

Power Amplifiers: Basic Idea

Multistage amplifiers deliver a large amount of power to the load

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graph LR
    Input[Input signal] --> A1[Amplifier-1]
    A1 --> A2[Amplifier-2]
    A2 -.- An[Amplifier-n]
    An --> Output[Output signal]
  
```

- For large current, load resistance is low (such as audio speaker)
- For large voltage, load resistance is high (such as switching power supply)

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Power Transistors

for power amplifiers:

- Larger area
- Different geometry
- Different doping concentration

Limiting factors

- Current
- Voltage
- Power
- Temperature

Temperature

- have fans
- have heatsinks

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Thermal runaway

Comparison Between Small-Signal and Power Transistors

Parameter	Small-signal 2N2222A	Power 2N3055	Power 2N6078
$I_{C(\max)}$ in A	0.8	15	7
$V_{CE(\max)}$ in V	40	60	250
$P_D(\max)$ in W	1.2	115	45
β	35-100	5-20	12-70

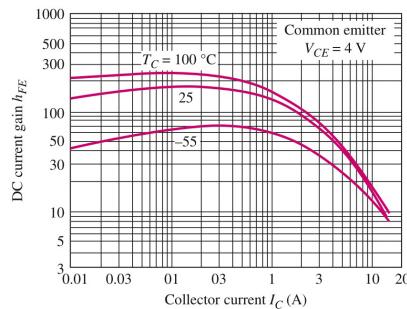
- Current gain (β) is generally low → compared to small-signal
- Notice that $I_{C(\max)} \times V_{CE(\max)} \neq P_D(\max)$

↑
 not simple multiplication * come in Exam



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Variation of β With Current and Temperature



- inc in current or temp decreases gain

- The current gain (β) decreases for higher currents
