

## DYNAMIC CHARACTERISTICS TESTS OF FULL-SCALE LEAD RUBBER BEARING (LRB)

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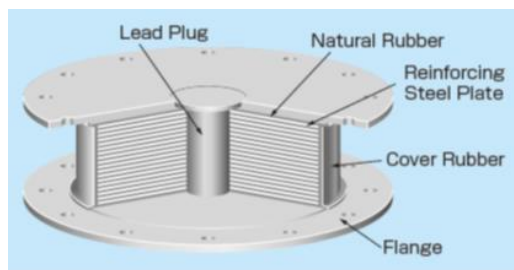
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### ABSTRACT

Several types of dynamic tests were performed using a full-scale lead rubber bearing (LRB) that has a lead plug embedded at the centre of laminated natural rubber. The horizontal and vertical characteristics of the LRB due to various shear strains, frequencies, cyclic effect and compressive stresses were obtained by the experiments. It was confirmed that the variations of the obtained horizontal and vertical characteristics satisfied allowable variations defined in European standard for Anti-seismic devices (EN15129-2009, See References 1).

### INTRODUCTION

In order to improve safety of nuclear power plants (NPPs) against high seismic condition, it had been studied to apply seismic isolation devices to reactor building in NPPs in a past project. A large size of lead rubber bearing (LRB) that has a lead plug embedded at the centre of laminated natural rubber had been developed by Bridgestone Corporation (Figure 1). In addition, static and quasi-static tests using full-scale of the LRB had been conducted to confirm its failure capacity in the project (See Reference 2). Dynamic tests using small size LRBs for typical industries had been conducted to confirm dynamic characteristics, but there was no data of dynamic characteristics of the LRB. In this experiments, dynamic tests were performed to confirm dynamic characteristics of the LRB. Taking into consideration the size and weight of the LRB, dynamic tests were performed using Seismic Response Modification Device (SRMD) at University of California San Diego.



Diameter of isolator $D_f$	1600	mm
Total thickness of rubber $h_R$	260	mm
Thickness of rubber sheet $t_R$	10.0	mm
Number of rubber layers $n_R$	26	-
Thickness of inner steel plate $t_s$	6.8	mm
Number of steel plate layers $n_s$	25	-
Diameter of lead plug $D_p$	392	mm

Figure 1. Specifications of Full-Scale LRB

## OUTLINES OF TESTS

Several types of dynamic tests are performed using full-scale LRBs in this study. Table 2 shows a test series of the dynamic tests. Dependence of horizontal and vertical characteristics due to various shear strains, frequencies, cyclic effect and compressive stresses (ID 2 through 5) were confirmed in accordance with European standard for Anti-seismic devices (EN15129-2009) followed by basic characteristics tests (ID 1). As basic characteristics of the LRB, a horizontal stiffness (post yield stiffness)  $K_2$ , a yield strength  $Q_d$  and a vertical compressive stiffness  $K_v$  are confirmed in this test series. Total three (3) specimens are used for the tests.

Table 2: A Series of Full-Scale Tests

ID	Test Objectives
1	Basic characteristics ( $K_2$ , $Q_d$ and $K_v$ )
2	Dependence of horizontal characteristics on rubber shear strain
3	Dependence of horizontal characteristics on frequency
4	Dependence of horizontal characteristics on repeated cycling
5	Dependence of vertical stiffness on compressive stresses

## TEST RESULTS

### Basic characteristics test (ID1)

The purpose of this test is to confirm the basic characteristics ( $K_2$ ,  $Q_d$  and  $K_v$ ) of the LRB. The test condition is as follows.

- Shear strain of LRB:  $\pm 100\%$  (horizontal displacement is 260mm)
- Compressive stress: 5 MPa const.
- Shaking frequency: Horizontal 0.33Hz (sinusoidal wave)
- Number of test specimen: 2 specimens

Figure 2 shows horizontal load-displacement curve in 3<sup>rd</sup> cycle. Test results match well to the target of basic characteristics of the LRB. It is also confirmed that there are little differences between the specimens.

