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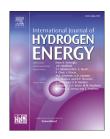
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## **Review Article**

## A state of the art review on biomass processing and conversion technologies to produce hydrogen and its recovery via membrane separation

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#### HIGHLIGHTS

- Thermochemical conversion technologies for hydrogen production.
- Gasification technologies review for hydrogen production.
- Biological routes for hydrogen production.
- Potential of membrane applications for hydrogen separation from syngas.
- Prospective of hydrogen as future of energy.

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#### ABSTRACT

Hydrogen is a zero-emission green fuel containing sufficient energy potentially suitable for electricity generation. Currently, large quantities of hydrogen are produced using classical fossil fuels. Nevertheless, the finite quantities of these resources have compelled the global community to look into using more sustainable and environmentally friendly resources such as bio-based waste. There are several approaches, to convert biomass to hydrogen, among which the thermochemical and biological processes are considered as the most important ones. The aim of this review paper is twofold, namely, (a) to evaluate hydrogen

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Gasification
Fermentation
Membrane separation

Introduction

production and biomass processing methods to give a better insight into their potential merits and identify gaps for sustainable hydrogen generation, and (b) to evaluate current and future opportunities in membrane technology for hydrogen separation and purification from biomass processing. By fulfilling these gaps, the objectives of economical, sustainable, and environmentally-friendly resources for hydrogen production and separation can be recommended.

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## Introduction

Hydrogen is ever-growing in its demand over other conventional fuels due to its wide range of diverse applications [1,2]. Its high energy content offers a comprehensive benefit [3], in terms of lower heating value (LHV)/kg over their fossil fuel-based counterparts such as methane and gasoline, which are 2.4 and 2.8 times higher respectively [4]. Furthermore, hydrogen is extensively used in fuel cells, which have minimal emissions and merely release water-vapor as the net emissions and might be regarded as zero-

emission green fuel [5,6]. On the other hand, fossil fuels have contributed to global warming by supplementing the CO<sub>2</sub>release with additional SOx and NOx into the environment [7]. Additionally, hydrogen is a principal component of many chemical and fuel products such as ammonia, methane, urea, ethanol, etc [8,9]. Due to these reasons, further research in the domain of hydrogen production is necessary so that future technology will meet these requirements [10]. Moreover, the hydrogen is useful in fuel cell applications and many integrated processes have been investigated for hydrogen production processes with fuel cells [11–13].

The hydrogen economy is known as a system in which hydrogen is used as a prime energy source and becomes a key component of future power generation [14]. Many countries have started to determine the value of the hydrogen economy and make efforts to take significant steps towards a hydrogen economy and planned the polices and methods as reviews by many researchers, such as, for Malaysia [15], Pakistan [16], Taiwan [17], China [18], Portugal [19], and Canada [20], etc. The value of the hydrogen economy was 107 billion \$ in 2016 [21], 115.25 billion \$ in 2017 and is expected to rise to 154.74 billion \$ by 2022 [10]. In a recent research report, world hydrogen demand has been reported as 50 million metric tons/year or 45 billion kg/year in 2006 and has been increasing at the rate of 10% annually [11]. Currently the worldwide cumulative hydrogen consumption is in the range 400-500 million Nm<sup>3</sup> per annum [12,13] and will continue beyond 2025 [14]. It is anticipated that in the near future hydrogen will be the most important energy carrying fuel for the reasons that it is environmentally friendly and possesses efficient burning characteristics [15,16]. Additionally, hydrogen is used as a major constituent in the synthesis of ammonia and methanol for many decades, which is conventionally obtained from the methane-steam reforming reaction [17,22].

Hydrogen is obtained from both fossil and non-fossil fuels and about 96% of the total hydrogen produced is obtained from carbonaceous raw materials, which are comprised mainly fossil fuels [21]. The continuing supply of fuel is under threat due to the finite sources of fossil fuels, hence the world must divert its dependence from fossil to non-fossil renewable sources [23,24]. Reforming and pyrolysis are the major processes to produce hydrogen from fossil fuels [3,25]. On the other hand, it can be produced using non-fossil fuel either by thermochemical or biological methods [26]. Among the non-fossil fuels, biomass is an abundant renewable source of energy that is available in many forms such as; agricultural, forest, and biowastes, etc. Biomass has been utilized in many ways for energy production for centuries and it is still contributing about 10-14% of the total energy supply of the world, whereas, for the developed countries, this share is substantially higher, i.e., 40-45% [27,28]. Biomass may be processed in numerous ways depending on the end-use and required products, which are obtained through chemical, thermal, thermochemical and biochemical pathways [25,29]. The resultant amount of hydrogen from biomass may reach 20% by volume via different conversion strategies [30,31].

Biomass processing routes, in principle, depend on the state of the available feedstock [32]. Hydrogen from bioresources can be produced using gasification, pyrolysis, fermentation, anaerobic digestion or even the steam reforming process [33]. A scheme of the different routes from biomass to hydrogen is shown in Fig. 1. The quantity of hydrogen produced depends on the source of biomass and the efficiency of the process method/route utilized [34]. The technologies, to convert biomass into hydrogen, are useful and acceptable as compared to other typical technologies incorporating fossil fuels due to less and/or zero emissions into the environment [27,35].

Several reviews have been published over time to study the developments in the area of hydrogen production. A detailed

analysis of these review papers published for hydrogen production from biomass using thermochemical or biological conversion technologies is shown in Table 1, which also indicates how these insightful reviews have served to this domain of knowledge especially in the case of the separation of hydrogen through membrane technology. Most of these reviews are based on a single technology for hydrogen production. No review paper has been found which compares all available technologies for hydrogen production. Singh et al. [36] discussed hydrogen production through both direct and indirect bio-photolysis processes with the effect of catalysts. The most important reviews covering biological methods were presented by Mudhoo et al. [37] and Anoop et al. [38]. The hydrogen production processes by thermochemical based techniques have been reviewed and are available for pyrolysis and gasification [25,39,40]. A review was published in 2009, which gives a very brief review of the thermochemical and biological conversion processes for hydrogen production, as most of the technologies were at the initial stages of development [25]. Most of the literature studies available are for gasification processes such as steam gasification, supercritical water gasification, solar gasification, etc [41-44]. Based on the extensive literature reviews, there has not been a critical discussion, assessment, and comparison of the operating principles. Also, the costs relating to H<sub>2</sub> production for most processes are missing in the literature. The major contribution of this review paper lies in providing an in-depth analysis of hydrogen production and biomass processing methods for relevant advantages and shortcomings for a sustainable energy future. Furthermore, the usefulness of membrane technology for hydrogen separation and purification specifically obtained via biomass processing are included as a key highlight, followed by the future potential in this area of research. Within this context, the remainder of this review is categorized as follows. In section Thermochemical methods, a literature survey on thermochemical methods is presented which will assist researchers and the scientific community to select the suitable process according to type of biomass and applications. Section Non-Thermal/biological methods addresses the non-thermal/biological methods of hydrogen production and its usage. The separation of hydrogen via membranes through biomass based processes is reviewed in Section Implementation of membrane for biomass-based Hydrogen Separation. The next section discusses the challenges to continue the way forward to sustainable hydrogen production.

## Thermochemical methods

Thermochemical processes are typically considered as viable and effective to produce hydrogen from biomass [23,35,48], whereas, these processes have many challenges in terms of commercialization [49]. These technologies mainly include pyrolysis [50], gasification [51], combustion [52] and liquefaction [53]. Fig. 1 also shows the schematic diagram for pathways of biomass thermochemical technologies with subsequent downstream processes for hydrogen production and purification using membrane technology.

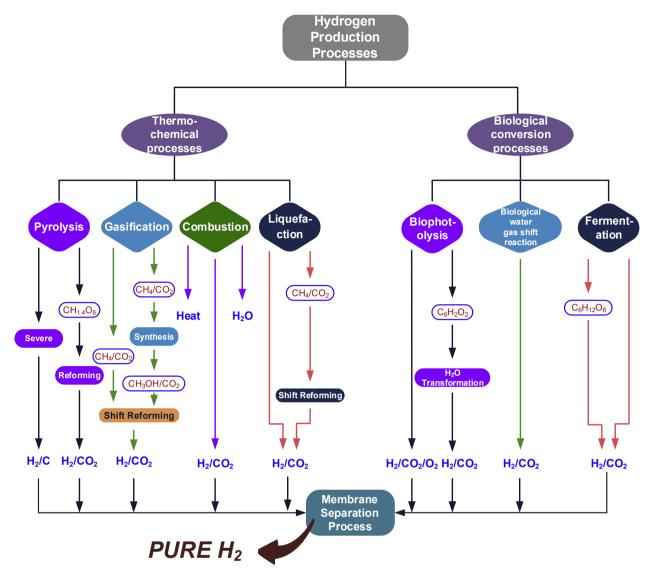


Fig. 1 – Schematic diagram for the pathway of biomass thermochemical technologies with subsequent downstream processes for hydrogen production.

## Biomass combustion

The process of burning any fuel in the presence of air to release its energy in the form of heat of reaction is termed a combustion process. In this process, the biomass burns directly in the presence of excess air in a boiler or furnace, which might be used to produce steam and the resultant steam serve as the driver for turbines, pumps or compressors in any chemical process, and represents the conversion of heat energy into mechanical energy [48]. Due to the less efficacy of thermal power plants, i.e., 40%, this process is considered as an energy-inefficient process [49]. Furthermore, biomass combustion is typically not preferred for hydrogen production due to high formation of carbon dioxide. The hydrogen production was 9.56 vol% for the combustion of algal biomass [54]. In practice, however, many other gases such as COx, SOx, NOx, and CH4 are also emitted which depend upon the source and composition of the biomass.