- The current gain (β) decreases with the increase of temperature

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Safe Operating Area (SOA)

what is the avalanche breakdown?

- Maximum voltage is generally related to the avalanche breakdown in the reverse biased base-collector junction
- All the curves tend to merge to the same V_{CE} upon reaching breakdown voltage. This voltage is called sustainable voltage $V_{CE(sus)}$.

$V_{CE(sus)}$ is the minimum voltage necessary to sustain the transistor in breakdown

- Example: $V_{CEO} = 130 \text{ V}$ and $V_{CE(sus)} = 115 \text{ V}$

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Second Breakdown

Second breakdown occurs in a BJT operating at high voltage and at a fairly high current.

- Higher current increases heat
- Higher temperature reduces resistance, more current
- Increased current increases the current further
- This is a positive feedback
- This is called thermal runaway
- This is also known as second breakdown

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Power Dissipation Example

Example: Assume $V_{CC} = 24 \text{ V}$ and $R_L = 8 \Omega$

top of load line

$$I_{C(max)} \cong \frac{V_{CC}}{R_L} = \frac{24}{8} = 3A$$

bot of load line

$$V_{CE(max)} \cong V_{CC} = 24V$$

Power dissipation

$$P_T = V_{CE} I_C = (V_{CC} - I_C R_L) I_C$$

$$P_T = V_{CC} I_C - I_C^2 R_L$$

take derivative

This leads to

$$\frac{V_{CC} - 2I_{C(p,max)}R_L}{2R_L} = 0$$

