

Common-mode input
Voltage

if $V_1 = V_2$

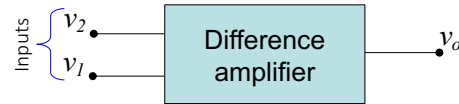
$$V_{cm} = \frac{V_1 + V_2}{2}$$

then would
 $V_o = 0$?

$$V_o = A_v \cdot V_d$$

Differential Amplifier: Basic Idea

- Most widely used building block in analog integrated circuit
- Basis of very-high-speed logic circuit family



- Ideally V_o is proportional to $(V_2 - V_1)$
- $V_o = A_v(V_2 - V_1)$
- Here, A_v = open-loop voltage gain
- If $V_1 = V_2$, the input voltage is called **common-mode input voltage**, denoted by V_{cm}
- If $V_1 = V_2$, $V_{cm} = V_1 = V_2$ and

$$V_{cm} = \frac{V_1 + V_2}{2}$$

- $(V_2 - V_1) = V_d$
- V_d = differential input voltage

$$\therefore V_o = A_v V_d$$

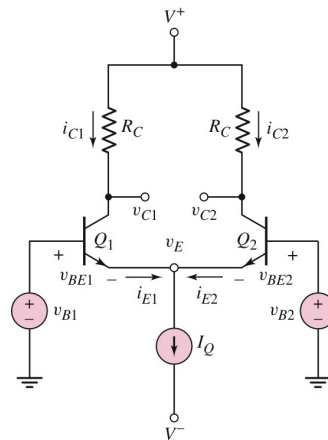
Handwritten notes in a box:

- $A_v = \frac{V_o}{V_d}$ (with V_o labeled as output voltage and V_d as differential input voltage)
- open loop voltage gain

1

A BJT Differential Pair Circuit

- The **difference of the two input signals**, V_{B1} and V_{B2} will be amplified at the output ✓
- For both transistors, the **B-E junctions are forward biased** and the **C-E junctions are reversed biased**, i.e., the transistors operate in active region.
- If the input signals become zero, i.e., $V_{B1} = V_{B2} = 0$, the transistors will still remain in the active region because of the current source.
- Both transistors **must remain in active region** for differential amplifier operation



BE is fwd
CE is rev

2

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Differential Pair: Basic Operation (Case-A)

- Q_1 and Q_2 are identical
- Q_1 and Q_2 are in active region
- The circuit has a floating ground
- Here, both transistors are ON
- The current source I is ideal

$$i_{E1} = i_{E2} = I/2$$

$$i_{C1} = i_{C2} = (\alpha I)/2$$

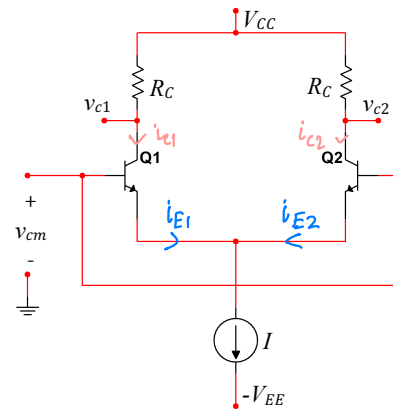
$$V_{E1} = V_{E2} = (V_{cm} - V_{BE})$$

or, $V_{E1} = V_{E2} \approx (V_{cm} - 0.7)$

$$V_{C1} = V_{C2} = V_{cc} - \left(\frac{\alpha I}{2}\right) R_C$$

$$V_{C1} - V_{C2} = 0$$

$V_{C1} - V_{C2} = 0$ remains valid for any values of V_{cm} as long as Q_1 and Q_2 remain in active region.



Thus differential pairs REJECT the common mode input signal.

$$I = i_{E1} + i_{E2}$$

$$I = 2 i_E$$

$$i_E = \frac{I}{2}$$

- differential pairs usually in practice don't work in common-mode

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Differential Pair: Basic Operation (Case-B)

- Q_1 and Q_2 are identical
- The current source is ideal
- Transistor Q_1 is ON
- Transistor Q_2 is OFF

$$V_{E1} = V_{E2} \approx 1 - 0.7 = 0.3 \text{ V}$$

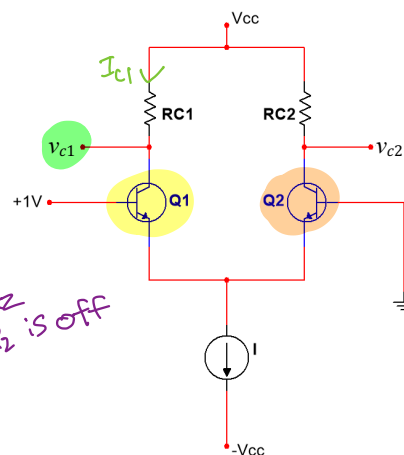
$$i_{C1} = \alpha I \quad \text{and} \quad i_{C2} = 0 \quad \leftarrow \begin{matrix} i_{C2} \text{ is off} \\ Q_2 \text{ is off} \end{matrix}$$

$$V_{C1} = V_{CC} - \alpha I R_C \quad \text{and} \quad V_{C2} = V_{CC}$$

$$\text{Thus, } V_{C2} - V_{C1} = \alpha I R_C \approx I R_C$$

$$v_{C2} \approx 1$$

$$* V_{C2} - V_{C1} = I R_{C1}$$



- there will be output in cases B and C

4

4

↙ opposite of case B

Differential Pair: Basic Operation (Case-C)

