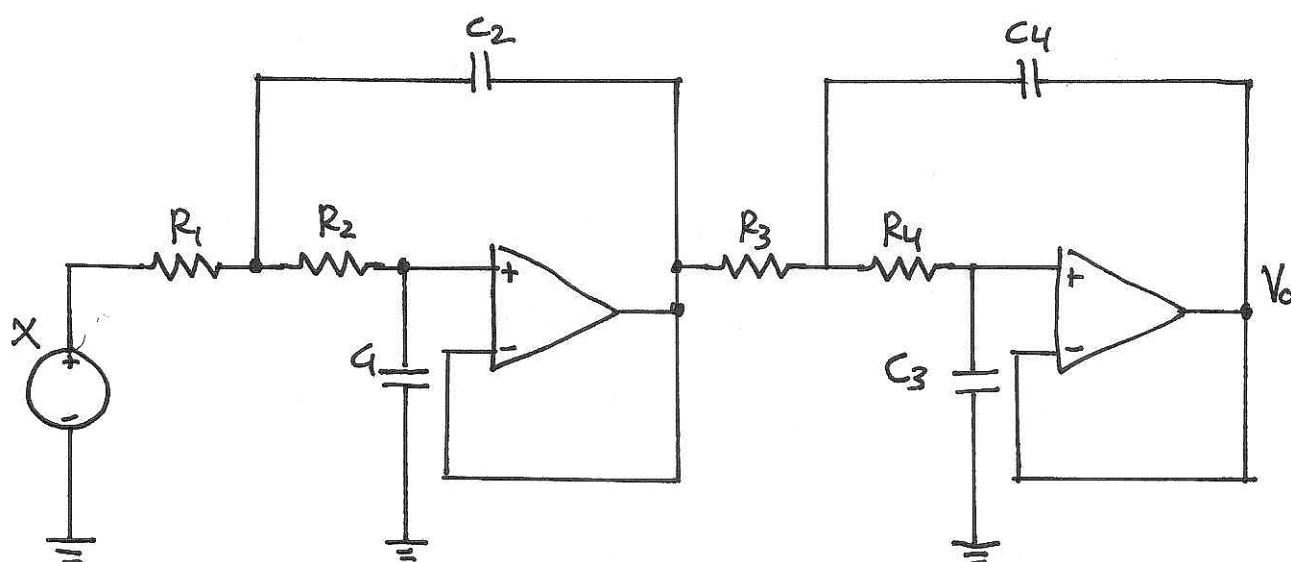


SIGNALS AND SYSTEMS - WEEK 13

Problem 1

Design a 4th order Butterworth lowpass filter with unity gain and cutoff frequency at 500 Hz. The filter must be insensitive to component drift.



Sol

It's a 4th order filter, so we need 2 stages:

$$H(s) = \frac{1}{s^2 + 0.765367s + 1} \cdot \frac{1}{s^2 + 1.84776s + 1} \quad (\text{Normalized})$$

For lowpass resistors should be identical to reject drift.

$$\frac{C_2}{C_1} = \frac{4a_0}{a_1^2} = \frac{4 \cdot 1}{(0.765367)^2} = 6.828 \Rightarrow C_1 = 8.2 \text{ F}, C_2 = 56 \text{ F}$$

$$R_1 = R_2 = \frac{a_1}{2a_0C_1} = \frac{0.765367}{2 \cdot 1 \cdot 8.2} = 0.0466 \Omega$$

Frequency scale to move ω_c from $1 \frac{\text{rad}}{\text{s}}$ to 500 Hz.

$$K_f = \frac{2\pi \cdot f_{c,\text{new}}}{\omega_{c,\text{old}}} = \frac{2\pi \cdot 500 \text{ Hz}}{1 \frac{\text{rad}}{\text{s}}} = 3141.5$$

Scale both capacitors with this k_f .

$$C_{1f} = \frac{C_1}{k_f} = \frac{8.2 \text{ F}}{3141.5} = 2.610 \text{ mF}$$

$$C_{2f} = \frac{C_2}{k_f} = \frac{56 \text{ F}}{3141.5} = 17.83 \text{ mF}$$

Currently: $C_1 = 2.610 \text{ mF}$, $C_2 = 17.83 \text{ mF}$, $R_1 = R_2 = 0.0466 \Omega$.

These values are impractical.

