



ANALOG COMPUTER

TEAM HYPERTRONICS

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XXX

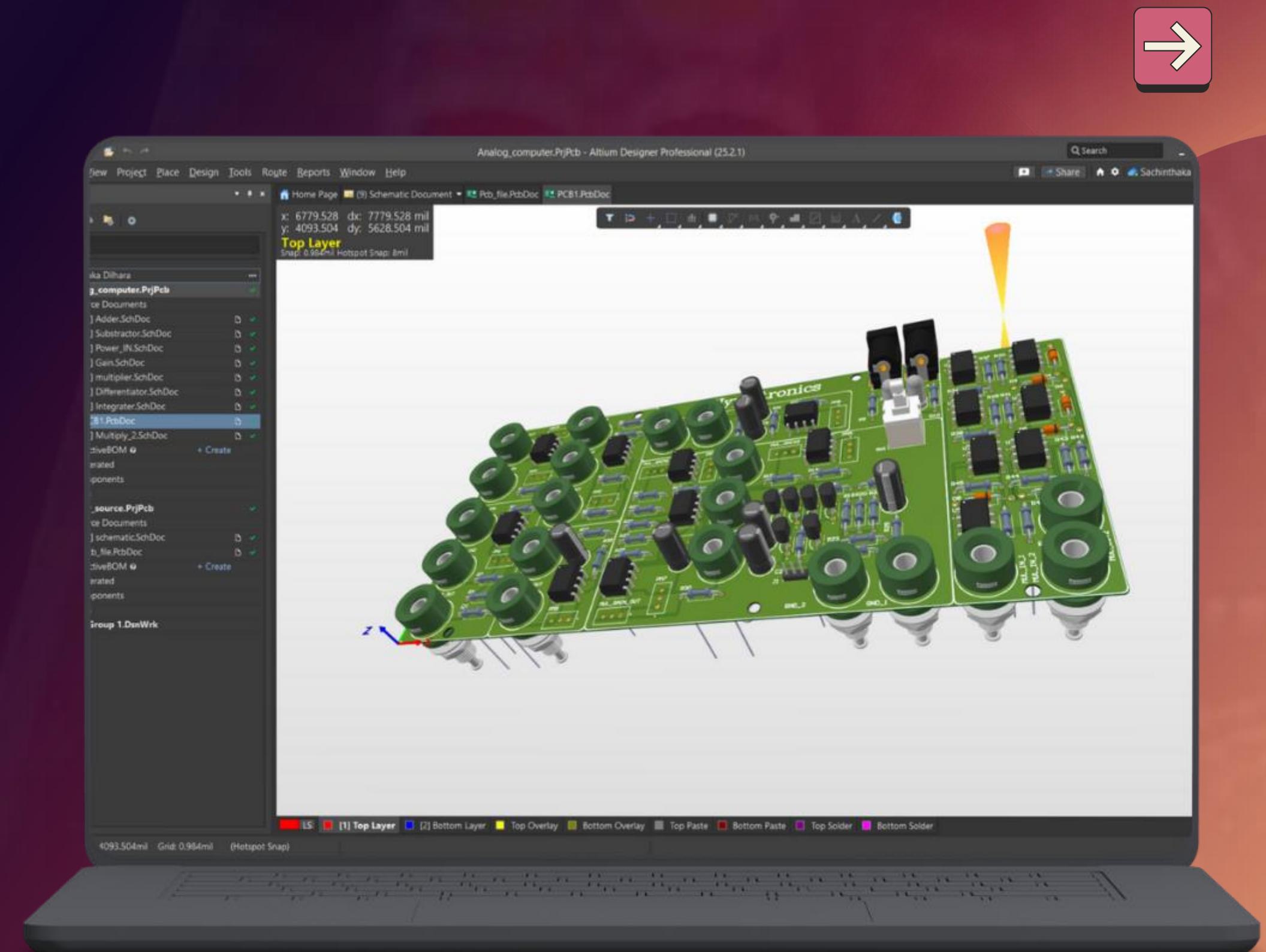


PROJECT INTRODUCTION

Our project aims to demonstrate the functionality of op-amp circuits in performing fundamental analog computations such as:

- addition
- subtraction
- multiplication
- integration
- differentiation

within the 1 Hz to 10 kHz frequency range. It consists of a dual-channel input interface for each operation with control mechanisms for easily adjustable gain and is powered by a stable and clean power supply system, which acts as a separate module.





XXX COMPONENTS & WHY?



UA741

General Purpose OP-Amp

- Widely available and affordable.
- Ideal for basic operations like addition, subtraction
- Bandwidth ($\sim 1 \text{ MHz}$) is sufficient for 1 kHz to 10 kHz signals.
- Stable and easy to implement without complex compensation.



IN4148

Diode

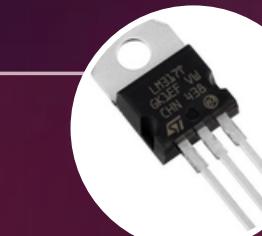
- Widely available and affordable
- IN4148 works linearly at low currents; 1N4007 doesn't.
- Faster response: IN4148 has low junction capacitance and fast switching.
- IN4148 has lower leakage and better temperature stability for small signals.



LM7812/LM7912(Option02)

Fixed 12v voltage regulator

- cheap and widely available
- regulator circuit is simple, not complicated like Adjustable regulator

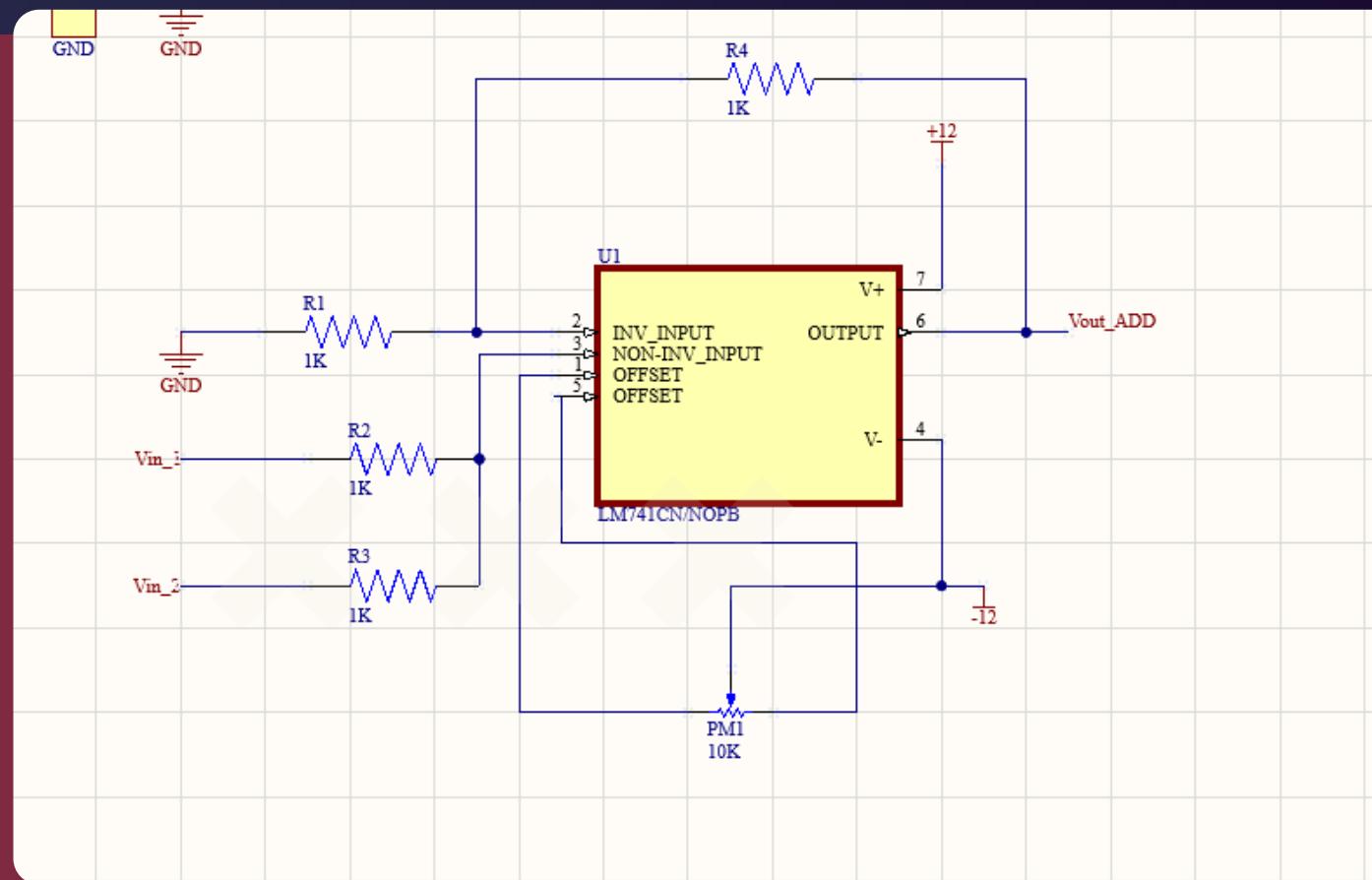


IN4007

Diode

- cheap and widely available
- Withstands up to 1000 V (Peak Reverse Voltage), making it ideal for AC to DC rectifier applications
- Can handle 1 A continuous current

ADDER CIRCUIT



WHY 1KOHM RESISTORS?

Small resistors, such as $100\ \Omega$, draw more current compared to $1\ k\Omega$ resistors, leading to increased power consumption. While higher resistances, like $10\ k\Omega$, are permissible, they tend to produce lower bandwidth. Utilizing very high values, such as $100\ k\Omega$, can even filter out portions of the input signal. Consequently, a $1\ k\Omega$ resistor serves as an excellent choice in this scenario.

