Control Systems

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Abstract—This manual is an introduction to control systems based on GATE problems.Links to sample Python codes are available in the text.

Download python codes using

svn co https://github.com/gadepall/school/trunk/ control/codes

2.1.2. part(a): We have to find the expressions for G(open loop gain) , H(the feedback factor) and hence the amount of feedback.

^{1.1.} We are given with a feedback voltage amplifier shown in 2.1.1. We can neglect r_o and given with $R_1 + R_2 >> R_D$. V_i

Fig. 2.1.1

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Solution: For this , first we have to draw the Small-Signal Model for the above Circuit, we ground all constant voltage sources and open all constant current sources. All Small-Signal paramters are obtained from DC-Analysis of the circuit.In Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{gs}$ flowing from Drain to Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{sg}$ flowing from Source to Drain.

$$H = \frac{V_f}{V_o}$$
 (2.1.5.1)

$$V_f = \frac{R_1}{R_1 + R_2} V_o (2.1.5.2)$$

$$H = \frac{R_1}{R_1 + R_2} \tag{2.1.5.3}$$

Amount of feedback is defined as : 1 + GH

$$1 + GH = 1 + \frac{g_m R_D R_1}{R_1 + R_2}$$
 (2.1.5.4)

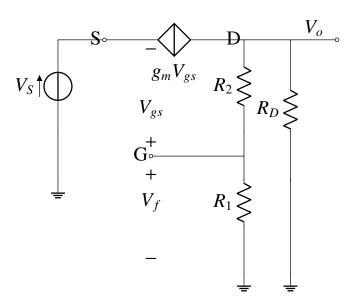


Fig. 2.1.2: Small Signal Model

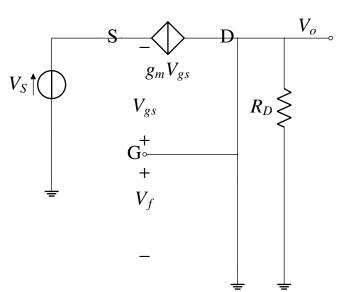


Fig. 2.1.5: CG amplifier

2.1.3. For finding open loop gain (G) and the feedback factor (H).

Solution: For finding the open loop gain we have to remove R_2 and R_1 and the gate should be grounded.

2.1.4. Finding the open loop gain(G)

Solution:

$$V_o = -g_m V_{gs} * R_D (2.1.4.1)$$

$$V_{gs} = -V_S {(2.1.4.2)}$$

$$G = \frac{V_o}{V_s}$$
 (2.1.4.3)

$$G = g_m R_D \tag{2.1.4.4}$$

2.1.5. Finding the Expression for the feedback factor *H*.

Solution:

2.1.6. Part(b): We have to eliminate the feedback by removing R_1 and R_2 and connecting the gate of Q to a constant DC voltage (signal ground). We have to find the expression of the input resistance R_i and the output resistance R_o of the open loop amplifier.

Solution:

When the R_1 and R_2 and gate of Q is connected to a constant DC voltage (signal ground) it becomes a CG(Common gate amplifier) without feedback. We can directly see from the 2.1.5 the expression of input resistance R_i and output resistance R_o .

For finding input resistance, output constant voltages are grounded and hence the only current flowing is $g_m V_{gs}$. Hence R_i is:

$$I_{in} = -g_m V_{gs} (2.1.6.1)$$

$$V_{in} = V_S$$
 (2.1.6.2)

$$V_S = -V_{gs} (2.1.6.3)$$

$$R_i = \frac{V_{in}}{I_{in}} {(2.1.6.4)}$$

$$R_i = \frac{1}{g_m} \tag{2.1.6.5}$$

Similarly, for finding output R_o , V_{in} that is V_S will be zero and hence $g_m V_{gs}$ will be zero. Hence only R_D will be left which is the output resistance.

$$R_o = R_D$$
 (2.1.6.6)

2.1.7. Part(c): Using standard circuit analysis that is without using feedback approach we have to find the input resistance R_{if} and output resistance R_{of} and how they relate to R_i and R_o , which we find earlier.

Solution:

We will find them one by one.

