ASSIGNMENT 1 EE330A 2020

GROUP.NO - 11

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Introduction

In the following project, our team solved the power flow problem using both MATLAB and Power world software. We computed the power flow solution using the Gauss-Seidel method in both the software. We verified our solution using both the software and find that they match very closely .

Problem Statement

Use the following data to solve the power flow problem using Gauss-Seidel method. Take bus 1 as the slack bus and base MVA as 100.

Build the system with the following data in Power World software. Present the power flow result from Power World software, using Gauss-Seidel method. How does it compare with the computed power flow solution?

What is the real power loss in the system? Can you reduce the real power loss by at least 5 MW by rescheduling the real power outputs of the generators? Verify your solution with the software, and show the results.

DATA FOR 5 BUS SYSTEM

Number	Nom (kV)	PU (Volt)	Angle (Deg)	Load (MW)	Load (Mvar)	Gen (MW)	Gen (Mvar)	B-Shunt (Mvar)
1	15	1	0	0	0	394.8	114.18	0
2	345	1	0	800	280	0	0	0
3	345	1.05	0	80	40	920	337.35	0
4	345	1	0	0	0	0	0	0
5	345	1	0	0	0	0	0	0

LINE DATA

From Number	To Number	Branch Device Type	R	Х	В
5	1	Transformer	0.0015	0.02	0
4	2	Line	0.009	0.1	1.72
5	2	Line	0.0045	0.05	0.88
3	4	Transformer	0.00075	0.01	0
5	4	Line	0.00225	0.025	0.44

Results

Power Flow Solution for part (a)

MATLAB Solution

Gauss Seidel Load-Flow Study Report of Power Flow Calculations

25-Nov-2020

Number of iterations : 75
Total real power losses : 42.5934.
Total reactive power losses: 225.534.

			Ger	neration		Load
Bus	Volts	Angle	Real	Reactive	Real	Reactive
1.0000	1.0000	0	2.5953	151.1791	0	0
2.0000	0.8233	-16.3606	0	0	800.0000	280.0000
3.0000	1.0500	11.3428	919.9985	394.3550	80.0000	40.0000
4.0000	1.0132	6.9578	0	0	0	0
5.0000	0.9697	0.1033	0	0	0	0
		Line Flow	vs.			
#Line	From Bus	To Bus	Real	Reactive		
1.0000	5.0000	1.0000	-2.2524	-146.6068		
2.0000	4.0000	2.0000	350.8089	140.7150		
3.0000	5.0000	2.0000	480.0963	264.8954		
4.0000	3.0000	4.0000	839.9985	354.3550		
5.0000	5.0000	4.0000	-477.8439	-118.2886		
1.0000	1.0000	5.0000	2.5953	151.1791		
2.0000	2.0000	4.0000	-335.4225	-116.3343		
3.0000	2.0000	5.0000	-464.5777	-163.6656		
4.0000	4.0000	3.0000	-834.3443	-278.9659		
5.0000	4.0000	5.0000	483.5351	138.2509		

real power in MW and reactive power in MVar

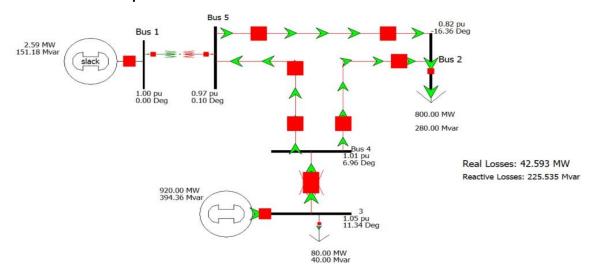


Figure 1. Five Bus system for part (a)



Conclusions:-

- 1. Total real power loss is 42.593 MW.
- 2. MVA rating of each Line/Transformer flow pie chart is 100 MVA.

Power Flow Solution for part (b)

MATLAB Solution

real power in MW and reactive power in MVar

Gauss Seidel Load-Flow Study Report of Power Flow Calculations

26-Nov-2020

Number of iterations : 73
Total real power losses : 35.0897.
Total reactive power losses: 134.004.