- Q1 and Q2 are identical
- The current source is ideal
- Transistor **Q1 is OFF**
- Transistor **Q2 is ON**
- $V_{BE2} \approx 0.7 \text{ V}$
- $V_{E1} = V_{E2} \approx -0.7 \text{ V}$
- $V_{BE1} = -1 - (-0.7) = -0.3 \text{ V}$
- $I_{C2} = \alpha I$ and $I_{C1} = 0$
- $V_{C2} = V_{CC} - \alpha I R_C$ and $V_{C1} = V_{CC}$

Thus, $V_{C2} - V_{C1} = -\alpha I R_C \approx -I R_C$

$V_{C2} - V_{C1} = -I R_C$

-check which is more +ve, that would be ON

5

5

end here

Fri Oct 27

Determine the collector currents in each circuit

cuz $-1 > -2$

No R_{C2}

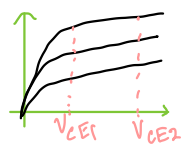
$-V_{CE}$'s are equal if collector resistors are equal

Effect of V_A ?

6

6

there is an effect



$-V_A$ affects r_o in small signal analysis

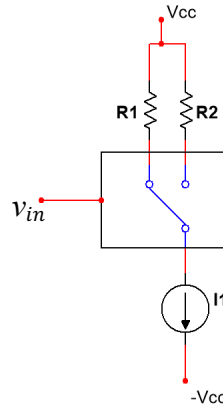
$$r_o = \frac{V_A}{I_C}$$

can perform
very fast switching

*go to
textbook

Differential Pair as a Switch

- A change in input signal can switch the transistors
- A single-pole double-throw (SPDT) switch
- A small signal can steer the current



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Q7

-how exactly
does it work?
-ex question?

~Simply diagram
of last slide

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Transfer Characteristics

Consider a BJT differential pair

$$i_{C1} = I_S e^{\left(\frac{v_{B1} - v_{E1}}{v_T}\right)} \dots \dots \dots (1)$$

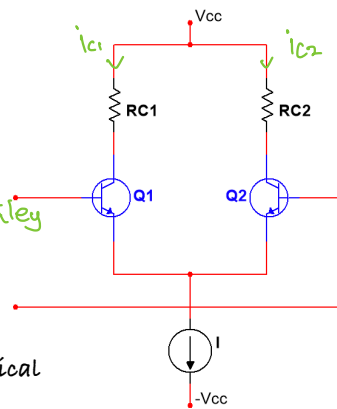
$$i_{C2} = I_S e^{\left(\frac{v_{B2} - v_{E2}}{v_T}\right)} \dots \dots \dots (2)$$

Shockley

Assumed that the two transistors are identical and operating at the same temperature.

Dividing eq(1) by eq(2), we have, $v_{E1} = v_{E2}$

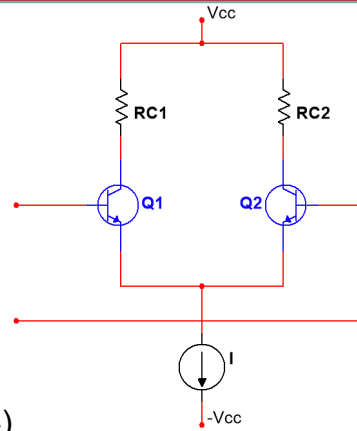
$$\frac{i_{C1}}{i_{C2}} = e^{\left(\frac{v_{B1} - v_{B2}}{v_T}\right)} = e^{\left(\frac{v_{id}}{v_T}\right)} \dots \dots \dots (3)$$



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Transfer Characteristics (Continued ...)



