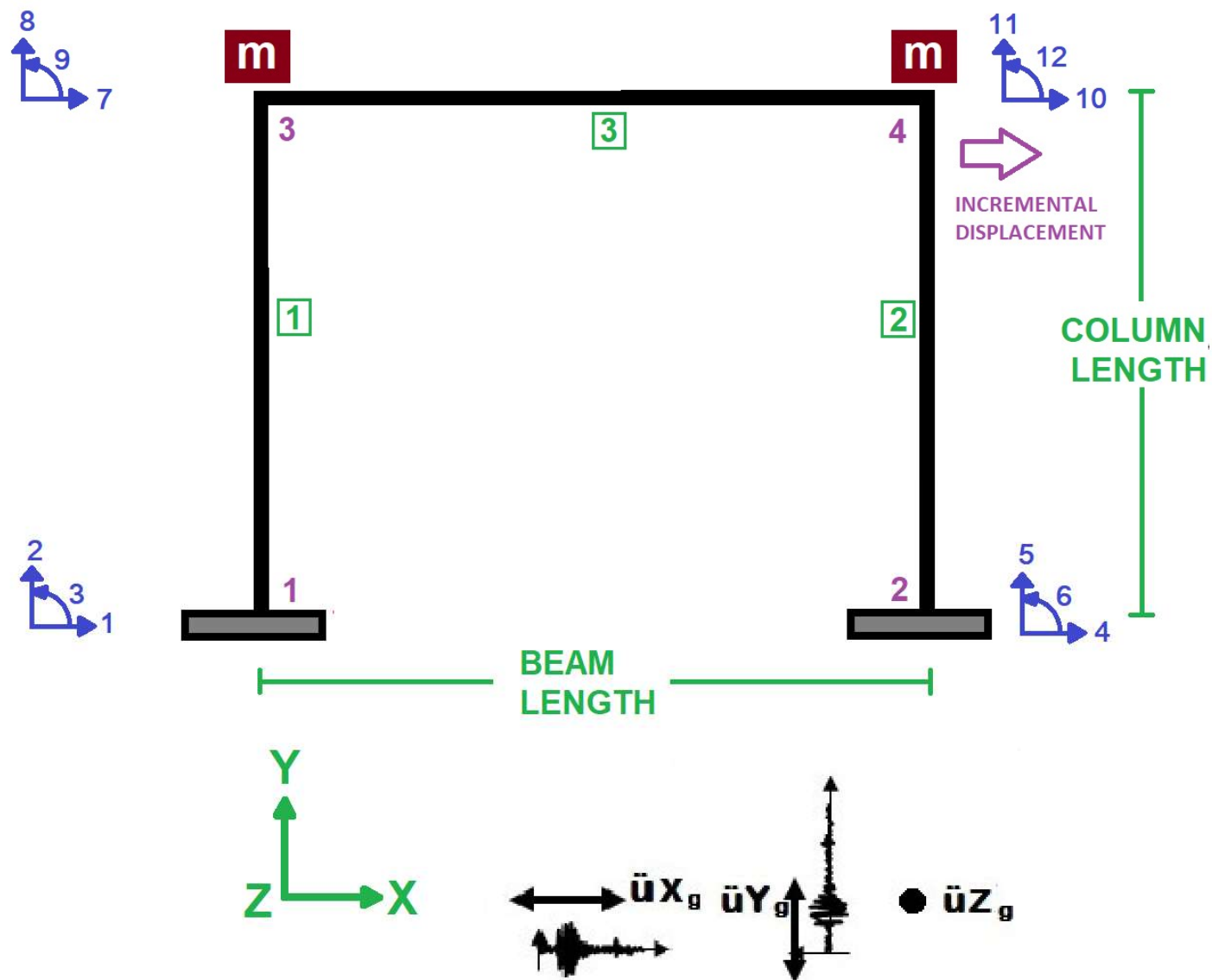
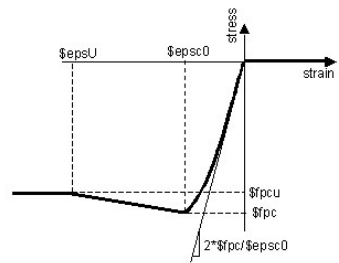


IN THE NAME OF ALLAH, THE MOST GRACIOUS, THE MOST MERCIFUL

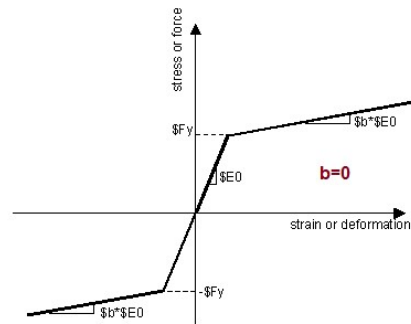
OPTIMIZATION OF COLUMN SECTION DEPTH BASED ON TARGET STRUCTURAL PERIOD FOR CONCRETE FRAME USING OPENSEES

WRITTEN BY SALAR DELAVAR GHASHGHAEI (QASHQAI)

