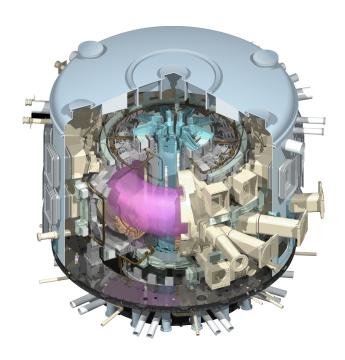
10401

Fusion Energy and Plasma Physics

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Abstract: Abstract

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I. INTRO

In recent years a large and quickly growing collaboration between plasma physcisists and engineers have materialised in one of the most ambitious energy producing projects ever seen. The proof-of-concept plasma fusion tokamak reactor ITER¹ in Cadarache is currently taking shape in order to adress the issue of growing energy demands and climate changes.

The mission is simple: Prove that plasma fusion is a viable source of electricity.

Whilst not being the most surmountable task, many researchers and institutions have gathered from across the world, including the Department of Physics at DTU.

In this paper, three assignments are solved as part of the course "10401 Fusion Energy and Fusion Plasma Physics". Some key aspects of fusion plasma fueled reactors are adressed and discussed in the assignments.

Symbol	Quantity
b	Blanket-and-shield thickness [m]
c	Magnet coil thickness [m]
a	Minor radius [m]
R_0	Major radius [m]
A	Aspect ratio []
A_p	Plasma surface $[m^2]$
V_p	Plasma volume $[m^3]$
$P_{\rm dens}$	Power density $[W \cdot m^{-1}]$
p	Plasma pressure [Pa]
n	Particle density $[m^{-3}]$
B_0	Magnetic field at magnetic axis [T]
β	Normalised plasma pressure []
$ au_{E_{\min}}$	Min confinement time for satisfaction of $(p \times \tau_E)_{\min}$ [s]
$C_{\text{per watt}}$	The cost of the powerplant [\$]

Table I: Quantities calculated by the model in Freidberg's².

II. ASSIGNMENT 1: A SIMPLE REACTOR MODEL

A. Freidberg's simple reactor model

In the 5th chapter of the textbook by Freidberg², he makes a simple model for designing a fusion reactor power plant. Table I shows a list of quantities necessary for the construction of a power plant. The model finds these quantities using simple geometric and electromagnetic assumptions with little involvement of plasma physics. The variables put into the model are shown in Table II. This model has been implemented in a matlab script provided for the course. The script is shown included in Appendix A. As an example, the model is run with the following parameters:

$$n_{\text{flux fraction}} = 0.01$$
 $P_E = 1000 \text{ MW}$
$$P_W = 4 \text{ MW} \cdot \text{m}^{-2} \quad B_{\text{max}} = 13 \text{ T}$$
 (1)
$$\sigma_{\text{max}} = 3000 \text{ atm} \qquad \eta_t = 0.4$$

Symbol	Quantity
$n_{ m flux\ fraction}$	n flux in breeder end/n flux in breeder start []
C_F	Fixed cost propotionality constant [\$]
C_I	Nuclear island cost propotionality constant $\left[\$\cdot\mathbf{W}\cdot\mathbf{m}^{-3}\right]$
P_E	Desired output power [MW]
P_W	Maximum wall load [MW·m $^{-2}$]
$B_{ m max}$	Magnetic field at the edge of the coil [T]
$\sigma_{ m max}$	Tensile strenght of the magnetic field coils [atm]
$\frac{\eta_t}{\eta_t}$	Energy conversion efficiency []

Table II: Variables in the Freidberg's model

Symbol	Quantity
b	1.20 m
c	$0.799~\mathrm{m}$
a	2.01 m
R_0	4.96 m
A	2.4670
A_p	393 m^2
V_p	395 m^3
$P_{\rm dens}$	$4.97\times10^6~\mathrm{W}\cdot\mathrm{m}^{-1}$
p	$7.37 \times 10^5 \text{ Pa}$
n	$1.53 \times 10^{20} \text{ m}^{-3}$
B_0	4.57 T
β	8.85%
$ au_{E_{\min}}$	1.14 s

Table III: Obtained parameters by running Freidberg's model.

Note that C_F and C_I has been ommitted as these serve no purpose for this assignment. It is not of interest how expensive the plant will be. Rather the geometries and physical quantities are of interest. The results from the model is given in Table III.