$i_{C1} = i_E$

One can manipulate equation (3) to yield

individual \rightarrow $\frac{i_{C1}}{i_{C1} + i_{C2}} = \frac{i_{C1}}{I} = \frac{1}{1 + e^{-\left(\frac{v_{id}}{v_T}\right)}} \dots \dots (4)$

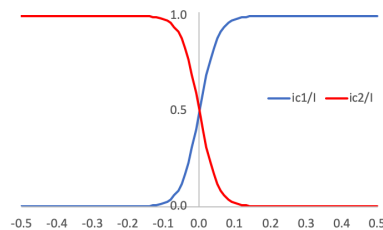
total \rightarrow

$$\frac{i_{C2}}{i_{C1} + i_{C2}} = \frac{i_{C2}}{I} = \frac{1}{1 + e^{\left(\frac{v_{id}}{v_T}\right)}} \dots \dots (5)$$

9

9

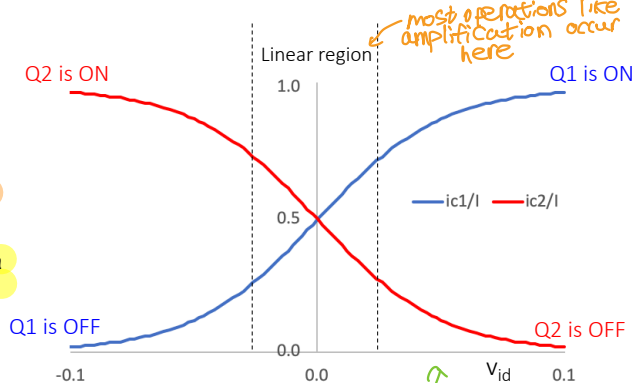
Transfer Characteristics (Continued ...)



- The amplifier responds only to v_{id} . Hence, a difference amplifier
- When $v_{id} = 0$, I divides equally
- $v_{id} \approx 100$ mV can switch the current (Thus, fast switching)
- In the linear region the gain is proportional to the slope

$$v_{id} = V_{be1} - V_{be2}$$

- In order to maintain a linear amplifier, the excursion of v_{id} must be kept small
- For linear operation, v_{id} is limited to $V_T/2$ ($\approx \pm 12.5$ mV)



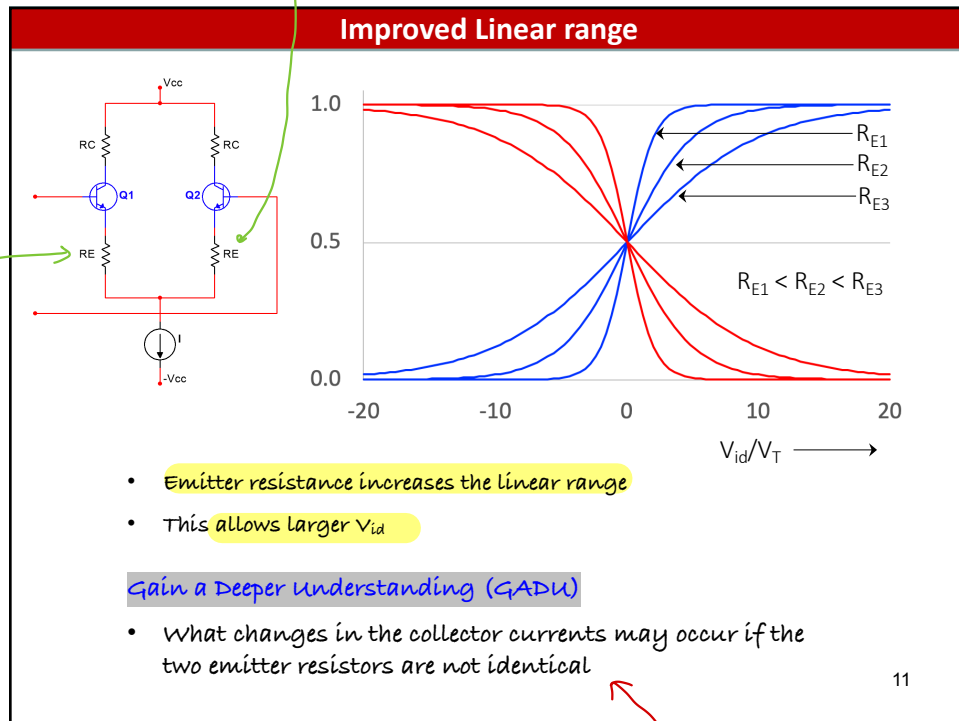
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* Memorise

outside linear region you are at risk of producing harmonics

R_E must be on both sides
and must be equal

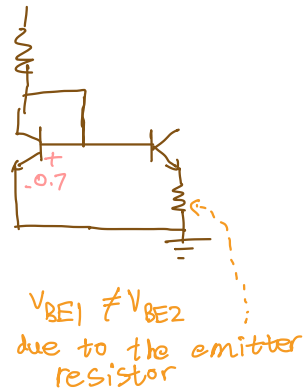
To increase
linear region
add R_E
 $\therefore 12.5$ is no
longer valid



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- what are the
changes??

- might not be symmetrical



Example: Differential Pair

Example: $|V_{BE}|$ of a conducting transistor is $0.7V$ and $\alpha \approx 1$.