Among these, SOx forms, if the sulfur is present in biomass, CO due to incomplete combustion and NOx in case of nitrogen present either in air or biomass [50]. The effective implementation of environmental laws helps in maintaining the amount of these pollutants to a certain level to avoid both environmental and health problems. The cost of remedial treatment for these unwanted gases is very high, which adversely increases the overall cost of this process [48]. Correspondingly, the cost per unit of energy is intensified. Additionally, this is an inefficient energy process for the reason of wasting a large amount of energy in the form of flue gas enthalpy [51]. Nevertheless, this wastage of energy can be controlled by installing a waste heat recovery boiler/economizer. These options have limited applications due to the little amount of heat which can be recovered [52]. The combustion process has certain other limitations, such as the high value of acid dew point (ADP) and water dew point (WDP), and emissions of un-wanted polluted gases and ashes [53]. Generally,

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Reviews	Description		Thermochemical of	conversion m	ethods		I	Biologi	cal conv	ersion m	ethods	Separation
		combustion	Pyrolysis Liquefaction		Gasification		Pho fermen		Bio-Ph	otolysis	Biological water gas	via membrane
				Gasification	Solar- gasification	Water – gasification	Photo	Dark	Direct	Indirect '	shift reaction	
Pandey et al. 2019 [40]	Recent development in gasification, pyrolysis process for H <sub>2</sub> production		√	V		<b>√</b>						
Singh et al.2018 [36]	Detail about the use of catalyst and mechanism								$\sqrt{}$	$\sqrt{}$		
Rezania et al. 2017 [41]	Detail about the effect of parameters, optimization, wheat straw, rice husk, etc						$\checkmark$	$\sqrt{}$				
Arregi et al. 2018 [1]	This is about reactor designs, process parameters, and use of catalysts		$\checkmark$	$\checkmark$		$\checkmark$						
Rafal et al. 2018 [9]	Use of many wastes for substrate and operating parameters issues							$\sqrt{}$				
Kalinci et al. 2009 [25]	A brief review on H <sub>2</sub> production process with gasification case study		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\sqrt{}$	$\sqrt{}$	$\sqrt{}$	$\checkmark$	
Azwar et al. 2014 [45]	This covers theoretical principals, bacterial selection of strains and substrates, operating parameters and mathematical models						$\checkmark$	$\checkmark$	$\checkmark$	$\sqrt{}$		
Singh et al. 2014 [46]	Review covers pre-treatment, cell immobilization, sequential and combined fermentation,						$\checkmark$	$\sqrt{}$				
Chen et al. 2011 [39]	It covers the use of bio-oil. CO <sub>2</sub> reduction, thermodynamic principle to enhanced H <sub>2</sub> , catalysts used		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$					
Mudhoo et al. 2010 [37]	This deals in detail about pre- treatments, modifications in the design of reactors and						$\checkmark$	$\sqrt{}$	$\checkmark$	$\sqrt{}$		
Anoop et al. 2015 [38]	process to enhance yield This covers biological method with some LCA based study and kinetic models						$\sqrt{}$	$\sqrt{}$	$\sqrt{}$	$\checkmark$		

Table 1 $-$ (continued)	continued)										
Reviews	Description		Thermoch	emical co	Thermochemical conversion methods	thods		Biolog	Biological conversion methods	nethods	Separation
		combustion	combustion Pyrolysis Liquefaction	faction	9	Gasification		Photo- fermentation	Bio-Photolysis Biological	Biological water gas	via membrane
				0	Gasification Solar- gasificatic	Solar- Water — gasification gasification	Water – gasification	Photo Dark	Photo Dark Direct Indirect shift reaction	shift reaction	۲.
Prakash et al	Prakash et al. This deals for biomass type,				^		^				
[42]	particle size, reaction										
	parameters temperature, and										
	catalyst										
Tanksale	This review described the		>	>	>		>			>	
et al. [47]	catalytic h production using biomass										
This review	A comparative study for all	>	>	>	>	>	>	> >	> >	>	>
	process with membrane										
	process for H <sub>2</sub> separation										

the main purpose of the combustion process is for energy production, however, research is in high demand for technology resulting in the lower production of greenhouse gases (GHG), and the utilization of flue gas heat for energy production. Some new processes have been proposed with the integration of power and energy production such as the chemical looping process to economize the process for hydrogen production [55,56]. The main challenge is the lower content of  $\rm H_2$  in the flue gase, that make it unattractive in the case of hydrogen production.

## Biomass pyrolysis

Pyrolysis is the process in which biomass is thermally treated in the temperature range of 400–600 °C and at atmospheric pressure in the absence of air to convert biomass feedstocks into liquid(bio-oils), solid(char), and gaseous components(syngas) [57,58]. The pyrolysis process consists of devolatilization, fragmentation and product formation that effects the yield of the process [59]. Pyrolysis may also be further classified into slow and fast types [57]. Slow pyrolysis normally occurs at a temperature between 400 and 450 °C, with a low heating rate of 1–5 °C/s and longer residence time (4–8 min). Whereas, in the case of fast pyrolysis, the temperature is maintained in the range of 450–950 °C, along with a higher heating rate and shorter residence time, which are in the range of 100–300 °C/s and 1–5 s respectively [60].

The process of pyrolysis and its product is demonstrated in Fig. 2; these products may occur in gas, liquid or solid phases, which are outlined below:

- (i) Gaseous products: mixtures of H<sub>2</sub>, CH<sub>4</sub>, CO, CO<sub>2</sub>, and other gases, which depend upon the organic nature of the biomass [57].
- (ii) Liquid products: tar and oils left over in liquid form at room temperature.
- (iii) Solid products: char and inorganic components, where the char is almost pure carbon and the latter contains ash and alkali metals from the biomass.

The major objective of the pyrolysis process is to produce bio-oil, nevertheless, it may lead to the production of hydrogen either directly via flashing or fast pyrolysis at high temperatures and a suitable residence time [61]. The following reactions are involved in biomass pyrolysis for hydrogen production.

Biomass pyrolysis 
$$\rightarrow$$
 H2 + CO + CO2  
+ hydrocarbon gases + tar + char (1)

$$C_nH_m + nH_2O \rightarrow nCO + (n + \frac{1}{2}m)H_2$$
 (2)

$$CO + H_2O \rightarrow CO_2 + H_2 \tag{3}$$

The yield of hydrogen from biomass pyrolysis is strictly dependent upon the feedstock nature, catalyst type, process temperature and residence time [62]. Both the organic liquid and solid products of pyrolysis process can be processed to produce hydrogen. The pyrolysis oil can be separated into two

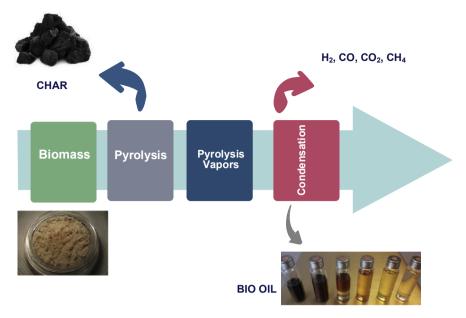


Fig. 2 - Biomass pyrolysis route for hydrogen production.

fractions based on water solubility [1]. These fractions can be used either separately or as mixtures for hydrogen production through the gasification or steam reforming process [63,64]. The expected cost of hydrogen production from the pyrolysis process lies in the range of (1.25–2.220 \$/kg) depending on biomass type and the production facility type [65].

To evaluate the hydrogen production from biomass pyrolysis, various catalysts have been tested through ex-situ or in-situ processes [66–68]. Table 2 summarizes the information about hydrogen yield from the pyrolysis for various types of biomass in the presence of various catalysts and reactor types, as reported in the literature. The pyrolysis technology has been under consideration by researchers and it has developed from laboratory scale to pilot scale that involved tubular reactors, fixed bed reactors, and fluidized bed reactors [59]. In Table 2 it can be observed that the type of reactor, catalyst, biomass and process conditions affect the hydrogen yield.

Char is a byproduct of pyrolysis, which is generated during slow pyrolysis; therefore this type of pyrolysis is not preferred for hydrogen production, while bio-oil is produced as a result of fast pyrolysis, making it a desirable and feasible process for hydrogen production [65]. The fast pyrolysis of biomass results in a mixture of gases and liquids [87]. For hydrogen production, fast pyrolysis is integrated with steam reforming [30]. This is a two-step process, where bio-oil is the intermediate product obtained from first stage and may lead to hydrogen and carbon dioxide generation through reforming in the presence of a catalyst and steam [88]. Fast pyrolysis is advantageous over slow pyrolysis in many ways. Firstly, it is easy to transport bio-oil instead of biomass (charcoal) [89]. Secondly, valuable products have been recovered from bio-oil along with hydrogen. Furthermore, fast pyrolysis produces highly efficient fuels [30]. Bio-oil produced in fast pyrolysis is further reformed in the presence of steam in fluidized bed reactors. Vortex and fluidized bed reactors are currently the subjects of research and it appears that they will be

economically viable options [90]. Catalysts are used to improve the process conditions as well as the product quality of the process. Experimental results have shown that at 850  $^{\circ}$ C, 90% of the stoichiometric hydrogen is recovered when a Ni-based catalyst of 300-350 μm size was used with 9:1 steam to biomass carbon ratio. Another type of Ni catalyst was reported by Waheed et al. [81]. The estimated cost of hydrogen produced from this process is \$7.7/GJ, which is considerably less than that of hydrogen produced from wind electrolysis (\$20/GJ) [30]. Considering the technology readiness level of the pyrolysis process is still on par for bio-oil production, but for the application of hydrogen production it is still not popular. The most likely reason of this is that most of the research and technology development has been focused towards bio-oil and char production [58,91]. It is concluded that there is a need to further explore some new technology developments: such as microwave pyrolysis as well as more development on the catalyst and reactor for hydrogen production. In addition, there are some techno-economic and life cycle assessment analyses still needed to compare its cost with other technologies.