B. Model sensitivity

At this point Freidberg has provided a model that produce some reasonable results for a powerplant. It could be interesting to see how this model behaves when some vital parameters are changed. In the last section the model used the parameters shown in Eq. (1). Now the model will be iterated over variations in the following parameters, while retaining the rest. The variable parameters are the electric power P_E , the maximum wall loading P_W , the maximum magnetic field B_{max} and the maximum stress σ_{max} . Appendix B includes the code for iterating the matlab model over various paremeters.

C. Elliptic Cross section

Freidberg's model assumes a circular cross section of the plasma. In reality this is not the case, and as of such we will now make a more realistic, yet still approximate reactor for an elliptic plasma cross section.

ACKNOWLEDGMENTS

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¹ https://www.iter.org/.

² Jeffrey P. Freidberg, *Plasma physics and fusion energy* (Cambridge University Press, 2007).

LIST OF FIGURES

LIST	\mathbf{OF}	$T\Lambda$	$\mathbf{R}\mathbf{I}$	$\mathbf{E}\mathbf{S}$
1/10/1	()r	1 /4	DI.	, ,,,,

I	Quantities calculated by the model in Freidberg's ²	2
II	Variables in the Freidberg's model	
III	Obtained parameters by running Freidberg's model	5

LISTINGS

Appendices

Appendix A: tokamakDTU_asign_1

```
Name:
                    tokamakDTU
3
      Version:
                    1.0
4
5
                    Contains the function 'tokamakDTU' which gives parameters
      Purpose:
6
                    for a tokamak fusion power plant as output based on a
                    simplified model. The equations used are derived in
8
                    chapter 5 in Friedberg, Plasma physics and Fusion
9
                    Energy, 2007 (all references are referring thereto).
10
11
     To do (NOT for 10401 - Fusion Energi students):
12
                 1. Rewrite the code to a class (this is not done on purpose so
13
                    that the code is more readable for students not familiar
14
                    with classes). Can from that merge the files which takes
15
                    R_0/a and/or the ellipticity as an input into one file.
16
17
      Changelog:
18
                 1. December 2014:
19
                    Written by Michael Løiten based on a similar code written
20
                    as a bachelor project by Elias Pagh Sentius
                    mailto: mmag@fysik.dtu.dk
22
23
24
    function [b, c, a, R_0, A, A_p, V_p, P_dens, p, n, B_0, beta, tau_E_min,...
25
              C_per_watt] =...
26
        tokamakDTU_asign_1(...
27
            n_flux_fraction, C_F, C_I, P_E, P_W, B_max, sigma_max, eta_t)
28
```

```
TOKAMAK_DTU Function which returns the parameters of a power plant
29
30
    % Output parameters
31
32
    % b
                  - Blanket/shield thickness [m]
33
                  - Magnet coil thickness [m]
     С
34
                  - Minor radius [m]
35
     a
    % R_0
                  - Major radius [m]
36
      Α
                  - Aspect ratio []
37
    % A_p
                  - Plasma surface [m^2]
38
                  - Plasma volume [m^3]
    % V_p
39
                 - Power density [W/m]
    % P_dens
40
                  - Plasma pressure [Pa]
    % p
41
                  - Particle density [m^-3]
42
                  - Magnetic field at magnetic axis [T]
    % B_0
43
                 - Plasma beta in the centre []
    🕻 beta
44
    m \langle tau_E_min - Min confinement time for satisfaction of (psttau_E)_min [s]
45
     C_per_watt - The cost of the powerplant [$]
46
47
     Input parameters
48
49
     n_flux_fraction - n flux in breeder end/n flux in breeder start []
50
                       - Fixed cost propotionality constant [$]
    % C_F
51
                       - Nuclear island cost propotionality constant [$W/m^3]
    % C_I
52
    % P_E
                       - Desired output power [MW]
53
                       - Maximum wall load [MW/m^2]
    % P_W
54
                       - Magnetic field at the edge of the coil [T]
    % B_max
55
    % sigma_max
                       - Tensile strenght of the magnetic field coils [atm]
56
                       - Energy conversion efficiency []
     eta_t
57
58
59
     The function starts by defining fixed constants
60
```

```
R. K. F. Wiuff
```

```
Note that this is inefficient if we are looping over the function, but it
61
     makes the code easier to use, as these are not needed as input parameters
62
63