KVL

$$V_{out+} - V_+ = i^{\circ} R_4$$

$$V_+ - 0 = i^{\circ} R_1$$

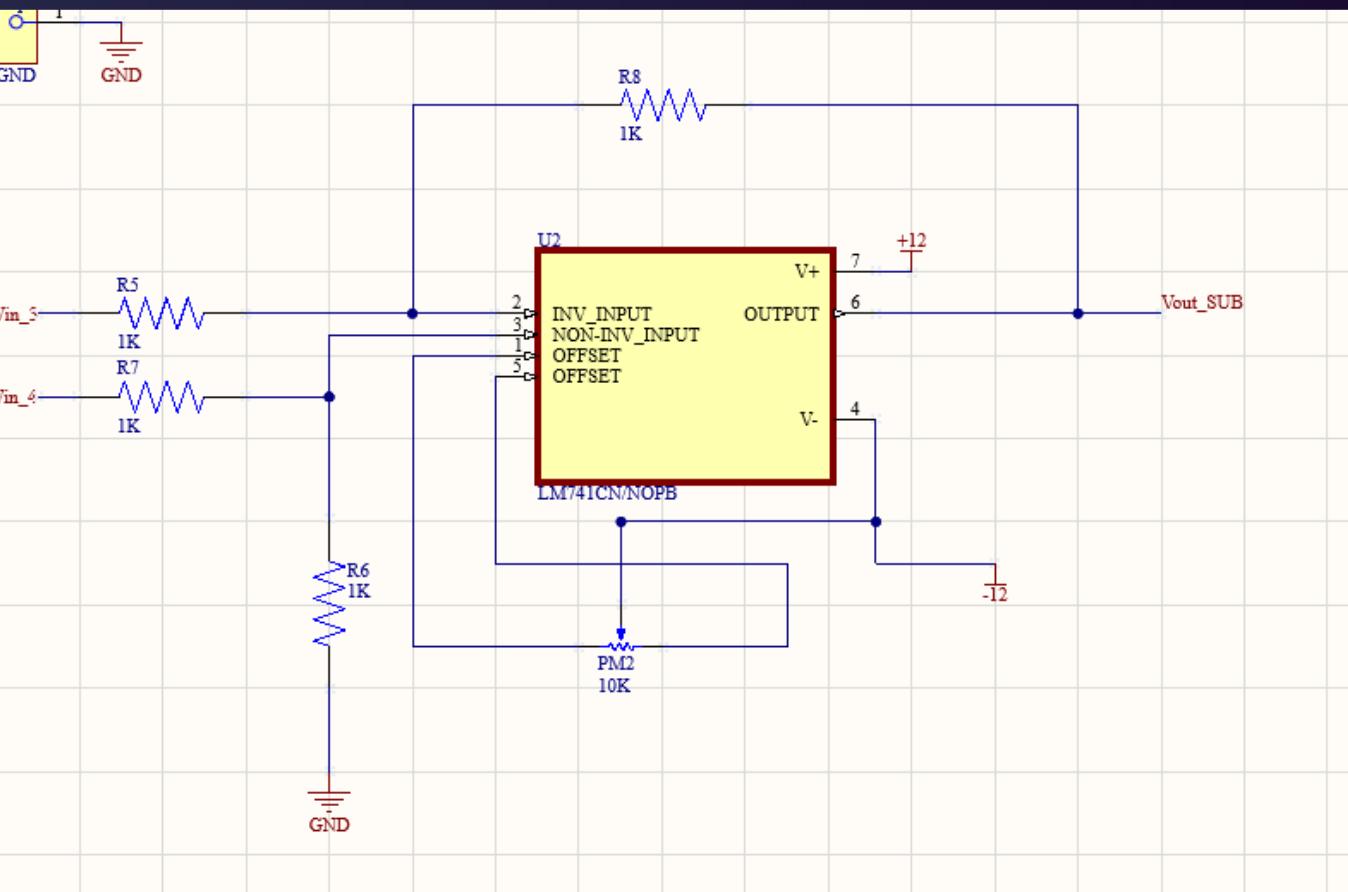
$$V_{out+} = \left(1 + \frac{R_4}{R_1}\right) V_+$$

By superposition theorem;

$$V_+ = V_1 \left(\frac{R_3}{R_2+R_3}\right) + V_2 \left(\frac{R_2}{R_2+R_3}\right)$$

if $R_1 = R_4$ and $\Rightarrow V_+ = \left(\frac{V_1 + V_2}{2}\right)$ and $V_{out+} = 2V_+$
 $R_2 = R_3$

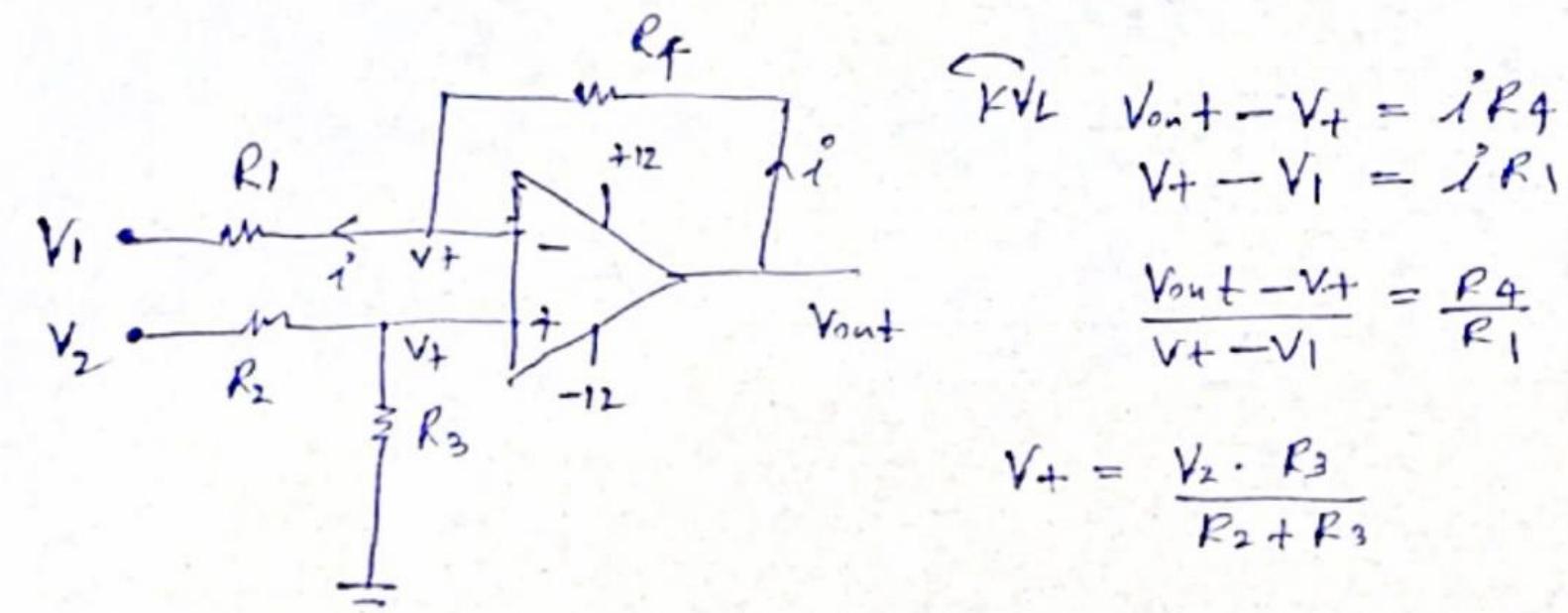
$$\therefore V_{out+} = V_1 + V_2$$



SUBTRACTOR CIRCUIT ✕ ✕ ✕

WHY 1KOHM RESISTORS?

Small resistors, like $100\ \Omega$, draw more current compared to $1\ k\Omega$, which leads to increased power consumption. While higher resistors, such as $10\ k\Omega$, are permissible, they tend to offer lower bandwidth. If we opt for an excessively high value, like $100\ k\Omega$, it may filter out certain portions of the input signal. Thus, a $1\ k\Omega$ resistor is an excellent choice in this scenario.



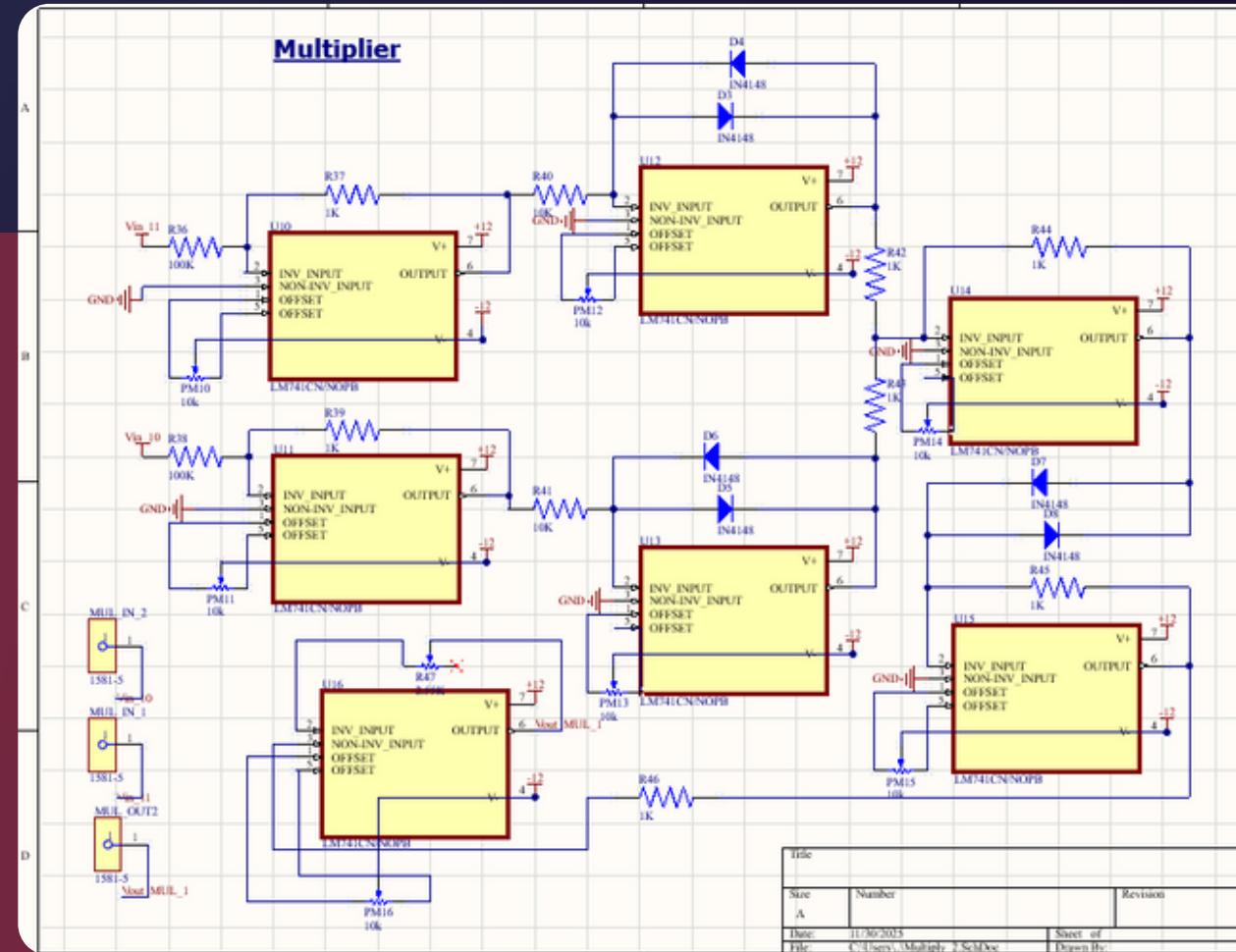
$$\text{if } R_1 = R_2 = R_3 = R_4 \Rightarrow V_{out} + V_1 = 2V_+$$