$$I_{C(p,max)} = \frac{V_{CC}}{2R_L} = \frac{24}{2 \times 8} = 1.5A$$

The current at maximum power is found by using the equation

$$\frac{dP_T}{dI_{C(p,max)}} = 0$$

Thus,

$$V_{CE(p,max)} = V_{CC} - I_{C(p,max)} R_L$$

$$V_{CE(p,max)} = 12 \text{ V}$$

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$$V_{CE(p,max)} = V_{CC} - I_{C(p,max)} R_L$$

$$I_{C(p,max)} = \frac{V_{CC}}{2R_L}$$

Power Dissipation Example (Continued)

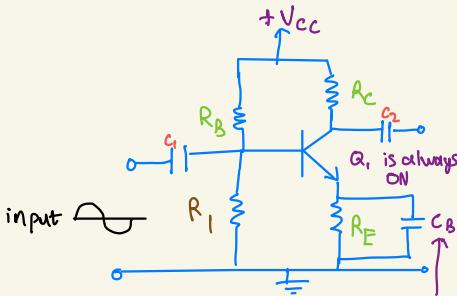
Thus, maximum power dissipates at the center of the load-line and

$$P_T = 12 \times 1.5 = 18W$$

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Class A Amplifier

function: increase power level of AC input by transferring power from DC power supply to input signal

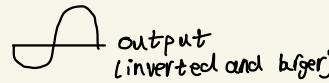


- R_B and R_1 form voltage divider

$$V_{BE} = 0.7$$

$$\beta = \frac{I_C}{I_B}$$

- C_1 and C_2 are coupling capacitors



allows AC signal to bypass emitter resistor, increasing voltage gain

max theoretical efficiency = 25%

↑
to get as close as possible to
max set $V_{CE} = \frac{1}{2} V_{CC}$

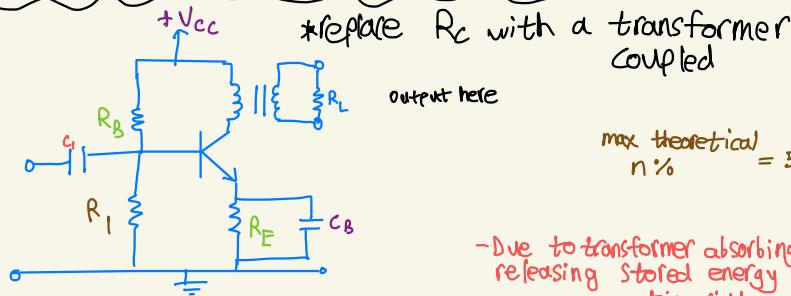
- low efficiency
- not good as power amplifier,
usually used as small signal
- conducts for entire 360° of input cycle
- very little to low distortion

$$AV = \frac{V_O}{V_{IN}}$$

$$\eta \% = \frac{P_L}{P_{DC}} \times 100$$

↑
efficiency
power delivered by DC power source

To increase efficiency



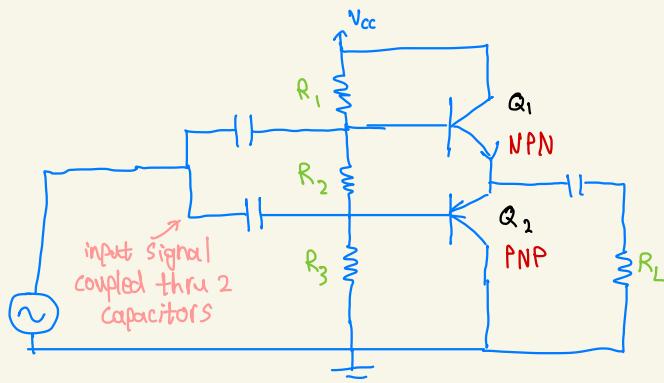