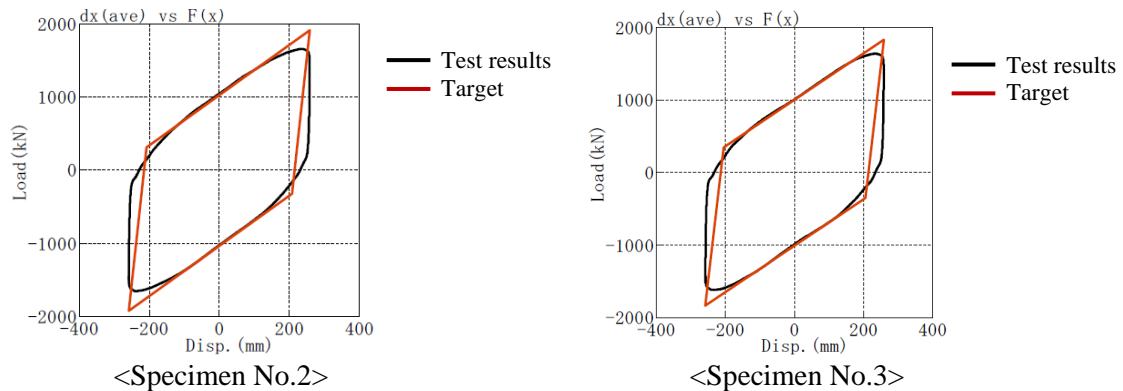


Figure 2 Horizontal Load-Displacement Curve in 3<sup>rd</sup> cycle

Table 3 shows the basic characteristics test results. The test results ( $K_2$ ,  $Q_d$  and  $K_v$ ) are averaged by the results of two (2) specimens. The allowable variations to the basic specifications are specifically set for NPPs considering the seismic design. It is confirmed that the basic characteristics obtained by the test satisfy the allowable variations, except yield strength  $Q_d$ . It is considered that the variation of  $Q_d$  of the

LRB is caused by an increasing of a diameter of lead plug comparing to LRBs for typical buildings. It is confirmed that a dependence of  $Q_d$  on frequency based upon the test data should be incorporated into a basic specification of the LRB which is calculated in delivery inspection (static test). In the following dynamic tests (ID 2 through 5), the basic specification of  $K_2$  and  $Q_d$  are set based upon the test results. The basic specification of  $K_v$  is set as same as original spec., since  $K_v$  is NOT sensitive depend on frequency and it is based upon a lot of delivery inspection data in the past tests (See References 2).

Table 3 Basic Characteristics Test Results

Characteristics	Test Results (Average)	Original Spec.	Ratio	Allowable Variations
$K_2$ (kN/mm)	<u>3.34</u>	3.17	1.04	0.9~1.1 ( $\pm 10\%$ )
$Q_d$ (kN)	<u>1058</u>	890	1.19	0.9~1.1 ( $\pm 10\%$ )
$K_v$ (kN/mm)	6122	<u>7480</u>	0.82	0.8~1.2 ( $\pm 20\%$ )

#### ***Dependence of horizontal characteristics on rubber shear strain (ID2)***

The purpose of this test is to confirm the dependence of horizontal characteristics ( $K_2$  and  $Q_d$ ) on rubber shear strain of the LRB. The test condition is as follows.

- Shear strain of LRB:  $\pm 50\%$ ,  $\pm 75\%$ ,  $\pm 100\%$ ,  $\pm 150\%$ ,  $\pm 200\%$ ,  $\pm 250\%$
- Compressive stress: 5 MPa const.
- Shaking frequency: Horizontal 0.33Hz (sinusoidal wave)
- Number of test specimen: 2 specimens

Table 4 shows the minimum and maximum variations of  $K_2$  and  $Q_d$ . The variations is calculated by “Test result at 3<sup>rd</sup> cycle in ID2/basic spec. in ID1” and the allowable variations is set as  $\pm 20\%$  in accordance with EN15129. Both  $K_2$  and  $Q_d$  satisfy the allowable variation in case that the shear strain is greater than  $\pm 75\%$ . It is confirmed that  $K_2$  decreases slightly with the increasing shear strain and  $Q_d$  is constant with shear strains.

Table 4 Variations of horizontal characteristics ( $K_2$  and  $Q_d$ )

Contents	Test results		Allowable variation
	Min.	Max.	
$K_2$	-20%	+17%	$\pm 20\%$
$Q_d$	-8%	+2%	$\pm 20\%$

#### ***Dependence of horizontal characteristics on frequency (ID3)***

The purpose of this test is to confirm the dependence of horizontal characteristics ( $K_2$  and  $Q_d$ ) on frequency of shaking. The test condition is as follows.