   K Fixed constants
64
    65
    % Nuclear
66
67
   % Energies
68
              = 2.5e-8; % [MeV] Energy of slow (thermal) neutron (eq 5.6)
   E_t
69
              = 14.1;
                       % [MeV] Neutron energy after fusion (eq 2.17)
70
              = 3.5;
                       % [MeV] alpha energy after fusion (eq 2.17)
   E_a
71
   E_Li
              = 4.8;
                       % [MeV] Heat produced by breeding Li (under eq 4.31)
72
   % Cross section and main free paths
73
   sigma_v_avg = 3.0e-22;% [m^3/s] DT fusion cross section 0 15keV (table 5.2)
74
              = 0.0031; % [m] Breeding mean free path (under eq 5.7)
   lambda_br
75
   lambda_sd
              = 0.055; % [m] Mean free path from sigma_sd (eq 5.3)
76
77
   % Plamsa physics
78
79
   % Parameters for infinity gain at the minimum of p tau_E (eq 4.20)
80
               = 15.0; % [keV] Temparature for obtaining min tripple product
81
   tripple_min = 8.3; % [atm s] Min tripple prod to obtain Q=inf 0 T=15 keV
82
83
   % Natural constants
84
85
                            % Vacuum permeability [T*m/A]
   mu_0 = 4.0*pi*1e-7;
86
                           % Elementary charge [C]
   e = 1.602176565e-19;
87
   88
89
90
   \% Secondly we convert everything to SI units, so that the variables are
91
     easier to handle
92
```

```
% Again, this is computationally inefficient, but it suffices for our use
93
     Conversion to SI-units
94
    95
    % Conversion factors
96
   W_per_MW
              = 1.0e6;
97
   Pa_per_atm
               = 1.01325e5;
98
   eV_per_keV
               = 1.0e3;
99
   eV_per_MeV
               = 1.0e6;
100
   J_per_eV
               = e;
101
   J_per_keV
              = J_per_eV * eV_per_keV;
102
   J_per_MeV
103
              = J_per_eV * eV_per_MeV;
   % Conversions
104
   P_E
                                      % Desired output power
              = P_E * W_per_MW;
105
   P_W
              = P_W * W_per_MW;
                                      % Wall Loading limit on first wall
106
              = E_t * J_per_MeV;
                                      % Energy of slow (thermal) neutron
   E_t
107
                                      % Neutron energy after fusion
   E_n
              = E_n * J_per_MeV;
108
                                      % alpha energy after fusion
   E_a
              = E_a * J_per_MeV;
109
   E_Li
              = E_Li * J_per_MeV;
                                      % Heat produced by breeding Li
110
   sigma_max
               = sigma_max * Pa_per_atm;  % Max allowable structural stress
111
               T * J_per_keV;
                                      % Temparature for minimum p*tau_E
112
   113
    114
115
116
   % Calculate the geometrical factors
117
118
   % Find the breeder thickness
119
   b = get_b(lambda_sd, E_n, E_t, lambda_br, n_flux_fraction);
120
    % Find the minor plasma radius and the coil thickness
121
    [a, c] = get_a_and_c(B_max, mu_0, sigma_max, b);
122
    % Find the major radius
123
   R_0 = get_R_0(a, eta_t, E_n, E_a, E_Li, P_E, P_W);
```

```
K Find the resulting geometrical factors
125
       = R_0/a;
                                        % Aspect Ratio
126
    A_p = (2.0*pi*a)*(2.0*pi*R_0);
                                        % Plasma surface area
    V_p = (pi*a^(2.0))*(2.0*pi*R_0); % Plasma volume
128
129
130
     Calculate the plasma physics parameters
131
132
     \% Find the power density {	t in} the plasma
133
    P_dens = get_P_dens(E_a, E_n, E_Li, P_E, eta_t, V_p);
134
    % Find the plasma pressure
135
    p = get_p(E_a, E_n, P_dens, T, sigma_v_avg);
136
    % Calculate the density from the definition of p under eq 5.36
137
    n = p/(2.0*T);
138
     % Find the magnetic field strength on the magnetic axis
139
    B_0 = get_B_0(R_0,a,b,B_max);
140
     % Find the plasma beta on the magnetic axis
141
    beta = get_beta(p, B_0, mu_0);
142
     % Find the minimum required confinement time from the definition of the
143
     % minimum tripple product.
144
     NOTE: A higher confinement time is advantegous, and could in principle
145
      yield a smaller (and cheaper) reactor. However, the effect is not
146
     included in this model
147
    tau_E_min = tripple_min/p;
148
150
    % Calculate the cost
151
      (details about the cost can be found in the function get_a_and_c)
152
153
     Find the volume of the nuclear island
154
     (the material surrounding the plasma)
155
    V_I = get_V_I(R_0,a,b,c);
156
```

```
Find the reactor volume per power out
157
