Source: 1. Computer Graphics by Donald Hearn and M. Pauline Baker

Introduction to Computer Graphics, NPTEL Course by Prof. Prem Kalra

2. Computer Graphics by Donald Hearn and M. Pauline Baker

Extending this idea to set of a points.



Joining of segments
2 SEGMENTS: P1 P2 P3 (Points)
P1 P2 P3' (Tangents)

where l_2 and l_2' are the futermediate point and its tangent vector which is determined through some continuity contraint.

A Precewing spline of degree k has condinuity of order (k-1) at the internal joints.

Thus lubic splines have second order continuity i.e. P," (t) is continuous over the joint.

$$\begin{aligned}
f(t) &= \beta_1 + \beta_2 t + \beta_3 t^2 + \beta_4 t^3 \\
&= \underbrace{\frac{1}{\beta_1}}_{i=1}^{\beta_1} \delta_i t^{i-1} + \xi_1 \leq t \leq \xi_2
\end{aligned}$$

$$\rho'(t) = \beta_{2} + 2\beta_{3}t + 3\beta_{4}t^{2}$$

$$= \sum_{i=1}^{4} (-i)\beta_{i}t^{i-2}$$

$$\rho''(t) = 2\beta_3 + 6\beta_4 t
= \frac{4}{5!} (i-1)(i-2)\beta_i t^{i-3} \qquad \xi \le t \le t_2$$

Flust Segment $(t=t_2)$ $P'' = 6B_4t_1 + 2B_3$ Second Segment (t=0) $P'' = 2B_2$



 e_1^{\prime} e_2^{\prime} e_3^{\prime}

$$P' = 28_{3}$$

$$C_{9} (6 B_{9} t_{2} + 28_{3})_{\text{leg }1} = (28_{3})_{\text{seg }2} - 0$$
We know,
$$b_{1} = P_{1}$$

$$b_{2} = P_{1}'$$

$$b_{3} = \frac{3(P_{2} - P_{1})}{t_{2}^{3}} + \frac{P_{1}'}{t_{2}} + \frac{P_{1}'}{t_{2}^{3}}$$

$$(6 B_{9} t_{2} + 2B_{3})_{\text{leg }1} = (28_{3})_{\text{seg }2} - 0$$

$$Cubeltiluttry b_{3} \text{ and } b_{4} \text{ from } \text{ in } \text{ in } \text{ or } \text{ or } \text{ for } \text{ in } \text{ or } \text{ for } \text{ for } \text{ or } \text{ or } \text{ for } \text{ for } \text{ or } \text{ for } \text{ or } \text{ for }$$

$$= \left[\frac{3(\rho_{3}-\rho_{2})}{t_{3}^{2}} - \frac{2\rho_{2}'}{t_{3}} - \frac{\rho_{3}'}{t_{3}}\right]$$

$$= \left[\frac{3(\rho_{3}-\rho_{2})}{t_{3}^{2}} - \frac{2\rho_{2}'}{t_{3}} - \frac{\rho_{3}'}{t_{3}}\right]$$

$$= \frac{6(\rho_{1}-\rho_{2})}{t_{2}^{2}} + \frac{3\rho_{1}'}{t_{2}} + \frac{3\rho_{2}'}{t_{2}} + \frac{3(\rho_{2}-\rho_{1})}{t_{2}} - \frac{2\rho_{1}'}{t_{2}} - \frac{\rho_{1}'}{t_{2}}$$

$$= \frac{3(\rho_{3}-\rho_{2})}{t_{3}^{2}} - \frac{2\rho_{2}'}{t_{3}} - \frac{\rho_{3}'}{t_{3}}$$

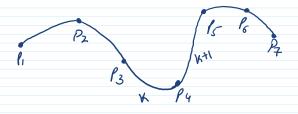
$$= \frac{3(\rho_{3}-\rho_{2})}{t_{2}^{2}} - \frac{6(\rho_{1}-\rho_{2})}{t_{2}^{2}} - \frac{3(\rho_{2}-\rho_{1})}{t_{2}^{2}}$$

$$= \frac{3(\rho_{3}-\rho_{2})}{t_{3}^{2}} - \frac{6(\rho_{1}-\rho_{2})}{t_{2}^{2}} - \frac{3(\rho_{2}-\rho_{1})}{t_{2}^{2}}$$

