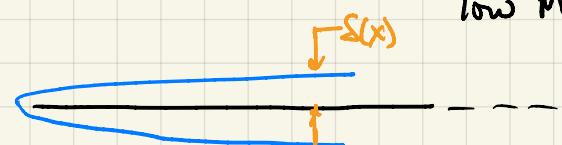


Lecture 25

- BL - shock interaction
- Shock tube BL



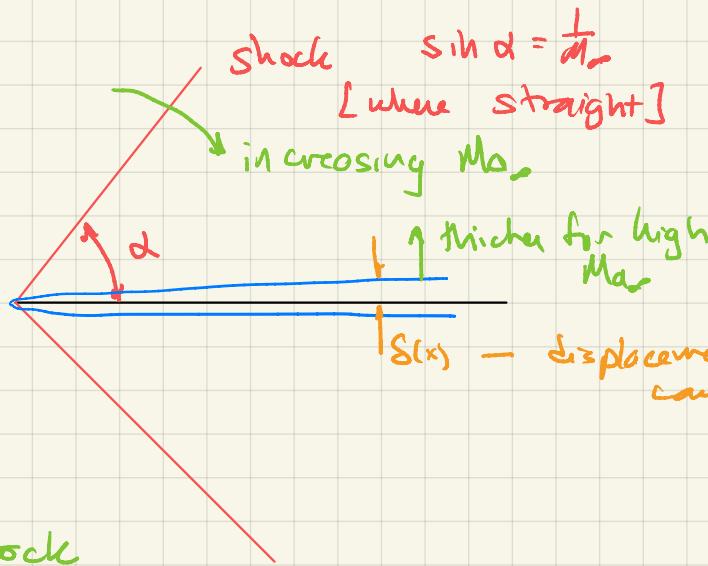
Semi-infinite flat plate



low Ma_∞ ~ essentially incompressible

white

BL has small effect on outer flow

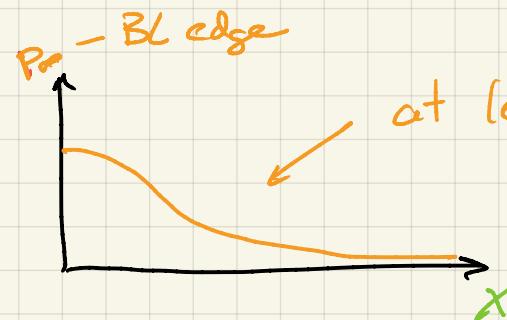
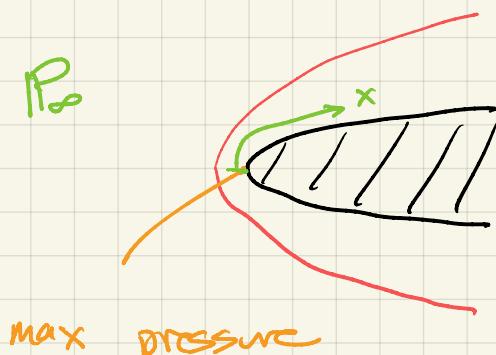


$\rightarrow \text{7-4} \rightarrow 2^{\text{nd}}$ order \rightarrow flow over a narrow parallelogram

\rightarrow "cavating" stays close to wall

Consider shock
- BL interaction

Q: when does the extra S -displacement matter?



at least qualitatively ... due to shock + shape

semi-empirical formulae

$$\frac{P_x}{P_\infty} = 1 + \frac{x}{4} (\kappa+1) k^2 + \kappa k \left\{ 1 + \left[\frac{(\kappa+1) k}{x} \right] \right\}^{1/2}$$

change in displacement

$$\frac{dS}{dx} \approx \phi$$

deflection angle

$$K = Ma_\infty \phi$$

↑ flow deflection by body / body + BL

→ flat plate → just BL*

$$K=0 \rightarrow$$

$$P_\infty \approx P_\rho$$

* for our thinking

K large

$$P_\infty > P_\rho$$

BL shape → "body" shape → flow deflection ϕ →

$$\text{via } \frac{\partial P_\infty}{\partial x} \dots$$

local shock angle/shape → P_∞ (post shock) → BL shape

strong interaction ... or not?

