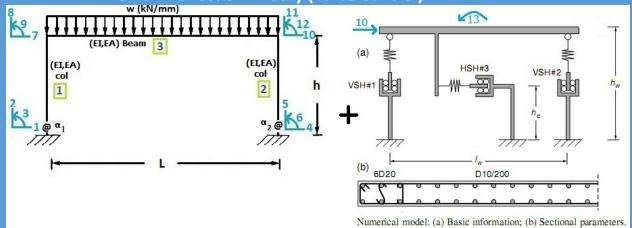
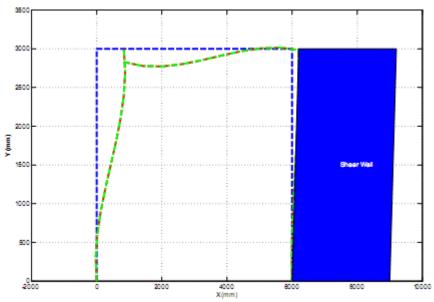


Pushover 1st and 2nd order Analysis Interaction of Concrete Shear wall with Steel Frame Nonlinear Semi Rigid Conection Frame subjected to lateral load Small Deflection Theory (Force Control) in MATLAB



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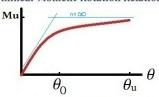


Figure(1) Deformed shape model in MATLAB

Semi-Rigid Connection Number 1

Elastic Perfect Plastic

Nonlinear Moment-Rotation Relation



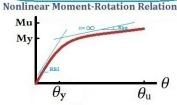
$$\mathsf{M}(\theta) = \frac{R_{ki}\theta}{\left(1 + \left(\left|\frac{R_{ki}\theta}{M_u}\right|\right)^n\right)^{\frac{1}{n}}} \quad \therefore \ R_{ki} = \frac{M_u}{\theta_0} \qquad \quad \mathsf{M}(\theta) \ = \frac{(R_{ki} - R_{kp})\theta}{(1 + \left(\left|\frac{R_{ki}\theta}{M_y}\right|\right)^n)^{\frac{1}{n}}} + R_{kp}\theta \quad \therefore \ R_{ki} = \frac{M_y}{\theta_y} \quad \therefore \ R_{kp} \ = \frac{M_u - M_y}{\theta_u - \theta_y}$$

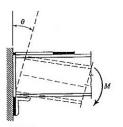
Nonlinear stiffness-Rotation Relation

$$\mathbf{K}(\theta) = \frac{R_{ki}}{\left(1 + \left(\left|\frac{R_{ki}\theta}{M_{ti}}\right|\right)^{n}\right)^{\frac{1}{n}}}$$

Semi-Rigid Connection Number 2

Elasto-plastic with hardening





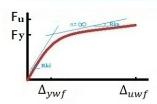
$$\mathbf{M}(\theta) = \frac{\frac{(R_{ki} - R_{kp})\theta}{(1 + (\left|\frac{R_{ki}\theta}{M_{m}}\right|)^{n})^{\frac{1}{n}}} + R_{kp}\theta$$

$$\therefore R_{ki} = \frac{My}{\theta y} \quad \therefore R_{kp} = \frac{M_u - M_y}{\theta_u - \theta_y}$$

Nonlinear stiffness-Rotation Relation

$$K(\theta) = \frac{(R_{ki} - R_{kp})}{(1 + (\left|\frac{R_{ki}\theta}{M_y}\right|)^n)^{\frac{1}{n}}} + R_{kp}$$

Flexural Behavior of spring - shear wall

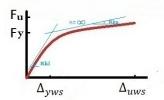


$$\mathsf{F}(\theta) = \frac{\frac{(R_{ki} - R_{kp})\Delta}{(1 + (\left|\frac{R_{ki}\Delta}{\mathsf{Fy}}\right|)^n)^{\frac{1}{n}}} + R_{kp}\Delta$$

Nonlinear siffness-Displacement

$$K^{f}(\theta) = \frac{(R_{ki} - R_{kp})}{(1 + (\left|\frac{R_{ki}\Delta}{F_{y}}\right|)^{n})^{\frac{1}{n}}} + R_{kp}$$

Shear Behavior of spring - shear wall



$$\mathbf{K} = \begin{bmatrix} K^s & -K^s(h_w - h_c) \\ -K^s(h_w - h_c) & K^s(h_w - h_c)^2 + K^t \frac{l_w^2}{2} \end{bmatrix} \leftarrow \mathbf{0}$$