## Biomass liquefaction

Liquefaction of biomass is another thermochemical process that can be used to produce hydrogen. Liquefaction of biomass can be classified into two processes, namely: direct liquefaction and hydrothermal liquefaction [92]. Hydrothermal liquefaction, also known as hydrous pyrolysis [93], is defined as the conversion of biomass into liquid fuels in the presence of water, while maintaining a temperature between 226 and 362 °C and a pressure ranging from 5 to 20 MPa, preferably in the presence of a catalyst [94]. The positive point about hydrothermal liquefaction over pyrolysis is that the biomass prerequisite treatment such as drying is eliminated, thus resulting in energy savings. Only due to this reason, this

Biomass	Catalyst	Reactor type	Reaction Temperature (°C)	Hydrogen yield	References
Wheat straw	0.25 5KCl/CaO	Two-stage reactor	500 (1st stage) 650 (2nd stage)	55.5 vol%	[69]
Pine wood	Ni/MgO	Spouted bed reactor + fluidized bed reactor	500 (SBR) 600 (FBR)	9.08 wt%	[70]
Pine wood	Blast-furnace slag	Rotary pyrolysis reactor	800	45.4 vol%	[71]
Corncob	Limonite ore	Two-stage fixed bed quartz reactor	650	21.65 mmol/g	[72]
Wood sawdust	35NiZn4Al	Two-stage fixed bed reactor	800	20.1 mmol/g	[73]
Pine wood sawdust	Ni commercial	Spouted bed reactor + fluidized bed reactor	500 (SBR) 600 (FBR)	110 g/kg	[74]
Wood sawdust	Ni/CaAlOx	Two-stage fixed bed quartz reactor	800	15.57 mmol/g	[75]
Rice Husk	10 wt%Ni-dolomite	Two-stage fixed reactor	850-1050	20.03-30.62 mmol/g	[76]
Japsnese cedar	20 wt%Mo2C/biochar	Fixed-bed reactor	650	20 mmol/g	[77]
Water hyacinth	Ni-based catalyst	Two-stage pyrolyzer	600 (1st) 800 (2nd)	59.96 g/kg biomass (1st) 101.17 g/kg biomass (2nd)	[78]
Sawdust	NiO/MgO	Three-stage integrated reactor	700-850	43.58-75.96 g/kg biomass	[79]
Bagasse	12%Ni6%Fe/Al <sub>2</sub> O <sub>3</sub>	Dual stage bed microreactor	850	15 mol.%	[80]
Bagasse, Rice Husk, wheat straw	10 wt% Ni-dolomite	Two-stage pyrolyzer	950	25.41 mmol/g, 25.44 mmol/g, 24.47 mmo/g	[81]
Rice stalk	Molten alkali	Stainless steel tank reactor	550	66.5 g/kg biomass	[82]
Pine	NiMo/Al <sub>2</sub> O <sub>3</sub>	Dual-particle powder fluidized-bed	500	33.6 g/kg biomass	[83]
Wood	Cu-Al-MCM-41	Fixed bed	500	9 vol%	[84]
Oil palm wastes	Ni, La/Al <sub>2</sub> O <sub>3</sub>	Fixed bed	900	37.28 vol% (Ni) 38.45 vol% (La/Al <sub>2</sub> O <sub>3</sub> )	[68]
Rice straw, Sawdust	Cr <sub>2</sub> O <sub>3</sub>	Fixed bed	850	49.5 wt% (RS), 51.4 wt% (SD)	[67]
Pine sawdust	Ni/slag	Entrained flow fixed bed	900	29.0 vol%	[85]
Coconut shell	ReC	Fixed bed	800	57 vol%	[86]

Table 3 – Hydrogen prod	duction through lique	faction process from different biomas	s.	
Feed	Catalyst	Reactor type and conditions	Hydrogen yield	References
Glucose	Ni/activated charcoal	Packed-bed reactor, 28 MPa, 650 °C	15.6 mmol/g	[103]
Olive mill waste water	_	Coiled tubular reactor, 25 MPa, 600 °C	10.79 mol%	[104]
Switchgrass biocrude	Ni/ZrO <sub>2</sub>	Packed-bed reactor, 600 °C, 25 MPa	81.67 mol/g carbon reacted	[105]
Bark	Ni/hydrotalcite	Batch reactor, 380 °C, 23 MPa	2.05 mmol/g	[106]
Sewage sludge	КОН	Fluidized bed reactor, 540 °C, 30 MPa	15.49 mmol/g	[107]
Maize silage hydrochar	K <sub>2</sub> CO <sub>3</sub>	Micro-autoclaves, 400 °C, 30 MPa	8.9 mol%	[94]
Coconut shell	K <sub>2</sub> CO <sub>3</sub>	Tubular batch reactor, 600 °C, 23–25 MPa	4.8 mmol/g	[93]
Fruit pulp	RU/activated charcoal	Batch reactor, 600 °C, 25 MPa	54.8 mmol/g	[95]
Microalgae		Batch reactor, 385 °C, 26 MPa.	4 mmol/g	[108]
(Cenedesmus quadricauda)	Nickel/α-Al <sub>2</sub> O <sub>3</sub>	Batch microreactor, 440 °C, 25 MPa	12.28 mmol/g	[109]
Microalgae		Continuous reactor, 600 °C, 25 MPa	40 vol%	[110]

process is highly desirable for processing aquatic biomass, garbage, and organic sludge for hydrogen production. This process has some serious concerns, which originate from the severe reaction conditions that may not be easily achieved and the low yield of hydrogen from the reformation of oil produced as a result of hydrothermal liquefaction. Due to these facts, no commercial-scale plant has been implemented so far [95]. Table 3 provides insights to the published hydrogen yields obtained via biomass liquefaction. From Table 3, it can be concluded that the effect of process parameters such as temperature, pressure, catalyst loading, biomass type and its ratio with solvent, and heating rate and residence time are significantly important for H<sub>2</sub> production [96-98]. Besides, it can be observed that liquefaction is mostly focused on liquid fuel production. Furthermore, the research level is still at a laboratory scale and a pilot-scale experience still needs to be investigated and eventually, it will be necessary to progress

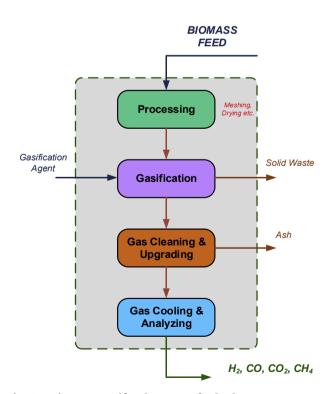


Fig. 3 - Biomass gasification route for hydrogen production.

from a batch process to a continuous process. Elliott et al. [99] pointed out the limitation of a continuous process for the liquefaction of biomass. The case of issues of design and performance of reactors has been identified by Tran et al. [100,101], who suggested the use of plug flow reactors for more research. In addition, Fernandes et al. [102] proposed an integrated gasification and liquefaction system for hydrogen production and presented an exergy analysis to economize the process. The main challenge for its commercialization is the cost of a process that is very rarely studied. The economic and environmental feasibility needs to be assessed in terms of techno-economic analysis and a life cycle assessment.

## Biomass gasification

Gasification is a thermochemical process, which converts biomass into gaseous fuels at elevated temperatures, and may occur both in the presence or absence of a catalyst [111]. In this process, the energy contained in the biomass is not directly released but converted into bond energies of lighter fuels rather than into the sensible heat of combustion products. Fossil or non-fossil carbonaceous materials are heated at high temperatures (almost 700 °C or above) in the presence of steam/air/O2 or combination of those known as gasifying agents. The resulting product is comprised of a mixture of H<sub>2</sub>, CO, and CO<sub>2</sub> gases and more commonly known as syngas and some solid product known as char [42,112]. The process flow of gasification is shown in Fig. 3The product gas obtained can be either used as a fuel directly or it may be converted into other fuels and chemicals such as methane, methanol, ethanol, dimethyl ether and diesel [2,113]. Hydrogen can be separated from the product gas [114]. The general conversion process can be expressed by the following equations 112,115,116

Biomass + Heat + Steam 
$$\rightarrow$$
 H2 + C0 + C02 + CH<sub>4</sub>  
+ Light & Heavy HCs + Char (4)

The reactions that take place during the gasification process are given in Table 4 [26,117,118].

In liquefaction, the moisture contents of biomass limit the process effectiveness, however, in gasification the moisture contents are also critical it also should be less than 35%, as highlighted by Demirbas et al. [115]. Other important issues related to biomass gasification are discussed below.

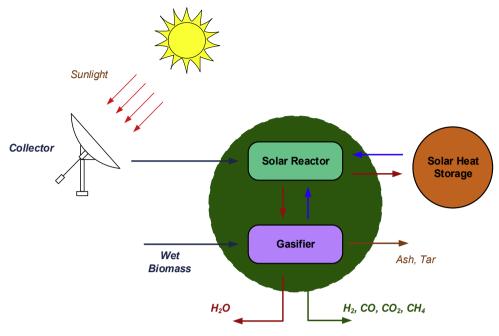


Fig. 4 – Solar gasification route for hydrogen production.

#### Tar formation

Hydrogen production through steam gasification is effected by tar production [115]. Tar is a mixture of higher hydrocarbons produced during the gasification process [116]. Tar, produced along with synthetic gas during gasification of biomass, cannot be easily separated via physical methods proposed for dust removal. Therefore, the removal of tar seems necessitated both for the reasons of qualitative hydrogen production and process economics [115]. The most frequently employed parameters for this purpose are listed below [119,120].

- (i) engineered design of the gasifier [121,122];
- (ii) suitable process control and/or operation [123,124];
- (iii) additives/catalysts [125,126].

Besides operating parameters, i.e., temperature and residence time, gasifying agents have a significant role in the formation and decomposition of tar which needs to be

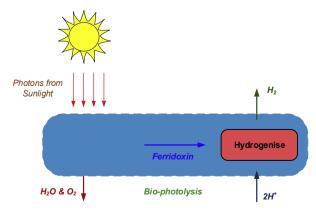


Fig. 5 – Direct bio-photolysis route for hydrogen production.

optimized. Operating temperaturea of about 1273 °C could enhance thermal cracking of produced tar [120,127] and the utilization of a catalyst and other additives could reduce the tar formation, improve the efficiency of the process and the quality of the product as well [127]. The catalyst positively impacts the process through enhanced cracking of higher hydrocarbons into lighter ones as well as augmenting the hydrogen yield via enhancing the water gas - shift reaction [128]. Dolomite, the source of CaO, has been used for tar reduction, as reported by many researchers, to increase the hydrogen yield in the gasification process [119,129]. Abu et al. [115] have discussed nine groups of catalysts both synthesized and mineral types for tar reduction. The use of catalysts is not only good for tar reduction as well as enhancing the yield of H2 but it has some issues in terms of cost and regeneration that should be addressed to enhance the hydrogen yield through the gasification process. Mazumder et al. [130] discussed the operating conditions and aspects of tar reduction in the gasification process to enhance the yield of hydrogen. It can be concluded that tar reduction appears to be the main challenge that needs to be addressed not only at the laboratory scale but

Table 4 — Reactions pre [26,117,118].	sent in biomass gasification
Name	Chemical Reactions
Combustion reaction	$C + O_2 \rightarrow CO_2$ $C + 1/2O_2 \rightarrow CO$
Boudouard reaction water-gas reaction	$C + CO_2 \leftrightarrow 2CO$ $C + H_2O \leftrightarrow CO + H_2$ $CO + H_2O \leftrightarrow CO_2 + H_2$
Reforming reaction	$CH_4 + H_2O \leftrightarrow CO + 3H_2$ $CH_4 + CO_2 \leftrightarrow 2CO + 2H_2$
Tar reforming reaction	$C_nH_m + nH_2O \leftrightarrow (n + (m/2))H_2 + nCO$ $C_nH_m + nCO_2 \rightarrow (\frac{m}{2})H_2 + 2nCO$

also during testing at the pilot-scale. Many researchers have reviewed the work leading to a reduction in the tar content using catalysts [131,132] and other mechanical and thermal methods both experimental and modeling [133–136]. Although much R&D has been undertaken in tar reduction, there is still a gap in simulation modeling that needs to be addressed for a general tar reduction model for biomass instead of a specific component model.