$$t_{2}t_{3} \times \left[\frac{\rho_{1}'}{t_{2}} + \frac{2\rho_{2}'}{t_{2}} + \frac{2\rho_{2}'}{t_{3}} + \frac{\rho_{3}'}{t_{3}} \right] = \underbrace{\frac{3(\rho_{3} - \rho_{2})}{t_{3}^{2}} + \frac{3(\rho_{2} - \rho_{1})}{t_{2}^{2}}}_{t_{3}^{2} + 2(t_{3} + t_{2})\rho_{2}' + t_{2}\rho_{3}'} = \underbrace{\frac{3t_{2}(\rho_{3} - \rho_{2})}{t_{3}} + \frac{3t_{3}(\rho_{2} - \rho_{1})}_{t_{2}}}_{t_{2}}$$

$$t_{3}\rho_{1}' + 2(t_{3} + t_{2})\rho_{2}' + t_{2}\rho_{3}' = \underbrace{\frac{3t_{2}(\rho_{3} - \rho_{2})}{t_{3}} + \frac{3t_{3}(\rho_{2} - \rho_{1})}_{t_{2}}}_{t_{2}^{2} + 2(\rho_{3} - \rho_{2})} + \underbrace{\frac{3t_{3}(\rho_{2} - \rho_{1})}{t_{2}}}_{t_{2}^{2} + 2(\rho_{3} - \rho_{2})}$$

$$\begin{bmatrix} t_3 & 2(t_3+t_2) & t_2 \end{bmatrix} \begin{bmatrix} \rho_1^{11} \\ \rho_2^{11} \\ \rho_3^{11} \end{bmatrix} = \underbrace{\frac{3}{t_2 t_3}} (t_2^{2}(\beta_3-\beta_2) + t_3^{2}(\beta_2-\beta_1))$$



In general, for the kth and
$$(k+1)^{th}$$
 segment $(1 \le k \le n-2)$

$$\begin{bmatrix} t_{k+2} & 2(t_{k+1} + t_{k+2}) & t_{k+1} \end{bmatrix} \begin{bmatrix} \rho_{k} \\ \rho_{k'} \\ \rho_{k'} \end{bmatrix}$$

$$= \frac{3}{t_{k+1}} \frac{1}{t_{k+2}} \left(t_{k+1}^2 \left(\rho_{k+2} - \rho_{k+1} \right) + t_{k+2}^2 \left(\rho_{k'} - \rho_{k'} \right) \right)$$

Set of n-2 equations form a linear system for the target vectors P_{k}

This system of equations can be used to salve for the tangent vectors P, 1/2-- Pn

Columny for
$$\beta_1, \beta_2, \beta_3$$
 and β_y

$$\beta_{1K} = \rho_{k_1}$$

$$\beta_{2K} = \rho_{k_1}$$

$$\beta_{3K} = \frac{3(\rho_{K+1} - \rho_{K})}{t_{k+1}} - \frac{2\rho_{K}'}{t_{k+1}} - \frac{\rho_{K+1}}{t_{k+1}}$$

$$\beta_{4K} = \frac{2(\rho_{K} - \rho_{K+1})}{t_{K+1}} + \frac{\rho_{K}'}{t_{K+1}} + \frac{\rho_{K+1}'}{t_{K+1}}$$

Rearranging,

$$\begin{bmatrix}
B_{1K} \\
B_{2K} \\
B_{3K}
\end{bmatrix} = \begin{bmatrix}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
-3/t_{K+1}^2 & -2/t_{K+1} & 3/t_{K+1}^2 & -1/t_{K+1} \\
2/t_{K+1} & 1/t_{K+1}^2 & -2/t_{K+1} & 1/t_{K+1} & 1/t_{K+1}
\end{bmatrix} \begin{bmatrix}
\rho_{K} \\
\rho_{K} \\
\rho_{K+1} \\
\rho_{K+1}
\end{bmatrix}$$

$$\int_{K} (t) = \sum_{i=1}^{4} \beta_{ik} t^{k+1} \qquad 0 \le t \le t_{k+1}$$

$$= \left[1 + t^2 + t^3 \right] \left[\beta_{1K} \beta_{2K} \beta_{3K} \beta_{4K} \right]^T$$

New Section 2 Page

Substituting
$$u=t/t_{k+1}$$
 rearranging
$$\int_{R}(u) = \left[F_{1}(u) \quad F_{2}(u) \quad F_{3}(u) \quad F_{4}(u)\right] \left[f_{k}\right]$$

$$\left[f_{k+1}\right]$$

$$\left[f_{k+1}\right]$$

$$\left[f_{k+1}\right]$$

05451 15K5n-1

$$F_{1}(u) = 2u^{3} - 3u^{2} + 1$$
 $F_{2}(u) = -2u^{3} + 3u^{2}$
 $F_{3}(u) = u(u^{2} - 2u + 1) t_{k+1}$
 $F_{4}(u) = u(u^{2} - u) t_{k+1}$

where $F_{1}, F_{2}, F_{3}, F_{3}$ are alled the Bundly Functions.