     % In the current model, this is the only non-constant in the expression for
158
     % cost per watt
159
    V_I_per_P_E = V_I/P_E;
160
    C_per_watt = get_C_per_watt(C_F, C_I, V_I_per_P_E);
161
    end
162
164
165
    function [b] = get_b(lambda_sd, E_n, E_t, lambda_br, n_flux_fraction)
166
     GET_B Calculates b from the need of slowing down and breeding neutrons
167
168
    \% Thickness of the moderator-breeding region so that 1 - n_flux_fraction
169
     % have slowed down and undergone a breeding reaction
      [m]
171
     % Equation 5.10
172
    delta_x = 2.0*lambda_sd*...
173
               log(1.0-(1.0/2.0)*(E_n/E_t)^(1.0/2.0)*...
                     (lambda_br/lambda_sd)*log( n_flux_fraction )...
175
                   );
176
      Set b from delta_x
178
     % = 0.000 Friedberg argues above equation 5.11 that b should be between 1 and 1.5 m
179
     % Therefore a self chose constant is set to 0.38
180
    self_chosen_constant = 0.32;
181
    b = delta_x + self_chosen_constant;
182
    end
183
184
185
186
187
    function [a,c] = get_a_and_c(B_max, mu_0, sigma_max, b)
188
```

```
GET_A_AND_C Calculates a and c
189
190
    % c is obtained from requiring that the magnets are so thin that they are
191
     on the limit of the tensile strenght
192
     % a is obtained from minimizing the costs
193
194
     % xi defined when making the magnetic coil c as thin as possible
195
     % Under equation 5.27
196
    xi = B_{max}(2.0) / (4.0*mu_0*sigma_max);
197
198
    % a is found from optimization of the cost, where
199
    % total cost = fixed cost + nuclear island cost
200
     %...........
201
     % Fixed cost
202
203
     % K_F = Fixed cost for building, turbines, generators etc (also applies to
204
     % fusion, fission, fossil)
205
      Assumption: The fixed cost is proportional to power output:
206
     % Equation 5.13
207
     K_F = C_F*P_E;
208
209
     Nuclear island cost (mainly cost of magnets, blanket and shield)
210
211
     % Assumption: The proportional to reactor volume:
212
    % Equation 5.14
213
    K_I = C_I*V_I;
214
      Equation 5.15
215
      V_I = 2.0*pi^(2.0) * R_0 * ((a+b+c)^(2.0) - a^(2.0)); % Reactor volume
216
217
     % Cost per watt:
218
219
     % Defined as C_p_watt = (K_F + K_I)/P_E, rewritten to
```

```
% C_p_watt = C_F + C_I*(V_I/P_E);
221
     Since the cost per watt contains two constants, we can minimize the
222
     % V_I/P_E in order to optimize the cost
223
     Given by equation 5.20 inserted in 5.17
224
     Equation 5.21
225
     % V_I_per_P_E = V_I/P_E; % Reactor volume per power out
226
     \frac{1}{6} a is found by setting the derivative of V_I_per_P_E = 0
     % Equation 5.29
228
    a = ((1.0 + xi)/(2.0*xi^(1.0/2.0))) * b;
229
230
    % Knowing xi, a, and, b, we can calculate c
231
    % c found by comparing tensile force and magnetic force working on the coil
232
    % Equation 5.27
233
    c = 2*xi/(1-xi)*(a+b);
    end
235
236
237
238
    function [R_0] = get_R_0(a, eta_t, E_n, E_a, E_Li, P_E, P_W)
239
     GET_R_0 Calculate the major radius
240
     \% Divide eq 5.18 (electric power out) by
242
     % = 0.00 eq 5.19 (wall loading * area = total neutron production) and solve for R0
243
     % Equation 5.20
244
    R_0 = (1.0/(4.0*pi^(2.0)*eta_t))*(E_n/(E_n + E_a + E_Li))*(P_E/(a*P_W));
245
    end
246
247
248
249
    function [P_dens] = get_P_dens(E_a, E_n, E_Li, P_E, eta_t, V_p)
250
     GET_P_DENS Calculate the power density
251
```

```
7 The power density is found by the sum of the power from the alphas plus
253
     the power from the neutrons, divided by the plasma volume
254
     % Equation 5.35
255
     P_{dens} = (E_a + E_n)/(E_a + E_n + E_Li)*P_E/(eta_t*V_p);
256
257
258
259
260
    function [B_0] = get_B_0(R_0, a, b, B_max)
261
     \% {
m GET\_B\_0} Calculte the magnetic field strength on the magnetic axis
262
263
    % B_{max} is found in the edge of the magnet (at R = R_0-a-b)
264
     % BO is the magnetic field at RO
265
     % As B propto 1/R. we have that B_0/B_{max} = (R_0-a-b)/R_0, which leads to
266
     % Equation 5.42
267
    B_0 = ((R_0-a-b)/R_0)*B_max;
268
     end
269
270
271
272
     function [beta] = get_beta(p, B_0, mu_0)
273
     GET_beta Calculte the magnetic field strength on the magnetic axis
274
275
     \% Plasma beta {	ext{in}} the center (kinetical pressure over magnetical pressure):
276
     % Equation 5.43
     beta = p / (B_0^2/(2.0*mu_0));
278
     end
279
280
281
282
    function [p] = get_p(E_a, E_n, P_dens, T, sigma_v_avg)
283
     GET_P Calculate the plasma pressure
```