## Catalytic steam gasification

Catalytic steam reforming of the intermediate volatiles formed is carried out either by fractionation of pyrolysis biooil or biomass gasification that enhanced the hydrogen yield
[130]. Catalysts are very important to enhance the hydrogen
yield by accelerating the water gas shift reaction, steam
reforming reaction [132]. Two groups of catalysts are mainly
used for biomass gasification [131,137,138], which are categorized based upon their function. These categories are (i) precatalyze the raw biomass termed as group-1 catalysts (ii) postcatalyze the gases produces as a result of gasification classified as group-2 catalysts [139].

#### Group-1

These catalysts are better known as the primary catalysts [140] and are typically added directly to the raw biomass before gasification either through wet impregnation or via dry mixing with biomass. The primary purpose of these catalysts is to reduce the tar content, however, these have little effect on the conversion of tar into lighter gases [141]. Group 1 catalysts aid the gasification reaction and enhance the yield of the product and operate under the same condition as the gasifier [142-144]. Three types of primary catalysts have been commonly used in gasification processes. Shahbaz et al. [132] have reviewed the effect of catalysts in the gasification process for hydrogen yield and tar reduction. Dolomite and alkali metal have been reported as primary catalysts [145]. In this context, dolomite (MgCO<sub>3</sub>·CaCO<sub>3</sub>) is used in the gasifier for the reasons that it is cheap, easy to dispose of and reduces the tar content significantly [125]. Ono et al. [146] have also reported different dolomite catalysts with variations of Fe2O3 in the steam reforming of wood in a catalytic reactor at 805-850 °C. A few other works on dolomite catalyst are also available in the literature [146-150]. Dolomite is a very useful catalyst as it provides aid for improving the hydrogen yield as well as reducing CO<sub>2</sub> through the carbonation reaction [151-153]. The removal of CO2 is directly related to the cost of gasification process. In this regard, Khan et al. [154] used in-situ removal of CO2 with the help of a dolomite catalyst for the steam gasification of palm kernel shell and obtained 82 vol% hydrogen with significant reduction of CO<sub>2</sub> [144,155,156]. Therefore, dolomite has emerged as a popular in-situ catalyst. Many experimental and modeling studies were made to investigate dolomite (catalyst) effect on the gasification process for hydrogen production [142,157]. Inayat et al. [158] made the mathematical model for the steam gasification of empty fruit bunches (EFB) using CaO which resulted in 76 vol% of hydrogen production [159,160]. Additionally, alkali metals have a positive contribution to tar reduction, and the quality and quantity of the product yields [161,162]. In some cases, its recovery is difficult and may multiply the operational cost. The challenges associated with the use of catalysts have also been pointed out by many researchers [115,148,163—165]. Each type of catalyst has some pros and cons associated with it, among which the regeneration and the cost of catalysts are of the utmost importance [140]. Coal bottom ash is a waste product of the power generating industry. Its typical characterization reveals that it contains reasonable amounts of alkaline metals as well as CaO and may serve as a catalyst [137,166,167]. The use of bottom ash in gasification has demonstrated very prominent results in terms of hydrogen production, i.e., 79 vol% and might be considered as a cheap catalyst for the gasification process [143,168,169].

The plant biomass contains a certain amount of ash which consists of Mg, Ca, and K [170,171]. According to thermodynamic principles, the ash formed a liquid solution with the molten salt known as the melted salt, which did not reduce the tar formation [170,172]. The molten salt directly affected the kinetics of the reaction and enhanced the reactivity of reactions from the conversion of biomass into gaseous products [173]. Brandon et al. [170] performed the steam gasification of switchgrass cellulose using the molten salt of Li, K, and Na and a 25% increase in syngas was observed and a 77% decrease in tar formation, which is due to an increase in the reactivity of reactions and was confirmed by the 49% increase in the reactivity index. Kirtania et al. [174] investigated the kinetics of different alkaline salts in the catalytic gasification of char and reported the effect on reaction rates of different alkali salt types and loading. Jin et al. [175] reported the increase in 16.2 vol% of H2 using the molten salts of Li, Na, and K carbonated in the steam gasification of biomass due to the excellent heat and mass transfer. Many researchers have shown the effective use of molten salt for hydrogen production in biomass gasification [176-178]. Franginei et al. [171] reviewed the application of molten salt in the biomass gasification process.

### Group-2

These catalysts, also known as secondary catalysts, which are placed in reactors situated after the gasification reactors [179]. These catalyze the reforming reactions and also enhance the energy quality of the final product [180]. The reactors, which engage these catalysts, are independent of the type of gasifier and may have the same or even different operating conditions. Transition metals are frequently used as secondary catalysts in secondary reformers [181]. A lot of research has been done on these metals since it has been an area of concern for many years [75]. Nickel is a widely used metal in the gasification industry and it plays an important role in reducing tar content, at the same time it reforms the methane in the product gas. At temperatures higher than 750 °C, H<sub>2</sub> and CO contents increase quite significantly [182-184]. Ni is one of the commercial catalysts used for hydrogen production however it has limitations in terms of its sintering potential [185]. To avoid this problem many other metals with Ni are used for its productive usage [140]. The metals such as Rh [141,142], Fe [143], Pt [144], dolomite [145,146], Mg [130,148], Al [147,149], and Zn [150] are used with Ni to overcome this issue and further enhance the hydrogen contents in the product gas.

## Supercritical water gasification

The supercritical water gasification of biomass is one of the most widely used and commercially exploited techniques for hydrogen production from biomass. Water has been used as a gasifying medium due to the reasons that it is abundantly and easily available, non-toxic, inexpensive, and environmentally friendly. It has an important advantage in that, the feed to be used does not require any pre-drying, therefore it saves time as well as energy and cost [186]. Sewage sludge, sea algae, waste vegetables, and fruits can be gasified using this process. The products of gasification in this type have a high molar fraction of hydrogen which makes it easier to be separated from other gases. The production of char and tar is very low, however, these may have the problem of plugging in the apparatus. This problematic issue can be reduced by the efficient use of catalysts. Corrosion of reactor walls due to the formation of hydrogen peroxide is a major issue in this technique and much less information is available regarding this issue [153]. This process was also discussed by Modell et al. [151] in a patent released in 1978 for the gasification of glucose and the sawdust of the maple tree. Gasafi et al. [152] studied and found that sewage sludge may be a potential market for supercritical water gasification and might have a bright future [152]. Supercritical water is used as a gasifying agent in this technique, as the critical point of water is at 374 °C temperature and 22.1 MPa pressure. Under these conditions, there is no distinction between water and steam and only a single phase exists, which is better known as supercritical water [153,155]. Reactors used for these processes have been operated at different conditions. An example is the continuously operating tubular flow reactor that operates at 700 °C and pressures up to 35 MPa [31]. There are two methods for the supercritical gasification of biomass [156], as described below.

Non-Catalytic supercritical water gasification (NCSCWG) Non-catalytic supercritical water gasification (NCSCWG) is also called the high-temperature supercritical gasification or steam-only gasification process because the temperature for this process ranges from 500 to 750 °C [157]. It has been shown that the amount of hydrogen is governed by two parameters namely reaction temperature and steam to carbon ratio. The hydrogen fraction increases with reaction temperature up to  $900 \,^{\circ}$ C [159,160]. Some authors have observed that the fraction of hydrogen decreases as the temperature exceeds 1100 °C [161]. The overall reaction is provided by Guo et al. and is given in Eq. (5) [187].

$$CH_xO_y + (2 - y)H_2O \rightarrow CO_2 + \frac{2 - y + \frac{x}{2}}{H_2}$$
 (5)

This reaction is divided into two steps [162]. The first is steam reforming while the second is the water-gas shift reaction. The advantage of this method is that these two reactions are carried out in a single reactor. The previous researchers demonstrated in their studies that the water-gas shift reaction is necessary only for steam gasification [164,165]. Supercritical water gasification is a very important hydrogen production technique, but a lot of improvement is needed in this field to make it viable for future applications. Suzuki et al. [181] has shown from their studies that one of the

important factors affecting the efficiency of the process is the recovery of the process water and the reactivity of steam that is less than that of air/oxygen. For this type of gasification, a fluidized bed gasifier is preferred because in fluidized bed gasifier, moving particles assist in homogenizing the temperature of the gasifier by shifting heat from char combustion to an endothermic gasification reaction [166]. Djesus et al. [168] studied the effect of particle size and his investigation explained the effect of particle size on the efficiency of the process. It was observed that a decrease in feed particle size increases hydrogen yield, which also results in efficient heat and mass transfer due to increased reactive surface area. In future, this technology could be more attractive and promising, if it is integrated with solar energy to achieve the supercritical conditions of water [169].

### Catalytic supercritical water gasification (CSCWG)

Catalytic Supercritical Water Gasification (CSCWG) is also known as low-temperature catalytic gasification due to its low temperature operating ranges, i.e., 350–600  $^{\circ}$ C. The catalyst along with reduced reaction temperature also reduces the formation of char and tar. Resende et al. [188] studied and presented the result for the use of metal catalysts for the supercritical water gasification of cellulose and lignin. Laboratory scale experiments have been conducted by several researchers which laid the foundation for implementation of the concept on pilot and commercial scales. The first pilot plant for CSCWG was established by Jesus et al. and Rauzan et al. [168,169] in San Diego at the General Atomics facility to explore the earlier results of laboratory-scale experiments. It was found that the yield of hydrogen was comparable with the results of laboratory experiments as 10 g of hydrogen per 100 g of feed was produced [43]. The catalysts are very useful in the water gasification process that enhances hydrogen production [189,190]. Watanabe et al. [191] found that the amount of hydrogen produced in the case of catalytic supercritical water gasification was doubled when compared with non-catalytic supercritical gasification. Park et al. [192] used RuO2 for aromatic compounds. It was concluded from this investigation that RuO2 provided all the activity mechanism for the K2CO3 catalyst. In the gasification of cellulose in catalytic supercritical water gasification, K2CO3 was more active than Ca(OH)2 but did not capture CO2 [193]. Metallic nickel catalysts have been used for many years for the conventional gasification of fossil fuels and are still used for biomass catalytic supercritical gasification [137]. The cost of hydrogen production is very important for the development of a technology; a very comprehensive study was made by considering all parameters and the cost of hydrogen was 3.4 \$/kg for the hydrogasification of biomass wastes [194]. Zhang et al. [195] documented the literature about the exergy efficiencies of the SCWG process and reported values in the range of 0.04-42.05%. Table 5 summarizes the hydrogen production from supercritical gasification process for numerous biomass types.