$$\text{and } V_+ = \frac{V_2}{2}$$

$$\therefore V_{out} = V_2 - V_1$$



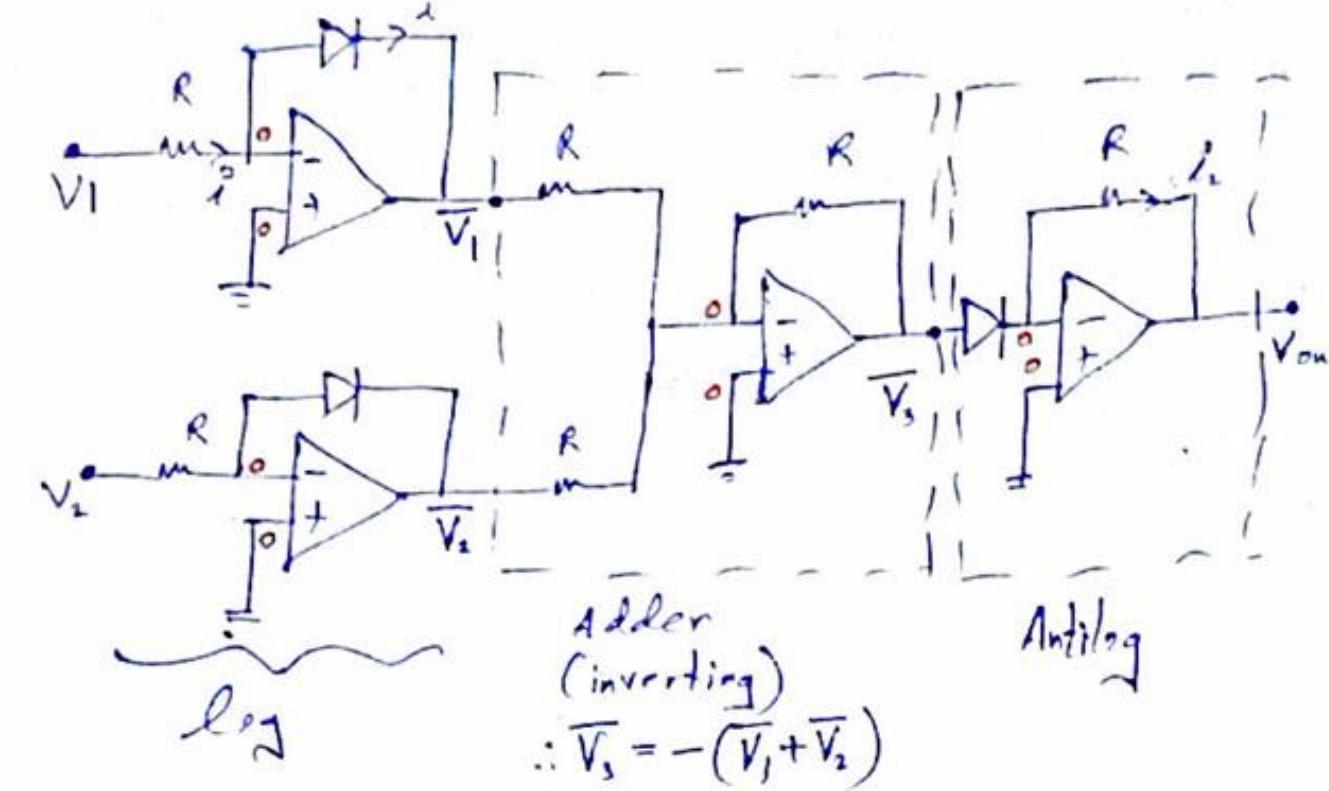
Multiplexer



MULTIPLIER CIRCUIT

WHY HIGHER INPUT RESISTORS?

In log/antilog multipliers, using large resistors helps ensure that the input voltage generates a small current. This approach maintains a more linear and predictable log function.



Suppose positive half cycle of V_1 :

$$\frac{V_1}{V_T} = -iR \rightarrow i = \frac{V_1}{R}$$

$$\text{Similarly; } V_2 = -V_T \ln\left(\frac{V_1}{R I_s}\right) \quad \text{---(1)}$$

$$\overline{V}_2 = -V_T \ln\left(\frac{V_2}{R I_s}\right) \quad \text{---(2)}$$

$$\left. \begin{aligned} V_3 &= (\overline{V}_1 + \overline{V}_2) \times -1 \\ &= +V_T \left[\ln\left(\frac{V_1}{R I_s}\right) + \ln\left(\frac{V_2}{R I_s}\right) \right] \\ &= +V_T \left[\ln\left(\frac{V_1 \cdot V_2}{R^2 I_s}\right) \right] \end{aligned} \right\}$$

$$-\frac{V_{out}}{R} + \sigma = i_2$$

$$i_2 = I_s e^{\frac{(\overline{V}_3 - \sigma)}{V_T}}$$

$$-\frac{V_{out}}{R I_s} = e^{\frac{+V_T \ln\left(\frac{V_1 V_2}{R^2 I_s}\right)}{V_T}} = \left(\frac{V_1 V_2}{R^2 I_s}\right)^{+1}$$

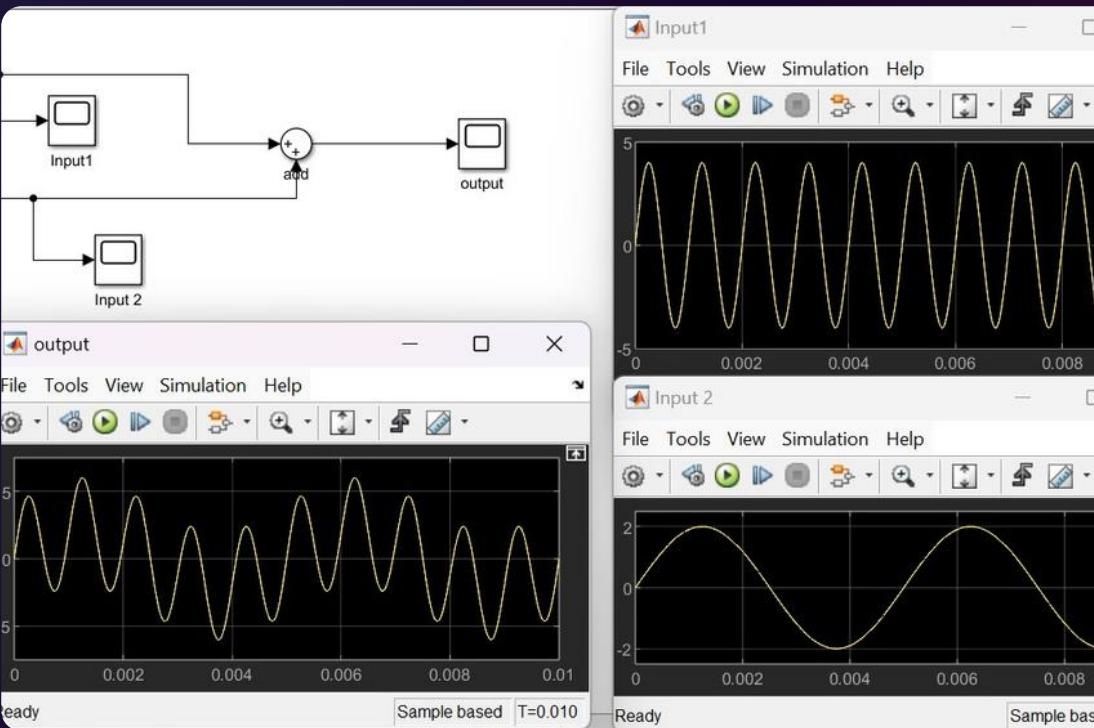
$$\therefore V_{out} = V_1 \cdot V_2$$



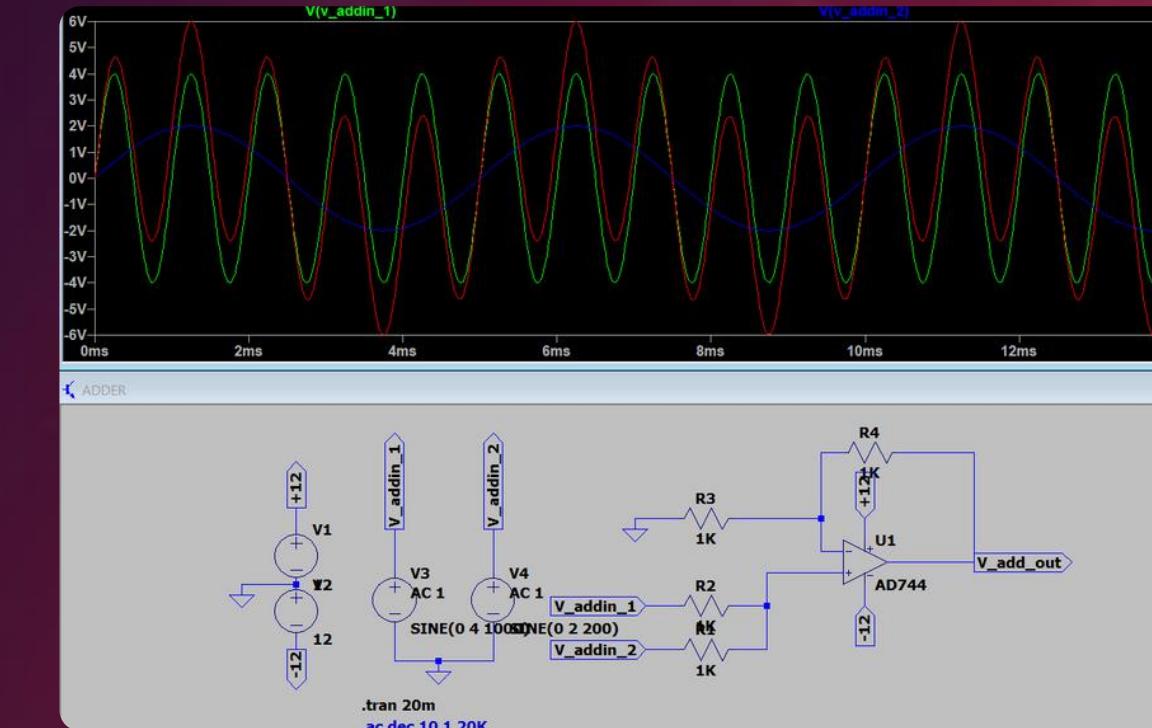
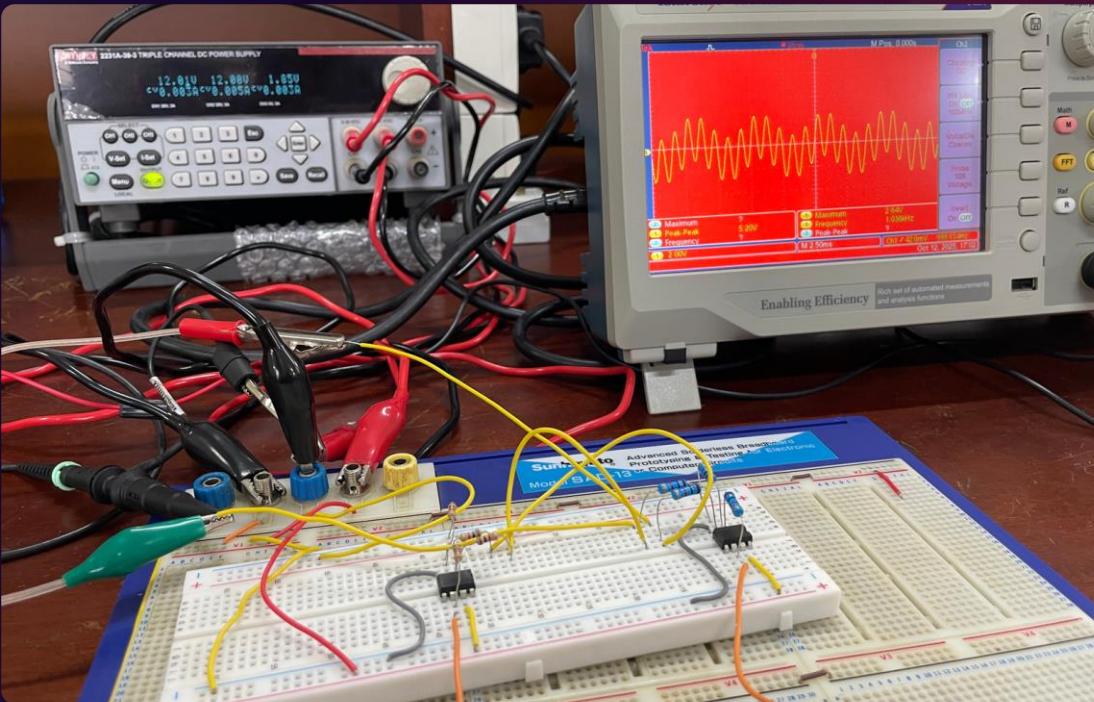
ADDER SIMULATION RESULTS & BREADBOARD/FINAL IMPLEMENTATION