$$\text{max theoretical } \eta \% = 50\%$$

- Due to transformer absorbing and releasing stored energy using magnetic fields

Class B amplifier

- uses 2 complementary transistors
npn and pnp

$$\eta\% = 78.5\%$$



- 2 transistors must be at cut off

- for each half cycles only one transistor should be conducting, other should be off

• conducting angle = 180°

disadvantage:

- presence of crossover distortion



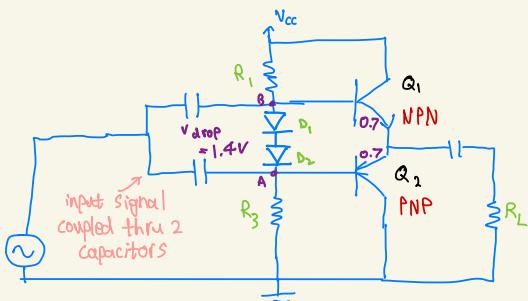
due to $V_{BE} = 0.7$

so until input sine wave reaches +ve or -ve 0.7 the 2 transistors will be off

and $V_{out} = 0$

improved by creating class AB amplifier

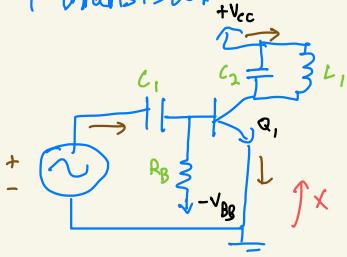
Class AB → replace R_2 with 2 diodes



- removes crossover distortion

Class C

-only uses 1 transistor



Tuned amplifier,
has inductor and
capacitor in
parallel with
each other

$$n\% = 99\%$$

Disadvantage

- distortion
- conducts for $< 180^\circ$ of input cycle



- for +ve half cycle,
 $> 0.7 \text{ V}$
- activate NPN transistor
- current flows from DC Supply
charging C_2 and L_1 , oscillations begin
- energy is transferred back and forth between C_2 and L_1 ,



- for -ve half cycle
 Q_1 is off
- current won't flow since BE is not biased

-there is another way of implementing class C amplifier, using Voltage gain

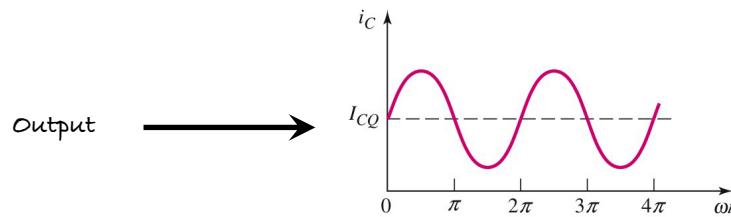
Classes of Amplifier Operations

- class-A operation
- class-B operation
- class-AB operation