## Solar biomass gasification

In this process, biomass is milled and dried to remove moisture contents. After drying it is placed in a high-temperature reactor at the temperature about 700–750  $^{\circ}$ C [196,197]. The

Table 5 – Hydrogen pro	oduction through supe	ercritical biomass gasification from dif	ferent biomass.	
Feed	Catalyst	Reactor type and conditions	Hydrogen yield	References
Glucose	Ni/activated charcoal	Packed-bed reactor, 28 MPa, 650 °C	15.6 mmol/g	[103]
Olive mill wastewater	_	Coiled tubular reactor, 25 MPa, 600 °C	10.79 mol%	[104]
Switchgrass biocrude	Ni/ZrO <sub>2</sub>	Packed-bed reactor, 600 °C, 25 MPa	81.67 mol/g carbon reacted	[105]
Bark	Ni/hydrotalcite	Batch reactor, 380 °C, 23 MPa	2.05 mmol/g	[106]
Sewage sludge	KOH	Fluidized bed reactor, 540 °C, 30 MPa	15.49 mmol/g	[107]
Maize silage hydrochar	K <sub>2</sub> CO <sub>3</sub>	Micro-autoclaves, 400 °C, 30 MPa	8.9 mol%	[94]
Coconut shell	K <sub>2</sub> CO <sub>3</sub>	Tubular batch reactor, 600 °C, 23–25 MPa	4.8 mmol/g	[93]
Fruit pulp	RU/activated charcoal	Batch reactor, 600 °C, 25 MPa	54.8 mmol/g	[95]
Microalgae (Cenedesmus quadricauda)	Nickel/α-Al <sub>2</sub> O <sub>3</sub>	Batch reactor, 385 °C, 26 MPa.	4 mmol/g	[108]
Microalgae Enteromorpha intestinalis	Fe–Ni–Ru/γ-Al <sub>2</sub> O <sub>3</sub>	Batch microreactor, 440 °C, 25 MPa	12.28 mmol/g	[109]
Sewage sludge		Continuous reactor, 600 °C, 25 MPa	40 vol%	[110]

molecules of the biomass are broken in the reactor and synthesis gas is produced that is integrated with the char combustor. The gas consists of a mixture of H<sub>2</sub>, CO, CH<sub>4</sub>, CO<sub>2</sub>. and some other molecules. Peter et al. [44] reviewed the advantages and disadvantages of solar gasification with all aspects such as yield, type of process, and process parameters. Exhaust gas coming out of the char combustor is used to dry the biomass. The exhaust gas coming from the char combustor and superheated steam coming from the combustor, in which methane and carbon monoxide are burnt, is recycled through the gasification chamber. As a result, the synthesis gas is produced in the gasification chamber having a temperature around 800 °C which is cooled in the heat exchanger with the saturated steam coming out from the solar field. The saturated steam is heated to a temperature of 700 °C [169]. The synthesis gas is cleaned in the water scrubber and hydrogen is separated from the CO2 in the separator. Other gases like carbon monoxide and methane are introduced to the combustor from the separating chamber, where they are burnt to raise the temperature of steam from 700 °C to 800 °C, which is used for fluidization purposes of the gasification bed [198]. In this way, steam is recycled throughout the process. Saturated steam is produced in the solar thermal field and then with the help of heat exchangers, it is superheated for heat integration and optimization. A feasibility study of this process was carried out by Antal et al. [199]. The high reaction temperature for promoting a high hydrogen yield is the main concern of this technology due to the extensive energy required for process initiation. To meet this challenge many researchers intended to utilize solar energy to attain the reaction temperature. Shahbazov et al. and Midilli et al. [200,201] used parabolic mirror reflectors for agriculture waste biomass to increase the yield of hydrogen. Solar gasification is emerging as an alternative source of conventional gasification to utilize the solar heat that has the potential to reduce the overall cost of the process. The main challenge in this field is to use the solar field area, storage capacity to attain a high temperature inside the reactor [202]. The combustion looping process with gasification is effective for hydrogen production through gasification and combustion which resulted in a cost reduction for the process [203,204]. The continuous driven solar reactor system was investigated, which increased the carbon conversion rate into gaseous

products about 74% and 70 mmol/g biomass was obtained [205]. Many modeling processes have been developed to study and encourage the utilization of solar heat for biomass gasification, such as the irradiated fluidized bed [206] and hybrid solar/autothermal operation [207], that enhances hydrogen enriched syngas production [208,209]. Hydrogen production from solar gasification has been studied by different researchers and a summary of the achievements is given in Table 6. Solar gasification is an important alternative that should be utilized in warm and hot countries to save the heating duty required during the gasification process to make it comparable to  $\rm H_2$  obtained through fossil fuel gasification.

## Non-thermal/biological methods

Hydrogen production from biological conversion of biomass is another important element of future bio-refinery systems. The production of hydrogen using biological methods was discussed by Levin et al. [212] and it gained prominence in the mid of 1970's when the oil crises shook the world economy. During that decade, many biological processes were developed and employed for hydrogen production. These processes are able to produce the hydrogen to meet the increasing demand for hydrogen and numerous research studies have documented these results in many review articles for further research, challenges, and commercialization [213-215]. It has some distinction as compared to other processes due to the zero accumulation of CO2 and a wide range of waste materials available for hydrogen production. Among other methods, it was considered to be less energy-intensive, as it is carried out at ambient pressure and temperature [216]. However, the biological route has limitations of low hydrogen production rate and low hydrogen yield. In this section, the biological route incorporating photolysis, fermentation, and the biological water-gas shift reaction has been discussed for further research.

### Direct bio-photolysis

In this process, a microalgae photosynthesis system converts the solar energy into chemical energy, which results in hydrogen production from biomass and this process involves a photo-autotrophic organism. Regularly, freshwater algae are

Table 6 $-$ Hydrogen production through solar gasification from different biomass.	rough solar gasification from di	fferent biomass.		
Feed	Light Source/Catalyst	Reactor type and conditions	Hydrogen yield	References
Glucose, corn meal, wheat stalk	Solar power/NaOH	Snake like tubular reactor, 500 °C, 24 MPa, DNI: 610 W/m² (Direct normal $$ 11 mmol/g irradiation) Supercritical water gasification	11 mmol/g	[210]
Glucose, corncob	Solar power/KOH	Spiral tube tubular reactor, 636 °C, 24 MPa, DNI (Direct normal irradiation): 571 W/m² Supercritical water gasification	27.1 mmol/g	[211]
Switchgrass biocrude	Ni/ZrO <sub>2</sub>	Packed-bed reactor, 600 °C, 25 MPa	81.67 mol/g carbon reacted	[105]
Bark	Ni/hydrotalcite	Batch reactor, 380 °C, 23 MPa	2.05 mmol/g	[106]
Sewage sludge	КОН	Fluidized bed reactor, 540 °C, 30 MPa	15.49 mmol/g	[107]
Maize silage hydrochar	$K_2CO_3$	Micro-autoclaves, 400 °C, 30 MPa	8.9 mol%	[94]
Coconut shell	$K_2CO_3$	Tubular batch reactor, 600 °C, 23–25 MPa	4.8 mmol/g	[63]
Fruit pulp	RU/activated charcoal	Batch reactor, 600 °C, 25 MPa	54.8 mmol/g	[62]
Microalgae (Cenedesmus quadricauda) Nickel/α-Al <sub>2</sub> O <sub>3</sub>	Nickel/ $\alpha$ -Al $_2$ O $_3$	Batch reactor, 385 °C, 26 MPa.	4 mmol/g	[108]
Microalgae Enteromorpha intestinalis	$Fe-Ni-Ru/\gamma-Al_2O_3$	Batch microreactor, 440 °C, 25 MPa	12.28 mmol/g	[109]
Sewage sludge	1	Continuous reactor, 600 °C, 25 MPa	40 vol%	[110]
Microalgae	Solar heat by high flux simulator	Batch reactor, 905 °C	64 vol%	[208]

used in fermentation, while marine algae are utilized in seawater. This bio-system offers some advantages, such as no need for substrate and it is a  $\rm CO_2$  neutral system with the use of sunlight [45]. Therefore, direct bio-photolysis is considered as both a renewable and environmentally friendly process. Biological hydrogen production is carried out in two steps, in the first step, growth of the cell takes place and in the second step, hydrogen is evolved as shown in Fig. 5 [217]. Two photosynthetic systems are used in producing hydrogen when water is utilized as feed: photosystem-1 and photosystem-2. Photosystem-1 is used for  $\rm CO_2$  reduction while photosystem-2 is engaged to split water for  $\rm O_2$  liberation. Two photons are produced to form either  $\rm CO_2$  or  $\rm H_2$  in the presence of hydrogenase. The equations involved are provided below.

$$2H_2O + SolarEnergy \rightarrow O_2 + 4H^+$$
 (6)

$$2H^+ + 2e^- \rightarrow H_2 \tag{7}$$

In this photosynthetic process, photosynthetic electrons reduce a proton to an atomic state and then molecular hydrogen. The oxygen produced in this process has some adverse impacts such as the hydrogen is poisoned and the photosynthetic system is disturbed, which is the major shortcoming of this process. To avoid these issues, oxygenabsorbing species, for instance, glucose oxidase, are used [218]. To address this issue, the electrochemical photoreactor for spirulina has been developed and hydrogen rate increase four times as well, and in another study, in order to solve the reduction of the increase in oxygen, four different reducing agents were used for the microalgae culture [219,220]. Many research studies have been reported to solve this problem [221,222], however, there has not been a commercial success due to the issues of limited production of hydrogen and low solar energy conversion efficiency. However, for hydrogen production, the employment of mutants can assist in overcoming the efficiency limitation, and efficiency has been increased significantly [223]. Benemann et al. [224] estimated the cost of direct bio-photolysis to produce hydrogen to be \$ 20/GJ, by assuming that the capital cost is about \$60/m<sup>2</sup> with a total solar conversion efficiency around 10%. In another report, the capital cost was proposed to be \$ 100/m<sup>2</sup> [225]. Despite these facts, this process has not yet been proved to be industrially economical, however, it has attracted the attention of researchers as it assists in understanding the basic concepts involved in the bio-hydrogen production process.