Find a) V_E , b) i_{C1} and i_{C2} , c) V_{C1} and V_{C2} , and d) V_{CE1} and V_{CE2} .

Solution:

Here, **Q1 is ON** and **Q2 is OFF**

a) $V_{BE} = V_{B1} - V_E$ $V_{BE} = -0.7$

or, $V_E = V_{B1} - V_{BE}$

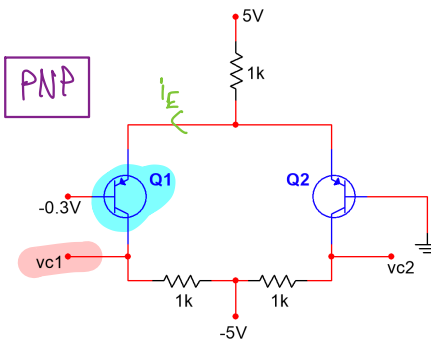
or, $V_E = -0.3 - (-0.7) = 0.4V$

b) $i_E = (5 - 0.4) / 1 \times 10^3$

$i_E = 4.6 \text{ mA}$

Thus, $i_{C1} = 4.6 \text{ mA}$, $i_{C2} = 0$

$\therefore I_C = \alpha I_E$



c) $V_{C1} = -5 + 4.6 \times 1 = -0.4$

$V_{C2} = -5V$

d) $V_{CE1} = -0.4 - 0.4 = -0.8V$ $-0.8V$

$V_{CE2} = -5 - 0.4 = -5.4V$

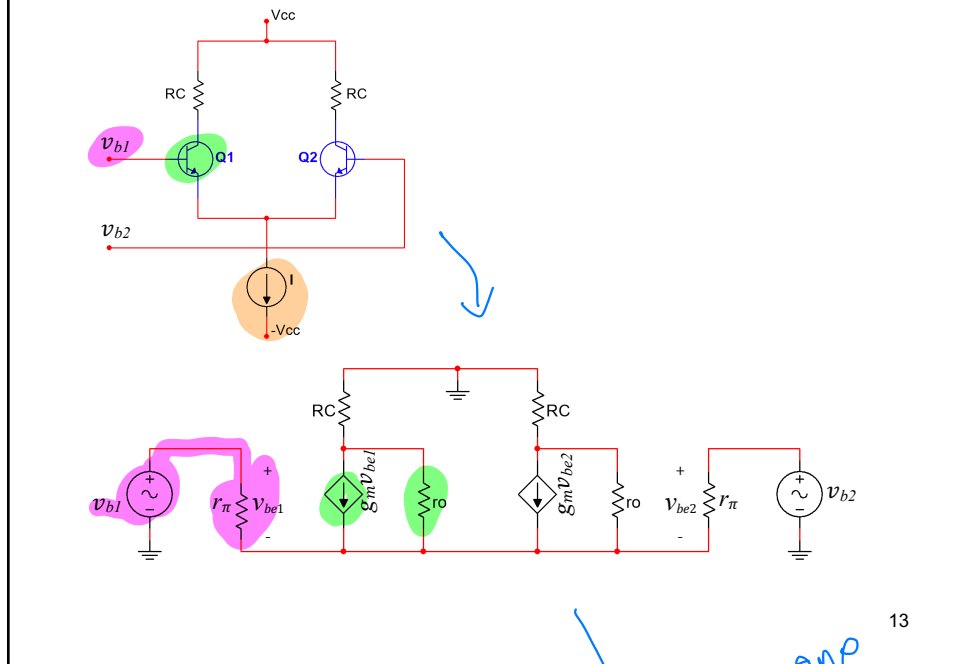
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Steps

