

$$P_t = 1092.59 \text{ N}$$

$$\therefore M_t = \frac{P_t d p'}{2}$$

$$M_t = \frac{78666.48 \text{ N} \cdot \text{mm}}{2} = 78.66 \text{ N} \cdot \text{m}$$

$$M_t = \frac{P \times 60}{2 \times N}$$

$$P = 8240 \text{ W} = 8.24 \text{ kW} \quad \underline{\text{Ans}}$$

Ans 6.

$$P_o \text{ angle} = 20^\circ$$

$$\text{Power} = 5 \text{ kW}$$

$$\sigma_v = 410 \text{ MPa}$$

$$v = 5 \text{ m/sec}$$

$$N_p = 720 \text{ rpm}$$

$$N_g = 144 \text{ rpm}$$

$$C_s = 1.25$$

$$f_s = 2.0$$

Assuming no. of teeth on pinion  
of  $Z_p = 18$

Since  $v = 5 \text{ m/s}$  (initial approx.)

$$C_v = \frac{3}{3+v} = \frac{3}{8} = 0.375$$

$$S_b = f_s P_{eff} = f_s \cdot \frac{C_s P_t}{C_v}$$

$$M_t = \frac{P \times G_0}{2 \pi N} = \frac{5 \times 10^3 \times 60 \times 10^3}{2 \times \pi \times 720} = 66348 \text{ N}\cdot\text{mm}$$

$$P_t = \frac{M_t}{d r / 2} = \frac{66348}{3 (18/2)} = \frac{7372}{\text{m}} \text{ N}$$

$$\sigma_{b y.m} = \frac{f_s C_s P_t}{C_0}$$

assuming  $b = 10 \text{ m}$  &  $y = 0.308$   
(for  $2P = 18$ )

further material is same surface finish is designed

$$\sigma_b = \frac{\sigma_u}{3} = \frac{410}{3} = 136.6 \text{ MPa}$$

Putting all the values

$$136.6 \times 10 \text{ m} \times 0.308 \times \text{m}$$

$$= (2.0) \times \left( \frac{1.25}{0.375} \right) \times \left( \frac{7372}{\text{m}} \right)$$

$$m = 4.88 \text{ mm} \sim 5 \text{ mm} \text{ Ans}$$

$$\text{So, } d_{p1} = m z_p = 90 \text{ mm}$$

$$d_g = m z_g = 5 \times 90 = 450 \text{ mm}$$

$$P_t = \frac{7372}{\text{m}} = 1474.4 \text{ N}$$

Now we need to find dynamic load  
We know for grade 6  
 $e = 8 + 0.63 \phi$



for pinion.  $\phi = m + 0.25 \sqrt{d_p}$

$$= 5 + 0.25 \sqrt{90}$$

$$= 8 + 0.63 \phi = 12.644 \text{ mm}$$

and  $e_g = 14.491$

$$e = e_p + e_g = 27.135 \text{ mm}$$

$$= 27.135 \times 10^{-3} \text{ mm}$$

Now we need to find dynamic load

$$P_d = \frac{210 (e_b + P_t)}{210 + \sqrt{e_b + P_t}}$$

We know for grade 6

$$e = 8 + 0.63 \phi$$

for pinion  $\phi = m + 0.25 \sqrt{d_p}$   
 $5 + 0.25 \sqrt{90}$

$$e_p = 8 + 0.63 \phi = 12.644$$

$$e_g = 4.421 \text{ mm}$$

$$e = e_p + e_g = 27.13 \text{ mm}$$

$$= 27.135 \times 10^{-3} \text{ mm}$$

The deformation factor  $c = 11400 \text{ MPa}$

$$W = \frac{\pi d_p' N_P}{6000} = \frac{\pi \times 90 \times 720}{6000}$$

$$W = 3.39 \text{ m/s}$$

$$\text{Now } P_d = \frac{210 (C_{eb} + P_t)}{210 + \sqrt{C_{eb} + P_t}}$$

putting all values

$$P_d = 5993 \text{ N } \underline{\text{Ans}}$$

so effective load,  $P_{eff} = C_s P_t + P_d$

$$= (1.25 \times 1474.4) + 5993$$

$$= 7836 \text{ N}$$

Beam strength

$$S_b = m \cdot b \cdot \sigma_b \cdot y$$

$$= 5 \times 50 \times \left(\frac{410}{3}\right) \times 0.308$$

$$= 10523.33 \text{ N}$$

Corrected factor of safety

$$S_b = f_s P_{eff}$$

or  $f_s = \frac{S_b}{P_{eff}} = \frac{10523.33}{7836} = 1.34$

Surface hardness

Given  $f_s = 2.0$  for wear strength  
so  $S_w = f_s P_{eff}$

$$\text{so } S_w = 2 \times 7836 = 15672 \text{ N}$$

$$S_w = d p^1 b \cdot Q \cdot K$$



Q4  $15672 = 90 \times 50 \times 1.66 \times K$

$$K = 2.097$$

We know for 20° fr. angle steel gears

$$K = 0.16 \times \left( \frac{\text{BHN}}{100} \right)^2$$

$$\therefore \text{BHN} = \sqrt{\frac{K \times 100 \times 100}{0.16}}$$

$$= 360 \text{ Ans}$$