Extending this idea to set of n points.



Joining of segments 2 GEAMENTS: P, P2 P3 (Points) Pi P2 P3 (Tangents)

where P2 and P2 are the intermediate point and its tangent vector which is determined through some continuity contraint.

order (k-1) at the internal joints.

Thus lubic oplines have second order continuity ie. ?"(t) is continuous over the joint.

$$\begin{aligned}
f(t) &= \beta_1 + \beta_2 t + \beta_3 t^2 + \beta_4 t^3 \\
&= \underbrace{\frac{1}{\beta_1}}_{i=1}^{n} \beta_i t^{i-1} \qquad t_1 \leq t \leq t_2
\end{aligned}$$

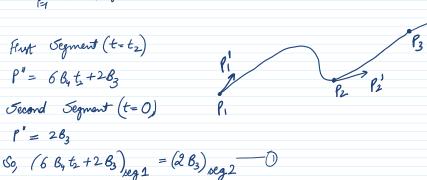
$$\rho'(t) = \beta_{2} + 2\beta_{3}t + 3\beta_{4}t^{2}$$

$$= \sum_{i=1}^{4} (-i)\beta_{i}t^{i-2}$$

$$\rho''(t) = 2\beta_3 + 6\beta_4 t$$

$$= \frac{4}{5}(i-i)(i-2)\beta_i t^{i-3} \qquad t \le t \le t_2$$

Flut Segment (t-t2) P"= 6B4 t2+2B3 Jecond Segment (t=0) P' = 2B2



We know,

$$\beta_{1} = \beta_{1}$$

$$\beta_{2} = \beta_{1}^{1}$$

$$\beta_{3} = \frac{3(\beta_{2} - \beta_{1})}{t_{2}^{2}} - \frac{2(\beta_{1}^{2})}{t_{2}} - \frac{\beta_{2}^{1}}{t_{2}}$$

$$\beta_{4} = \frac{2(\beta_{1} - \beta_{2})}{t_{2}^{3}} + \frac{\beta_{1}^{1}}{t_{2}^{2}} + \frac{\beta_{2}^{1}}{t_{2}^{2}}$$

Substituting by and by from A in

$$3 \left[\frac{2(\ell_{1} - \ell_{2})}{t_{2}^{3}} + \frac{\ell_{1}'}{t_{2}^{2}} + \frac{\ell_{2}'}{t_{2}^{2}} \right] t_{2} + \left[\frac{3(\ell_{2} - \ell_{1})}{t_{2}^{2}} - \frac{2\ell_{1}'}{t_{2}} - \frac{\ell_{2}'}{t_{2}} \right]$$

$$= \left[\frac{3(\ell_{3} - \ell_{2})}{t_{3}^{2}} - \frac{2\ell_{2}'}{t_{3}} - \frac{\ell_{3}'}{t_{3}} \right]$$

$$\frac{6(\rho_{1}-\rho_{2})}{t_{2}^{2}} + \frac{3\rho_{1}^{2}}{t_{2}} + \frac{3\rho_{2}^{2}}{t_{2}} + \frac{3(\rho_{2}-\rho_{1})}{t_{2}^{2}} - \frac{2\rho_{1}^{2}}{t_{2}} - \frac{\rho_{2}^{2}}{t_{2}}$$

$$= \frac{3(\rho_{3}-\rho_{2})}{t_{2}^{2}} - \frac{2\rho_{2}^{2}}{t_{3}} - \frac{\rho_{3}^{2}}{t_{3}}$$

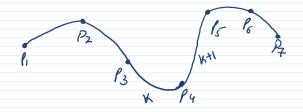
$$\frac{3P_{1}' + 3P_{2}' - 2P_{1}' - P_{2}' + 2P_{2}' + P_{3}'}{t_{2} t_{2} t_{2} t_{2}} + \frac{2P_{2}' + P_{3}'}{t_{3}} \\
= 3(P_{3} - P_{2}) - 6(P_{1} - P_{2}) - 3(P_{2} - P_{1}) \\
t_{3}^{2} t_{2}^{2} t_{2}^{2} t_{2}^{2}$$

$$t_{2}t_{3} \times \left(\frac{\rho_{1}'}{t_{2}} + \frac{2\rho_{2}'}{t_{2}} + \frac{2\rho_{2}'}{t_{3}} + \frac{\rho_{3}'}{t_{3}} = \frac{3(\rho_{3} - \rho_{2})}{t_{3}^{2}} + \frac{3(\rho_{2} - \rho_{1})}{t_{2}^{2}}$$

$$t_{3}\rho_{1}' + 2(t_{3} + t_{2})\rho_{2}' + t_{2}\rho_{3}' = \frac{3t_{2}(\rho_{3} - \rho_{2})}{t_{2}} + \frac{3t_{3}(\rho_{2} - \rho_{1})}{t_{2}}$$

$$t_{3}l_{1}' + 2(t_{3}+t_{2})l_{2}' + t_{2}l_{3}' = \frac{3}{t_{2}t_{3}} \left(t_{2}^{2}(l_{3}-l_{2}) + t_{3}^{2}(l_{2}-l_{1}) \right)$$

$$\begin{bmatrix} t_3 & 2(t_3+t_2) & t_2 \end{bmatrix} \begin{bmatrix} \rho_1^{\dagger} \\ \rho_2^{\dagger} \\ \rho_3^{\dagger} \end{bmatrix} = \underbrace{3}_{t_2 t_3} (t_2^2(\beta_3 - \beta_2) + t_3^2(\beta_2 - \beta_1))$$