## Indirect bio-photolysis

In this process, Cyanobacteria convert the biomass into hydrogen by coupling two stages of the biological processes namely photosynthesis and fermentation, in the presence of hydrogenase. The whole system results in environmental CO<sub>2</sub> fixation into carbohydrates and then their conversion into H<sub>2</sub> by the action of hydrogenase in darkness and sunlight as well. Solar energy is utilized for CO<sub>2</sub> fixation. For this purpose, the overall efficiency of solar light must be greater than 10% to compete with other processes [217,226]. A maximum of 16.3% conversion efficiency has been achieved until now [227]. Markov et al. [228] provided an estimate that requires light

intensities of 45–55  $\mu$ mol-1m<sup>-2</sup> and 170–180  $\mu$ mol-1m<sup>-2</sup>. This process is completed in a two-stage process as shown in Fig. 6 and mentioned in the following equations.

$$12H_2O + 6CO_2 \rightarrow C_6H_{12}O_6 + 6O_2 \tag{8}$$

$$C_6H_{12}O_6 + 12H_2O \rightarrow 12H_2 + 6CO_2$$
 (9)

The first reaction is responsible for the fixation of environmental CO2 to glucose while the later one for fermentation of glucose to H2. Commonly used cyanobacteria are the species of Oscillatoria, Anabaena and Calotherix [229]. The photoproduction rate of hydrogen increases with light intensity and optimized yield were reported with light intensity of 12.5 ml H<sub>2</sub>/g (cdw)h (cdw implies cell dry weight) and pH value ranging from 6.8 to 8.3. By increasing the temperature from 30 to 40 °C, the production of hydrogen is doubled. The estimated overall cost has reached up to 10\$/GJ of hydrogen [218]. Variation in cost depends on the technology used to produce hydrogen. This technology is still immature as the overall efficiency is as low as 1-2%. It is currently being investigated by many research groups [230], and outstanding research efforts seems necessitated to commercialize this technology for hydrogen production.

#### Photo-fermentation

In the photo-fermentation process, photosynthetic bacteria utilize the nitrogenous matter to convert biomass into hydrogen only and only if the sunlight is present. Photosynthetic bacteria donate electrons by undergoing an-oxygeno photosynthetic process with an organic acid or a reducing sulfur compound. The rate of H<sub>2</sub> production increases with the intensity of light, while on the contrary, the light conversion efficiency decreases. The photosynthetic bacteria used in the photo-fermentation has a comparatively high light conversion efficiency to cyanobacteria, which is used in indirect bio-photolysis. Basak et al. [231] studied purple non-sulfur bacteria that are used in an oxygen-deficient environment in the presence of nitrogenase whereas an organic acid is used as the reducing agent for the production of hydrogen. There are certain shortcomings of this method, which are listed below:

- a) The low conversion efficiency of solar energy (3–10%);
- b) Demand for anaerobic photo-bioreactors, which cover a large area;
- c) The use of nitrogenase enzymes requires high energy for their activation.

Nitrogenase activity plays a very important role in the production of hydrogen by photosynthetic bacteria. Hydrogenase is active under the same condition for hydrogen production and hydrogen uptake. The major benefit of this process is that the high concentration of H<sub>2</sub> in the product gas stream is significant; around 96% of H2 concentration was reported by Tao et al. [232]. Another advantage of this process is that the organic acid, used as a substrate, could be found in the effluent wastewaters of different industries. The effluent of dark fermentation can also be used as the substrate for photo-fermentation [233,234]. Different types of biomass wastes could also be employed for hydrogen production via this process [235]. The H2 production was found to be increased by 2-3 times using a sole carbon sources [236]. The bacteria system and the hydrogen conversion efficiency for different feedstocks have been provided by Fedorov et al. [237] and are shown in Table 7. The schematic for the photofermentation to produce hydrogen is provided in Fig. 7. There have been many research efforts reported in the literature for photosynthetic bacteria; however, the photofermentation process has never been identified as an economically viable method. Photo fermentation processes have some advantages such as large amount of feedstock and utilization of abundant heat available in the form of sunlight. The challenges which still need to be addressed include the lower volumetric flowrate of hydrogen, the conversion efficiency as well as wide surface area requirement.

## Dark-fermentation

From the name of this type, it is evident that darkness is a key element in this process. For dark fermentation, anaerobic bacteria and micro-algae are used to produce hydrogen where the temperature is maintained in the range of 30 °C-80 °C [238]. The simple process flow diagram is given in Fig. 8 for biomass processing and its conversion to hydrogen. This process has some merits, such as its simplicity, a continuous hydrogen production rate, a low energy requirement, and the use of low grade or waste biomass [45,239]. Along with hydrogen and carbon dioxide, a few other gases are also produced which are dependent upon the type of biomass substrate. A large number of substrates i.e., glucose, sucrose starch, and cellulose and anaerobic fermentative bacteria i.e., thermophilic, mesophilic and facultative are available for utilization in this process as compared to the process of photo fermentation [45,46]. For glucose as a substrate, theoretically, 12 mol of hydrogen can be produced, as shown in Eq. (10). On the contrary, practically only a maximum of 4 mol of H2 are produced per mole of glucose because of acetic acid production, as demonstrated in Eqs. 10-12 [240].

$$C_6H_{12}O_6 + 6H_2O \rightarrow 12H_2 + 6CO_2$$
 (10)

$$C_6H_{12}O_6 + 2H_2O \rightarrow 2CH_3COOH + 4H_2 + 2CO_2$$
 (11)

$$C_6H_{12}O_6 + 2H_2O \rightarrow CH_2CH_2CH_2OH + 2H_2 + 2CO_2$$
 (12)

Table 7 — Bacteria system	and hydrogen conversion efficiency for different feed	s.
Biomass type	Bacteria system	Hydrogen conversion efficiency
Lactic acid	Rhodobacter spheroids immobilized	86%
Lactate feedstock	Rhodobacter capsulatus	30%
Wastewater	Rhodobacter spheroids immobilized	53%

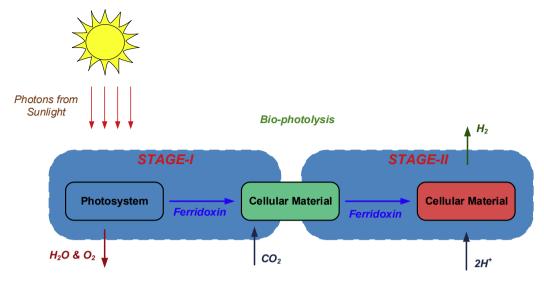


Fig. 6 - Indirect bio-photolysis route for hydrogen production.

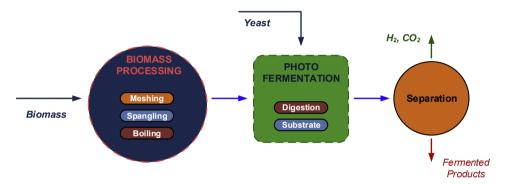


Fig. 7 - Hydrogen production mechanism through photo-fermentation.

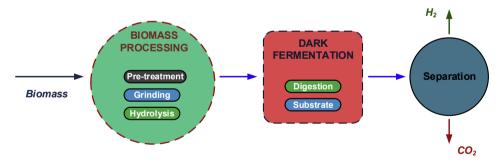


Fig. 8 - Hydrogen production mechanism through dark fermentation.

Production of  $H_2$  depends on the hydraulic retention time, pH value and partial pressure of gas. The pH value is a crucial parameter and must be controlled carefully; ranging between 5 and 6 [241]. Dark fermentation has some drawbacks, such as low yield and less energy efficient, longer residence time and production of byproducts. All these factors considerably influence the overall cost of the process [45]. Attention should also be paid to the hydraulic retention time, which also plays an important role in the production of hydrogen [240]. A hydraulic retention time of 0.5 day is optimal in the dark fermentation of wastewater. Hydrogen production decreases

with an increase in reaction time. Two types of reactors have been studied for this process, the continuous stirred tank reactor (CSTR) and the upflow anaerobic sludge blanket reactor (UASBR). Under the same condition, the yield from a USABR is higher than that of the CSTR using a comparatively low retention time [242,243]. Although the yield for the hydrogen production from this process is high compared to other processes, however, the product gases have a low concentration of hydrogen (40–46%) [235]. Due to this reason, the purification of the product seems necessary to improve the concentration of hydrogen before it can be used in a fuel cell.

Fermentation process	Reactor	bacterial strain	Substrate	Process condition	Hydrogen yield	References
Dark	CSTR	Microbial consortium/digester	Tofu waste (Glucose)	HRT 4, pH 5.5, 110 °C	12.01 H <sub>2</sub> L/day	[250]
Dark & photo	Batch	Clostridium butyricum (C. butyricum)	Grounded wheat (Glcouse)	pH 7.0 ± 0.002, 35 °C	1.59 mol H <sub>2</sub> /mol glucose, 4.16 molH <sub>2</sub> /mol glucose	[251]
Dark	CSTR	sorghum extract.	Sorghum bicolor L. Moench (glucose)	HRT 12, pH 4.7, 35 °C	$0.93 \pm 0.03 \text{ mol H}_2/\text{mol}$ glucose, $3.50 \text{ H}_2 \text{ L/day}$	[252]
Dark & photo	Batch	Clostridium species, (anaerobic), Rhodopseudomonaspalustrs species	Cassava starch	рН 6.3, 31.3 °С,	351 ml H <sub>2</sub> /g starch, 489 ml H <sub>2</sub> /g starch	[253]
Dark	Batch	Silage grass based Ruminobacilus xylanolyticum, Acetanaerobacteriumel, Ongatum	Silage grass	рН 7, 35 °C	37.8 ml $H_2$ /g silage	[254]
Dark	Batch	Rhodobacter sphaeroides-RV	Grounded wheat (Glucose)	HRT 17 h, pH 6.3,37 °C	4.55 mol H <sub>2</sub> /mol glucose	[255]
Photo	Tubular bio reactor	bacterium, Rhodobacter capsulatus	Acetate	pH,10-35 °C	0.6 mol H <sub>2</sub> /mol acetate	[256]
Dark	Batch	Bacterial hydrolysis seed microorganism	Dry grass (Glucose)	pH 7, 37 °C	72.21 mL/g-dry grass	[257]
Photo	Tubular reactor	(Rhodospirillum rubrum, Rhodobacter sphaeroides	Corn stove	pH 4.9, 30 °C	211.9 mL/L-material	[258]
Photo	CSTR	bacteria HAU-M1w	Corn stove	pH 5.4, 30 °C	58.73 mL/g	[259]
Dark	Bio-chemical reactor	Enterobacter aerogenes	Humulus scandens	рН 6.59, 35 °C	64.08 mL H <sub>2</sub> /g	[260]
Dark	CSTR	Seacoast sludge	Sucrose	pH 5.5-6, 35 °C	120 mol/m³-d	[249]