- Shear strain of LRB:  $\pm 100\%$
- Compressive stress: 5 MPa const.
- Shaking frequency: Horizontal 0.05Hz, 0.25Hz, 1.0Hz (sinusoidal wave)
- Number of test specimen: 3 specimens

Table 5 shows the minimum and maximum variations of the  $K_2$  and  $Q_d$ . Figure 3 shows the ratio of  $K_2$  and  $Q_d$  on various shaking frequencies. Both  $K_2$  and  $Q_d$  satisfy the allowable variation in accordance with EN 15129. According to the test results, it is confirmed that the dependence of horizontal characteristics ( $K_2$  and  $Q_d$ ) on frequency is greater than past experimental tests for LRBs for typical buildings whose size is smaller than the LRB (test specimens).

Table 5 Variations of horizontal characteristics ( $K_2$  and  $Q_d$ )

Contents	Test results		Allowable variation
	Min.	Max.	
$K_2$	-7%	+15%	$\pm 20\%$
$Q_d$	-13%	+19%	$\pm 20\%$

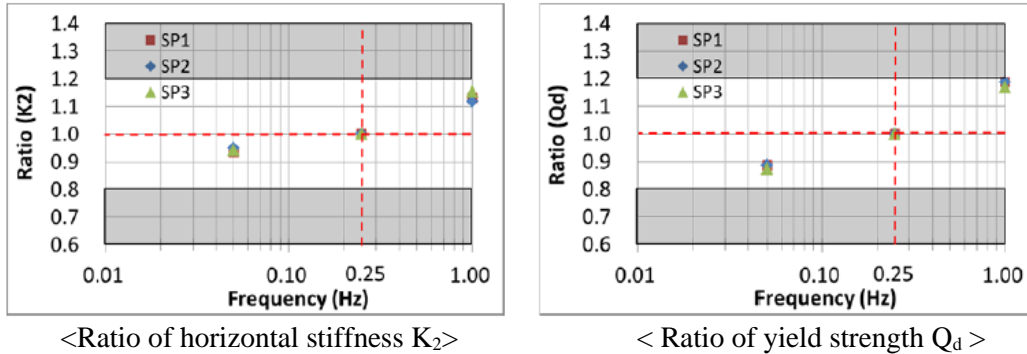


Figure 3 Horizontal characteristics on various shaking frequencies

#### ***Dependence of horizontal characteristics on repeated cycling (ID4)***

The purpose of this test is to confirm the dependence of horizontal characteristics ( $K_2$  and  $Q_d$ ) on repeated cycling. The test condition is as follows.

- Shear strain of LRB:  $\pm 100\%$
- Compressive stress: 5 MPa const.
- Shaking frequency: Horizontal 0.1Hz (sinusoidal wave)
- Number of cycle: 10 cycles
- Number of test specimen: 2 specimens

Table 6 shows the variations of the horizontal characteristics ( $K_2$  and  $Q_d$ ) at 10<sup>th</sup> cycle comparing to the one at 2<sup>nd</sup> cycle and 1<sup>st</sup> cycle. Figure 4 shows the ratio of  $K_2$  and  $Q_d$  on repeated cycling.  $K_2$  satisfy the allowable variations in accordance with EN 15129. It is confirmed that the dependence of  $Q_d$  on repeated cycling is greater than past experiences of LRBs for typical buildings whose size is smaller than the LRB. It is necessary to conduct a confirmatory analysis to confirm the LRB's behaviour using the test results in next phase study. It would also be necessary to accumulate an additional data of the full-scale LRBs on repeated cycling.

Table 6 Variations of horizontal characteristics ( $K_2$  and  $Q_d$ )

Contents	Test results	Allowable variation
$K_2$ (Ratio of 10 <sup>th</sup> cycle/ 1 <sup>st</sup> cycle)	-8%	$\pm 40\%$
$K_2$ (Ratio of 10 <sup>th</sup> cycle/ 2 <sup>nd</sup> cycle)	+2%	$\pm 30\%$
$Q_d$ (Ratio of 10 <sup>th</sup> cycle/ 2 <sup>nd</sup> cycle)	-38%	$\pm 30\%$