- ① Determine state of each transistor
- ② Find V_E , i_E , V_{C1} , V_{C2}

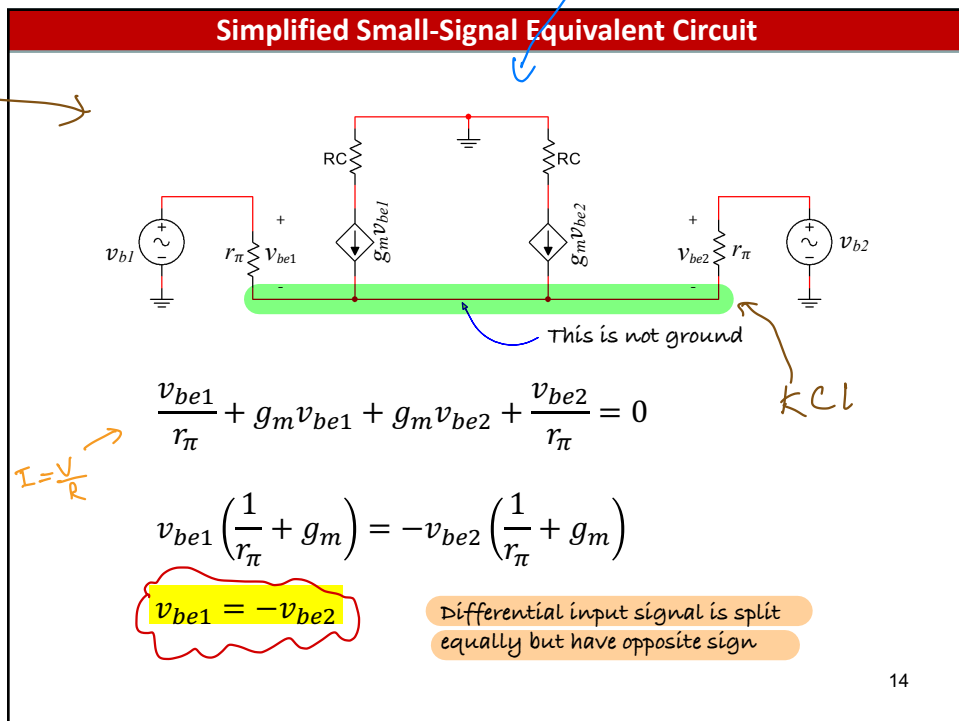
A BJT Differential Pair Circuit



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r_o is gone
- since $V_A = \infty$

Simplified Small-Signal Equivalent Circuit



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differential input signal = $V_{id} = V_{be1} - V_{be2}$

Differential Input and Common-Mode Input

v_{b1} v_{b2}

$v_{id} = v_{be1} - v_{be2}$

v_{id} v_{cm}

Q12 - how is this equivalent?

$v_{id} = v_{be1} - v_{be2} = v_{be1} - (-v_{be1}) = 2v_{be1}$

$v_{be1} = \frac{v_{id}}{2}$

Similarly,

$v_{be2} = -\frac{v_{id}}{2}$

← found in previous slides

$V_{cm} = \frac{V_1 + V_2}{2}$

$V_{id} = V_{be1} - V_{be2}$

***quiz 3 until here**

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Mon Nov 6th

Single Ended Voltage Gain

$$v_{c1} = -(g_m R_C)(v_{be1}) = -\frac{1}{2} g_m R_C v_{id}$$

$A_{d1} \equiv \frac{v_{c1}}{v_{id}} = -\frac{1}{2} g_m R_C$

$v_{be1} = \frac{1}{2} v_{id}$

Notice, the gain is negative, which is the same as **CE amplifier**

$v_{be1} = -v_{be2}$

$$v_{c2} = -(g_m R_C)(v_{be2}) = +\frac{1}{2} g_m R_C v_{id}$$

$A_{d2} \equiv \frac{v_{c2}}{v_{id}} = \frac{1}{2} g_m R_C$

results in +ve gain

Notice, the gain is positive

A_{d1} and A_{d2} are single ended gain

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Differential Voltage Gain

Differential gain, $A_d = A_{d1} - A_{d2}$

$$A_d = -\frac{1}{2}g_m R_C - \frac{1}{2}g_m R_C$$

$$A_d = -g_m R_C$$

If defined as, $A_d = A_{d2} - A_{d1}$

$$A_d = \frac{1}{2}g_m R_C - \left(-\frac{1}{2}g_m R_C\right)$$

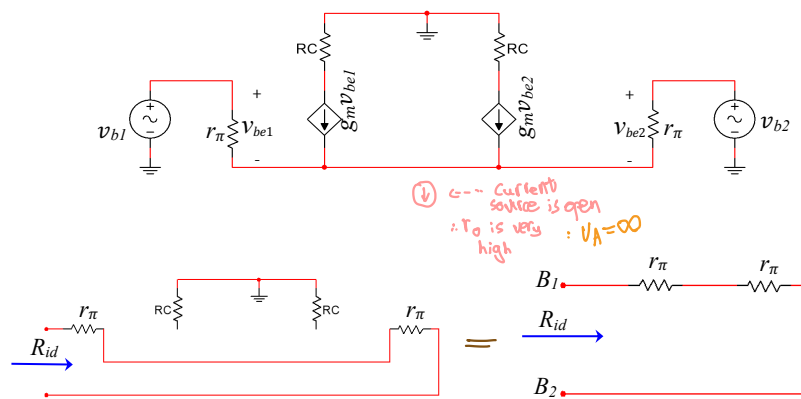
$$A_d = g_m R_C$$

no need to memorise

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Differential Input Resistance



