_0-0.06, -0.06, sprintf('f_0 = %0.2f', f_0)) % Lens annotation
138
    text(d_0+d_1+d_2-0.06, 0.06, '2^{nd} Lens') \% Lens annotation
139
    text(d_0+d_1+d_2-0.06, -0.06, ...
140
        sprintf('f_1 = \%0.2f', f_1))\% Lens annotation
141
    w1x = (d_0 + d_1); % w_1 coordinate
142
    w1x = repelem(w1x, 100); % w_1 x-coordinate array
143
    w1y = linspace(0, w_1); % w_1 y-coordinate array
144
    p4 = plot(w1x, w1y); % Plots w_1
145
    yline(0, '-'); % Plots optical axis
146
    xlabel('Distance from source [m]'); % x-axis label
147
    ylabel('Beam Waist [m]'); % y-axis label
148
    title('Beam Waist In A Gaussian Beam Interferometer'); % Figure title
149
150
    topstart = 2 * asin(r_p/(2 * r)) / 2; % Calculates reactor plot coordinates
151
    topend = (2 * pi - 2 * topstart) / 2; % Calculates reactor plot coordinates
152
    bottomstart = topend + topstart * 2; % Calculates reactor plot coordinates
153
    bottomend = 2 * pi - topstart; % Calculates reactor plot coordinates
154
155
    top = linspace(topstart, ...
156
         topend, 100); % Creates 100 datapoints for the top half reactor cutout
157
    x_t = d_0 + d_r + r + r * cos(top); % x-parameter of circle
158
```

```
y_t = r * sin(top); % y-parameter of circle
159
    bottom = linspace(bottomstart, ...
160
        bottomend, 100); % Creates 100 datapoints for the bottom half reactor
161
    x_b = d_0 + d_r + r + r * cos(bottom); % x-parameter of circle
162
    y_b = r * sin(bottom); % y-parameter of circle
163
    p5 = plot(x_t, y_t, 'color', ...
164
         [0.911, 0.4100, 0.1700]); Plot top half reactor
165
    plot(x_b, y_b, 'color', ...
166
         [0.911, 0.4100, 0.1700]); Plot bottom half reactor
167
    lgd = legend([p1, p2, p4, p5], ...
168
        {'Beam Waist +', 'Beam Waist -', 'w_1', 'Reactor'}); % Figure legend
169
    legend('boxoff')
170
    legend('Location', 'northwest')
171
    lgd.NumColumns = 2;
    hold off
173
174
175
     \%	ext{------}Saving figure as Encapsulated Postscript------\%
176
    epsfilename = 'Interferometer.eps'; % Savename for the figure
177
    foldername = sprintf('../MatlabFigures/Interferometer'); % Folder path
178
    fullfilename = fullfile(foldername, epsfilename); % Filename path
179
    saveas(1, fullfilename, 'epsc') % Save the figure as eps
180
181
182
                        -----Print Outputs-----
183
    w_1
184
    w_2
185
    d_1
186
    d_2
187
    d_3
188
189
```

Appendix E: PhaseShiftDensity.m

```
close all;
    clear all;
2
3
   mkdir('../MatlabFigures', 'PhaseShift'); % Create save directory
4
5
        ------Input Parameters-----
6
   f_0 = 60; % 1st beam frequency [GHz]
7
   f_1 = 98; % 2nd beam frequency [GHz]
8
   f_2 = 130; % 3rd beam frequency [GHz]
9
10
   n_0 = 10 16; % Lower electron density
11
   n_1 = 10 18; % Hihger electron density
12
13
14
    c = 299792458; % The speec of light [m/s]
15
16
   y = linspace(n_0, n_1, 1000); % Datapoints between n_0 and n_1
17
   Phi0 = []; % Phase shift array
18
   Phi1 = []; % Phase shift array
19
   Phi2 = []; % Phase shift array
20
21
   for i = 1:1000 % Calculates Phase Shifts for frequency = f_0
22
       Phi0 = horzcat(Phi0, 8.416e-8*(y(i) / (f_0 * 10 9)));
23
    end
24
    for i = 1:1000 % Calculates Phase Shifts for frequency = f_1
25
       Phi1 = horzcat(Phi1, 8.416e-8*(y(i) / (f_1 * 10 9)));
26
   end
27
    for i = 1:1000 % Calculates Phase Shifts for frequency = f_2
28
        Phi2 = horzcat(Phi2, 8.416e-8*(y(i) / (f_2 * 10 9)));
29
   end
```

```
31
   l = figure; % Creates figure
32
   hold on
33
   p0 = plot(Phi0, y); % Plot electron denisty as function of phase shift
34
   p1 = plot(Phi1, y); % Plot electron denisty as function of phase shift
35
   p2 = plot(Phi2, y); % Plot electron denisty as function of phase shift
   xlabel('Phase shift [^{1}/_{2\pi}]'); % x-axis label
37
   ylabel('Electron Density [m^-3]'); % y-axis label
38
    %title('Electron Density as function of measured phase shift'); % Figure title
39
   lgd = legend([p0, p1, p2], ...
40
        {'60GHz', '98GHz', '130GHz'});% Figure legend
41
    legend('boxoff')
42
   legend('Location', 'northwest')
43
    grid on
44
    grid minor
45
   hold off
46
            -----Saving figure as Encapsulated Postscript-----
48
   epsfilename = 'PhaseShift.eps'; % Savename for the figure
49
   foldername = sprintf('../MatlabFigures/PhaseShift'); % Folder path
50
   fullfilename = fullfile(foldername, epsfilename); % Filename path
51
    saveas(1, fullfilename, 'epsc') % Save the figure as eps
52
53
```