			Gen	eration		Load
Bus	Volts	Angle	Real	Reactive	Real	Reactive
1.0000	1.0000	0	315.0883	113.6161	0	0
2.0000	0.8335	-21.1270	0	0	800.0000	280.0000
3.0000	1.0500	1.7922	600.0010	340.3881	80.0000	40.0000
4.0000	1.0188	-0.8733	0	0	0	θ
5.0000	0.9745	-3.6074	0	0	0	θ
		Line Flow	s			

#Line	From Bus	To Bus	Real	Reactive
1.0000	5.0000	1.0000	-313.4055	-91.1783
2.0000	4.0000	2.0000	313.1225	123.8684
3.0000	5.0000	2.0000	516.3230	261.9582
4.0000	3.0000	4.0000	520.0010	300.3881
5.0000	5.0000	4.0000	-202.9175	-170.7799
1.0000	1.0000	5.0000	315.0883	113.6161
2.0000	2.0000	4.0000	-300.6819	-134.6389
3.0000	2.0000	5.0000	-499.3180	-145.3611
4.0000	4.0000	3.0000	-517.5478	-267.6775
5.0000	4.0000	5.0000	204.4255	143.8091

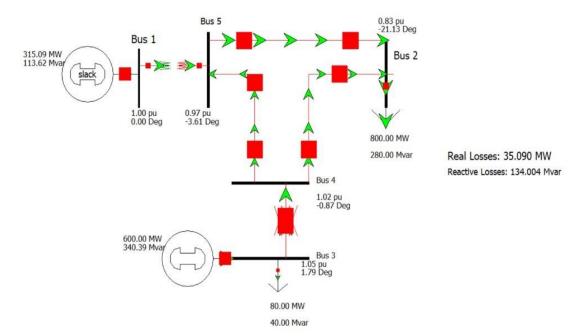


Figure 2. The Bus System after reducing initial/schedule real power at generator attached to bus 3

	Number	Name	Area Name	Nom kV	PU Volt	Volt (kV)	Angle (Deg)	Load MW	Load Mvar	Gen MW	Gen Myar	Switched Shunts Mvar	Act G Shunt MW	Act B Shunt Mvar	Area Num	Zone Num
1	1	Bus 1	1	15,00	1.00000	15.000	0.00		30,10,04	315.09	113.62		0.00	0.00	1	
2	2	Bus 2	1	345.00	0.83345	287.541	-21.13	800.00	280.00				0.00	0.00	1	
3	3	Bus 3	1	345.00	1.05000	362.250	1.79	80.00	40.00	600.00	340.39		0.00	0.00	1	
4	4	Bus 4	1	345,00	1.01878	351,479	-0.87						0.00	0,00	1	1
5	5	Bus 5	1	345.00	0.97448	336,196	-3.61						0.00	0.00	1	

Observations

- 1. Yes, we can reduce the power loss by decreasing the initial/schedule real power at generator attached to bus 3. If we reduce initial/schedule real power to 600 MW instead of 920MW the total real power loss get reduced by 7MW satisfying the condition given in the question.
- 2. MVA rating of each Line/Transformer flow pie chart is 100 MVA.