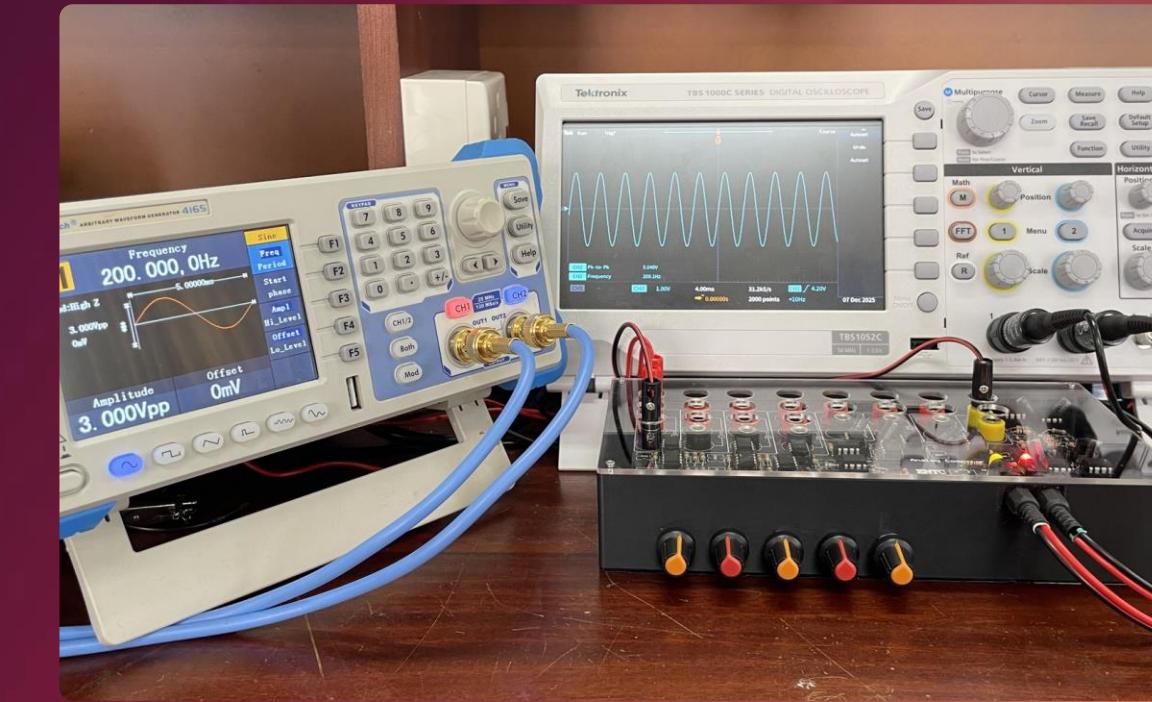
SIMULINK



BREADBOARD
IMPLEMENTATION



LT-SPICE



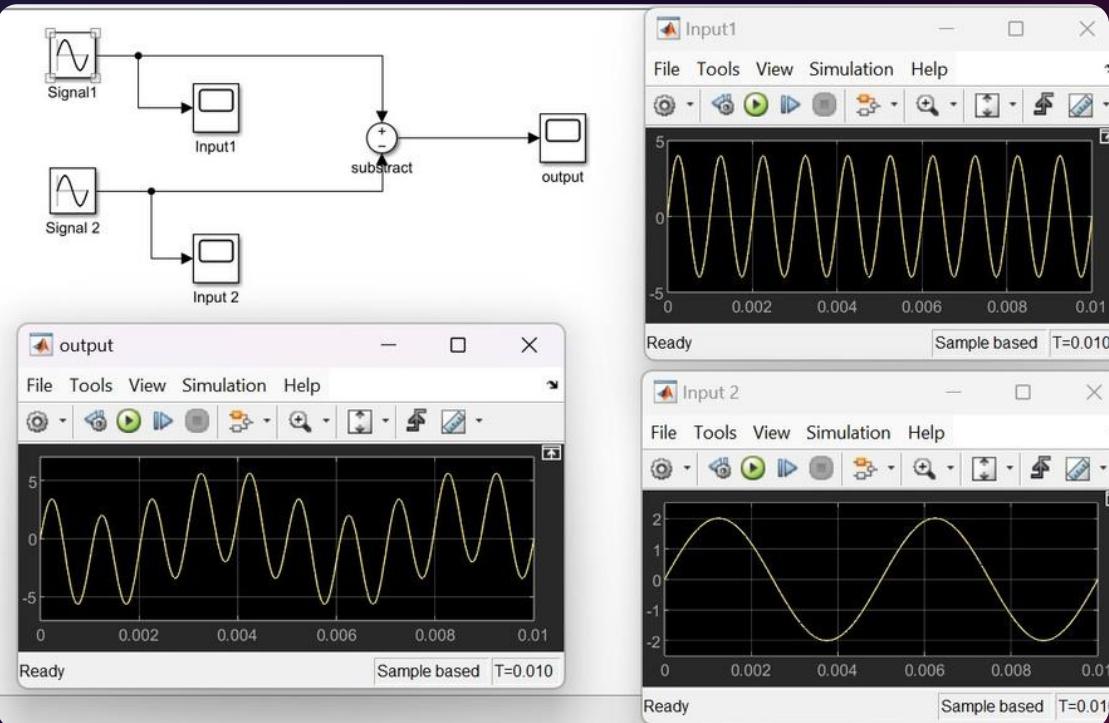
FINAL
IMPLEMENTATION



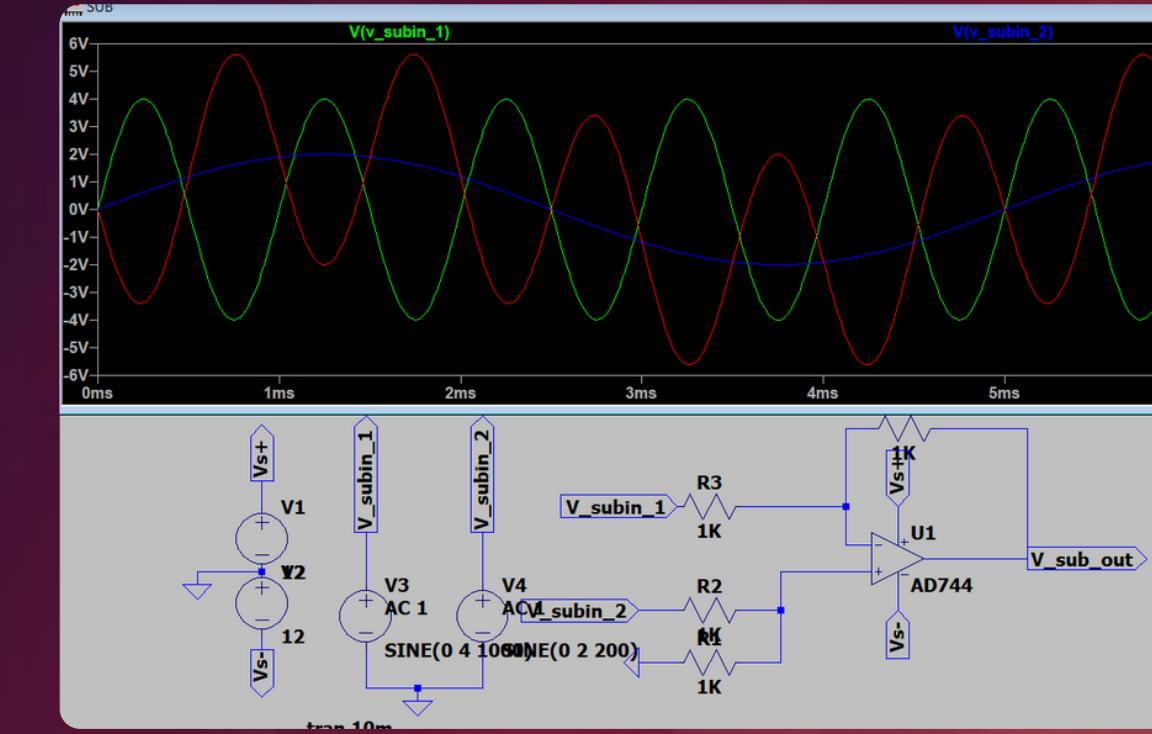
SUBTRACTOR SIMULATION RESULTS & BREADBOARD/FINAL IMPLEMENTATION



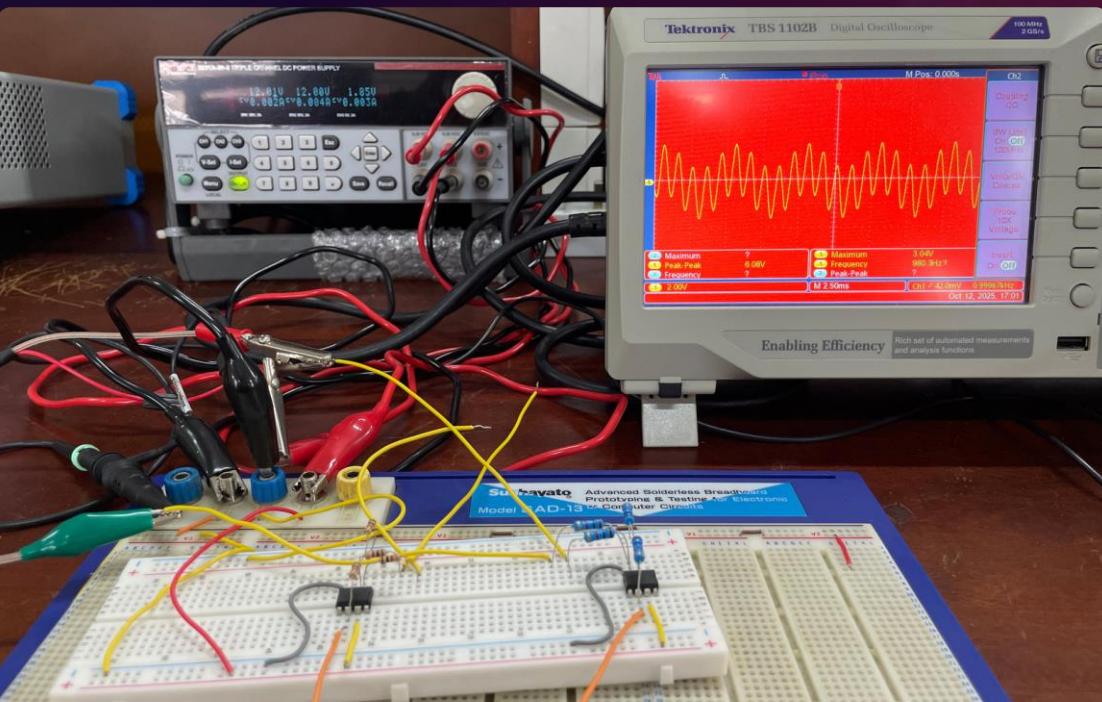
SIMULINK



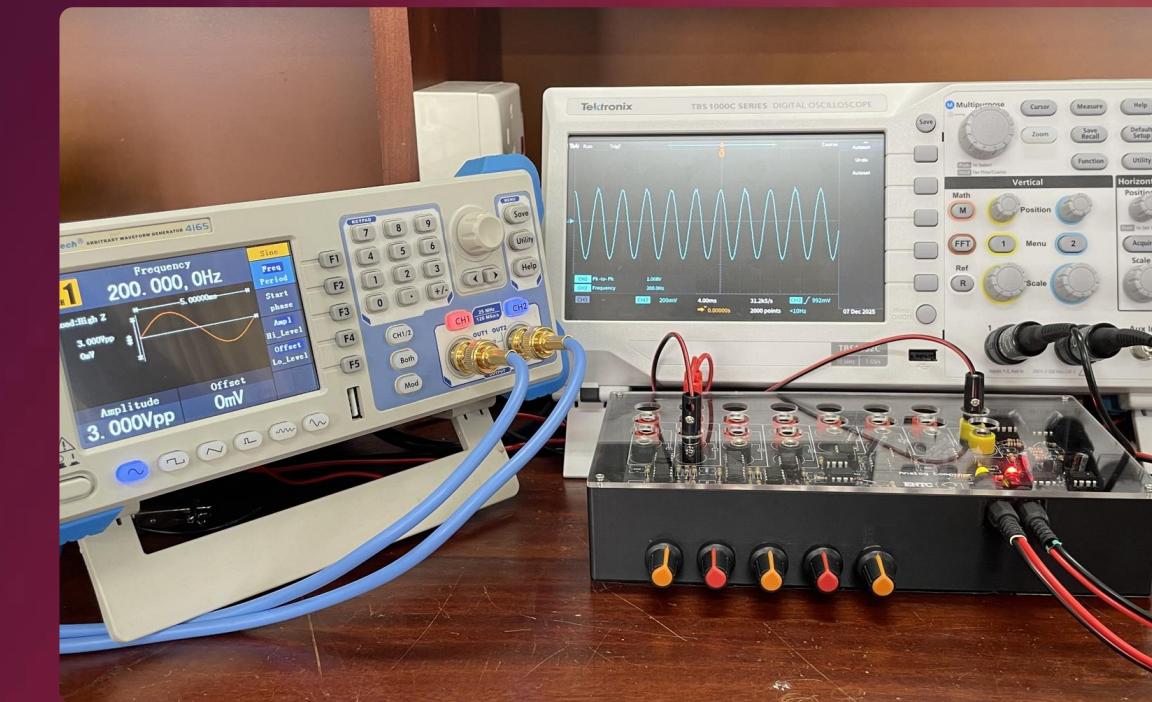
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**BREADBOARD
IMPLEMENTATION**