Q = how thick $\delta(x)$?

empirical fit

$$\frac{\delta}{x} \propto Ma^2 \left(\frac{C_w}{Re_x} \right)^{1/2}$$

fit of full solutions from last lecture

$$Re_x = \frac{S_0 U}{\mu}$$

$$\delta \propto Ma^2 \left(\frac{C_w}{\frac{S_0 U}{\mu}} \right)^{1/2} x^{1/2}$$

$$C_w = \frac{P_\infty - P_\infty}{P_\infty Ma}$$

$$\frac{ds}{dx} \propto Ma^2 \left(\frac{C_w}{Re_x} \right)^{1/2}$$

↓

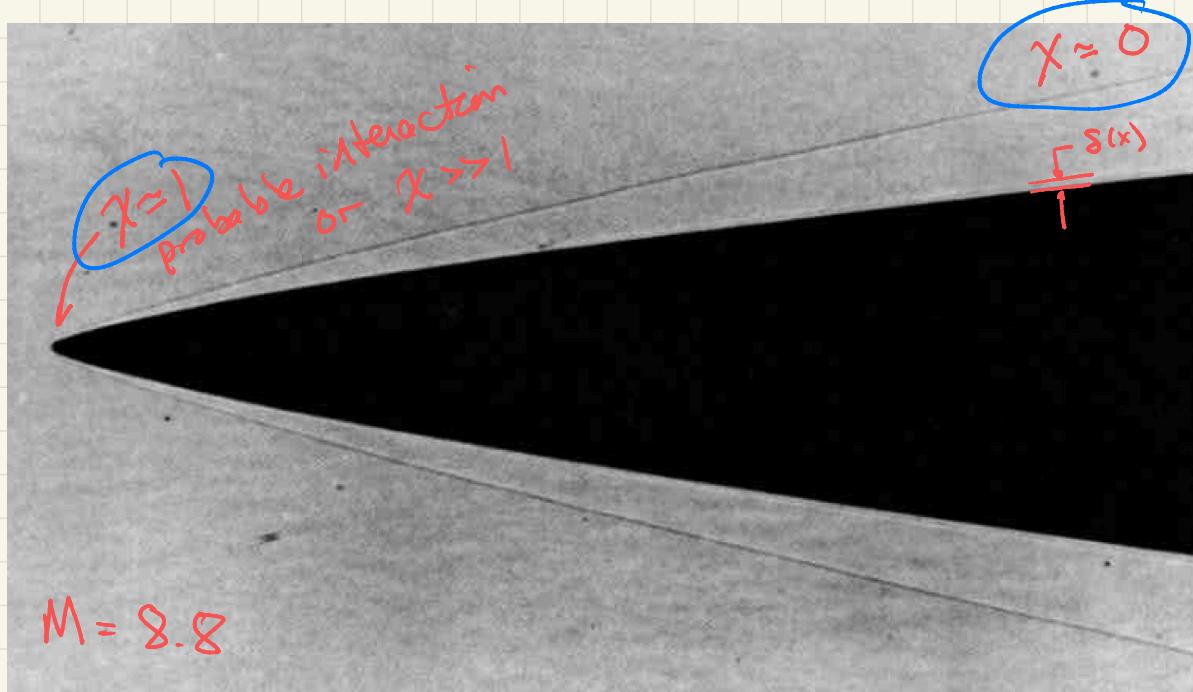
$$k = Ma_\infty \phi \propto Ma_\infty^3 \left(\frac{C_w}{Re_x} \right)^{1/2}$$

χ - interaction parameter

$$\chi \ll 1 \rightarrow \frac{P_\infty}{P_0} = 1 \quad \text{no / little interaction}$$

$$\chi \approx 1 \rightarrow \text{flow over body shape + } S(x)$$

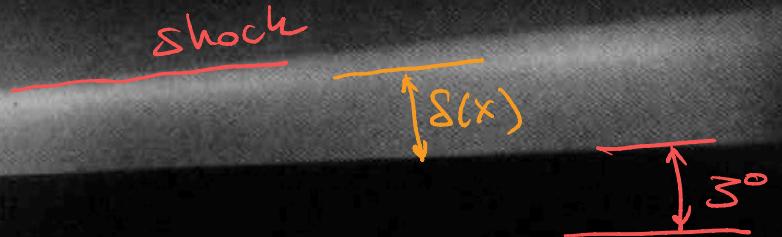
$$\chi \gg 1 \rightarrow \text{strong interaction} \rightarrow BL \text{ not a distinct "idea" from gas dynamics}$$