MATLAB Code for part (a)

```
clear all; close all; clc
% Information about the bus matrix
% nd V Ang. Pg Qg PL QL Gs jBs Type
% (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)
% Colum 11: if the bus has shunt element =1, if it hasnt shunt element =0
% nd V Ang. Pg Qg PL QL Gs jBs Type
bus = [ 1 1.0 0.0 3.948 1.1418 0.0 0.0 0.0 0.0 1 0.0;
2 1.0 0.0 0.0000 0.0000 8.0 2.80 0.0 0.0 3 0.0;
3 1.05 0.0 9.20 3.3735 0.8 0.40 0.0 0.0 2 0.0;
4 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 3 0.0;
5 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 3 0.0;];
%Information about the line matrix
%COL 1.- From bus
%COL 2.- to bus
%COL 3.- R P.U.
%COL 4.- X1 P.U.
%COL 5.- B (parallel) P.U.
%COL 6.- Type of line: 0==Line ; 1==Transformer
%COL 7.- phase shifter angle
line = [ 5 1 0.0015 0.02 0.00 1 0.0;
4 2 0.009 0.1 1.72 0 0.0;
5 2 0.0045 0.05 0.88 0 0.0;
3 4 0.00075 0.01 0.0 1 0.0;
5 4 0.00225 0.025 0.44 0 0.0;];
% Data of the power system is stored in the bus and line matrix of the
% following file
nbuses=length(bus(:,1)); % number of buses of the electric power system
V=bus(:,2); Vprev=V; % Initial bus voltages
The=bus(:,3); % Initial bus angles
% Net power (Generation - Load)
P=bus(:,4)-bus(:,6);
Q=bus(:,5)-bus(:,7);
% ++++++++++ First, compute the addmitance matrix Ybus ++++++++++++++++
[Y] = Y admi(line,bus,nbuses); % function to get the admittance matrix
tolerance=1;
iteration=0;
while (tolerance > 1e-8)
for k=2:nbuses
PYV=0;
for i=1:nbuses
if k ~= i
PYV = PYV + Y(k,i)* V(i); % Vk * Yik
end
end
if bus(k,10)==2 % PV bus
% Estimate Qi at each iteration for the PV buses
Q(k)=-imag(conj(V(k))*(PYV + Y(k,k)*V(k)));
end
V(k) = (1/Y(k,k))*((P(k)-j*Q(k))/conj(V(k))-PYV); % Compute bus voltages
if bus(k,10) == 2 % For PV buses, the voltage magnitude remains same, but the angle changes
V(k)=abs(Vprev(k))*(cos(angle(V(k)))+j*sin(angle(V(k))));
```

```
end
end
iteration=iteration+1; % Increment iteration count
tolerance = max(abs(abs(V) - abs(Vprev))); % Tolerance at the current iteration
Vprev=V;
end
% Now, we have found V and Theta, then, we can compute the power flows
% currents at each node
I=Y*V;
% Power at each node
S=V.*conj(I); % Complex power
for k=1:nbuses
if bus(k,10)==1
% Real and reactive generation at the Slack bus
Pgen(k)=real(S(k));
Qgen(k)=imag(S(k));
end
if bus(k,10)==2
% Real and reactive generation at the PV buses
Pgen(k)=real(S(k))+bus(k,6);
Qgen(k)=imag(S(k))+bus(k,7);
end
if bus(k,10)==3
Pgen(k)=0;
Qgen(k)=0;
end
end
% calculate the line flows and power losses
FromNode=line(:,1);
ToNode=line(:,2);
nbranch=5;
for k=1:nbranch
a=line(k,6); % Find out if is a line or a transformer, a=0 -> line, a=1 -> transformer, 0<a<1 ->
Transformer
switch a % for both cases use the pi model
case 0 %if its a line a=0
b=1i*line(k,5);
suceptancia(k,1)=b/2;
suceptancia(k,2)=b/2;
otherwise %if its a transformer
Zpq=line(k,3)+1i*line(k,4);
Ypq=Zpq^-1;
suceptancia(k,1)=(Ypq/a)*((1/a)-1);
suceptancia(k,2)=Ypq*(1-(1/a));
end
end
% Define admmitance of lines
r = line(:,3);
rx = line(:,4);
z = r + j*rx;
y = ones(nbranch, 1)./z;
% Define complex power flows
Ss = V(FromNode).*conj((V(FromNode) - V(ToNode)).*y ...
   + V(FromNode).*suceptancia(:,1)); % complex flow of the sending buses
```

```
Sr = V(ToNode).*conj((V(ToNode) - V(FromNode)).*y ...
   + V(ToNode).*suceptancia(:,2)); % complex flow of the receiving buses
% Define active and reactive power flows
Pij=real(Ss);
Qij=imag(Ss);
Pji=real(Sr);
Qji=imag(Sr);
% Active power lossess
P_loss=sum(Pij+Pji);
% Reactive power lossess
Q_loss=sum(Qij+Qji);
Gauss Seidel Load-Flow Study')
disp('
disp('
                        Report of Power Flow Calculations ')
disp(' ')
disp(date)
fprintf('Number of iterations
                                 : %g \n', iteration)
fprintf('Total real power losses
                                : %g.\n',P_loss)
fprintf('Total reactive power losses: %g.\n\n',Q_loss)
disp('
                                        Generation
                                                              Load')
disp('
                   Volts
                                                        Real Reactive ')
           Bus
                            Angle
                                       Real Reactive
ywz=[ bus(:,1)
                 abs(V) (180/pi)*angle(V) Pgen' Qgen' bus(:,6) bus(:,7)];
disp(ywz)
disp('
                          Line Flows
disp('
         #Line
                 From Bus To Bus
                                      Real
                                             Reactive
l=1:1:nbranch;
xy=[1' FromNode ToNode Pij Qij];
yx=[1' ToNode FromNode Pji Qji];
disp(xy)
disp(yx)
```