311

```
285
      Found from solving the sum of neutron and alpha power for n, and multiply
286
      the result with T
287
     % Equation 5.37
288
    p = ((16.0/(E_a + E_n)) * P_dens)^(1.0/2.0)*...
289
          (T^{(2.0)}/sigma_v_avg)^{(1.0/2.0)};
290
    end
291
292
294
    function [V_I] = get_V_I(R_0, a,b,c)
295
     \c GET_V_I Calculate the volume of the material surrounding the plasma
296
     % Equation 5.15
298
    V_I = 2.0*pi^(2.0) * R_0 * ((a+b+c)^(2.0) - a^(2.0));
299
    end
300
301
302
303
    function [C_per_watt] = get_C_per_watt(C_F, C_I, V_I_per_P_E)
304
     GET_C_PER_WATT Calculates the cost for one watt out from the power plant
305
306
     % For details in how the cost is derived, see comments in the function
307
     % get_a_and_c
309
    C_{per_watt} = C_F + C_I*(V_I_per_P_E);
310
```

Appendix B: IterateTokamakDTU

```
close;
1
    clear;
2
3
    titl = ["Desired output power [MW]", "Maximum wall load [MW m^-2]",...
4
        "Magnetic field at the edge of the coil [T]",...
5
        "Tensile strenght of the magnetic field coils [atm]"];
6
    foldertitl = ["DesiredOutputPower", "MaximumWallLoad",...
7
        "MagneticFieldAtTheEdgeOfTheCoil",...
8
        "TensileStrenghtOfTheMagneticFieldCoils"];
   1 = 5;
10
   p1 = [];
11
    x = [];
12
    mkdir('../MatlabFigures', foldertitl(1))
13
14
    for i = 2000:5000
15
        [b, c, a, R_0, A, A_p, V_p, P_dens, p,...
16
            n, B_O, beta, tau_E_min, C_per_watt] = ...
^{17}
            tokamakDTU_asign_1(0.01, 1, 2, 1000, 4, 13, 3000, 0.4);
18
        q=[b, c, a, R_0, A, A_p, V_p, P_dens, p,...
19
            n, B_0, beta, tau_E_min, C_per_watt];
20
        p1=cat(1,p1,q);
21
        x=cat(1,x,i);
22
    end
23
24
    T = ["Blanket-shield thickness [m]", "Magnet coil thickness [m]"...
25
        "Minor radius [m]", "Major radius [m]", "Aspect ratio []"...
26
        "Plasma surface [m^2]", "Plasma volume [m^3]", "Power density [W m^-1]"...
27
        "Plasma pressure [Pa]", "Particle density [m^-3]",...
28
        "Magnetic field at magnetic axis [T]", "Plasma beta in the centre []"...
29
        "Min confinement time for satisfaction of (p tau_E)_min [s]",...
30
```

```
"The cost of the powerplant [$]"];
31
    fileT = ["Blanket-shieldThickness", "MagnetCoilThickness"...
32
        "MinorRadius", "MajorRadius", "AspectRatio"...
33
        "PlasmaSurface", "PlasmaVolume", "PowerDensity"....
34
        "PlasmaPressure", "ParticleDensity",...
35
        "MagneticFieldAtMagneticAxis", "PlasmaBetaInTheCentre"...
36
        "MinConfinementTime",...
37
        "TheCostOfThePowerplant"];
38
    for k = 1:14
39
        q = figure;
40
        y = p1(:,k);
        CM = jet(14);
42
        plot(x, y,'color', CM(k,:));
43
        ylabel(T(k));
44
        xlabel(titl(1));
45
        ytickformat('%.2f');
46
        epsfilename = sprintf('%s.eps',fileT(k));
47
        foldername = sprintf('../MatlabFigures/%s', foldertitl(1));
48
        fullfilename = fullfile(foldername,epsfilename);
49
        saveas(q, fullfilename, 'epsc')
50
    end
```