Global stiffness matrices of shear wall

$$F(\theta) = \frac{(R_{ki} - R_{kp}) \Delta}{(1 + (\left|\frac{R_{ki}\Delta}{F_{\mathbf{v}}}\right|)^n)^{\frac{1}{n}}} + R_{kp} \Delta$$

Nonlinear siffness-Displacement

$$K(\theta) = \frac{(R_{ki} - R_{kp})}{(1 + (\left|\frac{R_{ki}\Delta}{F_{y}}\right|)^{n})^{\frac{1}{n}}} + R_{kp}$$

Figure(2) Nonlinear behavior of columns connection and concrete shear wall

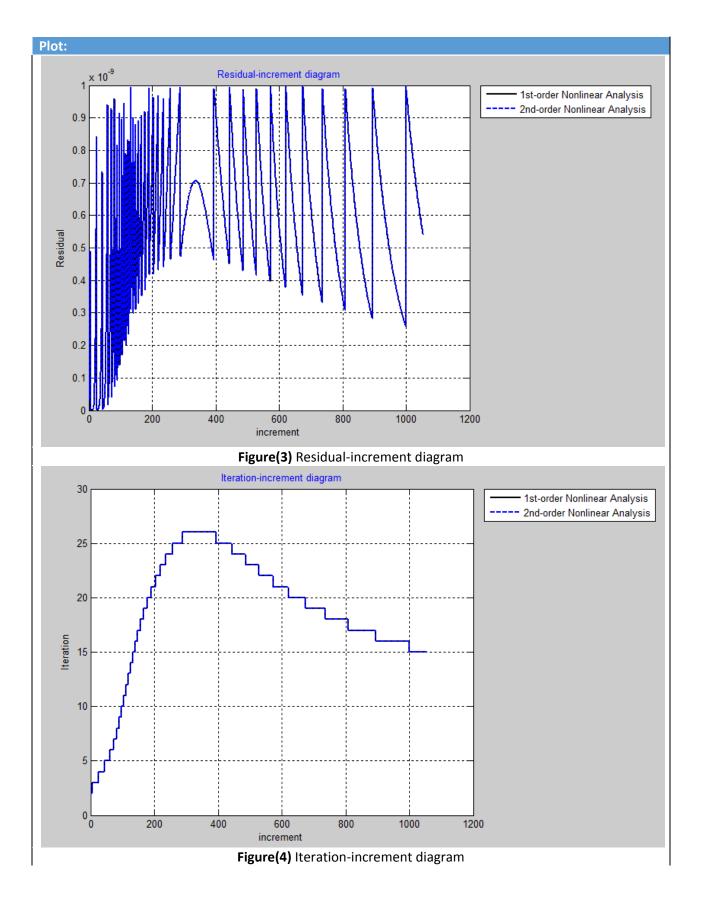
Define Parameters:

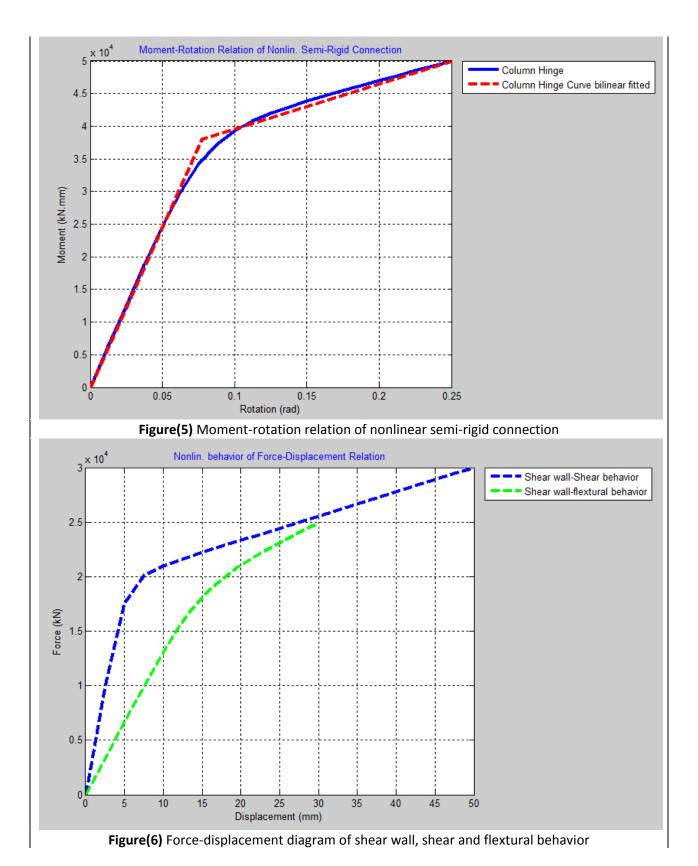
% Define Parameters in mm,kN W=.005; % [kN/mm] % Distributed load Value (+ : Down) h= 3000; % [mm] % column length L = 6000; % [mm] % beam lengthbw = 3000; % [mm] width of shear wall Lw = 3000; % [mm] Length of shear wall Ew = 200; % [kN/mm^2] modulus of elasticity of shear wall $EIc = 200*100^4/12; % [kN.mm^2] column$ EAc = 200*10000; % [kN] $EIb = 200*50^4/12; % [kN.mm^2] beam$ $EAb = 200*(50)^2; % [kN]$ m = 2000; % number of calculation (Load Steps) itermax = 400;% maximum number of iterations tolerance = 1e-9; % specified tolerance for convergence u = zeros(9,1);% initial guess value P3 =0; % [kN.mm] Moment [DOF (3)] P6 =0; % [kN.mm] Moment [DOF (6)] P7=50; % [kN] Horizental Force [DOF (7)] Incremantal Loading P8=-.5*W*L; % [kN] Vertical Force [DOF (8)]

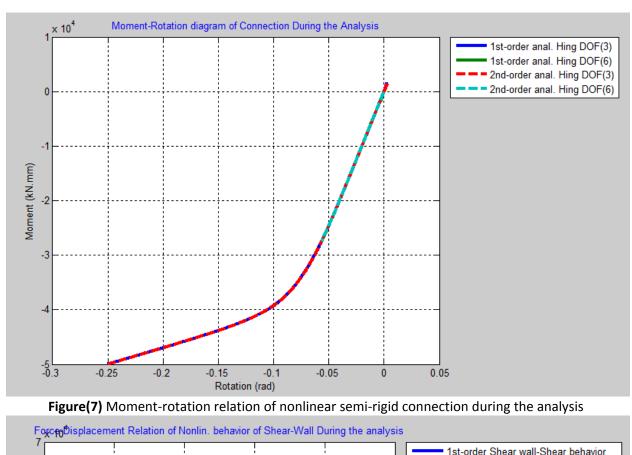
```
P9 = -(W*L^2)/12; % [kN.mm] Moment [DOF (9)]
P10=0; % [kN] Horizental Force [DOF (10)]
P11=-.5*W*L; % [kN] Vertical Force [DOF (11)]
P12=+(W*L^2)/12; % [kN.mm] Moment [DOF (12)]
lanXc=0;lanYc=1;
lanXb=1;lanYb=0;
%% Nonlinear Rotational Spring of columns
tyc=.08; % Yield rotaion
Myc=40e+3; % Yield moment
tuc=.25; % Ultimate rotation
Muc=1.25*Myc; % Ultimate moment
nc = 5; % Moment-rotation shape parameter
Rkic=Myc/tyc;
Rkpc=(Muc-Myc)/(tuc-tyc);
%% Nonlinear Displacement Spring of Shear Wall - Flexural Behavior
hw=h; Iw=bw*(Lw^3)/12; As=(2*Iw)/Lw^2; aw=(2*Iw)/(bw*Lw^3);
dywf=15; % Yield displacement
Fywf=20e+3; % Yield Shear Force
duwf=30; % Ultimate displacement
Fuwf=25e+3; % Ultimate Shear Force
nwf = 5; % Shear Force-displacement shape parameter
Rkiwf=Fywf/dywf;
Rkpwf=(Fuwf-Fywf)/(duwf-dywf);
%% Nonlinear Displacement Spring of Shear Wall - Shear Behavior
hc = hw/3; % [mm]
dyws=5; % Yield displacement
Fyws=20e+3; % Yield Shear Force
duws=50; % Ultimate displacement
Fuws=30e+3; % Ultimate Shear Force
nws = 5; % Shear Force-displacement shape parameter
Rkiws=Fyws/dyws;
Rkpws=(Fuws-Fyws)/(duws-dyws);
Analysis Report:
First-order Nonlinear Analysis
(+)It is converged in 2 iterations for increment 1
(+)It is converged in 2 iterations for increment 2
(+)It is converged in 2 iterations for increment 3
(+)It is converged in 2 iterations for increment 4
(+)It is converged in 3 iterations for increment 5
(+)It is converged in 3 iterations for increment 6
(+)It is converged in 3 iterations for increment 7
(+)It is converged in 3 iterations for increment 8
(+)It is converged in 3 iterations for increment 9
(+)It is converged in 3 iterations for increment 10
(+)It is converged in 15 iterations for increment 1045
(+)It is converged in 15 iterations for increment 1046
(+)It is converged in 15 iterations for increment 1047
(+)It is converged in 15 iterations for increment 1048
(+)It is converged in 15 iterations for increment 1049
(+)It is converged in 15 iterations for increment 1050
(+)It is converged in 15 iterations for increment 1051
(+)It is converged in 15 iterations for increment 1052
(+)It is converged in 15 iterations for increment 1053
(+)It is converged in 15 iterations for increment 1054
```