Differential resistance, $R_{id} = 2r_\pi$

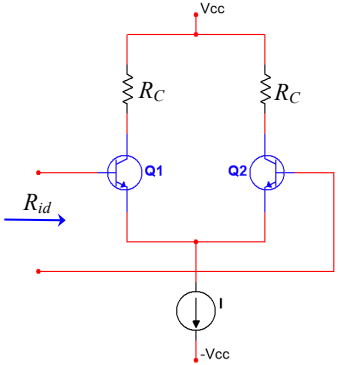
$$\text{or, } R_{id} = 2(\beta + 1)r_e$$

$$r_e = (\beta + 1)r_e$$

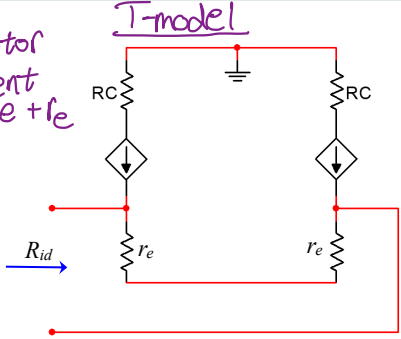
18

18

Differential Input Resistance



Transistor
= current
source + r_e



T-model

$R_{id} = 2r_{\pi}$

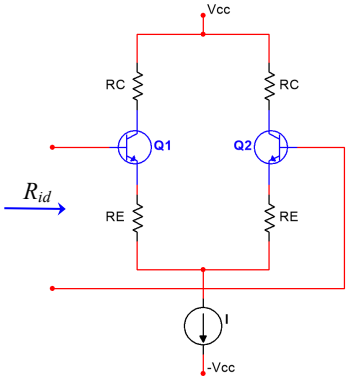
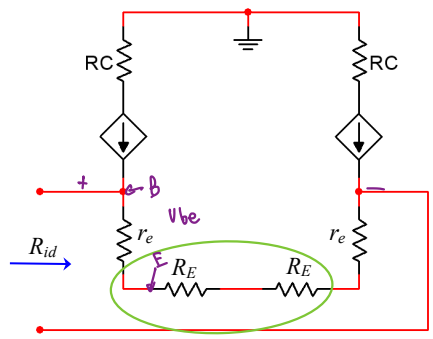
Differential resistance, $R_{id} = 2(\beta + 1)r_e$

$\therefore r_{\pi} = (\beta + 1)r_e$

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Differential Input Resistance With Emitter Resistor R_E

Differential resistance, $R_{id} = 2(\beta + 1)(r_e + R_E)$

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go over example again

Example: Differential Pair

Example: Given that $V_{id} = 0.1V$, $R_E = 100\ \Omega$, $R_C = 5k$, $I = 2\text{ mA}$, $\alpha = 1$, and $\beta = 100$. $|V_{BE}|$ of a conducting transistor is $0.7V$.

Find a) i_E and V_{be} , b) total emitter current, c) signal voltage at each collector, d) differential voltage gain ($V_{od} = V_{C1} - V_{C2}$), and e) differential input resistance R_{id} .

Solution:

a) $r_e = V_T / I_E = 25/1 = 25\ \Omega$

Here, $i_E = V_{id} / 2(r_e + R_E)$

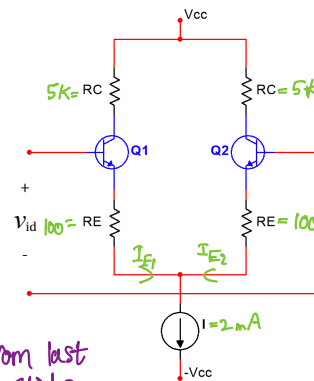
or, $i_E = 0.1 / 2(25 + 100) = 0.4\text{ mA}$

$V_{be1} = r_e \times i_E = 25 \times 0.4 \times 10^{-3}$

or, $V_{be1} = 10\text{ mV}$

and, $V_{be2} = -V_{be1}$

or, $V_{be2} = -10\text{ mV}$



b) $i_{E1} = I/2 + 0.4\text{ mA} = 1.4\text{ mA}$

and $i_{E2} = I/2 - 0.4\text{ mA} = 0.6\text{ mA}$

Note that $i_{E1} + i_{E2} = I$

how??

$$i_{E1} = \frac{I}{2} + i_E$$

$$i_{E2} = \frac{I}{2} - i_E$$

- due to diagram on prev slide
- follow current flow

- why is V_{be} not 0.7??

- since it's done in small signal analysis, not DC

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Example: Differential Pair (Continued ...)

Example: Given that $V_{id} = 0.1V$, $100\ \Omega$, $R_C = 5k$, $I = 2\text{ mA}$, $\alpha = 1$, and $\beta = 100$. $|V_{BE}|$ of a conducting transistor is $0.7V$.

Find a) i_E and V_{be} , b) total emitter current, c) signal voltage at each collector, d) differential voltage gain ($V_{od} = V_{C1} - V_{C2}$), and e) differential input resistance R_{id} .

