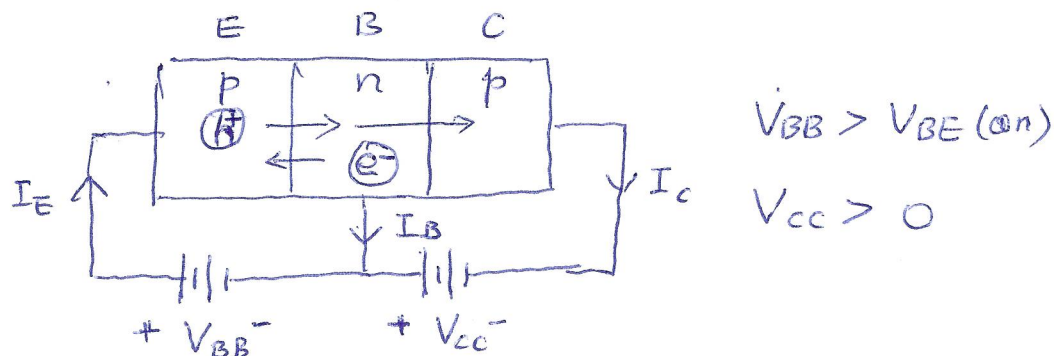


P1P2

① $V_I < V_{BE(on)}$, in cutoff

$$i_B = \frac{i_C}{\beta} = 0$$

$$V_O = V^+$$

② $V_I \geq V_{BE(on)}$, enters forward-active mode

$$I_B = \frac{V_I - V_{BE(on)}}{R_B}, \quad I_C = \beta I_B$$

$$V_O = V^+ - R_C I_C = V^+ - \frac{R_C}{R_B} \beta [V_I - V_{BE(on)}]$$

③ $V_I \geq V_I'$ too high, in saturation mode

$$V_O = V^+ - \frac{R_C}{R_B} \beta [V_I' - V_{BE(on)}] = V_{CE(sat)}$$

So $V_O = V_{CE(sat)}$ when $V_I \geq V_I'$

$$V_I' = V_{BE(on)} + \frac{R_B}{\beta R_C} [V^+ - V_{CE(sat)}]$$

P3

$$I_E = 1.2 \text{ mA}$$

If in forward-active mode

$$I_C = \frac{\beta}{1+\beta} I_E = \frac{80}{81} \times 1.2 \text{ mA} = 1.185 \text{ mA}$$

$$I_B = \frac{I_E}{1+\beta} = 0.0148 \text{ mA}$$

$$V_C = V^+ - R_C I_C = 5 - 2.37 = 2.63 \text{ V}$$

$$V_E = -V_{BE} = -0.7 \text{ V}$$

$$V_{CEQ} = V_C - V_E = 3.3 \text{ V}$$

$$V_{CE} > V_{CE}(\text{sat}) \quad \text{OK, in forward-active mode}$$

$$\begin{aligned} P_Q &= I_B V_{BE}(\text{on}) + I_C V_{CE} \\ &= 0.0148 \times 0.7 + 1.185 \times 3.3 \\ &= 3.956 \text{ mW} \end{aligned}$$

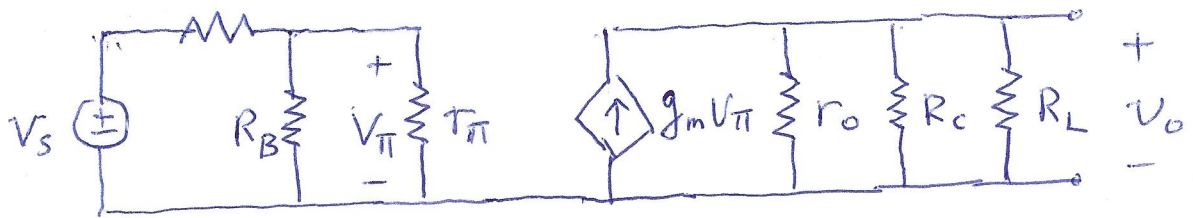
P4

(a) DC loadline

$$V^+ - V^- = I_E R_E + I_C R_C + V_{EC}$$

$$\text{DC loadline slope} = \frac{-1}{R_C + \frac{1+\beta}{\beta} R_E}$$

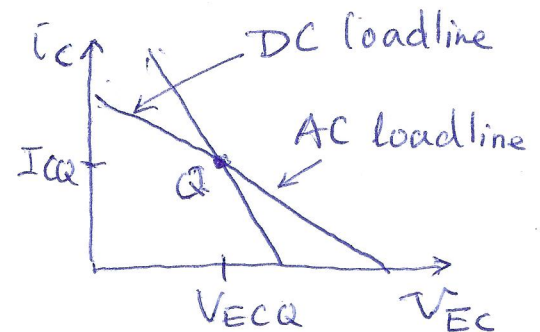
(b)