- class-C operation

textbooks
will have
more definitions

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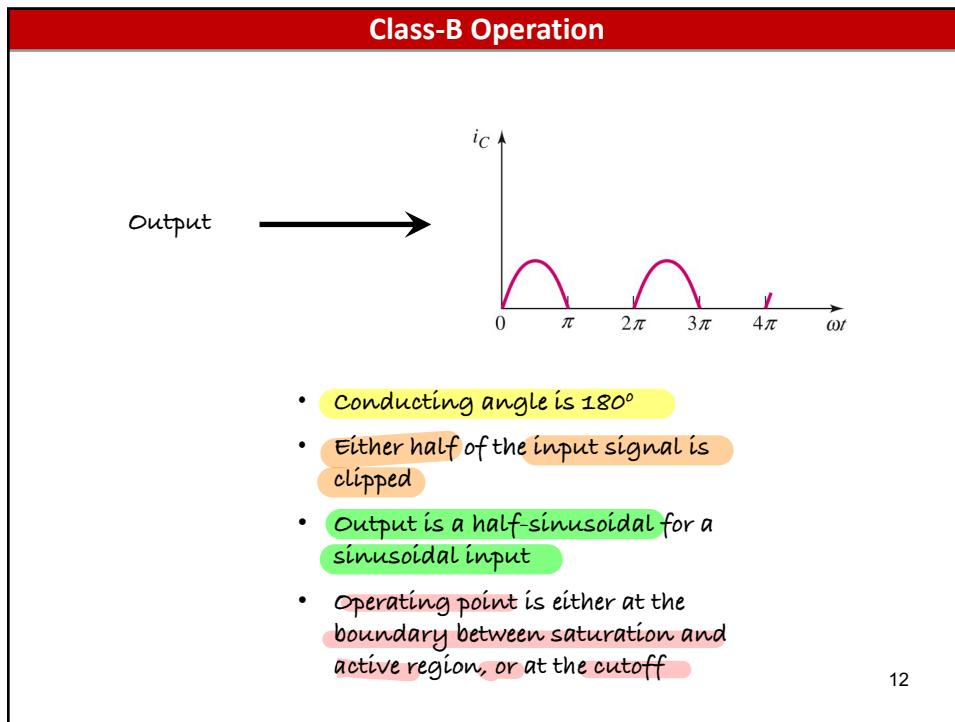
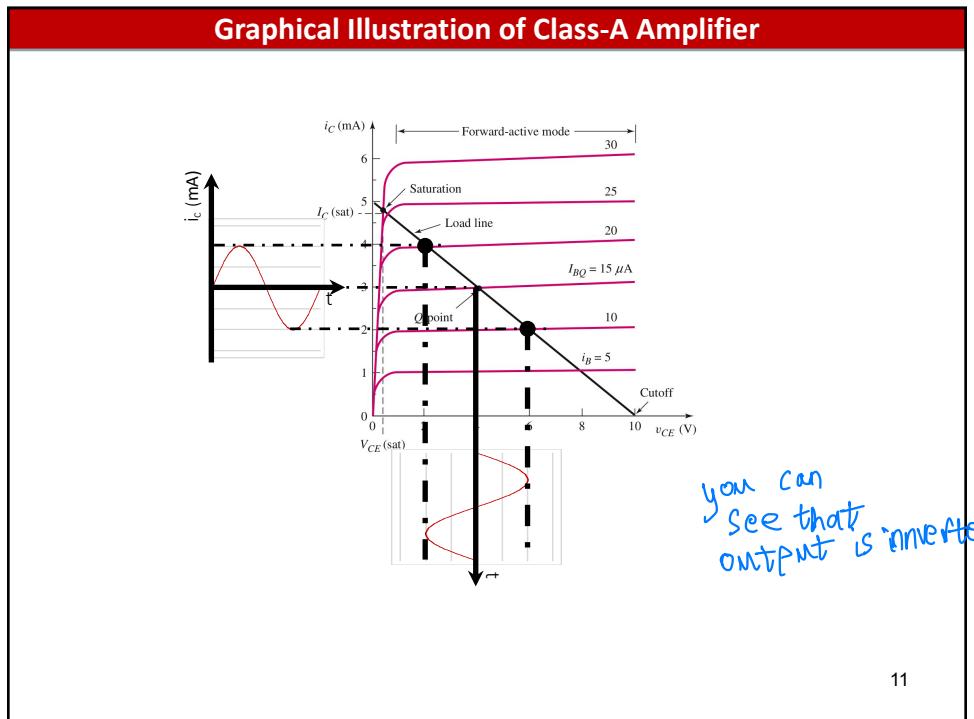
Class-A Operation

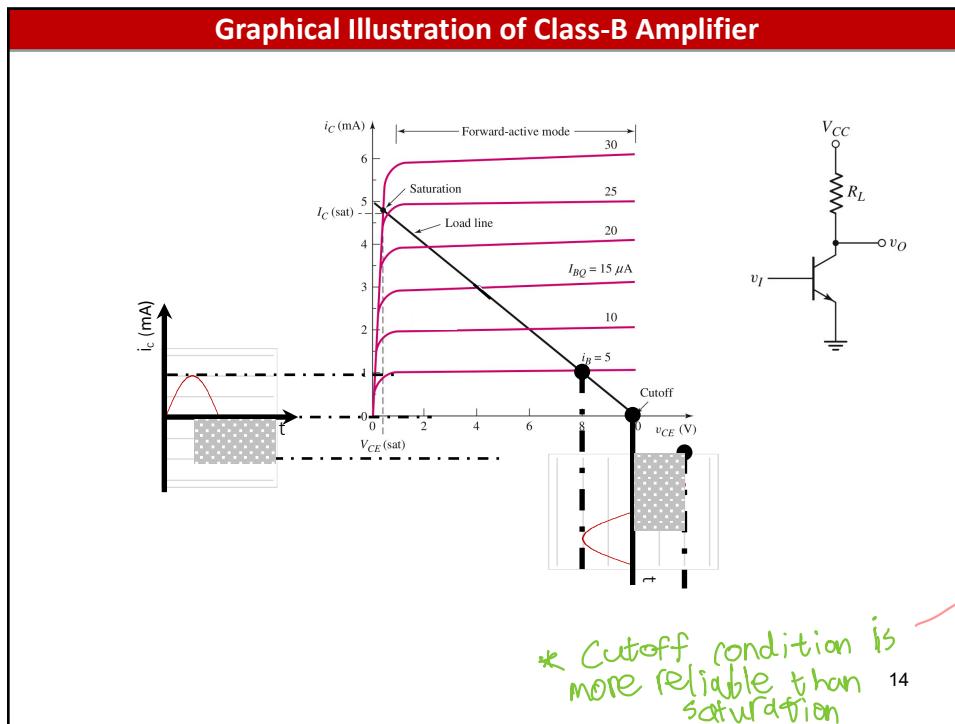
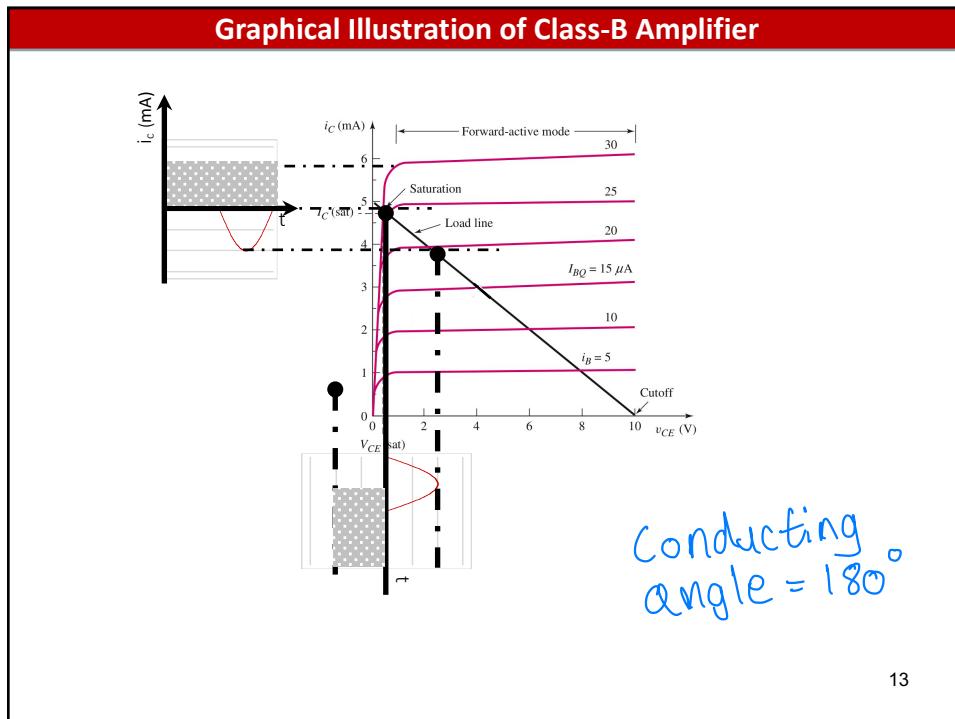


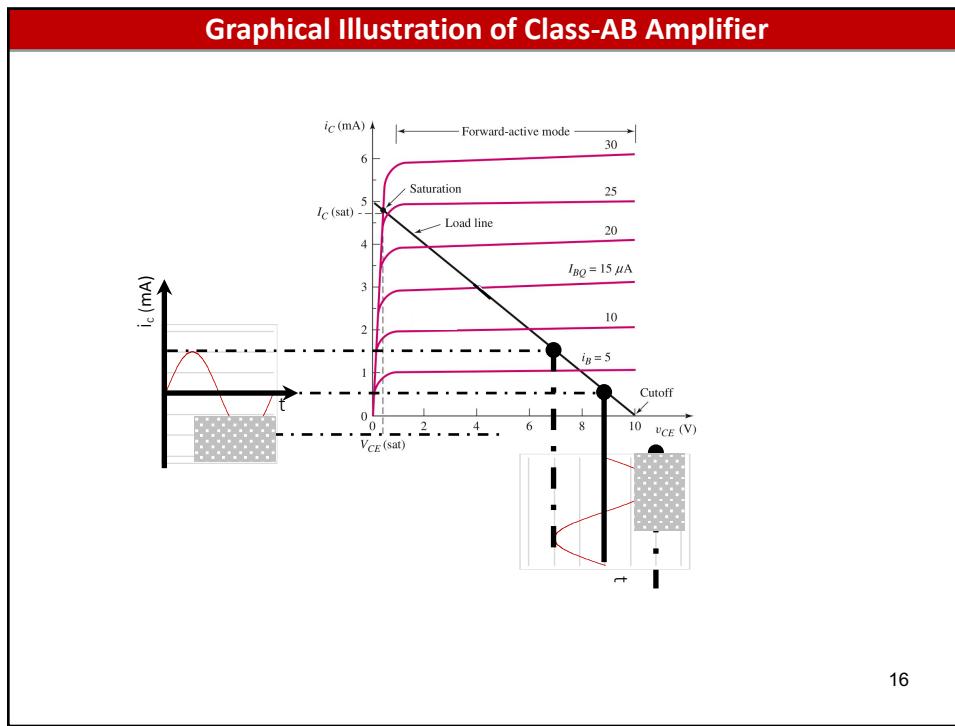
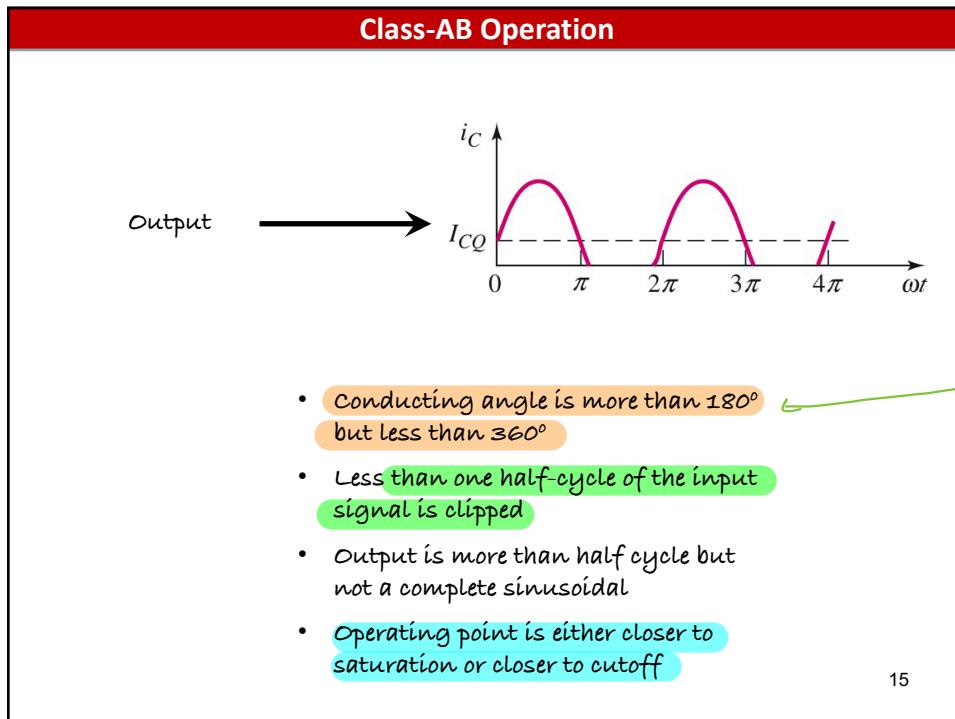
- conducting angle is 360°
- No clipping
- Output is a sinusoidal for a sinusoidal input
- Operating point is not necessarily in the middle of the load-line

clipped means
it doesn't
appear in
output

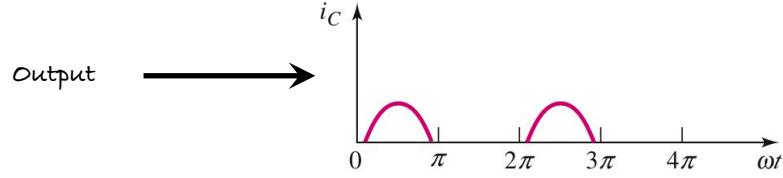
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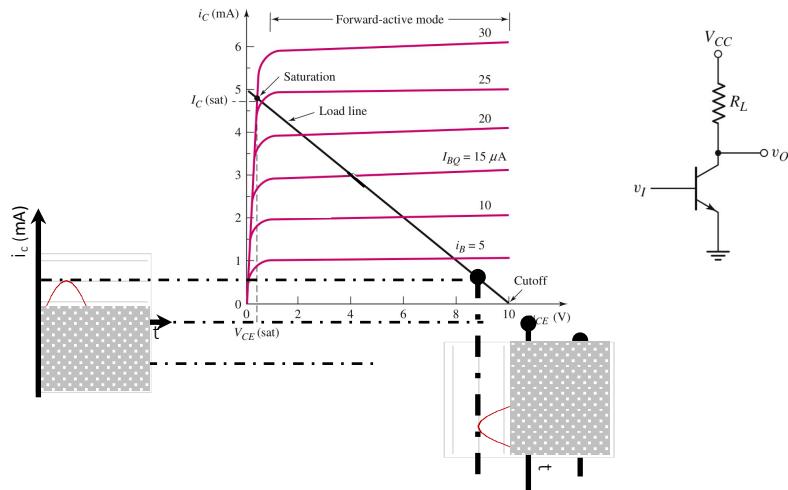
Class-C Operation



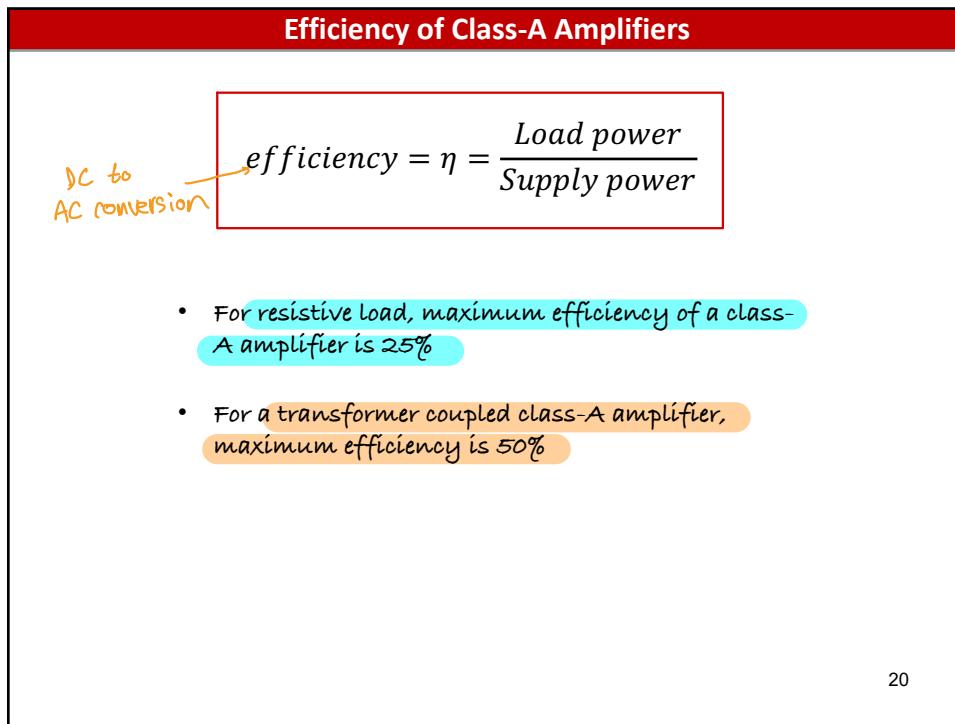
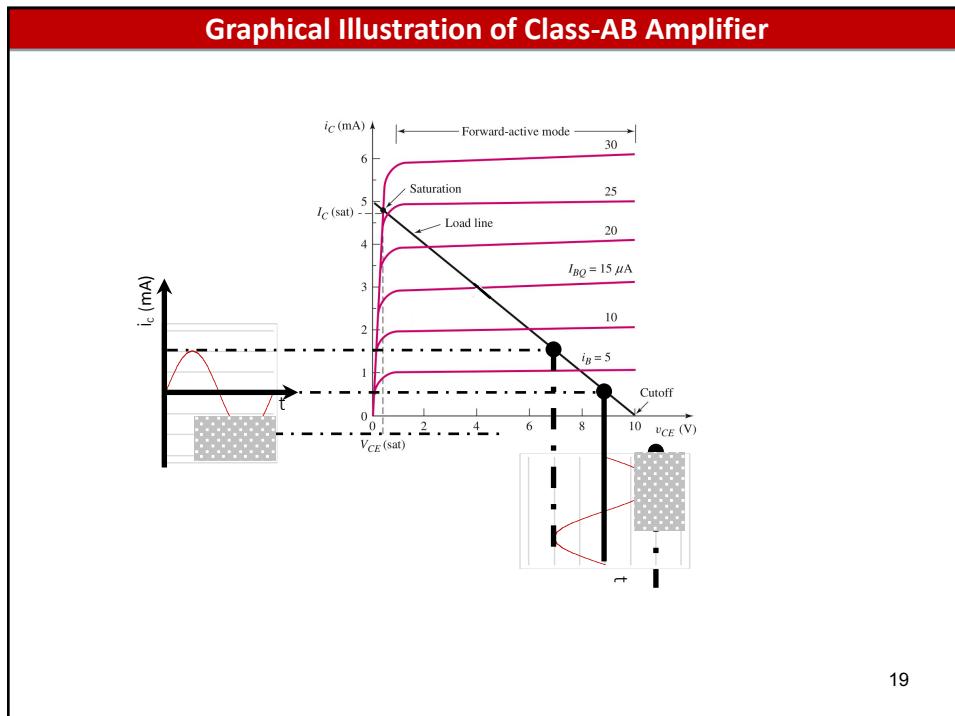
- Conducting angle is more than 0° but less than 180°
- More than one half-cycle of the input signal is clipped
- Output is less than half cycle but not zero
- Operating point is either deep in saturation or deep in cutoff

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Graphical Illustration of Class-C Amplifier



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Schematic of a Push-Pull Amplifier

A and B are two switches and given that when

$v_i > 0$, A is ON and B is OFF

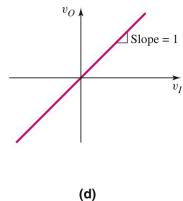
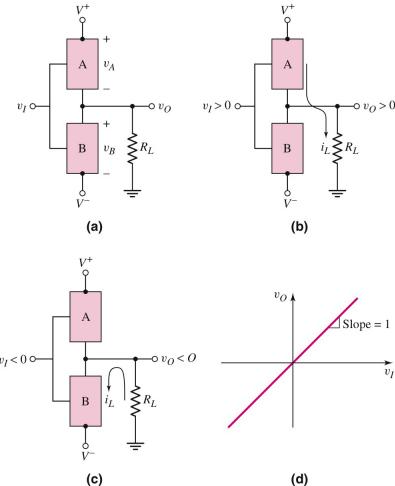
$v_i < 0$, A is OFF and B is ON

When $v_i > 0$