Solution:

c) $V_{C1} = -i_{C1} R_C \approx -i_{E1} R_C = -0.4\text{ mA} \times 5k$

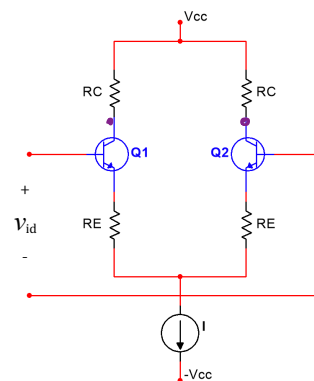
$V_{C1} \approx -2V$

Similarly, $V_{C2} = +i_{C2} R_C \approx 2V$

d) $V_{od} = (V_{C1} - V_{C2}) / V_{id}$

or, $V_{od} = (-2 - 2) / 0.1 = -40$

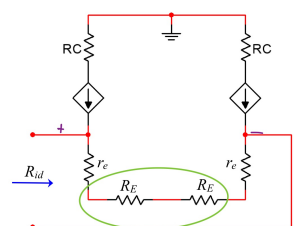
diff voltage gain



e) $R_{id} = 2(\beta + 1)(r_e + R_E)$

$R_{id} = 2(25 + 100) \times 101$

$R_{id} = 25\text{ k}\Omega$



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differential voltage gain = $\frac{V_{od}}{V_{id}}$

- know how to use equations in upcoming slides, no need to know derivation

Common-Mode Gain

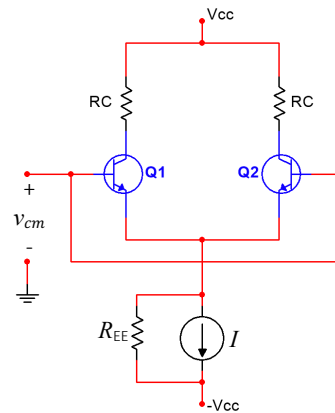
Ideally, the common-mode gain should be zero.

Because $V_{C1} - V_{C2} = 0$

However, it has a nonzero value in practice

$$A_{cm} \approx \frac{\Delta R_C}{2R_{EE}}$$

Here, R_{EE} = internal resistance of the current source



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CMRR and Common-Mode Input Resistance

CMRR (Common-Mode Rejection Ratio)

$$CMRR = 20 \log \left| \frac{A_d}{A_{cm}} \right| \text{ dB}$$

The common-mode input resistance

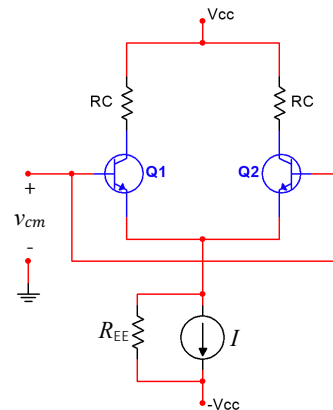
R_{icm} is given by

$$R_{icm} = (\beta + 1) \left[(R_{EE}) \parallel \left(\frac{r_o}{2} \right) \right]$$

output resistance of individual transistor

Here, R_{EE} = internal resistance of the current source

and $r_o = r_{o1} = r_{o2}$ = output resistance



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* solve at home *

Example: Differential Pair

Example: Given that $V_A = 100\text{ V}$ and $\beta = 100$. Find a) input differential resistance, R_{id} , b) overall differential, $|v_o/v_s|$, c) the worst-case A_{cm} if R_C has $\pm 1\%$ tolerance, and d) the input common-mode resistance, R_{icm} .

Solution:

a) $r_{e1} = r_{e2} = r_e = V_T/I_E = 25\text{ mV}/0.5\text{ mA}$

or, $r_e = 50\ \Omega$

$R_{id} = 2(\beta + 1)(r_e + R_E) = 40\text{ k}\Omega$

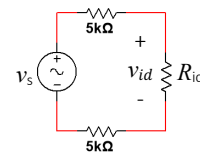
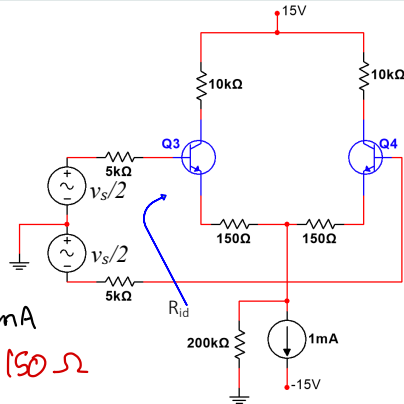
$R_E = 150\ \Omega$

- rounded

b) $v_{id} = v_s \frac{R_{id}}{5\text{ k}\Omega + 5\text{ k}\Omega + R_{id}}$

or, $v_{id} = v_s \frac{40 \times 10^3}{5\text{ k}\Omega + 5\text{ k}\Omega + 40 \times 10^3} = 0.8\ v_s$

or, $\frac{v_{id}}{v_s} = 0.8$



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Example: Differential Pair (continued ...)