van Dyke

$X \gg 1$

We



$$M_\infty = 41$$

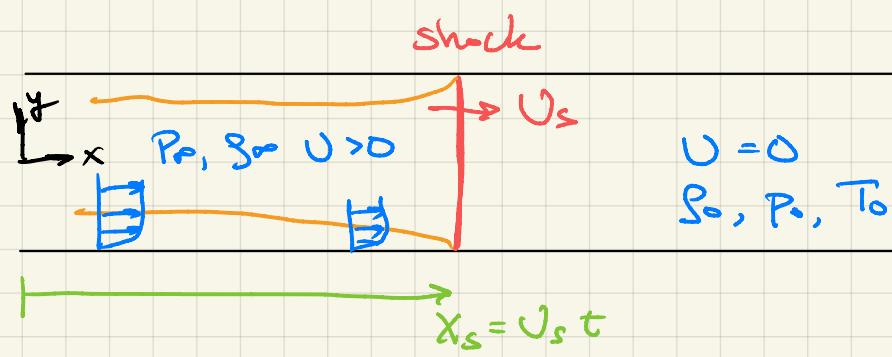
$$\sin^{-1} \frac{1}{41} = 1.4^\circ$$

274. Hypersonic flow past a slender cone. A cone of 3° semi-vertex angle is shown by the glow-discharge method in helium at Mach number 41 and Reynolds number

560,000 based on length. In this strong-interaction regime the boundary layer is seen to extend about four-fifths of the distance to the shock wave. Horstman & Kussoy 1968

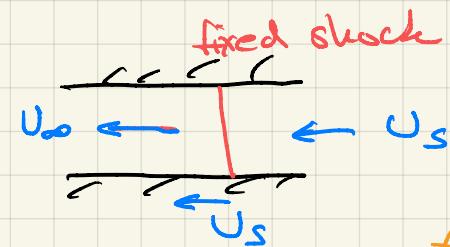
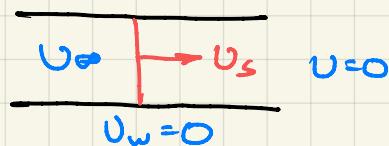
Schlichting

and
 x



t dependent

Move to shock's frame

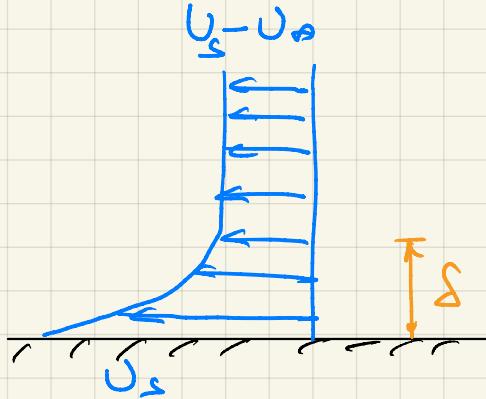


t independent

$$\text{mass} = g_0 U_\infty = g_0 U_s$$

$$U_\infty = \frac{g_0}{g_\infty} U_s$$

$\hookrightarrow g_0 > g_\infty$ (compression)



$\rightarrow U_\infty$ - flow to the left \rightarrow slower than the walls

incompressible

$$\gamma = \frac{y}{\sqrt{v_x}}$$

$$\gamma = \int_0^y \frac{\rho}{\rho_\infty} dy$$

now

$$\gamma = \frac{y}{2\sqrt{v_\infty(t - x/v_s)}}$$

stream function: $\psi = \int \rho_\infty U_\infty \sqrt{v_\infty(t - x/v_s)} f(\gamma)$

$$\cancel{\delta u} = \frac{\partial \psi}{\partial y} = \cancel{\int \rho_\infty U_\infty \sqrt{v_\infty(t - x/v_s)}} + \frac{\partial \gamma}{\partial y}$$

$$u = U_\infty f'$$

$$\frac{1}{\cancel{\int v_\infty(t - x/v_s)}} \frac{\partial}{\partial y} \int_0^y \frac{\rho}{\rho_\infty} dy$$

S/V_∞

ansatz : $\frac{T}{T_\infty} = 1 + \frac{\gamma-1}{2} M_\infty^2 r(\gamma) + \frac{T_w - \overline{T}_{ad}}{T_\infty} S(\gamma)$