In general, for the kth and
$$(k+1)^{th}$$
 segment $(1 \le k \le n-2)$

$$\begin{bmatrix} t_{k+2} & 2(t_{k+1} + t_{k+2}) & t_{k+1} \end{bmatrix} \begin{bmatrix} \rho_k \\ \rho_{k+1} \\ \rho_{k+2} \end{bmatrix}$$

$$= \frac{3}{t_{k+1}} \frac{1}{t_{k+2}} \left(t_{k+2}^2 - \rho_{k+1} + t_{k+2}^2 (\rho_{k+1} - \rho_{k}) \right)$$

Set of n-2 equations form a linear system for the tangent vectors P_K

$$\begin{bmatrix}
t_{3} & 2(t_{2} + t_{3}) & t_{2} & 0 & - \cdots \\
0 & t_{4} & 2(t_{3} + t_{4}) & t_{3} \\
- \cdots & - \cdots & t_{m} & 2(t_{m} + t_{m}) t_{m-1}
\end{bmatrix}
\begin{bmatrix}
\rho_{1} \\ \rho_{2} \\ \rho_{1} \end{bmatrix}$$

$$= \int \frac{3}{t_{2} t_{3}} \left(t_{2}^{2}(\rho_{3} - \rho_{2}) + t_{3}^{2}(\rho_{2} - \rho_{1})\right)$$

$$\frac{3}{t_{3} t_{4}} \left(t_{3}^{2}(\rho_{4} - \rho_{3}) + t_{4}^{2}(\rho_{3} - \rho_{2})\right)$$

$$\frac{3}{t_{m-1} t_{m}} \left(t_{m-1}^{2}(\rho_{m-1} - \rho_{m-1}) + t_{m}^{2}(\rho_{m-1} - \rho_{m-2})\right)$$

This system of equations can be used to salve for the tangent vectors l_1' , $l_2' - l_n'$

Golving for
$$\beta_1$$
, β_2 , β_3 and β_y

$$\beta_{1K} = \rho_{K_1}$$

$$\beta_{2K} = \rho_{K_1}^{\prime}$$

$$\beta_{3K} = \frac{3(\rho_{K+1} - \rho_{K})}{t_{K+1}^{2}} - \frac{2\rho_{K}^{\prime}}{t_{K+1}} - \frac{\rho_{K+1}}{t_{K+1}}$$

$$\beta_{4K} = \frac{2(\rho_{K} - \rho_{K+1})}{t_{K+1}^{2}} + \frac{\rho_{K}^{\prime}}{t_{K+1}^{2}} + \frac{\rho_{K+1}^{\prime}}{t_{K+1}^{2}}$$

Rearranging,

$$\begin{bmatrix}
B_{1K} \\
B_{2K} \\
B_{3K} \\
B_{4K}
\end{bmatrix} = \begin{bmatrix}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
-3/t_{K+1}^2 & -2/t_{K+1} & 3/t_{2}^2 - 1/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} \\
2/t_{K+1}^3 & 1/t_{K+1}^2 & -2/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} & 1/t_{K+1}
\end{bmatrix}$$

$$\int_{K} (t) = \sum_{i=1}^{4} \beta_{iK} t^{K-1} \qquad 0 \le t \le t_{K+1}$$

$$= \left[1 + t^2 + t^3 \right] \left[\beta_{1K} + \beta_{2K} + \beta_{3K} + \beta_{4K} \right]^T$$

$$\int_{K} (t) = \begin{bmatrix} 1 & t & t^{2} & t^{3} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -3/t_{K+1}^{2} & -2/t_{K+1} & /t_{K+1} & /t_{K+1} \\ 2/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} \\ 2/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} & 1/t_{K+1} \end{bmatrix}$$

$$\frac{1}{2} \int_{t_{K+1}}^{3} \frac{1}{t_{K+1}} \frac{1$$

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Substituting $u=t/t_{k+1}$ rearranging $P_{K}(u) = \left[F_{I}(u) \quad F_{2}(u) \quad F_{3}(u) \quad F_{4}(u)\right] \begin{bmatrix} f_{K} \\ f_{K+1} \\ f_{K} \\ f_{K+1} \end{bmatrix}$

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 $F_{1}(u) = 2u^{3} - 3u^{2} + 1$ $F_{2}(u) = -2u^{3} + 3u^{2}$ $F_{3}(u) = u(u^{2} - 2u + 1) t_{k+1}$ $F_{4}(u) = u(u^{2} - u) t_{k+1}$ where $F_{1}, F_{2}, F_{3}, F_{3}$ are alled the Bundly Functions.