- Voltage drop across A (V_A) is zero
- Voltage drop across B (V_B) is $|V^+|$
- The current flows downwards in the load

When $v_i < 0$

- Voltage drop across A (V_A) is $|V^+|$
- Voltage drop across B (V_B) is zero
- The current flows upwards in the load



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Class B Push-Pull Amplifier

Q_n and Q_p are two CC amplifiers.

When

$v_i > 0$, Q_n is ON and Q_p is OFF

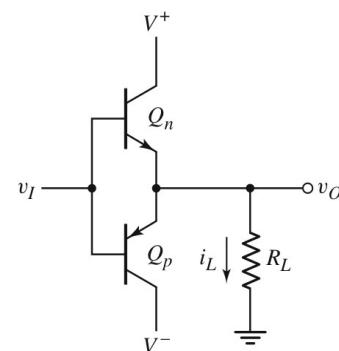
$v_i < 0$, Q_n is OFF and Q_p is ON

When $v_i > 0$

- $V_{CE,n} = V_{CE(\text{sat})} \approx 0$
- $V_{CE,n} = |V^+|$
- $v_o \approx v_i$ and i_L is positive (downwards)

When $v_i < 0$

- $V_{CE,p} = V_{CE(\text{sat})} \approx 0$
- $V_{CE,n} = |V^-|$
- $v_o \approx -v_i$ and i_L is negative (upwards)



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The Load-Line of Class B Push-Pull Amplifier

The circuit diagram shows a Class B push-pull amplifier with two transistors, Q_n and Q_p , connected to a common-emitter configuration. The collector voltage is V_{CC} and the emitter voltage is $-V_{CC}$. The load resistor is R_L . The output voltage v_O is shown. The load-line graph plots current i_Cn against voltage v_{CEn} and v_{ECP} . The graph shows two linear regions: Q_n conducting (top) and Q_p conducting (bottom). The operating point is at the midpoint of the load line. The output voltage v_O is also plotted, showing a full-wave oscillation between $-V_{CC}$ and V_{CC} .