**FINAL
IMPLEMENTATION**

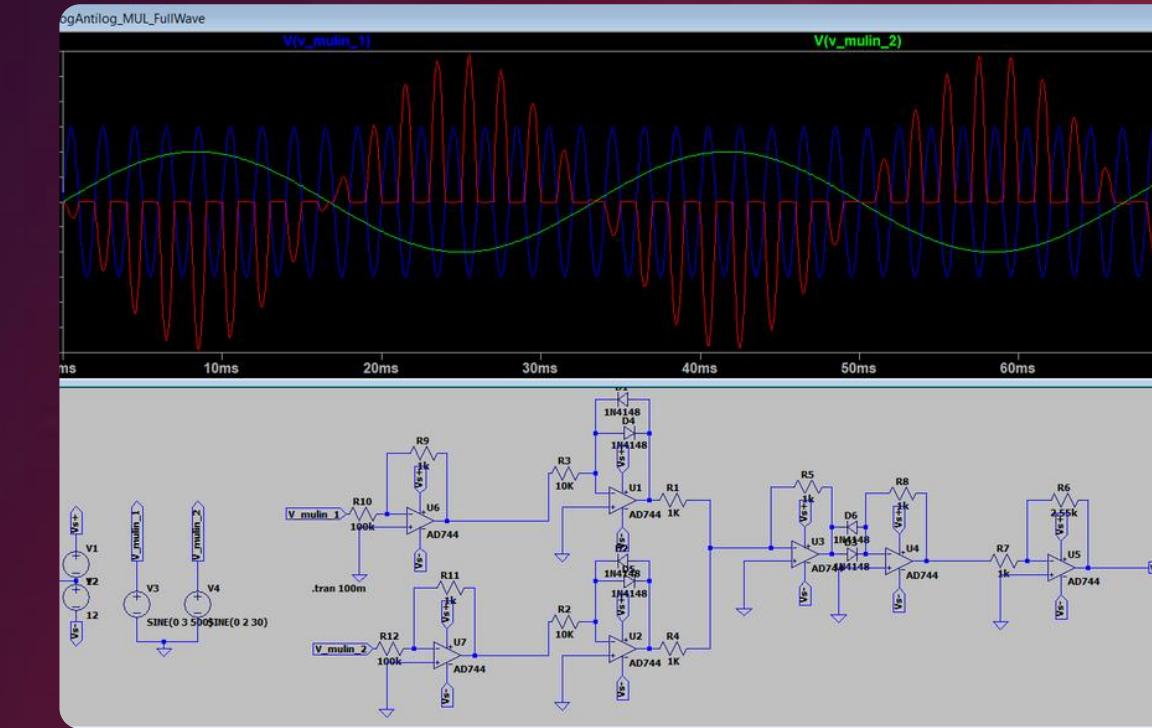
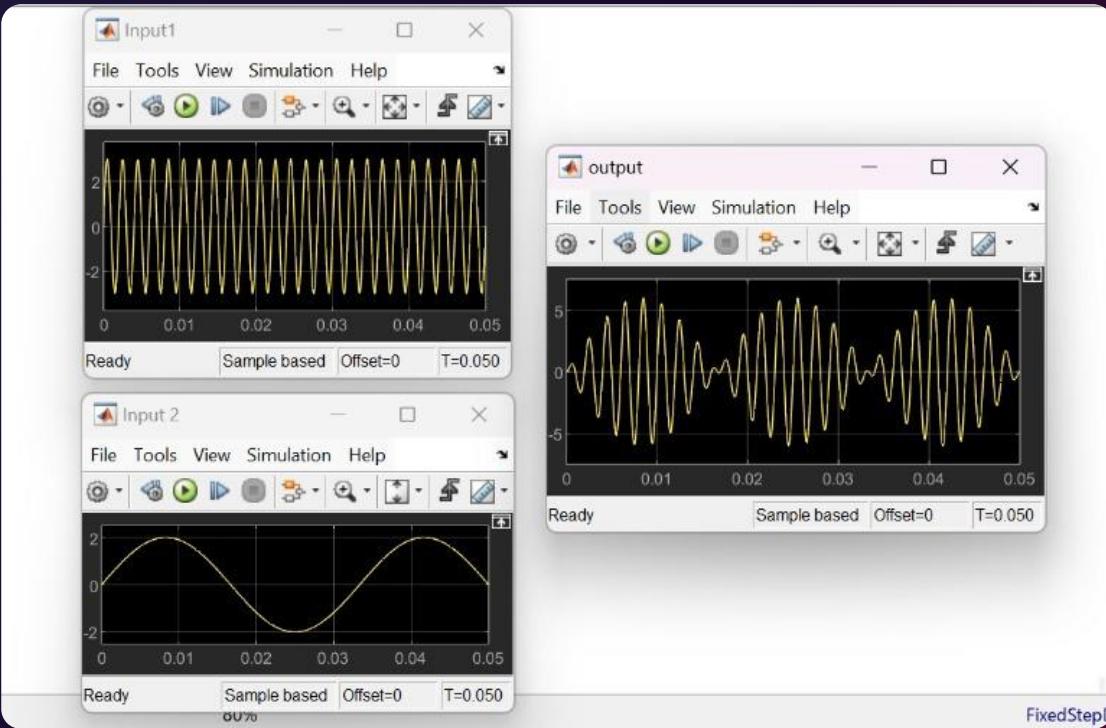




MULTIPLIER SIMULATION RESULTS & BREADBOARD/FINAL IMPLEMENTATION

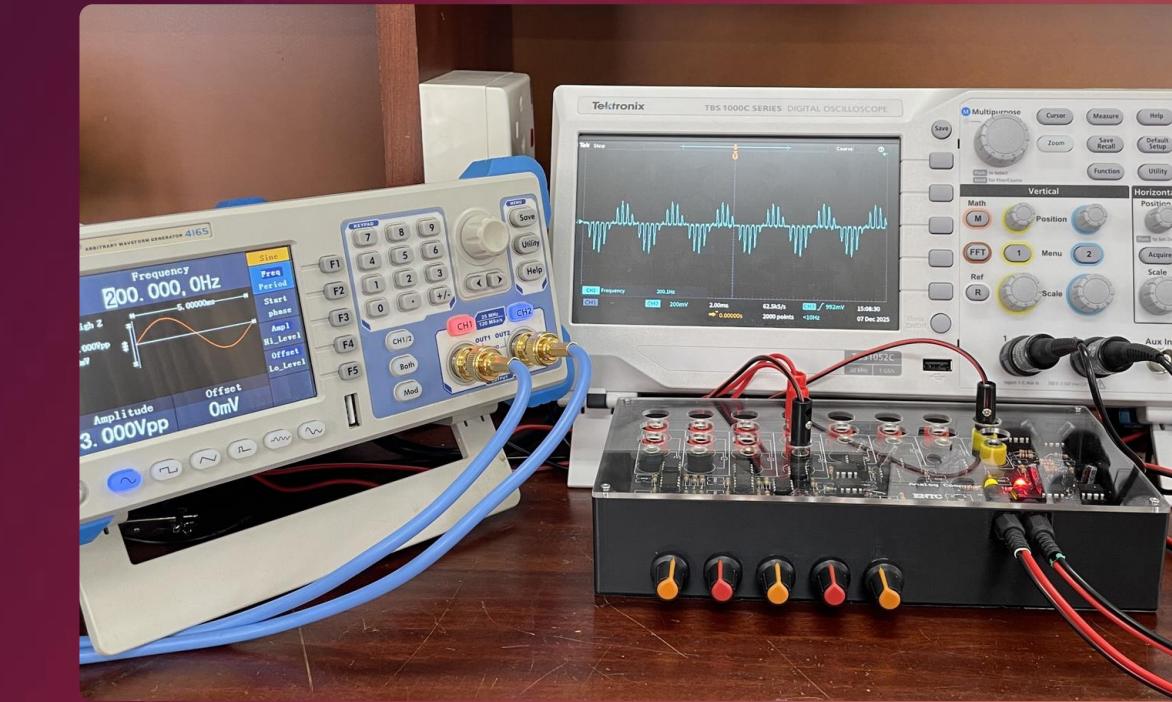
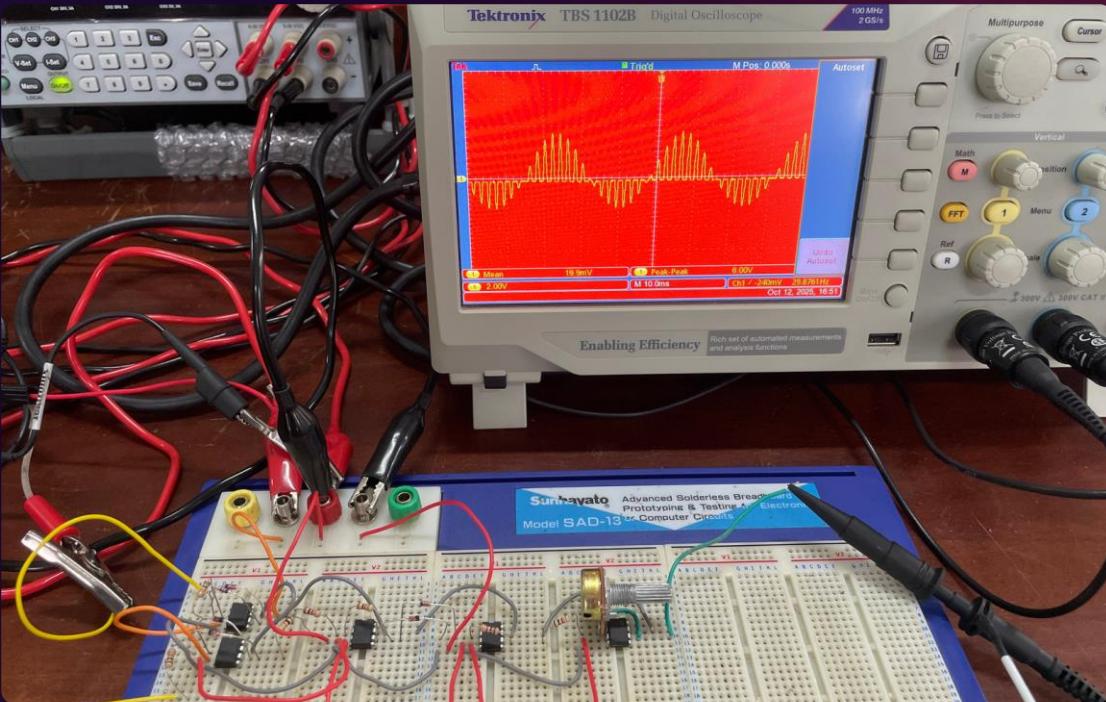