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Table 9 – Comparison of	separation technologies.		
Separation technologies	Advantages	Dis advantages	References
Pressure swing adsorption (PSA)	<ul> <li>Very effective separation is &gt;99.99% in part per million</li> <li>Useful at small and large scale, commercially available</li> </ul>	<ul> <li>The 20% produced hydrogen lost during the separation</li> <li>Very high-cost process about 50% of the total H<sub>2</sub> production process.</li> <li>Energy-intensive process</li> </ul>	[275–279]
Temperature swing adsorption (TSA)	<ul><li> Useful at a higher temperature</li><li> Commercially available</li></ul>	<ul><li>Dilution of the separated gas</li><li>Energy and cost-intensive process</li></ul>	[280-283]
Electric Swing adoration	<ul><li>Energy-efficient than TSA</li><li>An improved form of TSA</li></ul>	<ul><li>Dilution of separated gas</li><li>Intensive energy and cost process</li></ul>	[281,284]
Cryogenic separation technologies	<ul><li>Suitable for large scale</li><li>Work at high pressure on</li></ul>	<ul> <li>Purity is less than 99%</li> <li>Required many equipment's and costly process</li> <li>Suitable for only large scale</li> </ul>	[285–288]
Amine based separation	<ul> <li>Old and commercialize the technology.</li> <li>Available technology for separation.</li> </ul>	<ul> <li>Corrosive and harmful,</li> <li>Affected by the SOx and NOx in flue gases,</li> <li>Loss of amine solution due to volatility, Degradation issues</li> </ul>	[289,290]
Membrane separation	<ul> <li>Low cost, lightweight, simple and easy operation. Less maintenance and operation</li> <li>less energy-intensive, less carbon footprint, and environment issue</li> <li>No problem for scale-up, effective in every system</li> </ul>	Still not able to industrial level due to permeability level is still less than 100 barrar	[288,291–293]

Bélafi-Bakó et al. [244] reported that by using a two-stage gas membrane separation system 73%  $\rm H_2$  concentration can be achieved in the biogas. Balachandar et al. [245] successfully scaled up the dark-fermentation process from bench to pilot scale and observed a 1.2 times increase in  $\rm H_2$  production with a good energy gain 4.6 kJ g-1 COD, which is good news for its technological development. This process has certain advantages, as solar energy is not required, land requirements are low and the weather conditions do not affect the process. Recently, a study utilized the corn stove for hydrogen production through the following processes: photo fermentation, dark fermentation and dark photo co-fermentation and reported the  $\rm H_2$  production as 141.2, 36.02, and 90.13 mL  $\rm H_2/g$  respectively [246]. Recently, many pilot scale studies in the range of 380–3000 L reactor size for commercialization have

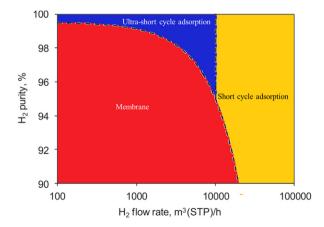


Fig. 9 — Technological zones for hydrogen purification processes. Modified from Ref. [271]. Copyright 2015 Elsevier.

been performed [247–249]. Table 8 summarizes some important reported research work in terms of hydrogen yield through dark and photo-fermentation. In the case of hydrogen production, dark fermentation has some advantages such as higher production rates, ease in operation, bearable cost due to no need of light for fermentation, but the main changes are still questionable such as higher content of by-products, a large amount of CO<sub>2</sub> and electricity requirement is high [41].

## Biological water-gas shift reaction

Biological water gas shift reaction based technology is developed for hydrogen production using some photoheterotrophic bacteria like Rhodospirillum feedstock or Rubrivivax gelatinosus, which is non-sulfur, purple photosynthetic bacteria, and can perform the water-gas shift reaction at 25 °C and 4 atm [261]. These bacteria do not require light and use CO as a raw carbon source to reduce the  $\rm H^+$  ion, hence producing  $\rm H_2$ .

$$CO + H_2O \leftrightarrow CO_2 + H_2$$
  $\Delta H = 154kJ$  (13)

In this process, the main products are  $CO_2$  and  $H_2$ , hence it favors the production of hydrogen. Currently, this process is reported at laboratory scale for which only research works are available so far. The challenge of this study was to identify the suitable microorganisms for high CO uptake and to estimate high rate of production. Non-sulfur purple bacteria have the ability to perform the bacterial reaction in darkness and convert up to 100% of the CO based on the stoichiometric value. For this process industrial effluents are used as the substrate.

A higher rate of hydrogen production has been observed compared to other process. The literature reports that  $96~\text{mmol}\,H_2\,L^{-1}h^{-1}$  has been produced by the biological water-

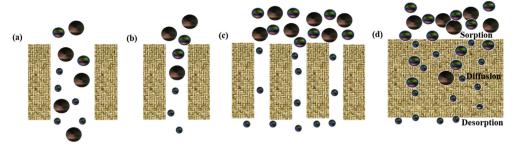


Fig. 10 — Gas separation mechanisms through porous and dense membranes; (a) Convective flow, (b) Knudsen diffusion, (c) Molecular sieving, (d) Solution-diffusion.

gas shift reaction, which was considerably high compared to 20-50 mmol  $\mathrm{H_2}$   $\mathrm{L^{-1}h^{-1}}$  obtained via anaerobic fermentation process [29]. It was reported that this reaction could be economically viable, if the methane concentration is below 3%. The cost of hydrogen production from this process ranges from 1.75 to 2.25 \$/kg when the concentration of methane is between 1 and 10% [262]. In another report, 3.4\$/kg was estimated as the cost of hydrogen production for this process. This cost of hydrogen production is comparatively much less than that for other biological processes (12–20 \$/kg) [19]. The cost of the biological water-gas shift process is lower as compared to thermochemical water-gas shift process for the reason that fewer equipment items are involved. Due to the low cost of hydrogen production, this process has become an area of interest of several researchers [263–265].

# Implementation of membrane for biomass-based hydrogen separation

Membrane, absorption, adsorption such as pressure swing adsorption (PSA), temperature swing adsorption (TSA), electrical swing adsorption (ESA) and cryogenic technologies are often used at an industrial scale for the separation and purification of hydrogen produced from biomass [266–269]. Although the above-mentioned technologies are commercialized, but they are facing many issues of cost and energy-intensive performance. Membrane separation is a very good, important and emerging technology, successfully tested at laboratory and pilot scale and has the potential for commercialization. Table 9 provides the pros and cons of different H<sub>2</sub> separation technologies. Membranes, ultra-short cycle adsorption, and short cycle adsorption are less energy intensive processes and technological zones for optimal target purity of product and installed productivity are established for

these, depicted in Fig. 9. Membrane technology for H<sub>2</sub> recovery and purification provides a broad range opportunity in comparison to the other ones as shown in Fig. 9. Membrane technology occupies a particular place because energy is not required for phase transitions. Among all available technologies for hydrogen recovery in biomass processing, membrane separation has unique opportunities such as reduced energy consumption, small footprint, simplicity and continuity of operation, improved efficiency and low cost. In particular, a combination of a membrane separation process and a catalytic reactor would result in enhanced shifted reaction equilibrium, concentrated products and higher conversion [270]. The first flat sheet membrane to separate gases was developed at industrial scale in 1977 in Russia and membrane technology for H<sub>2</sub> separation and recovery was introduced in the market in 1980 for the first time [271]. In recent years, more than 500 patents are covered on hydrogen selective membranes and syntheses of polymeric membranes are dedicated with more than 50% patents. The non-porous inorganic membranes covered around 25% patents and also about 25% patents are dedicated to porous inorganic membranes [272-274].

### Theoretical background

A membrane is a selective barrier that is dependent on the selective permeation of hydrogen from mixed gases and the selectivity depends on the membrane properties. The typical driving force for the permeation is the  $\rm H_2$  partial pressure in the feed stream, which is balanced by the permeate's side  $\rm H_2$  partial pressure. The membranes, inorganic - manufactured from such materials as metallic or ceramic, and organic - such as polymer or carbon, are applied for hydrogen separation [294,295]. Generally, hydrogen separation, using membranes, is based on three mechanisms including Knudsen diffusion, molecular sieving and solution diffusion (Fig. 10). The gas

Table 10 — Commercially available	polymeric membranes	and their selectivity.		
Polymer		Sele	ctivity	
	H <sub>2</sub> /CO <sub>2</sub>	H <sub>2</sub> /N <sub>2</sub>	H <sub>2</sub> /CO	H <sub>2</sub> /CH <sub>4</sub>
Cellulose acetate (Separex)	2.4	72–80	30–66	60-80
Polysulfone (Permea)	2.5	56–80	40-56	80
Polyaramide (Medal)		>200	100	>200
Tetrabromopolycarbonate (MG)	3.5	90	100-123	120
Polyimide (Ube)	3.8	88-200	50-125	100-200
Silicon rubber	0.2	22	0.69	0.8

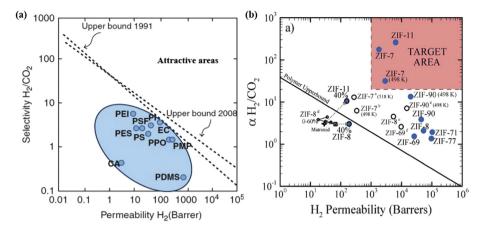


Fig. 11 — Roberson upper boundary for H<sub>2</sub>/CO<sub>2</sub> separation (a) performance of the membranes prepared from commercially available polymers [80,304–306]; CA: cellulose acetate, PSF: polysulfone, PI: Polyimide, PEI: Polyetherimide, PDMS: polydimethylsiloxane, PMP; polyme polymetylpentene, PPO: poly (phenylene oxide), PS: polystyrene, EC: ethyl cellulose; (b) Experimental (empty) and predicted intrinsic (solid) performance of ZIF (Zeolitic Imidazolate Framework) membranes [307].

molecules would non-selectively pass through the membrane under convective flow if the kinetic diameter of the molecules is much lower than that of the relatively larger pores (Fig. 10). In contrast, gas molecules are separated depending on the square root ratio for the molecular weight by Knudsen diffusion when the pores of the membranes are much smaller in comparison with gas mean free path (Fig. 10), whereas, large gas molecules are sieved out to separate the gases through the molecular sieving mechanism (Fig. 10), which is the predominant mechanism in H2 separation applying microporous membranes. Conversely, the permeation through dense membranes is based on solution-diffusion mechanism, which comprised sorption of penetrants at the upstream side of the membranes, then diffusion of gaseous penetrants through the membrane followed by desorption at the downstream side of the membranes [294,296]. On the other hand, metallic membranes dissociate the hydrogen molecule into atoms to pass the membrane and the atoms recombine to molecules at the permeate side. Dense ceramic membranes recover H2 by passing electrons and protons (hydrogen ions) through the membrane [297]. The specific productivity of dense ceramic and metallic membranes (such as pure metals, metal alloys, and metallic-ceramic composites) is generally dependent on a higher temperature to achieve a sufficiently high permeation rate compared to other membranes, which in turn, require higher energy expenditure [297].