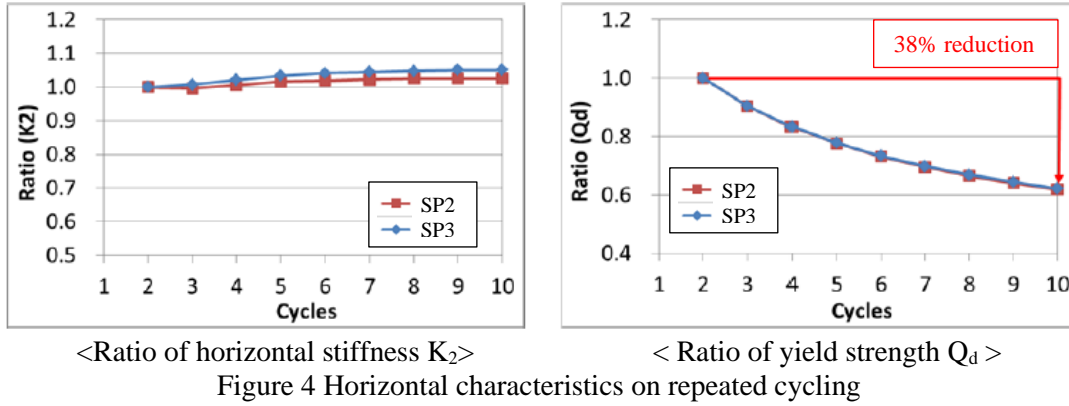


Figure 4 Horizontal characteristics on repeated cycling

### Dependence of vertical stiffness on compressive stresses (ID5)

The purpose of this test is to confirm the dependence of vertical stiffness ( $K_v$ ) on compressive stresses. The test condition is as follows.

- Shear strain of LRB:0% (const.)
- Compressive stress: 5 MPa  $\pm$  2.5MPa
- Shaking frequency: Vertical 0.0125Hz, 0.33Hz (sinusoidal wave)
- Number of test specimen: 2 specimens

Figure 5 shows the variations of the vertical stiffness ( $K_v$ ) on compressive stresses. The ratio of  $K_v$  is calculated by “test results at 3<sup>rd</sup> cycle in ID 5/basic spec. in ID1”. The maximum variation of  $K_v$  is -18% comparing to the basic specification of the LRB. It is confirmed that the variation obtained by the test is within the allowable variations in accordance with EN 15129 ( $\pm 30\%$ ).

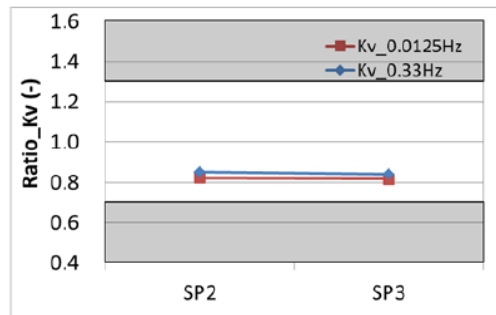


Figure 5 Vertical stiffness on compressive stresses

### **Summary of Test Series (ID 2 through 5)**

Table 7 shows the summary of the results. The horizontal and vertical characteristics of the LRB obtained by the experiments satisfy the allowable variations in accordance with EN 15129. It is confirmed that further investigations are necessary regarding a reduction of  $Q_d$  of the LRB on repeated cycling to confirm an impact on seismic design of base isolated reactor building in an NPP.

Table 7 Summary of the Results (ID 2 through 5)

ID	Test Objectives	Allowable Variations	Test Results
2	Dependence of horizontal characteristics on rubber shear strain	$K_2 : \pm 20\%$ $Q_d : \pm 20\%$	$K_2 : -20\% \sim +17\%$ $Q_d : -8\% \sim +2\%$
3	Dependence of horizontal characteristics on frequency	$K_2 : \pm 20\%$ $Q_d : \pm 20\%$	$K_2 : -7\% \sim +15\%$ $Q_d : -13\% \sim +19\%$
4	Dependence of horizontal characteristics on repeated cycling	$K_2 : \pm 30\%$ (2 <sup>nd</sup> /10 <sup>th</sup> cycle) $\pm 40\%$ (1 <sup>st</sup> /10 <sup>th</sup> cycle) $Q_d : \pm 30\%$ (2 <sup>nd</sup> /10 <sup>th</sup> cycle)	$K_2 : +2\%$ (2 <sup>nd</sup> /10 <sup>th</sup> ) $-8\%$ (1 <sup>st</sup> /10 <sup>th</sup> ) $Q_d : -38\%$ (2 <sup>nd</sup> /10 <sup>th</sup> )
5	Dependence of vertical stiffness on compressive stresses	$K_v : \pm 30\%$	$K_v : -18\%$

## **CONCLUSIONS**

Several types of dynamic tests were performed using full-scale lead rubber bearings (LRBs) that have a lead plug embedded at the centre of laminated natural rubber. The horizontal and vertical characteristics of the LRB due to various shear strains, frequencies, cyclic effect and compressive stresses were obtained by the experiments. It was confirmed that the variations of the obtained horizontal and vertical characteristics satisfied allowable variations defined in European standard for Anti-seismic devices (EN15129-2009).

## **REFERENCES**

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