## Coupled Oscillators

These notes don't cover the basics of simple hormonic motion.
If you need a recap, book at Freegorde's Section 5 notes.

#### Time Translational hydriance.

Time translation invariance causes us to use complex exponential time dependence in our trial solutions. Spatial translation invariance gives complex exponential time dependence in our trial solutions as well.

consider a simple damped harmonic oscillator with ear of motion:

$$M\ddot{x} = -2M\ddot{x}\dot{x} - MW_0^2\dot{x}$$
 we rearrange this to:

x + 2 x x + wo x = 0

To some thise, use ansatz x = Ae

where I and it are in general complex. We can take real parts later when looking for physical solution.

The reason we can take this areat & is time translational invarious:

if x(t) is a solution than x(t+c) is a solution for any constant c

The simplest possibility is x(t+c) = f(c)x(t) for some proportionality context f(c)

We can some this. Tom the page.

 $x(t+c) = f(c) x(t) \qquad \text{differentiate w.r.t. } c$   $\dot{x}(t+c) = \dot{f}(c) x(t) \qquad \text{set } c=0$   $\dot{x}(t) = \Lambda x(t) \qquad \text{where } \Lambda = \dot{f}(0)$ 

This has known solution X(t) = Aert which is where our ansatz earlier comes from.

I must have a non-zero imaginary port it we want to get oscillatory solutions:

From now on, we will say  $\Omega = i\omega$  so  $x(t) = Ae^{i\omega t}$ 

we can't just choose any value for us, it is determined by democify Ae'ust somes eqn. of motion:

 $(-\omega^2 + 2i\gamma\omega + \omega_0^2)$  A  $e^{i\omega t} = 0$ For non-trivial solutions,  $A \neq 0$  so we require  $-\omega^2 + 2i\gamma\omega + \omega_0^2 = 0$ solve this for values of  $\omega$ 

#### Normal Modes

we are trying to generalise from a single oscillator to a set of compled oscillators.

For a oscillators with individual position x:(t), we denote "position" of whole system with vector x(t):

The differential egas satistical by x; win involve time dependence only as time derivatives so we will be able to use the time translational invariance described previously.

So all the oscillators have some complex exp. thre dependence eint so:  $\underline{x}(t) = \begin{pmatrix} A_1 \\ A_2 \end{pmatrix} e^{i\omega t} \quad A_i \text{ are constants}$ 

which destibes situation where an oxidators have some prequency but in general different amplitudes and phases.

The estillator displacements are in fixed ration determined by A:

This kind of motion is called a normal mode.

The overall normalisation is arbitrary, i.e multiplying all Ai by the same constant still gives the same normal mode.

Our job is to determine which we are allowed and that determine a set of A: for allowed w.

For a oscillators obeying and order complet equations, there are an independent solutions.

## Coupled Oscillators

consider a set of coupled oscillators described by coordinates

q....q. ... The potential v(q) win be complicated. Consider

small oscillations about a position of stable equilibrium,

which, we can take to occur when q:=0

Expanding the potential it a taylor series about this point:

$$V(4) = V(0) + \sum_{i=0}^{\infty} \frac{\partial f_{i}}{\partial f_{i}} \Big|_{0} d_{i} + \frac{1}{2} \sum_{i=0}^{\infty} \frac{\partial^{2} V}{\partial f_{i}} \partial_{i} d_{i} \Big|_{0} d_{i} d_{i} + \cdots$$

we add a contact to V so we can choose V(0) = 0. Since we are at a position of equilibrium, all first derivative terms value.

we can also drop all nigher derivatives, since they will be very small.

Thus the equations of motion are:

$$M_i \stackrel{\circ}{Q}_i = - \stackrel{r}{\sum} \kappa_{ij} \, Q_j$$

For i = 1 ... N

the Mi one the masses of the oscillators and K is a matrix of spring constants.

$$\underline{M} = \begin{bmatrix} M_1 & 0 & \dots & 0 \\ 0 & M_2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & M_2 \end{bmatrix} \qquad \underline{K} = \begin{bmatrix} K_{11} & K_{12} & \dots & K_{1A} \\ K_{21} & K_{22} & \dots & K_{2A} \\ \vdots & \vdots & \ddots & \vdots \\ K_{A1} & K_{A2} & \dots & K_{An} \end{bmatrix}$$

Likewise q and q are colon vectors

with this notation:  $M\ddot{q} = -Kq$  or:  $\dot{q}' = -M'Kq$ 

Now we look for a normal solution  $q = Ae^{i\omega t}$  whe A is a column vector we have:  $q = -\omega^2 q$ , so concelling  $e^{i\omega t}$  factors gives:

$$M^{-1}KA = \omega^2 A$$
 this is the eigenvalue expection  $\omega^2$  values are eigenvalues of  $M^{-1}K$  and A is eigenvectors.