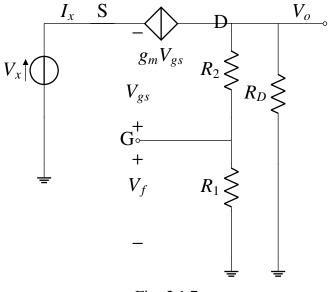


Fig. 2.1.7

2.1.8. finding expression for R_{if}

Solution:

To obtain R_{if} consider the figure 2.1.7: We gave test input voltage V_x and current I_x to find the input resistance from the input side to find R_i .

$$R_{if} = \frac{V_x}{I_x}$$
 (2.1.8.1)

$$I_x = -g_m V_{gs} (2.1.8.2)$$

$$V_o = I_x R_D (2.1.8.3)$$

$$V_f = \frac{V_o R_1}{R_1 + R_2} = \frac{I_x R_D R_1}{R_1 + R_2}$$
 (2.1.8.4)

$$V_x = -V_{gs} + V_f (2.1.8.5)$$

$$V_x = \frac{I_x}{g_{yy}} + \frac{I_x R_D R_1}{R_1 + R_2}$$
 (2.1.8.6)

$$\frac{V_x}{I_x} = \frac{1}{g_m} + \frac{R_D R_1}{R_1 + R_2} \tag{2.1.8.7}$$

$$rearranging:$$
 (2.1.8.8)

$$R_{if} = \frac{1}{g_m} (1 + \frac{g_m R_D R_1}{R_1 + R_2})$$
 (2.1.8.9)

$$R_{if} = R_i(1 + GH)$$
 (2.1.8.10)

The input impedance is increased by a factor of (1 + GH). R_{if} is related to R_i by :

$$R_{if} = R_i(1 + GH) (2.1.8.11)$$

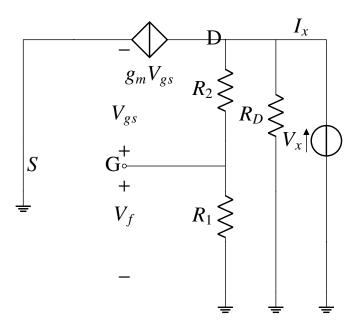


Fig. 2.1.8

2.1.9. finding expression for R_{of}

Solution:

To obtain R_{of} consider the figure 2.1.8 : We gave test input voltage V_x and current

 I_x from the output side to find the output resistance and made the input constant voltages as zero.

$$R_{of} = \frac{V_x}{I_x} \qquad (2.1.9.1)$$

$$I_x = g_m V_{gs} (\frac{V_x}{R_1 + R_2}) + (\frac{V_x}{R_D}) \qquad (2.1.9.2)$$

$$V_{gs} = \frac{R_1 V_x}{R_1 + R_2} \qquad (2.1.9.3)$$

$$I_x = \frac{g_m R_1 V_x}{R_1 + R_2} + \frac{V_x}{R_1 + R_2} + (\frac{V_x}{R_D})$$
 (2.1.9.4)

$$I_x = V_x(\frac{g_m R_1 + 1}{R_1 + R_2} + \frac{1}{R_D})$$
 (2.1.9.5)

$$R_{of} = \frac{V_x}{I_x}$$
 (2.1.9.6)

$$R_{of} = \frac{1}{\frac{g_m R_1 + 1}{R_1 + R_2} + \frac{1}{R_D}}$$
 (2.1.9.7)

rearranging and multiply both the numerator and denominator by R_D

$$R_{of} = \frac{R_D}{\frac{g_m R_1 R_D}{R_1 + R_2} + 1 + \frac{R_D}{R_1 + R_2}}$$
(2.1.9.8)

since
$$R_1 + R_2 \gg R_D \implies \frac{R_D}{R_1 + R_2} = 0$$

$$R_{of} = \frac{R_D}{1 + \frac{g_m R_1 R_D}{R_1 + R_2}}$$
 (2.1.9.9)

$$R_{of} = \frac{R_o}{1 + GH} \tag{2.1.9.10}$$

The output impedance is decreased by a factor of (1 + GH). R_{of} is related to R_o by :

$$R_{of} = \frac{R_o}{1 + GH} \tag{2.1.9.11}$$

The table showing all the expressions we find out in this problem :

G	$g_m R_D$
Н	R_1
11	$\overline{R_1 + R_2}$
_	1
R_i	_
	g_m
R_o	R_D
D	$1 g_m R_D R_1$
R_{if}	$(\frac{1}{g_m})(1 + \frac{g_m R_D R_1}{R_1 + R_2})$
	R_D
R_{of}	
	$1 + \frac{g_m R_D R_1}{R_1 + R_2}$
	$1+\frac{1}{R_1+R_2}$
	$1 \qquad N_1 + N_2$

TABLE 2.1.9

- 3 Bode Plot
- 4 SECOND ORDER SYSTEM
- 5 ROUTH HURWITZ CRITERION
 - 6 STATE-SPACE MODEL
 - 7 Nyquist Plot
 - 8 Compensators
 - 9 Gain Margin
 - 10 Phase Margin
 - 11 OSCILLATOR
 - 12 Root Locus
 - 13 Polar Plot
 - 14 PID Controller