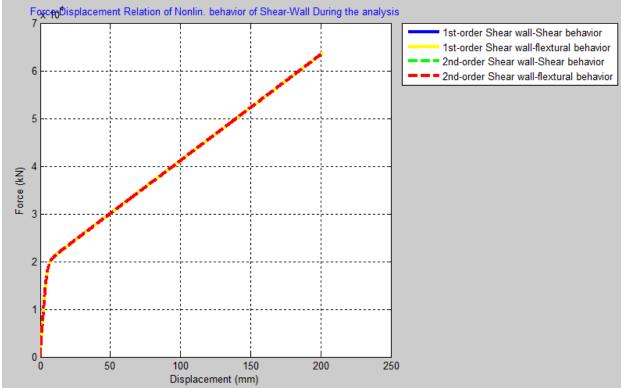
spring at support reached to Ultimate Rotation

```
Second-order Nonlinear Analysis
(+)It is converged in 2 iterations for increment 1
(+)It is converged in 2 iterations for increment 2
(+)It is converged in 2 iterations for increment 3
(+)It is converged in 2 iterations for increment 4
(+)It is converged in 3 iterations for increment 5
(+)It is converged in 3 iterations for increment 6
(+)It is converged in 3 iterations for increment 7
(+)It is converged in 3 iterations for increment 8
(+)It is converged in 3 iterations for increment 9
(+)It is converged in 3 iterations for increment 10
(+)It is converged in 15 iterations for increment 1045
(+)It is converged in 15 iterations for increment 1046
(+)It is converged in 15 iterations for increment 1047
(+)It is converged in 15 iterations for increment 1048
(+)It is converged in 15 iterations for increment 1049
(+)It is converged in 15 iterations for increment 1050
(+)It is converged in 15 iterations for increment 1051
(+)It is converged in 15 iterations for increment 1052
(+)It is converged in 15 iterations for increment 1053
(+)It is converged in 15 iterations for increment 1054
  ## spring at support reached to Ultimate Rotation ##
=== 1st-order Nonlinear ==+== 2nd-order Nonlinear =====
Disp.(D7) Base Shear(D1+D4) Disp.(D7) Base Shear(D1+D4)
______
(mm)
         (kN) (mm) (kN)
1.0e+004 *
         0 0
 0.0483 3.3045 0.0483 3.3046
 0.0834 5.2700 0.0834 5.2700
Semi-Rigid Column Connection Ductility Rito is: 3.235
1st-order Nonlinear Ductility Rito is (Du/Dy): 1.727
2nd-order Nonlinear Ductility Rito is (Du/Dy): 1.727
1st-order Nonlinear Over Strength Ratio is (Fu/Fy): 1.595
2nd-order Nonlinear Over Strength Ratio is (Fu/Fy): 1.595
1st-order Nonlinear Initial Strucural stiffness is (Ke): 68.418 [kN/mm]
1st-order Nonlinear Tangent Strucural stiffness is (Kt): 55.986 [kN/mm]
2nd-order Nonlinear Initial Strucural stiffness is (Ke): 68.412 [kN/mm]
2nd-order Nonlinear Tangent Strucural stiffness is (Kt): 55.980 [kN/mm]
```









Figure(8) Force-displacement diagram of shear wall, shear and flextural behavior during the analysis