voltage gain from the bases to the output ($v_{od} = v_{c1} - v_{c2}$) is

$$\left| \frac{v_{od}}{v_{id}} \right| = \frac{\text{total collector resistance}}{\text{total base resistance}}$$

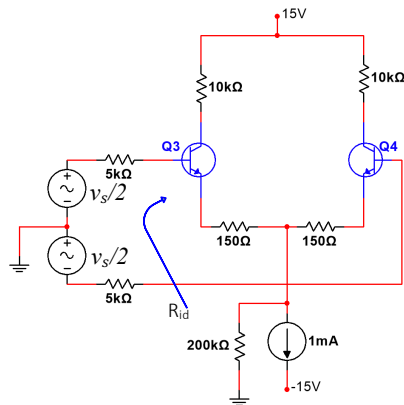
or, $\left| \frac{v_{od}}{v_{id}} \right| = \frac{2R_C}{2(r_e + R_E)} = \frac{20 \times 10^3}{2 \times 200} = 50$

50 150

Now,

$$\left| \frac{v_{od}}{v_s} \right| = \frac{v_o}{v_{id}} \times \frac{v_{id}}{v_s} = 50 \times 0.8 = 40$$

Thus, the overall voltage gain is 40



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Example: Differential Pair (continued ...)

c) With $\pm 1\%$ tolerance,

$\Delta R_{C(max)} = 2\%$ of R_C which is 200Ω .

Thus, the worst case A_{cm} is

$$A_{cm} = \frac{\Delta R_C}{2R_{EE}} = \frac{200}{2 \times 200 \times 10^3} = 5 \times 10^{-4}$$

d) We know,

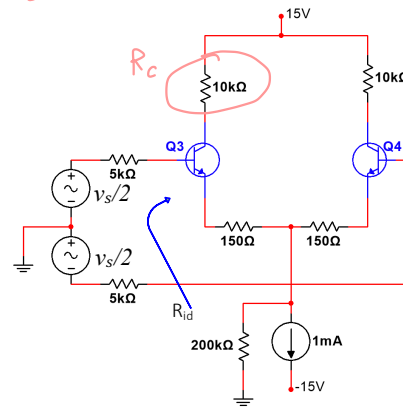
$$R_{icm} = (\beta + 1) \left[(R_{EE}) \parallel \left(\frac{r_o}{2} \right) \right]$$

Here, $r_o = (V_A) / (I/2) = 100 / (0.5 \times 10^{-3})$

or, $r_o = 200 \text{ k}\Omega$ **(r_o of Q_4)

Thus, $R_{icm} = 101(200 \text{ k} \parallel 100 \text{ k})$

or, $R_{icm} = 6.73 \text{ M}\Omega$



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very high

identical transistors → inherent parameters are equal → β, F_s

Example: Differential Pair

Example: Given that $V_A = 100 \text{ V}$ and $\beta = 100$. Find a) input differential resistance, R_{id} , b) overall differential, $|v_o/v_s|$, c) the worst-case A_{cm} if R_C has $\pm 1\%$ tolerance, and d) the input common-mode resistance, R_{icm} .

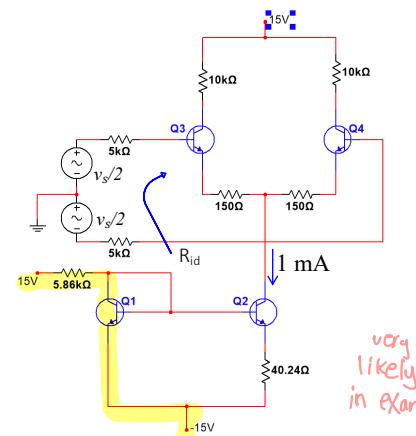
Solution:

R_{id} will remain the same ✓ $40 \text{ k}\Omega$

The overall gain will remain the same ✓ 40

The common-mode gain will have a different value

The common-mode input resistance will have a different value



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R_{EE} = output resistance of mirrored transistor

$$r_{o2} = \frac{V_A}{I_{C2}}$$

$$I_{C2} = \frac{15 - 0.7 - (-15)}{5.86 \times 10^3} = 5 \text{ mA}$$

$$\therefore r_{o2} = \frac{100}{5 \text{ mA}} = 20 \text{ k}\Omega$$

$$R_{icm} = (\beta + 1) \left[R_{EE} \parallel \frac{r_o}{2} \right]$$

$$= 101(20 \text{ k} \parallel 10 \text{ k})$$

$$= 673.3 \text{ k}\Omega$$

1% of $20 \text{ k} = 200$

$$A_{cm} = \frac{\Delta R_C}{2R_{EE}} = \frac{200}{2 \times 20 \text{ k}} = 5 \times 10^{-3}$$

common mode gain