SIMULINK



LT-SPICE

BREADBOARD
IMPLEMENTATION

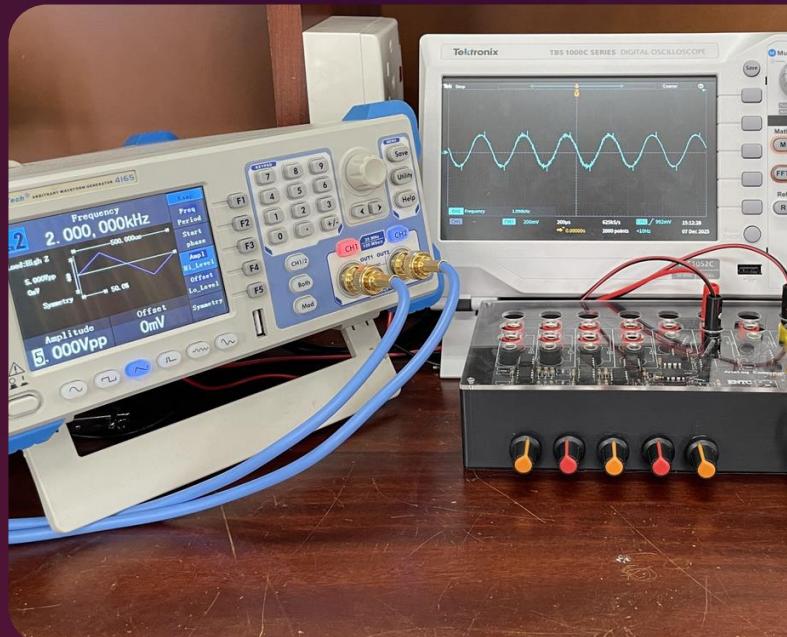
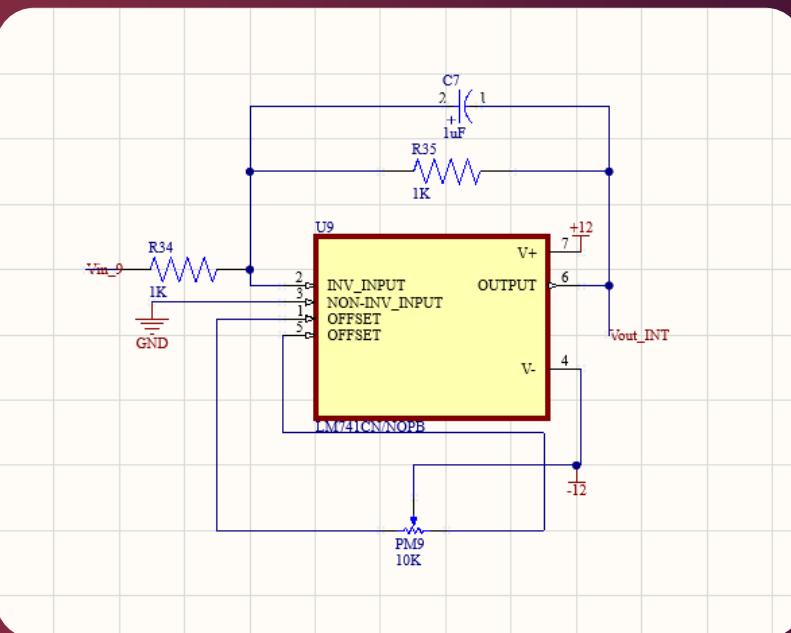


FINAL
IMPLEMENTATION

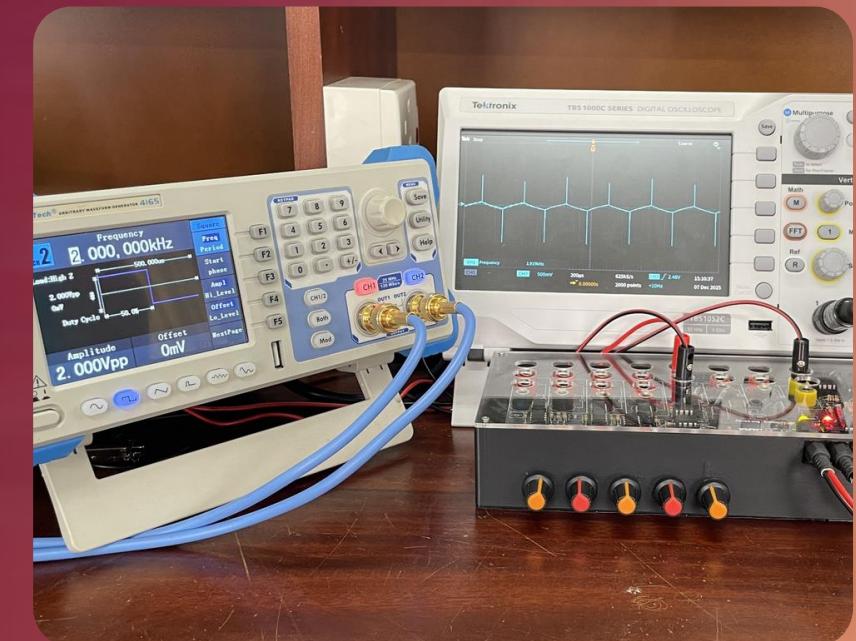
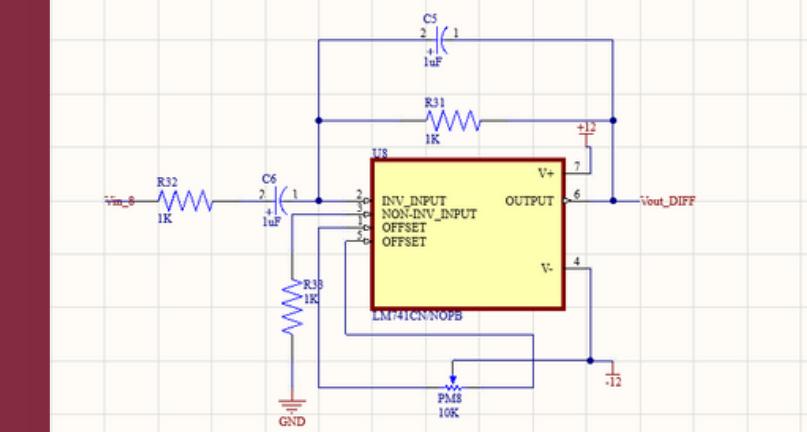


× × × ADDITIONAL CIRCUITS

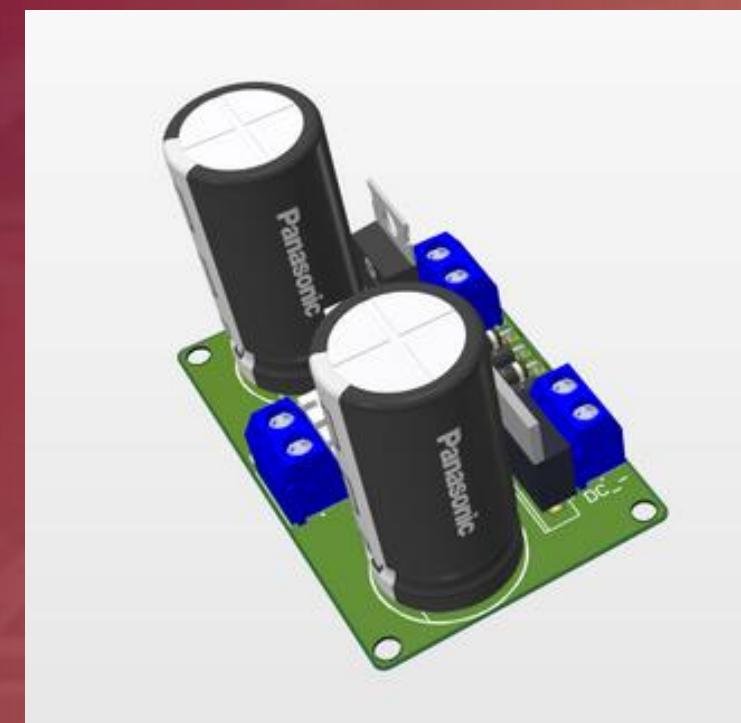
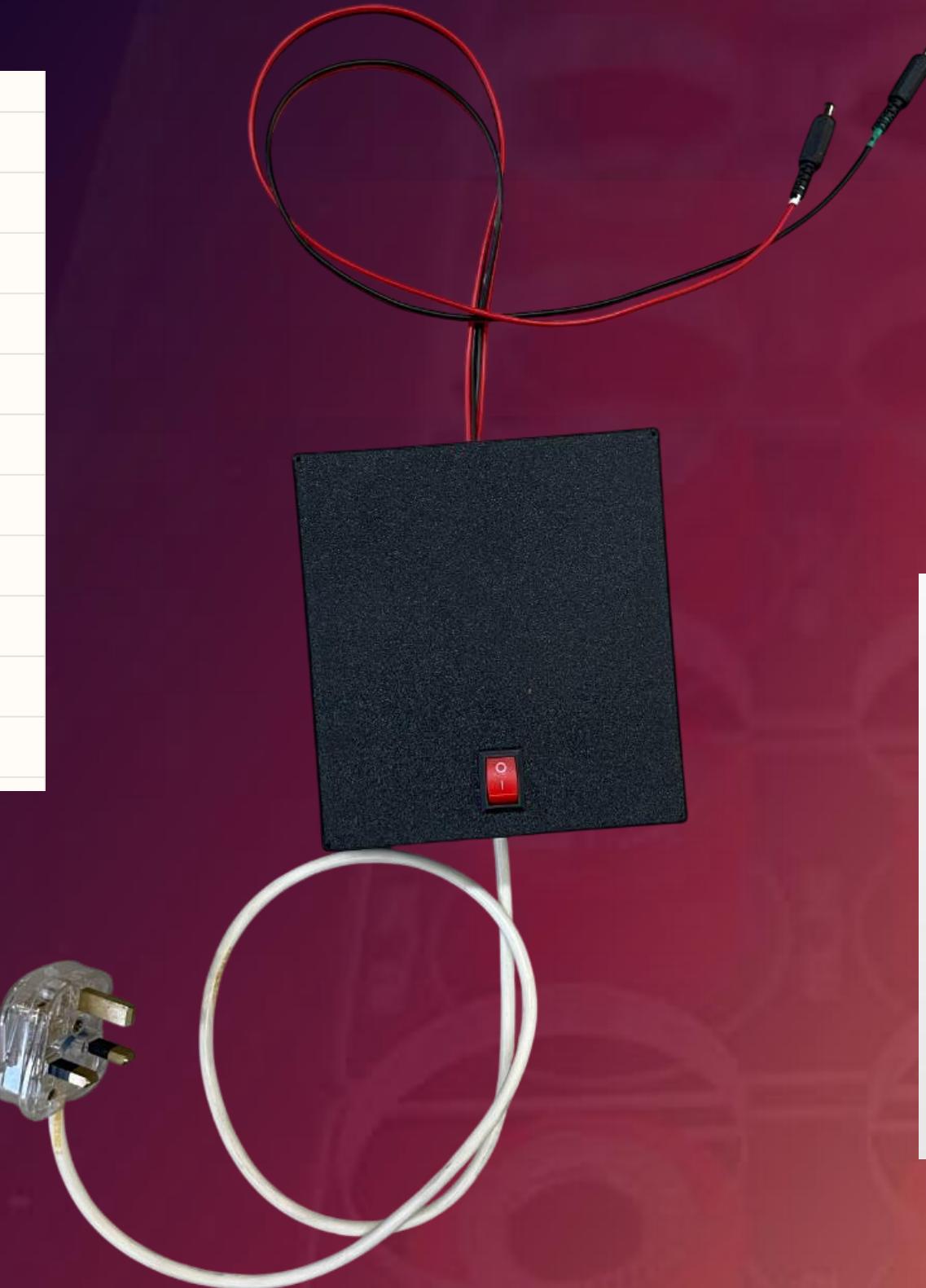
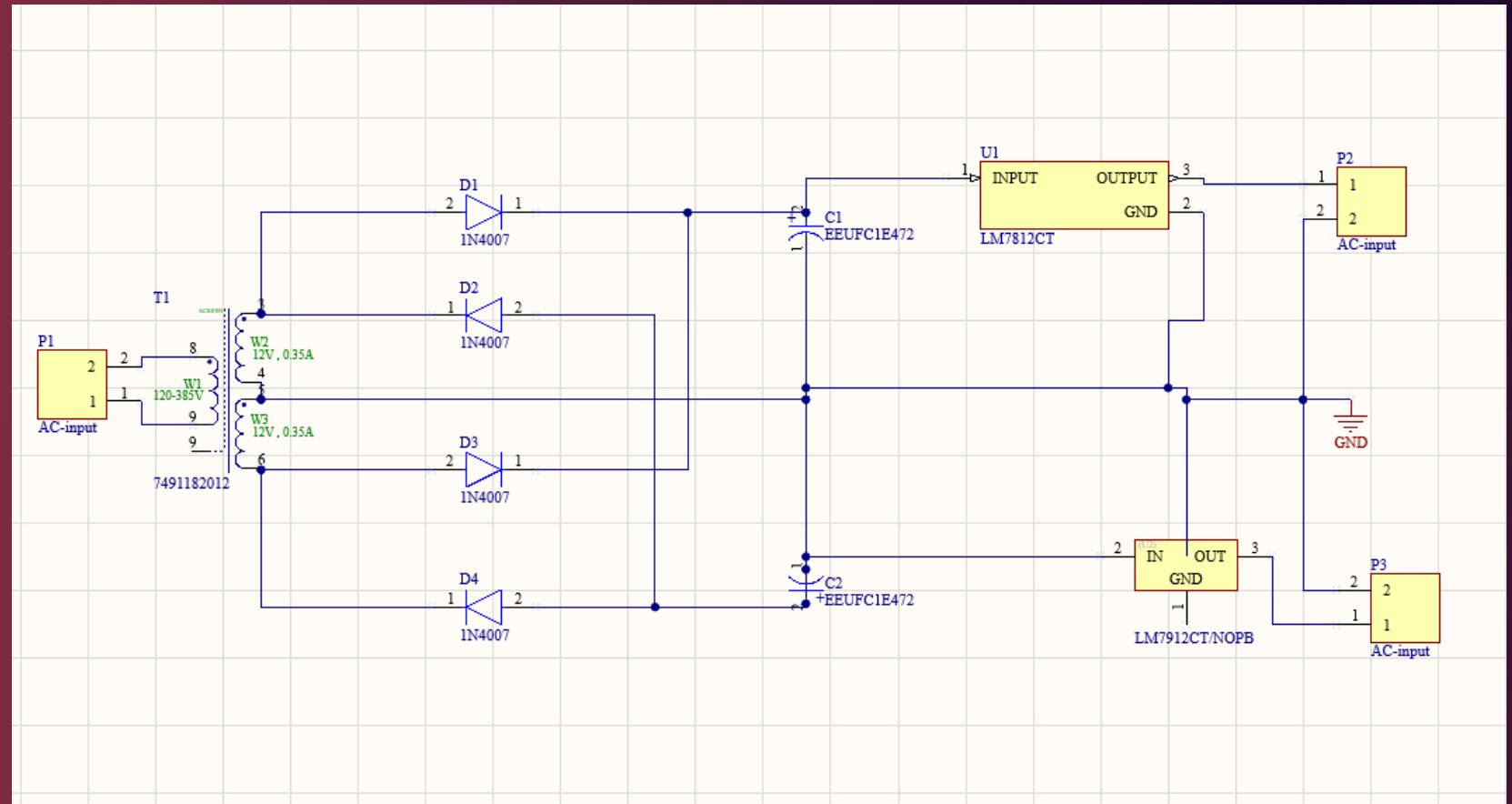
INTEGRATOR