The hydrogen selectivity and permeability are the key bottlenecks to evaluate the membrane performance for the production and purification of  $H_2$  derived from biomass processing from the technical perspective. There is a trade-off between permeability and selectivity. Higher selectivity yields higher purity of hydrogen, whereas higher permeability leads to better productivity of hydrogen. The selectivity and permeability of  $H_2$  selective membranes can be affected under various operating conditions of pressure, temperature, gas compositions and humidity etc. [298–300]. The hydrogen permeability is the product of diffusivity of  $H_2$  molecules penetrating in the polymer matrix and the solubility of the  $H_2$  molecules into the surface of the membranes. Hydrogen, due

to the smallest molecular size among all the gases, has a higher coefficient of diffusivity and a lower solubility coefficient due to its weak affinity with polymers [271,297].

#### Polymeric membranes

Polymeric membranes are the most advanced development in  $\rm H_2$  separation because these facilitate better permeability at lower material and manufacturing costs, mild operating conditions and easy accessibility, but its applications are limited by low temperatures for operation and relatively low selectivity of hydrogen. To date, polymeric membranes have been applied to separate hydrogen at a commercial scale. Both glassy and rubbery polymers have been used for membrane synthesis. The glassy polymers result in low permeability and higher selectivity with  $\rm H_2$  purity of membrane, whereas rubbery polymers lead to low selectivity with relatively higher permeability [301,302]. The selectivity of polymeric membranes available commercially is summarized in Table 10.

Polymeric membranes for hydrogen separation from biomass processing can be divided into two types; the first one is the hydrogen-selective membranes, which are synthesized with polymers including ethylcellulose, polyetherimide, polyphenylene oxide, polysulfone, polystyrene, polyvinylidene fluoride, and polymethyl methacrylate; the second one is the hydrogen rejecting membranes comprising polymers such as poly trimethylsilyl propane, poly 4-methyl-2-pentyne, polyphosphazene, polyamide-6-b-ethylene oxide, polyethylene glycol diacrylate, crosslinked PEG copolymer, polyether, poly styrene-co-butadiene, polyethylene oxide-poly butylene terephthalate and poly dimethyl siloxane [303]. As shown in Fig. 11, Roberson upper boundary lines reveal the selectivity permeability trade-off limits for the hydrogen and carbon dioxide pair for the polymeric membranes and most membranes prepared from available commercial polymers are still far from the attractive region [304]. However, ZIF (Zeolitic Imidazolate Framework) membrane showed better separation performance of H<sub>2</sub>/CO<sub>2</sub>. Experimental (empty) and predicted intrinsic (solid) performance of ZIF membranes are

demonstrated in the Roberson upper boundary lines in Fig. 11. Recently, polyimide (PI) and polybenzimidazole (PBI) showed promising performance for hydrogen separation, because of better thermal and structural stabilities under harsh operating conditions [80,305]. However, there is still a need to develop new polymers and modify existing polymers to fulfill industrial needs in harsh conditions.

Recently, several strategies; such as polymer blending to form an integrated membrane, chemical crosslinking and mixed matrix membranes (MMMs) using organic polymers and inorganic fillers (zeolites, metal-organic frameworks, etc.); have been applied to achieve simultaneously higher permeability and selectivity [297]. Apart from several opportunities for hydrogen separation and purification using membranes in biomass processing, polymeric membranes have some limitations such as physical aging, plasticization as well as chemical and thermal stability could be a key bottleneck limiting the applications in biomass processing [306].

### Dense metal membranes

Dense metal membranes are prepared form the metals such as nickel, palladium and platinum and their metallic alloys. The higher hydrogen selectivity and production of ultra-pure hydrogen is the prominent advantage of these membranes. This feature is associated with the innate ability of metals and its alloys structure to permit selective diffusion of hydrogen while rejecting other gases [308-310] Therefore, many dense metal membranes have been introduced at commercial scale to provide highly purified hydrogen. However, the permeability of hydrogen is relatively lower than that of other membranes because of the nonporous structure [310]. Among all dense metal membranes, palladium (Pd) based membranes have been extensively studied and were reported to have superior hydrogen solubility on the surface of the Pd at different temperatures, leading to excellent flux in comparison with other metal membranes. However, the high cost of Pd membranes restricted their economic practicality [310]. Various techniques to synthesis dense metal membranes have been used in literature, such as chemical vapor deposition (CVD), electroless plating (ELP) and physical vapor deposition (PVD). Research and industrial interest recently been emphasized to fabricate integrated supported metal membranes as well as a variety of porous substrates, such as glass, alumina and stainless steel, have also been considered [297]. However, the formation of the defect-free supported metal membrane is challenging due to the lack of compatibility between the supports and metal materials, particularly at high temperatures.

Although dense metal membranes provide a promising alternative to achieve high selectivity and purity of hydrogen, there are several issues in practical applications. The hydrogen embrittlement phenomenon and the poisoning of membranes due to chemical contaminants such as carbon monoxide, Sulfur, and hydrocarbons etc. are major limitations of the dense metal membranes particularly Pd membranes [308,310,311]. Among the metal elements, Copper (Cu) is considered to have the ability to resist contaminants poisoning and to suppress the phenomenon of hydrogen embrittlement. In addition, Cu could reduce the cost relative

to the cost of pure Pd membranes [312]. Recently, composite Pd-alloy membranes outperformed the single pure metal membranes and were also found to be suitable when applied in a large scale hydrogen purification plant during long-term operation [309].

## Research development and future direction

In this section, the research gaps, current challenges, and future research direction of biomass processing methods as well as for the separation of hydrogen using membranes are discussed.

## Research and development needs in biomass hydrogen separation using membranes

Membrane technology for the separation and purification of H<sub>2</sub> derived from biomass processing has the potential to improve efficiency, manufacturing flexibility, robustness and reduce costs. The hydrogen separation membranes can produce ultra-high pure hydrogen for fuel cell applications. The practical feasibility required high hydrogen flux with lowpressure drop across the membranes, operation at higher temperature and tolerance to contaminants especially sulfur and carbon monoxide. Moreover, the principle is to improve the H<sub>2</sub> selectivity along with maximizing its diffusivity for hydrogen-selective membranes. Therefore, the development of new materials for hydrogen separation membranes is needed. In addition, more robust membrane fabrication methods are also greatly needed to develop a more permeable and selective membrane with high mechanical strength. Current research works are focusing on the development of hydrogen separation membranes to employ under the operation conditions of biomass processing for hydrogen production to overcome the challenges lacking to practical feasibility such as inability to fabricate defect-free membranes at an industrial scale, catalyst or material failure due to thermal cycling and/or contaminants and the lack of suitable seals to apply under higher pressure.

## Research and development needs in biological and thermochemical conversion technologies

- Pyrolysis processes are mostly focused on bio-oil production. There is a challenge to make the pyrolysis process commercially viable for H<sub>2</sub> production both at the laboratory and pilot-scale; more effort is required especially in the techno-economic analysis to show the cost of H<sub>2</sub> while including the selling revenue of the char and bio-oil.
- Gasification is the most promising method for H<sub>2</sub> production. But it also has some challenges to overcome in relation to the cost of H<sub>2</sub> production as compared to fossil fuel H<sub>2</sub>. There is a need to make more progress in developing a new type of gasification such as solar gasification, water gasification as well as achieving further improvements in process optimization and tar reduction. In addition, more LCA and techno-economic analysis are required with the integration of the power production process.

- Liquefaction is an emerging potential route for hydrogen production, but it is still at an initial stage. Many areas need to be explored, such as the reaction mechanism, thermal and kinetic behaviors, optimization of process parameters, design of reactors and most important economic —analysis.
- The  $H_2$  yield is still very low from the photo and dark fermentation processes and is in the range of 4–8 mol  $H_2$ / mol (biomass) [313]. The production cost is very high per kg  $H_2$  is in the range 3.70–18.72 \$ [314]. In this regard, it is important to work on yield improvement as well as an improved design and operational cost reduction. In the case of commercialization, the production cost is the main obstacle for its scaling-up. Techno-economic and LCA should be made to compare the  $H_2$  production cost with other methods [315].
- Hydrogen production from the photolysis method is a
  promising method but it is still at the laboratory scale due
  to its high cost. There is a big gap for the researcher to
  improve the process upscaling parameters specially the
  use of sunlight efficiently with the integration fuel cell.

## **Conclusions**

This study reviewed the biomass processing and conversion technologies for hydrogen production. Biomass is typically converted to hydrogen via two main routes, either thermochemical or biological. The thermochemical route is credible via combustion, pyrolysis, and liquefaction, catalytic steam reforming of raw gases, gasification, supercritical water gasification, and solar gasification. The merits and demerits, process parameters, types and routes of all processes have been critically discussed in terms of processing and conversion technologies from both research and commercial points of view. Among the thermochemical studies, pyrolysis, gasification, and solar gasification appear to be the most feasible and economically viable methods. Research gaps have also been suggested for solar gasification to improve the efficiency of solar heat and intensity. For the biological routes for hydrogen production from biomass included: covered direct and indirect bio-photolysis, photo fermentation, dark fermentation, and biological water gas shift reaction. Among the processes, photo fermentation and dark fermentation methods seem to be more suitable for hydrogen production, due to their high conversion yield and possible commercial application. Furthermore, the biological water gas shift reaction has also been shown to have economic viability. Direct and indirect photolysis and biological water gas shift reaction are potential areas of interest for efficient and sustainable biohydrogen production. Membrane technology is a promising alternative to conventional technologies for hydrogen production and purification from biomass processing because it has considerable advantages than other ones. First, membrane systems have been well investigated and commercialized. The current available membrane systems in the market could meet the demands of hydrogen separation from biomass-derived gases including CO2, CH4, and CO, etc. Moreover, the cost of the membrane separation is lower in comparison to other separation processes because of the

relative ease in membrane development and the low-cost of the system operation. However, more research efforts are required to develop new industrial membrane materials to maximize the permeability and selectivity as well as to overcome the limitations to meet practical feasibility.

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