When the input satisfies $0 \leq \omega t \leq \pi$
then $v_o = V_{CC} - v_{CEn}$

When the input satisfies $\pi \leq \omega t \leq 2\pi$
then $v_o = -V_{CC} + v_{ECP}$

Maximum conversion efficiency is 78.5%

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Crossover Distortion

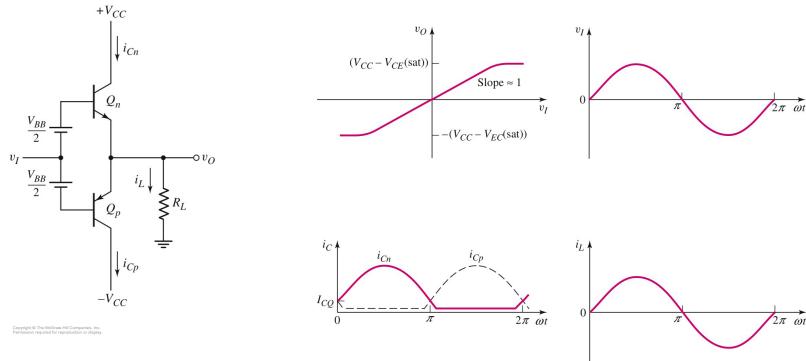
The circuit diagram is identical to the one above. The load-line graph shows the operating point at the midpoint of the load line. The graph is divided into four quadrants by the axes. The top-right quadrant is labeled "Slope $\equiv 1$ " and "Q_n conducting Q_p cutoff". The bottom-left quadrant is labeled "Slope $\equiv 1$ " and "Q_p conducting Q_n cutoff". The output voltage v_O is plotted, showing a distorted waveform with a flat-top region where the signal fails to amplify due to crossover distortion.

- Transistors need 0.7V at the base-emitter junction in order the junction to be properly forward biased
- Thus, the input signal doesn't amplify until its value exceed 0.7V in either direction
- This gives a distorted output signal

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quiz 4
until here

Elimination of Crossover Distortion: Class AB Operation

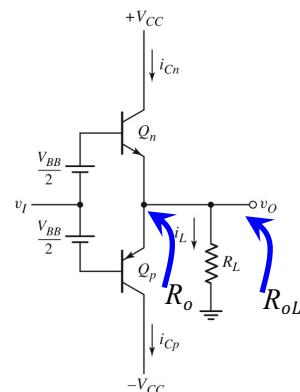


- A voltage of V_{BB} has been applied between the two bases
- Here, $V_{BB} = 0.7 \times 2 = 1.4 \text{ V}$
- This eliminates the crossover distortion

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Output Resistance

- $R_o = (r_{en}) \parallel (r_{ep})$
- $r_{en} = (V_T) / (I_{en})$
- $R_o = \frac{V_T}{I_p + I_n}$
- If $|I_p| = |I_n| = 0.5 \text{ A}$,
 $R_o = V_T / 1 = 25 \text{ m}\Omega$
- Even for small current such as
 $|I_p| = |I_n| = 1 \text{ mA}$,
 $R_o = V_T = 12.5 \Omega$



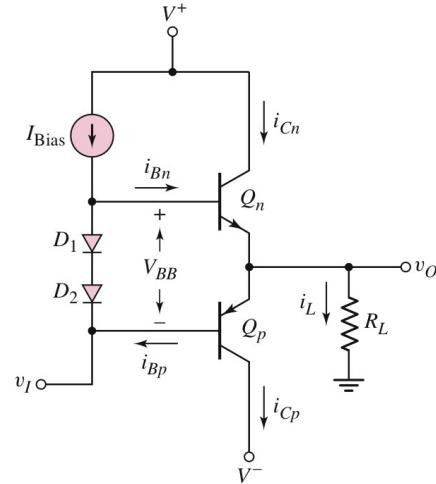
- $R_{oL} = (R_o) \parallel (R_L)$
- Thus, $R_{oL} < R_o$

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ends here

Class AB Output Stage With Diode Biasing

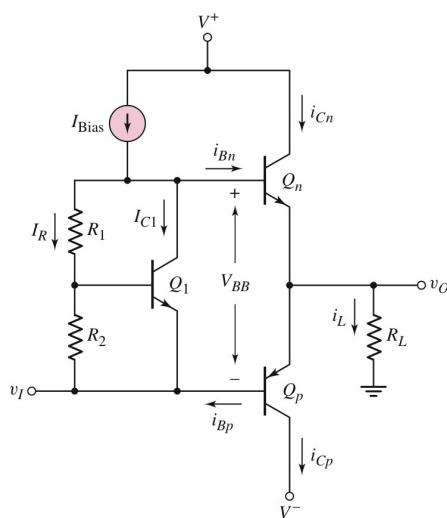
- D1 and D2 are biased by I_{Bias}
- V_{BB} provides the quiescent bias



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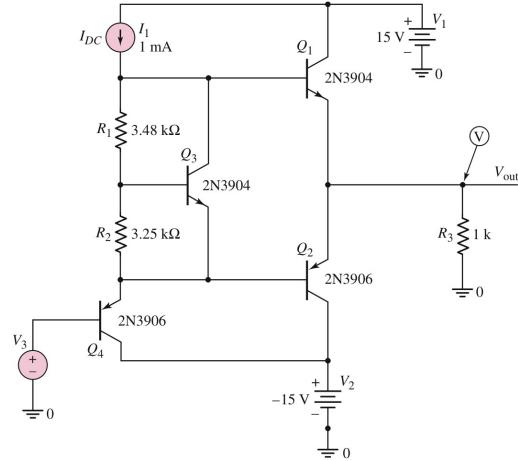
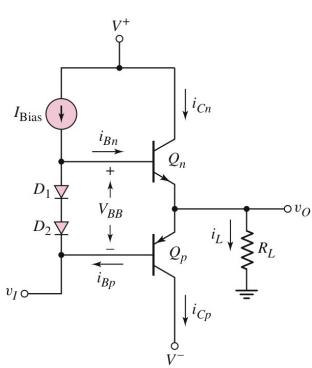
Class AB Operation Using V_{BE} Multiplier

- Assume, $I_{B1} = 0$
- $I_R = (V_{BE1})/(R_2)$
- $V_{BB} = I_R (R_1 + R_2)$
- $$V_{BB} = V_{BE1} \left(1 + \frac{R_1}{R_2}\right)$$
- V_{BE1} is multiplied by the factor $(1 + R_1/R_2)$
- One can control this factor to set the V_{BB}
- A potentiometer can be used in a discrete circuit