MATLAB SOLUTION FOR PART (B)

```
clear all; close all; clc
% Information about the bus matrix
% nd V Ang. Pg Qg PL QL Gs jBs Type
% (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)
% Colum 11: if the bus has shunt element =1, if it hasnt shunt element =0
% nd V Ang. Pg Qg PL QL Gs jBs Type
bus = [ 1 1.0 0.0 3.948 1.1418 0.0 0.0 0.0 0.0 1 0.0;
2 1.0 0.0 0.0000 0.0000 8.0 2.80 0.0 0.0 3 0.0;
3 1.05 0.0 6.00 3.3735 0.8 0.40 0.0 0.0 2 0.0;
4 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0;
```

```
5 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 3 0.0;];
%Information about the line matrix
%COL 1.- From bus
%COL 2.- to bus
%COL 3.- R P.U.
%COL 4.- X1 P.U.
%COL 5.- B (parallel) P.U.
%COL 6.- Type of line: 0==Line ; 1==Transformer
%COL 7.- phase shifter angle
line = [ 5 1 0.0015 0.02 0.00 1 0.0;
4 2 0.009 0.1 1.72 0 0.0;
5 2 0.0045 0.05 0.88 0 0.0;
3 4 0.00075 0.01 0.0 1 0.0;
5 4 0.00225 0.025 0.44 0 0.0;];
% Data of the power system is stored in the bus and line matrix of the
% following file
nbuses=length(bus(:,1)); % number of buses of the electric power system
V=bus(:,2); Vprev=V; % Initial bus voltages
The=bus(:,3); % Initial bus angles
% Net power (Generation - Load)
P=bus(:,4)-bus(:,6);
Q=bus(:,5)-bus(:,7);
% +++++++++++ First, compute the addmitance matrix Ybus +++++++++++++++
[Y] = Y_admi(line,bus,nbuses); % function to get the admittance matrix
tolerance=1;
iteration=0;
while (tolerance > 1e-8)
for k=2:nbuses
PYV=0;
for i=1:nbuses
if k ~= i
PYV = PYV + Y(k,i)* V(i); % Vk * Yik
end
end
if bus(k,10)==2 \% PV bus
% Estimate Qi at each iteration for the PV buses
Q(k)=-imag(conj(V(k))*(PYV + Y(k,k)*V(k)));
end
V(k) = (1/Y(k,k))*((P(k)-j*Q(k))/conj(V(k))-PYV); % Compute bus voltages
if bus(k,10) == 2 \% For PV buses, the voltage magnitude remains same, but the angle changes
V(k)=abs(Vprev(k))*(cos(angle(V(k)))+j*sin(angle(V(k))));
end
end
iteration=iteration+1; % Increment iteration count
tolerance = max(abs(abs(V) - abs(Vprev))); % Tolerance at the current iteration
Vprev=V;
end
% Now, we have found V and Theta, then, we can compute the power flows
% currents at each node
I=Y*V;
% Power at each node
```

```
S=V.*conj(I); % Complex power
for k=1:nbuses
if bus(k,10)==1
% Real and reactive generation at the Slack bus
Pgen(k)=real(S(k));
Qgen(k)=imag(S(k));
end
if bus(k,10)==2
% Real and reactive generation at the PV buses
Pgen(k)=real(S(k))+bus(k,6);
Qgen(k)=imag(S(k))+bus(k,7);
end
if bus(k,10)==3
Pgen(k)=0;
Qgen(k)=0;
end
end
% calculate the line flows and power losses
FromNode=line(:,1);
ToNode=line(:,2);
nbranch=5;
for k=1:nbranch
a=line(k,6); % Find out if is a line or a transformer, a=0 -> line, a=1 -> transformer, 0<a<1 ->
Transformer
switch a % for both cases use the pi model
case 0 %if its a line a=0
b=1i*line(k,5);
suceptancia(k,1)=b/2;
suceptancia(k,2)=b/2;
otherwise %if its a transformer
Zpq=line(k,3)+1i*line(k,4);
Ypq=Zpq^-1;
suceptancia(k,1)=(Ypq/a)*((1/a)-1);
suceptancia(k,2)=Ypq*(1-(1/a));
end
end
% Define admmitance of lines
r = line(:,3);
rx = line(:,4);
z = r + j*rx;
y = ones(nbranch,1)./z;
% Define complex power flows
Ss = V(FromNode).*conj((V(FromNode) - V(ToNode)).*y ...
   + V(FromNode).*suceptancia(:,1)); % complex flow of the sending buses
Sr = V(ToNode).*conj((V(ToNode) - V(FromNode)).*y ...
   + V(ToNode).*suceptancia(:,2)); % complex flow of the receiving buses
% Define active and reactive power flows
Pij=real(Ss);
Qij=imag(Ss);
Pji=real(Sr);
Qji=imag(Sr);
% Active power lossess
P_loss=sum(Pij+Pji);
```

```
% Reactive power lossess
Q_loss=sum(Qij+Qji);
Gauss Seidel Load-Flow Study')
disp('
disp('
                       Report of Power Flow Calculations ')
disp(' ')
disp(date)
fprintf('Number of iterations
                                : %g \n', iteration)
fprintf('Total real power losses
                                : %g.\n',P_loss)
fprintf('Total reactive power losses: %g.\n\n',Q_loss)
disp('
                                       Generation
                                                           Load')
disp(
          Bus
                  Volts
                           Angle
                                     Real Reactive
                                                       Real Reactive ')
ywz=[ bus(:,1)
                abs(V) (180/pi)*angle(V) Pgen' Qgen'
                                                     bus(:,6) bus(:,7)];
disp(ywz)
disp('
                        Line Flows
disp('
       #Line
                From Bus To Bus
                                    Real
l=1:1:nbranch;
xy=[1' FromNode ToNode Pij Qij];
yx=[1' ToNode FromNode Pji Qji];
disp(xy)
disp(yx)
```