DIFFERENTIATOR

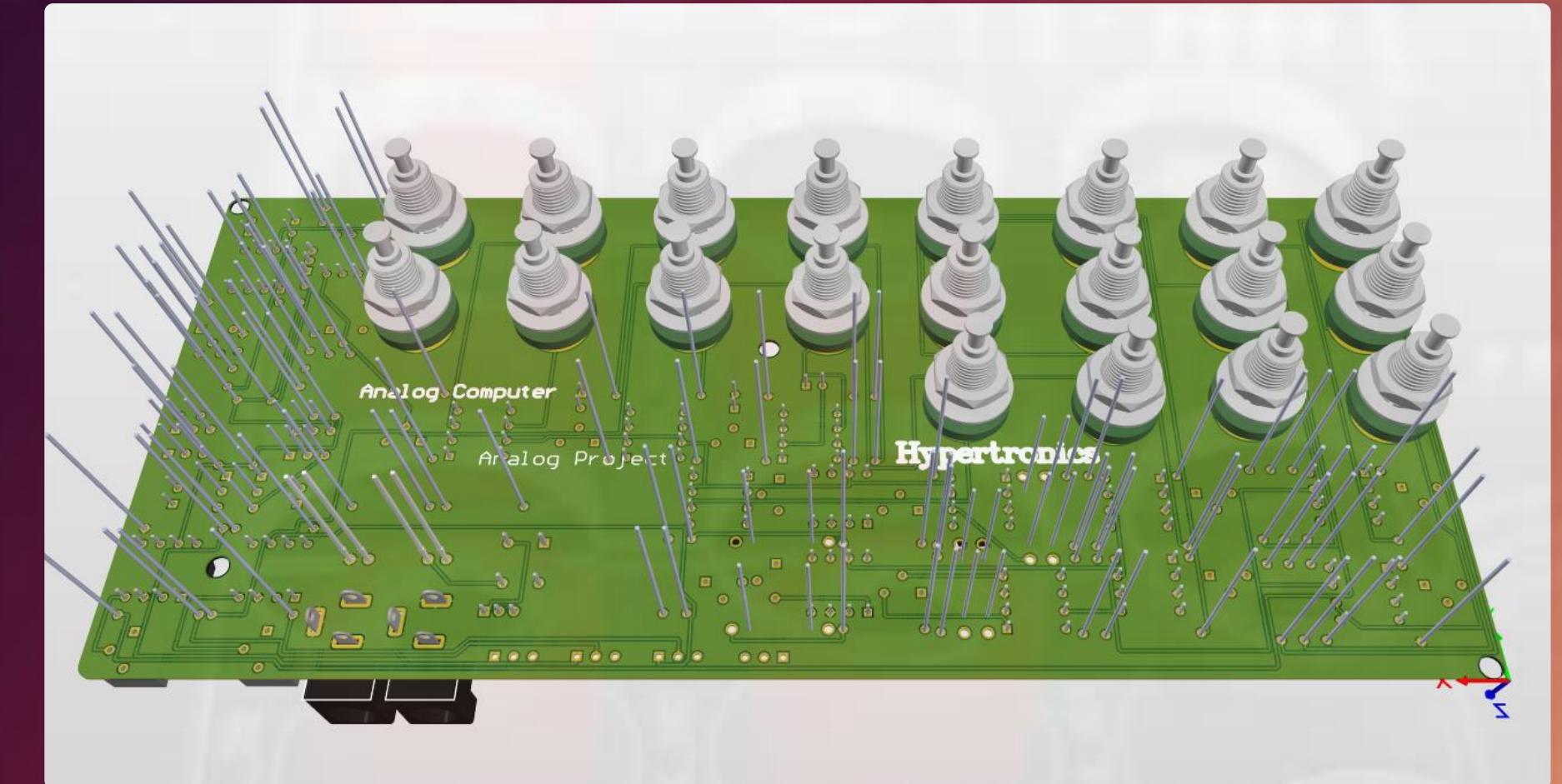
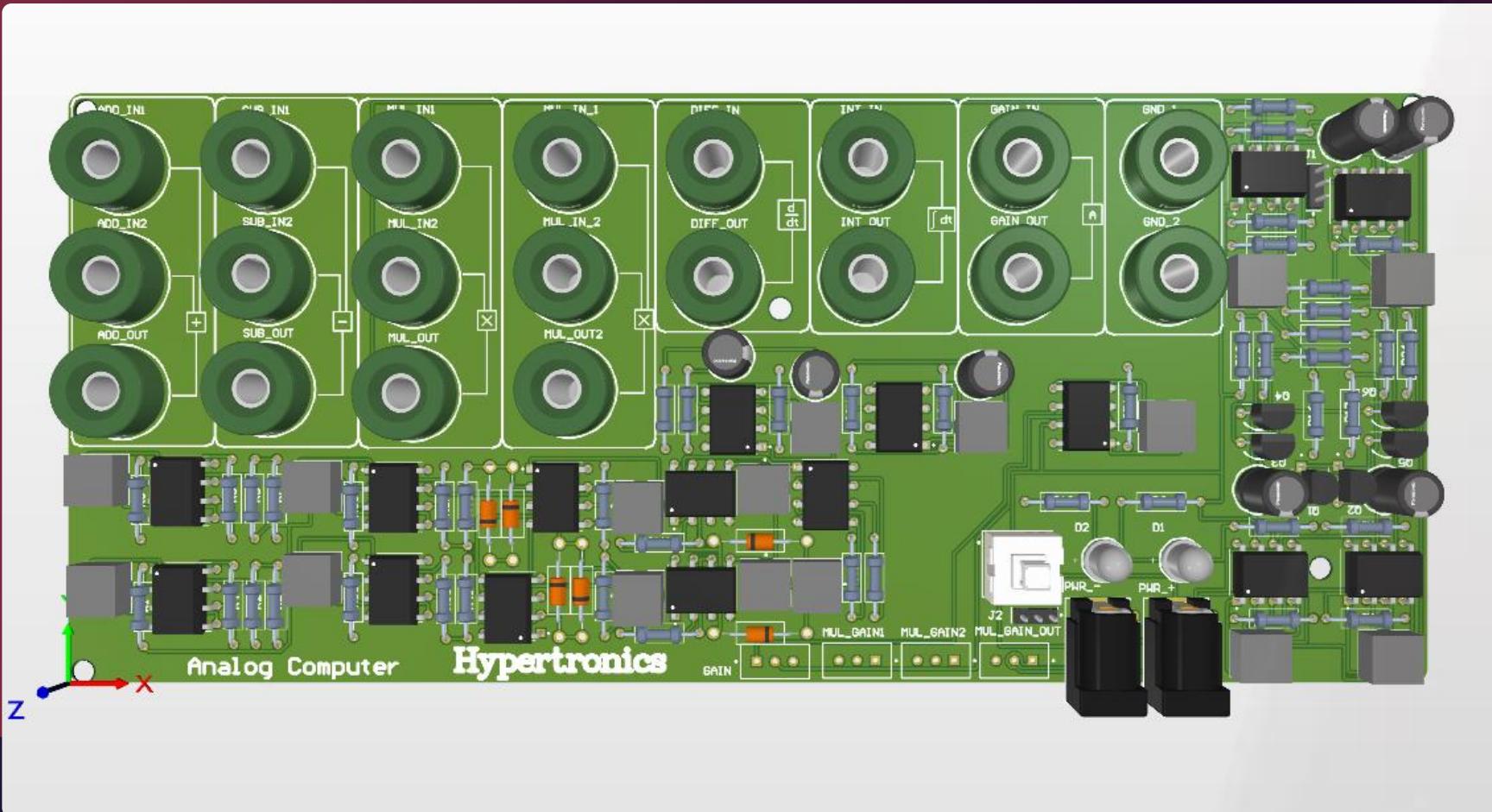