• • •

$$\overline{T}_{ad} = T_\infty \left[1 + \frac{\gamma-1}{2} M_\infty^2 R_w \right]$$

$$f''' + z(\gamma - \frac{1}{\rho_s} f) f'' = 0$$

recovery factor

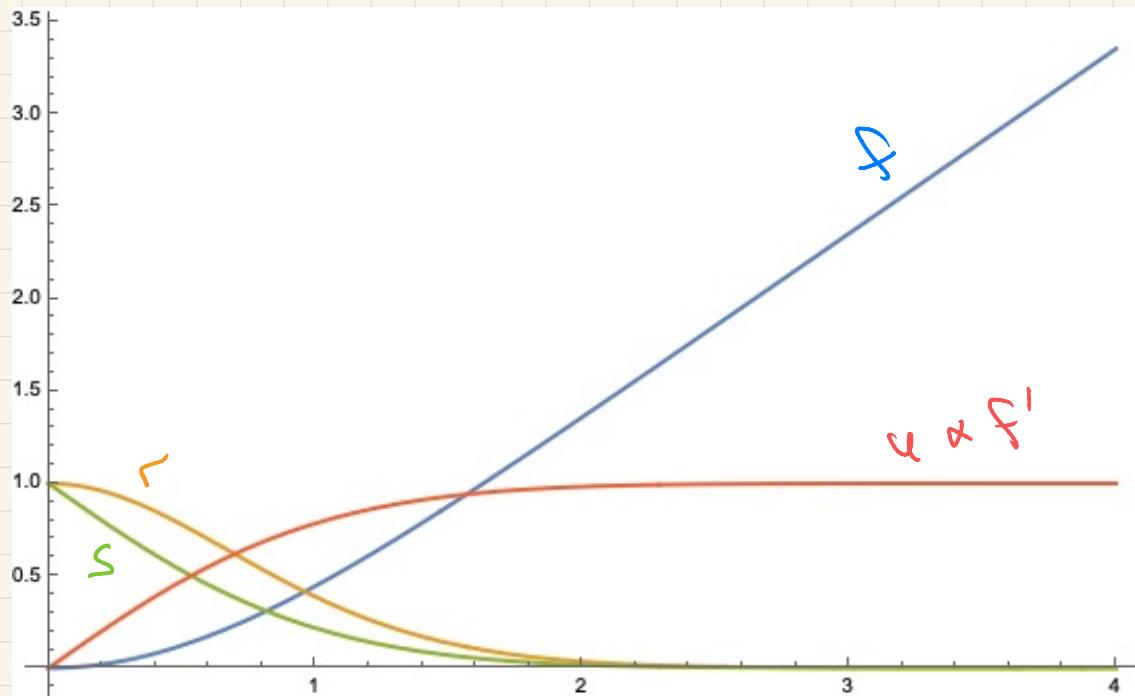
$$\frac{1}{P_f} r'' + z(\gamma - \frac{1}{\rho_s} f) r' = -2 f''^2$$

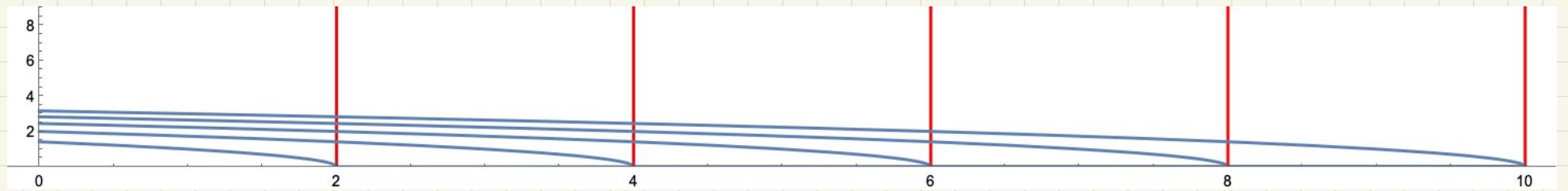
$(r_w \rightarrow 1)$
isentropic

$$\frac{1}{P_f} s'' + 2(\gamma - \frac{1}{\rho_s} f) s' = 0$$

$$\gamma = 0 : \quad f = 0 \quad f' = 0 \quad r' = 0 \quad s = 1$$

$$\gamma \rightarrow \infty : \quad f' = 1 \quad r = 0 \quad s = 0$$





STOP : Meeting #2 Material