Scale all components with k_z (multiply resistors, divide capacitors).

Impedance scaling:

$$k_z = \frac{C_{1f}}{C_{1,des}} = \frac{2.610 \text{ mF}}{10 \text{ nF}} = 261014$$

$$C_{1fz} = 10 \text{ nF}$$

$$C_{2fz} = \frac{17.83 \text{ mF}}{261014} = 68.29 \text{ nF} \approx 68 \text{ nF}$$

$$R_{1z} = R_{2z} = R k_z = 0.0466 \Omega \cdot 261014 = 12181 \Omega = 12 \text{ k}\Omega$$

Stage 2

$$\bullet \frac{C_4}{C_3} = \frac{4a_0}{a_1^2} = \frac{4.1}{(1.84776)^2} = 1.17157 \Rightarrow C_3 = 3.3 \text{ F}, C_4 = 3.9 \text{ F}$$

$$\bullet R_3 = R_4 = \frac{a_1}{2a_0C_3} = 0.2799 \Omega$$

Frequency scaling:

$$k_f = \frac{2\pi \cdot f_{c,new}}{\omega_{c,old}} = \frac{2\pi \cdot 500 \text{ Hz}}{1 \frac{\text{rad}}{\text{s}}} = 3141.5 \quad (\text{same as before})$$

$$C_{3f} = \frac{C_3}{k_f} = \frac{3.3 \text{ F}}{3141.5} = 1.046 \text{ mF}$$

$$C_{4f} = \frac{C_4}{k_f} = \frac{3.9 \text{ F}}{3141.5} = 1.236 \text{ mF}$$

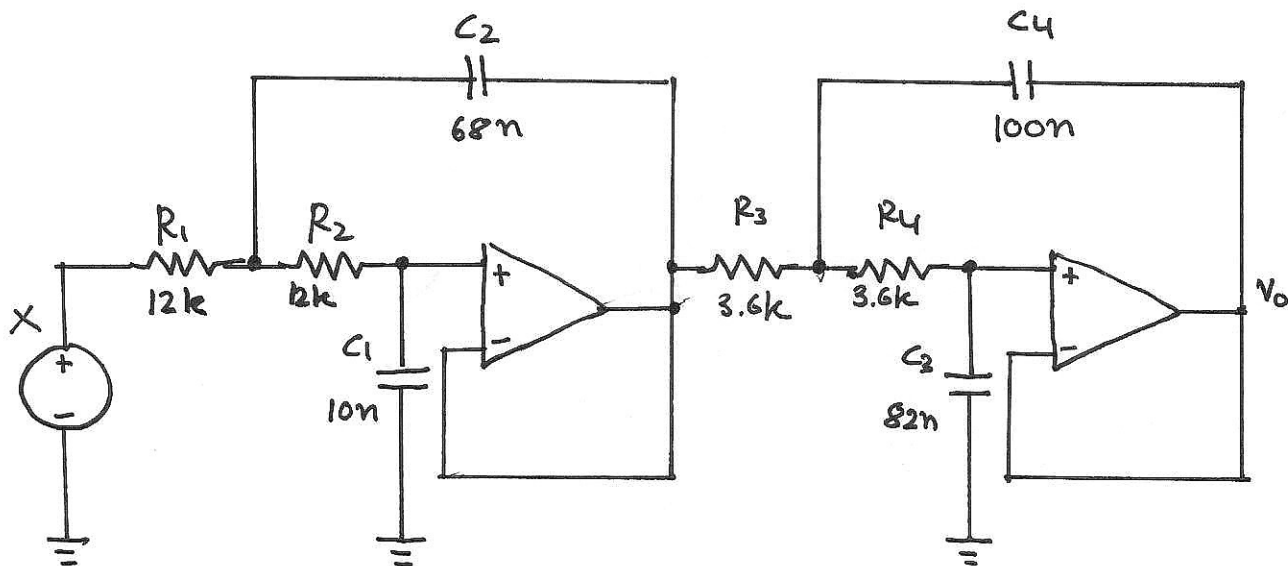
Impedance scaling:

$$k_z = \frac{C_{3f}}{C_{3,des}} = \frac{1.046 \text{ mF}}{82 \text{ nF}} = 12754$$

$$C_{3f} = 82 \text{ nF}$$

$$C_{4f} = \frac{C_{4f}}{k_z} = \frac{1.236 \text{ mF}}{12754} = 96.9 \text{ nF} \approx 100 \text{ nF}$$

$$R_{3f} = R_{4f} = R_{kz} = 0.2799 \Omega \cdot 12754 = 3570 \Omega = 3.6 \text{ k}\Omega$$



4th order Butterworth lowpass filter.