POWER SUPPLY FIXED $\pm 12V$



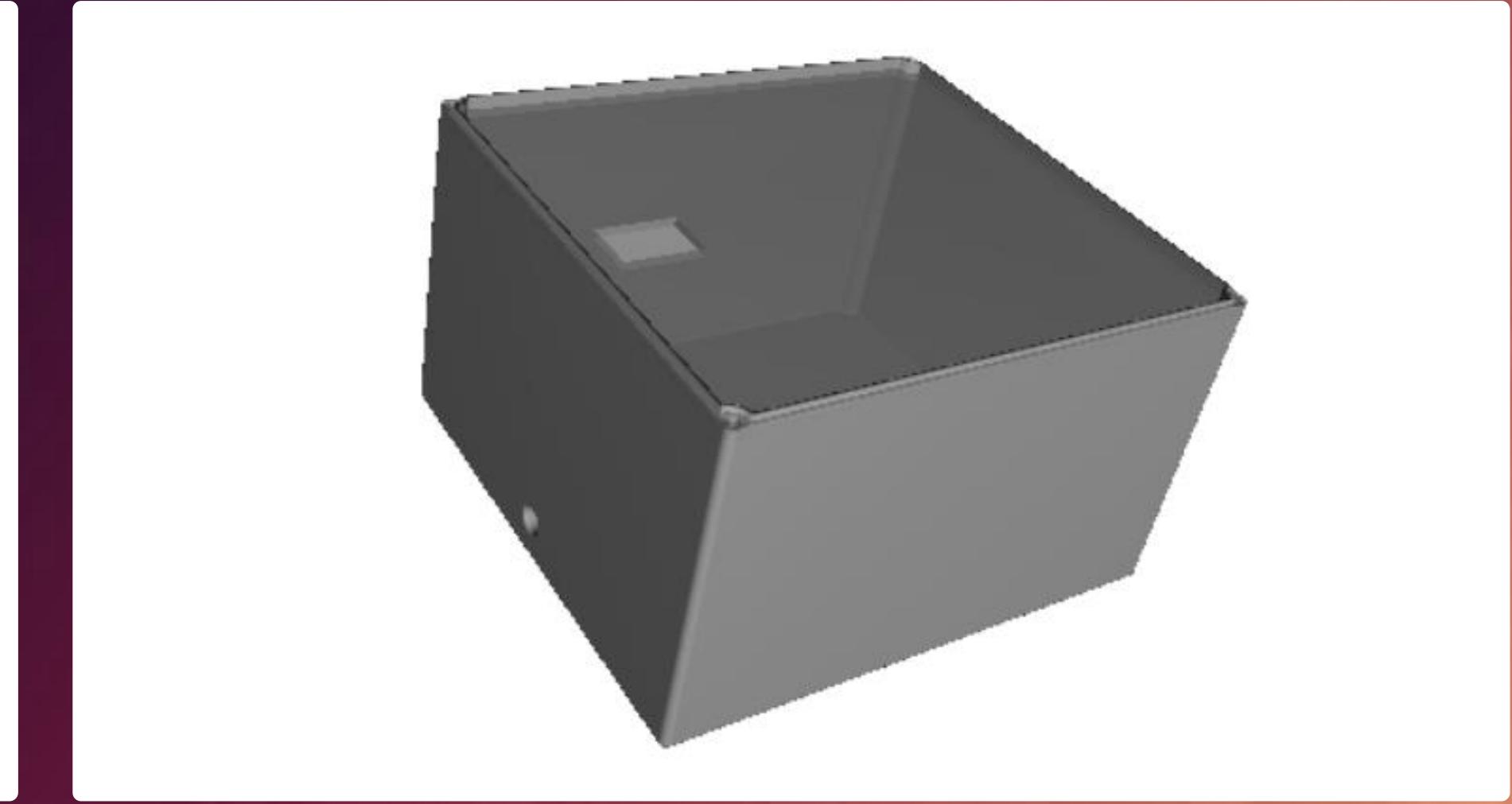
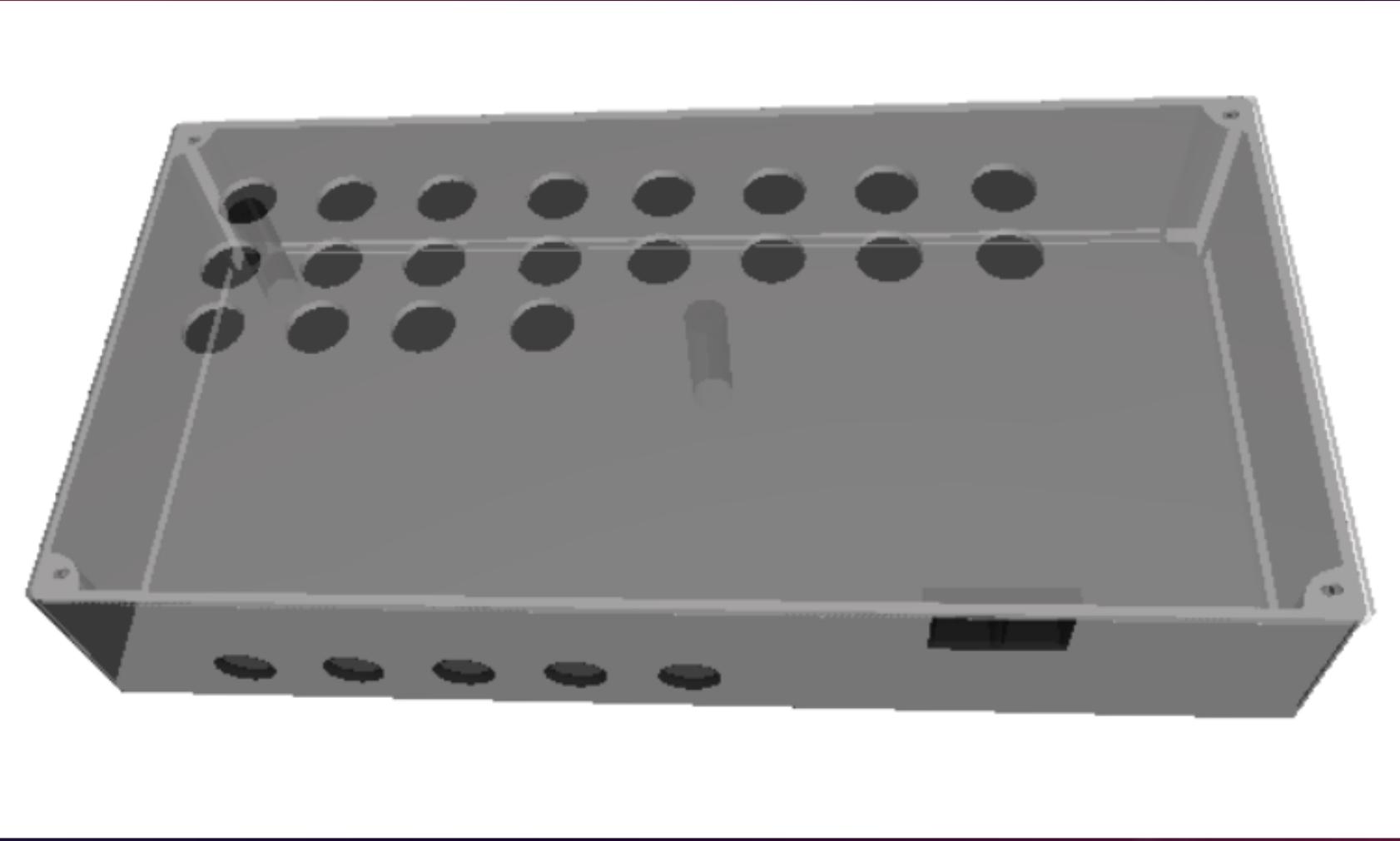


PCB DESIGN





ENCLOSURE DESIGN





CHALLENGES & RESULTS

- We Achieved the expected results with the project.
- Our Main challenge was the mismatch among BJTs in the Gilbert cell led to unexpected non-linear behavior in the multiplier circuit.
- We Overcome that issue by Replacing the Gilbert cell with a Log-Antilog multiplier with some modifications.
- It Improved linearity and allowed the circuit to produce the desired output.

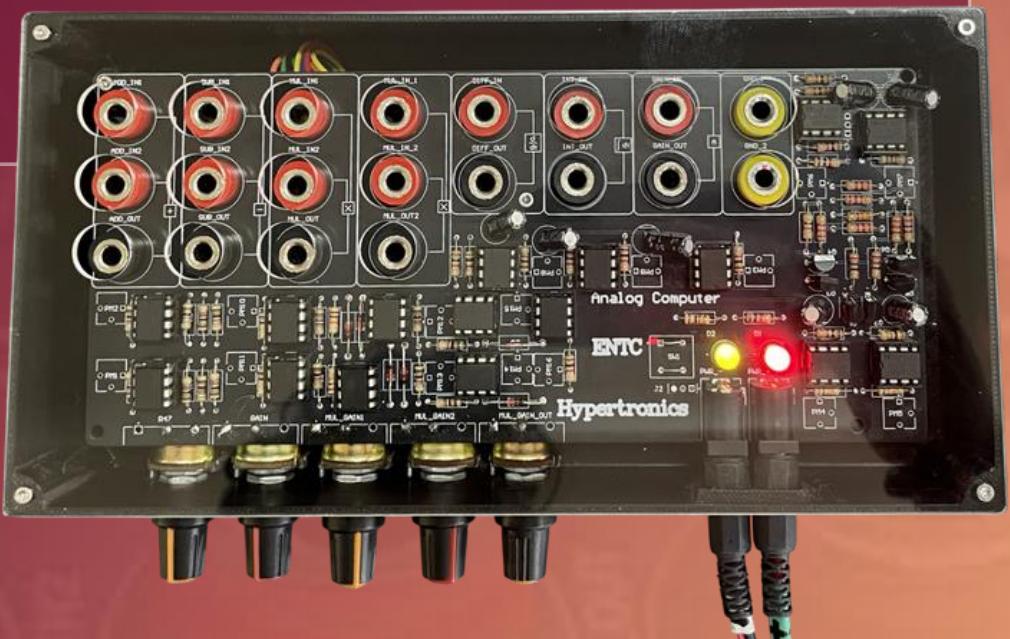




DEVICE PARAMETERS



• Maximum Supply Voltage	$\pm 18\text{v}$ ($\pm 12\text{v}$ Recommended)
• Maximum input Current	10mA
• Max/Min output Voltage	$\pm 12\text{V}$
• Bandwidth	1–10kHz
• Maximum Noise Level	100mV
• Accuracy	$\pm(1\text{--}10)\%$
• Maximum Gain	x10





TASK ALLOCATION



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Wijesinghe.U.G.S.K.D

*Simulation & component selection
PCB schematic design*



230724E

Wijesekara.W.A.G.S

*powersupply design
soldering*



230147L
DILHARA.D.S

*PCB design
breadboard implementation*



230659H

UPEKSHANI T. S.

*Enclosure Design
breadboard implementation*





THANK YOU

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