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An Example Circuit



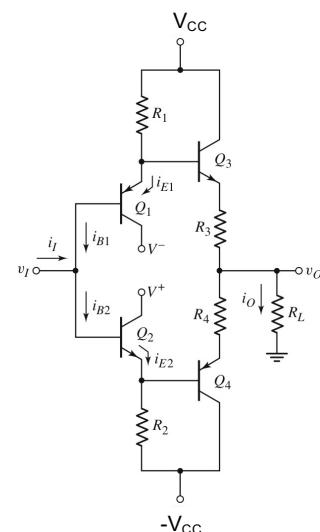
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Class AB with Input Buffer

- Q_1 and Q_2 are emitter followers
- High input resistance
- R_3 and R_4 provide thermal stability
- R_3 and R_4 are very small
- The overall voltage gain is approximately unity

When v_i increases, the following happens

- i_{B1} decreases and i_{B2} increases
- i_{E1} increases because of reduced i_{B1}
- Q_3 conducts
- Q_2 also conducts because of increased i_{B2}
- High input resistance
- Q_4 doesn't conduct because of increased i_{E2}
- i_L flows through Q_3 , R_3 , and RL (downwards)



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Class AB with Input Buffer

Let's consider the positive half cycle of the input signal is applied

- i_{B2} and i_{E2} increase
- Thus, $i_I = i_{B2} - i_{B1}$

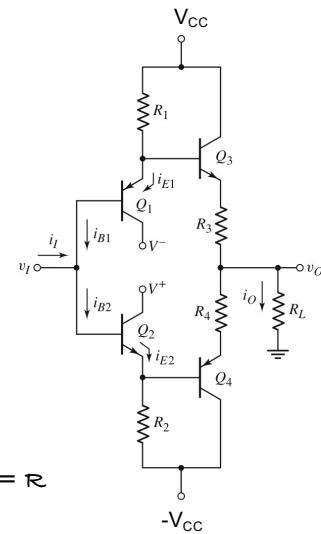
Neglecting the voltage drops across R_3 and R_4 , we can write

$$i_{B2} = \frac{(v_I - v_{BE2}) - (-V_{CC})}{(1 + \beta_n)R_2}$$

and $i_{B1} = \frac{V_{CC} - (v_I + v_{EB1})}{(1 + \beta_p)R_1}$

If $|v_{BE}| = |v_{EB}|$, $\beta_p = \beta_n = \beta$, and $R_1 = R_2 = R$

$$i_I = i_{B2} - i_{B1} = \frac{2v_I}{(1 + \beta)R}$$



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Class AB with Input Buffer

Here,

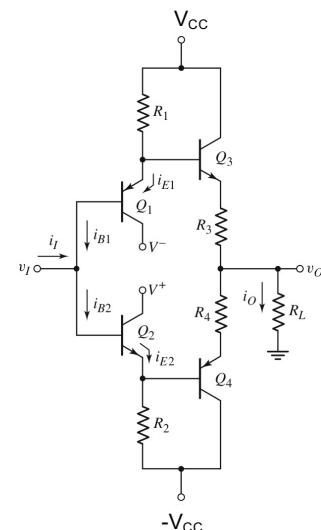
$$i_L = \frac{v_o}{R_L} \cong \frac{v_I}{R_L} = \frac{i_I(1 + \beta)R}{2R_L}$$

Thus, Current gain = $A_i = \frac{i_L}{i_I}$

or, $A_i = \frac{R}{2R_L}(1 + \beta)$

Example: If $R = 580\Omega$, $R_L = 8\Omega$, and $\beta = 30$, determine the current gain.

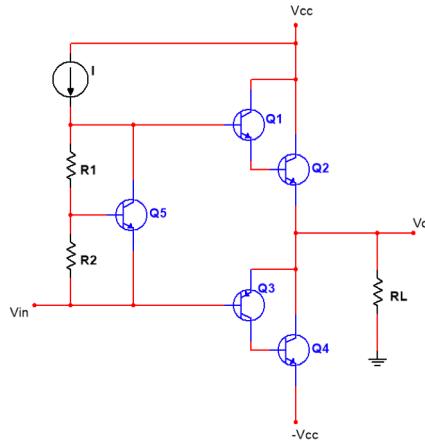
Current gain = 1123.8



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Class AB with Compound Devices

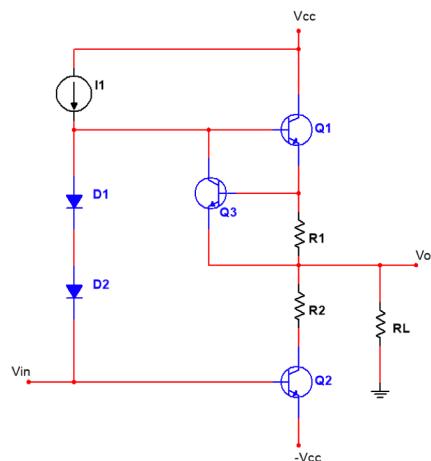
- The signal voltage gain is approximately unity
- If Q_1 , Q_2 , Q_3 , and Q_4 are identical, the current gain for the Darlington ($Q_1 \& Q_2$) is β^2 and
- The current gain for the composite pnp ($Q_3 \& Q_4$) is also β^2 .
- $V_{BB} = 0.7 \times 3 = 2.1 \text{ V}$



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Class AB with Short Circuit Protection

- If Q_1 is short-circuited because of overflow of current
- The voltage across R_1 increases
- Increased V_{R_1} turns Q_3 on
- I_{C3} will decrease I_{B1} to a safe level
- Thus, Q_3 protects overflow/short-circuit in Q_1



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