# Example: Masses and Springs

coulder the system shown above. The two masses are joined by a spring with spring contact K', and joined to the walls by springs of spring contacts K, and K2

The equilibrium position has each spring unstructured use displacements  $\infty$ , and  $\infty$  of the masses from their equilibrium position as coordinates.

force or made M:

$$F_1 = -K_1 x_1 - K'(x_1 - x_2)$$

Force on mass M2:

$$f_2 = -\kappa_2 x_2 - \kappa'(x_2 - x_1)$$

combining these and putting into matrix form:

$$\begin{pmatrix} 0 & M_1 \end{pmatrix} \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = -\begin{pmatrix} \kappa_1 + \kappa_1 \\ -\kappa_1 \end{pmatrix} \begin{pmatrix} \kappa_2 \\ \kappa_2 \end{pmatrix}$$

which is in the form  $M^{\frac{2}{4}} = -K^{\frac{4}{4}}$  as we saw on previous page. The eigenvalue equation:

so our eigenvalue equation is

$$\begin{pmatrix} \frac{C_1 + K'}{M_1} & -\frac{K'}{M_1} \\ -\frac{K'}{M_2} & \frac{C_2 + K'}{M_2} \end{pmatrix} \begin{pmatrix} A_1 \\ A_2 \end{pmatrix} = \omega^2 \begin{pmatrix} A_1 \\ A_2 \end{pmatrix}$$

we can consider the special case:  $N_1 = M$   $M_2 = 2M$  K' = 2K  $K_1 = K$   $K_2 = 2K$ 

The elgenvalue equation becomes:

$$\begin{pmatrix} 3k/M & -2k/M \\ -k/M & 2k/M \end{pmatrix} \begin{pmatrix} A_1 \\ A_2 \end{pmatrix} = \omega^2 \begin{pmatrix} A_1 \\ A_2 \end{pmatrix}$$

$$= (3 - 2) / A_1 \rangle \qquad M = 2 / A_1 \rangle$$

$$\Rightarrow \begin{pmatrix} 3 - 2 \\ -1 2 \end{pmatrix} \begin{pmatrix} A_1 \\ A_L \end{pmatrix} = \frac{M}{K} \omega^2 \begin{pmatrix} A_1 \\ A_2 \end{pmatrix} \quad \text{letting} \quad \lambda = \frac{M \omega^2}{K}$$

$$\begin{pmatrix} 3 - \lambda & -2 - \lambda \\ -1 - \lambda & 2 - \lambda \end{pmatrix} \begin{pmatrix} A_1 \\ A_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

for there to be a solution:

$$\det \begin{vmatrix} 3-\lambda & -2-\lambda \\ -1-\lambda & 2-\lambda \end{vmatrix} = 0$$

$$y_5 - 8y + h = 0 \Rightarrow y = h' y = 1$$

These are the eigenvalues

so the eigentrequencies one:

$$\lambda = 1$$
:  $\frac{M\omega^2}{1L} = 1$   $\omega = \sqrt{\frac{K}{M}}$ 

Eigenvalues & ore:

$$n = 4$$
: you find  $A_2 = -\frac{1}{2}A_1$  so  $A = \frac{1}{\sqrt{5}!} \binom{2}{-1}$  so we have found  $A_2 = 1$ : you find  $A_2 = A_1$  so  $A_3 = \frac{1}{\sqrt{2}!} \binom{2}{1}$  our number modes

in the second one  $(\lambda=1)$ , the two mouses swiny in phase and have some amplitude, and the middle spring remains unswetched. In the first one  $(\lambda=4)$ , the two masses more out of phase with each other (-amplitude) and one has twice the amplitude of the other.

### Weak Coupling and Beats

Now consider the case  $M_1=M_2=M$  and  $K_1=K_2=K$ Note  $K \neq K'$  recessorily in this case.

From the symmetry of the setup we expect one made where the masses suits in phase with some amplitude and sentral spring is unstretched.

we also expect a second mode when the springs are out of phase but oscillations have some apoplitude.
This one has higher frequency.

If the connecting spring has spring contact k' = EK then:

$$\omega_{1} = \sqrt{\frac{1}{M}}$$

$$\Delta_{1} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\omega_{2} = \sqrt{\frac{1}{1+2\ell}} \begin{pmatrix} 1 \\ M \end{pmatrix}$$

$$\Delta_{1} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\Delta_{2} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$
or previous page.

when middle spring is very weak exc1, the two modes have almost some frequency. In this case, we observe bests when a motion contains components from both normal modes.

Suppose we hold M, at equilibrium position and more

Me a distance of and release; the governd solution for

motion is:

 $\underline{\mathcal{I}}(t) = C_1 \underline{A}_1 \cos(\omega_1 t) + C_2 \underline{A}_2 \cos(\omega_2 t) + C_3 \underline{A}_1 \sin(\omega_1 t) + C_4 \underline{C}_2 \sin(\omega_2 t)$ Since we start from rest, we see  $C_3 = C_4 = 0$ 

Applying instinal condition  $\Sigma(0) = \begin{pmatrix} d \\ 0 \end{pmatrix}$ :

which is solved by  $C_1 = C_2 = \frac{d}{\sqrt{2}}$  so the notion is:

$$x_i(t) = \frac{d}{2} \left( (a(w_i t) + (a(w_i t)) \right)$$

$$x_{2}(t) = \frac{d}{2} \left( (a(\omega_{1}t) - (a(\omega_{2}t)) \right)$$

which we rewrite as :

$$\alpha_i(t) = d\cos\left(\frac{\omega_2 - \omega_i}{2} t\right) \cos\left(\frac{\omega_i + \omega_2}{2} t\right)$$

$$\pi_2(t) = d\sin\left(\frac{\omega_2 - \omega_1}{2} t\right) \sin\left(\frac{\omega_1 + \omega_2}{2} t\right)$$

of the difference trappercy  $\frac{\omega_1 - \omega_1}{2}$ 

These produce the beats we borned all about less semester.