MATLAB CODE FOR Y ADMITTANCE

```
function [Y] = Y admi(line,bus,nbuses)
%% Y BUS Building
orden=zeros(1,nbuses);
Y=zeros(nbuses);
for k=1:nbuses
   orden(k)=k; % vector which contains the order of building according to the bus information
end
for p=1:length(line(:,1));
   BusP=find(orden==line(p,1));
    BusQ=find(orden==line(p,2));
    a=line(p,6); %Tap value for the p iteration
    if a>0 % for transformers out of nominal position
   yl=(1/((line(p,3)+j*line(p,4)))); % line admittance
   Ad=(j*line(p,5)/2); % line charging
   Y(BusP,BusQ)=Y(BusP,BusQ)-yl/a; % a non diagonal element
   Y(BusQ,BusP)=Y(BusP,BusQ); % symmetry is declared for elements out of the diagonal
   Y(BusP,BusP)=Y(BusP,BusP)+(y1/a)+((1/a)*(1/a-1)*y1)+Ad; %Equivalent admittance at the P-terminal
plus line charging
   Y(BusQ,BusQ)=Y(BusQ,BusQ)+(yl/a)+(1-1/a)*yl+Ad; %Equivalent admittance at the Q-terminal plus
line charging
   else % for lines
        yl=(1/((line(p,3)+j*line(p,4)))); % line admittance
        Ad=(j*line(p,5)/2); % line charging
        Y(BusP,BusQ)=Y(BusP,BusQ)-yl; % a non diagonal element
        Y(BusQ,BusP)=Y(BusP,BusQ); % symmetry is declared for elements out of the diagonal
        Y(BusP,BusP)=Y(BusP,BusP)+yl; % diagonal element
        Y(BusQ,BusQ)=Y(BusQ,BusQ)+y1; % diagonal element
         c=line(p,5); % line charging for the whole line
         if c>0
             Y(BusP,BusP)= Y(BusP,BusP)+Ad; %add value of line charging to the diagonal element
```

```
Y(BusQ,BusQ)= Y(BusQ,BusQ)+Ad; %add value of line charging to the diagonal element end
```

```
end
end
% Susceptance and conductance
for m=1:nbuses
    dir=find(orden==bus(m,1));
    Y(dir,dir)=Y(dir,dir)+bus(m,8)+j*bus(m,9); % add the shunt admittance
end
end
```

Conclusion

The results from Gauss-Seidel Method match closely with the solution obtained from the Power-World Software. Thus, the problem has been solved and verified by both the methods.

Acknowledgement

We would like to express our gratitude to Prof. Saikat Chakrabarti who presented us with the opportunity to work on this project where we learnt to solve the power flow problem using both MATLAB and Powerworld software. We would also like to acknowledge the cohesive efforts of each member of the team so that we could learn and apply our theoretical knowledge.