(c) AC loadline

$$v_{ec} = -\tilde{i}_c (R_C \parallel R_L)$$

$$\text{AC loadline slope} = \frac{-1}{R_C \parallel R_L}$$



(d) For symmetric swing

$$\begin{cases} \tilde{i}_{c,\min} = 0 \\ \tilde{i}_{c,\max} = 2 I_{CQ} \end{cases} \quad \begin{cases} \tilde{i}_{c,\min} = i_{c,\min} - I_{CQ} = -I_{CQ} \\ \tilde{i}_{c,\max} = i_{c,\max} - I_{CQ} = I_{CQ} \end{cases}$$

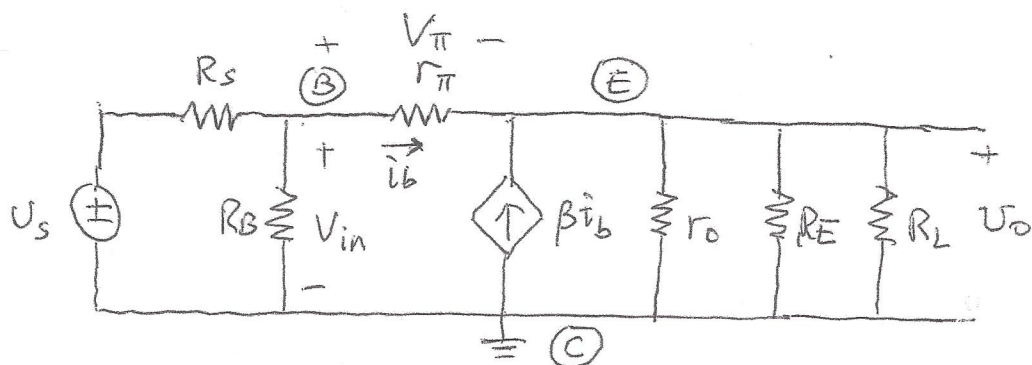
$$v_{EC} = V_{ECQ} + v_{ec} = V_{ECQ} - \tilde{i}_c (R_C \parallel R_L)$$

$$V_{EC,\max} = V_{ECQ} - \tilde{i}_{c,\min} (R_C \parallel R_L) = V_{ECQ} + I_{CQ} (R_C \parallel R_L)$$

$$V_{EC,\min} = V_{ECQ} - \tilde{i}_{c,\max} (R_C \parallel R_L) = V_{ECQ} - I_{CQ} (R_C \parallel R_L)$$

P5

(a)



$$r_\pi = \frac{V_T}{I_{BQ}}, \quad g_m = \frac{I_{CQ}}{V_T}, \quad r_o = \frac{V_A}{I_{CQ}} \quad \beta \hat{i}_b \equiv g_m V_\pi$$

(b) $V_{in} = \hat{i}_b r_\pi + (1+\beta) \hat{i}_b (r_o \parallel R_E \parallel R_L)$

$$R_{ib} \equiv \frac{V_{in}}{\hat{i}_b} = r_\pi + (1+\beta) (r_o \parallel R_E \parallel R_L)$$

(c) $U_o = (1+\beta) \hat{i}_b (r_o \parallel R_E \parallel R_L)$

$$\hat{i}_b = \frac{U_{in}}{R_{ib}}$$

$$R_i = R_B \parallel R_{ib}$$

$$U_{in} = V_s \frac{R_i}{R_s + R_i}$$

$$A_v = \frac{U_o}{U_s} = \frac{(1+\beta) (r_o \parallel R_E \parallel R_L) R_i}{R_{ib} (R_s + R_i)}$$

(d) emitter-follower

$$A_v \approx 1 \quad A_i > 1$$

$$R_o \text{ small} \quad R_i \text{ moderate}$$