Attenuation: $-80 \frac{\text{dB}}{\text{dec}}$ after $f_c = 500 \text{ Hz}$

Problem 2A

The presence of EMG-signals in the arms drops by $6 \frac{\text{dB}}{\text{oct}} = 20 \frac{\text{dB}}{\text{dec}}$ after 500 Hz.

• How much attenuation do we have if we include the 4th order lowpass filter?

sol

$$\text{Above } 500 \text{ Hz: } -20 \frac{\text{dB}}{\text{dec}} - 80 \frac{\text{dB}}{\text{dec}} = -100 \frac{\text{dB}}{\text{dec}}$$

~~100 dB/dec~~

$$-100 \frac{\text{dB}}{\text{dec}} = -30 \frac{\text{dB}}{\text{oct}}$$

Problem 2B

Assume that the EMG-signal is sampled at $f_s = 4 \text{ kHz}$ by a 12-bit ADC.

- How many bits are toggled at $\frac{f_s}{2}$?
- Do we avoid aliasing?

Sol

A 12-bit ADC has dynamic range: $DR = 12 \text{ bit} \cdot 6 \frac{\text{dB}}{\text{bit}} = 72 \text{ dB}$.

To avoid aliasing: -72 dB at $\frac{f_s}{2}$.

$$\frac{f_s}{2} = \frac{4 \text{ kHz}}{2} = 2 \text{ kHz}.$$

- 1 oct after 500 Hz = 1000 Hz: $-30 \frac{\text{dB}}{\text{oct}} \cdot 1 \text{ oct} = -30 \text{ dB}$
- 2 oct after 500 Hz = 2 kHz: $-30 \frac{\text{dB}}{\text{oct}} \cdot 2 \text{ oct} = -60 \text{ dB}$

We do not avoid aliasing. $-60 \text{ dB} > -72 \text{ dB}$

$$1 \text{ bit} \approx 6 \text{ dB}$$

$$2 \text{ bit} \approx 12 \text{ dB}$$

2 bits will be toggled due to aliasing at half the sampling frequency, when $f_s = 4 \text{ kHz}$.

Solution: Increase f_s or ~~or~~ filter order.

Problem 3

Design a 2nd order Butterworth highpass filter, with unity gain and $f_c = 2 \text{ Hz}$.

Sol

For Sallen-key highpass filters $C_1 = C_2$ for insensitivity.

$$\bullet \frac{R_1}{R_2} = \frac{4a_0}{a_1^2} = \frac{4}{(\sqrt{2})^2} = 2 \Rightarrow R_1 = 68 \Omega, R_2 = 33 \Omega$$

$$\bullet C_1 = C_2 = C = \frac{1}{\sqrt{a_0 R_1 R_2}} = \frac{1}{\sqrt{1 \cdot 68 \cdot 33}} = 0.021 \text{ F}$$

Where we used: $a_1 = \sqrt{2}$, $a_0 = 1$ (Butterworth 2nd order)

$$\text{Frequency scale: } k_f = \frac{2\pi \cdot f_{c, \text{new}}}{\omega_{c, \text{old}}} = \frac{2\pi \cdot 2 \text{ Hz}}{1 \frac{\text{rad}}{\text{s}}} = 12.56$$

$$C_{1f} = C_{2f} = \frac{C}{k_f} = \frac{0.021 \text{ F}}{12.56} = 0.00167 \text{ F}$$

$$\text{Impedance scale: } C_{1f2} = C_{2f2} = \frac{C_f}{\cancel{C_{des}} k_z} \Rightarrow k_z = \frac{C_f}{C_{des}} = \frac{0.00167 \text{ F}}{1 \text{ nF}} = 1670$$

$$C_{1f2} = C_{2f2} = 1 \mu\text{F}$$

$$R_{12} = R_1 k_z = 68 \Omega \cdot 1670 = 113560 \Omega \approx 120 \text{ k}\Omega$$

$$R_{22} = R_2 k_z = 33 \Omega \cdot 1670 = 55110 \Omega \approx 56 \text{ k}\Omega$$