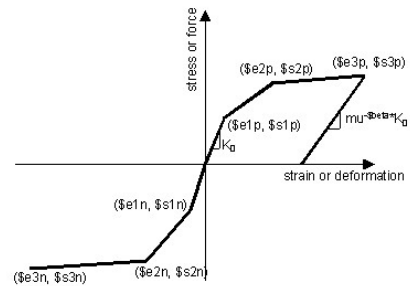




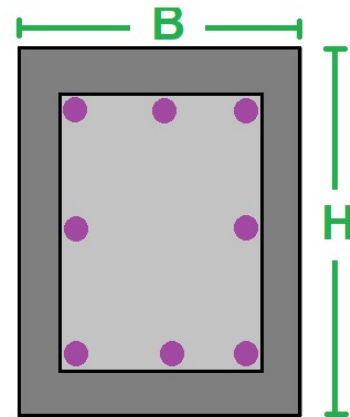
CORE AND COVER CONCRETE REALTION



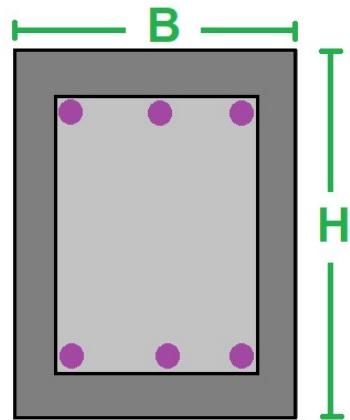
WITHOUT HARDENING AND ULTIMATE STRAIN



WITH HARDENING AND ULTIMATE STRAIN



COLUMN SECTION



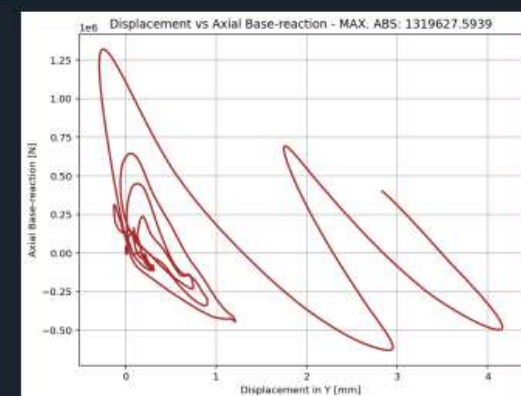
BEAM SECTION

C:\Users\ DELL\Desktop\OPENSEES_FILES\CONCRETE_FRA...TIMIZATION\DYNAMIC_Cdepth_PERIOD_OPTIMIZATION.py

DYNAMIC_Cdepth_PERIOD_OPTIMIZATION.py

```
1 #####
2 # >> IN THE NAME OF ALLAH, THE MOST GRACIOUS, THE MOST MERCIFUL <<
3 # OPTIMIZATION OF COLUMN SECTION DEPTH BASED ON TARGET STRUCTURAL PERIOD FOR CONCRETE FRAME USING
4 # -----
5 # OPTIMIZATION ALGORITHM: NEWTON-RAPHSON METHOD
6 # -----
7 # THIS PROGRAM WRITTEN BY SALAR DELAVAR GHASHGHAEI (QASHQAI)
8 # EMAIL: salar.d.ghashghaei@gmail.com
9 #####
10 """
11 1. This Python script performs nonlinear dynamic and pushover analysis of a 2D reinforced concrete fra
12 2. The code implements a Newton-Raphson optimization algorithm to determine optimal column depth basec
13 3. Advanced material models include confined/unconfined concrete (Concrete01) and hysteretic steel rei
14 4. The frame consists of two nonlinear beam-column elements (columns) and one beam element with distri
15 5. Dynamic analysis features Rayleigh damping calibrated using the first two modal frequencies.
16 6. The script can perform both displacement-controlled pushover and time-history analyses under seismi
17 7. Key outputs include force-displacement responses, stiffness degradation, and period-dependent behav
18 8. The analysis tracks base reactions, displacements, rotations, and section stiffnesses throughout la
19 9. Advanced features include corotational geometric transformations for large displacements.
20 10. The code implements logarithmic decrement analysis to estimate damping ratios from free vibration
21 11. Comprehensive plotting functions visualize hysteresis loops, P-M interactions, and time-history re
22 12. The optimization process automatically adjusts column depth to match a target fundamental period.
23 13. Results are exported to Excel for post-processing, including peak responses and cumulative maxima.
24 14. The model includes concentrated nodal masses and accounts for element mass contributions.
25 15. Both stiffness-proportional and mass-proportional damping components are considered.
26 16. The script handles convergence issues with automatic analysis restart capabilities.
27 17. Statistical analysis of results includes histograms and box plots of key response parameters.
28 18. The implementation demonstrates best practices for nonlinear frame analysis in OpenSees.
29 19. The code is well-commented with references to OpenSees documentation and theory manuals.
30 20. This provides a robust template for performance-based seismic design optimization of concrete fram
31
32 The script represents a sophisticated integration of structural dynamics theory, numerical optimizatio
33 and nonlinear finite element analysis for seismic design applications.
34 """
```

...E_EXAMPLES\OPTIMIZATION\DYNAMIC_Cdepth_PERIOD_OPTIMIZATION



Help Variable Explorer Debugger Plots Files

Console 1/A

```
Lobatto
End 1 Forces (P V M): 270408 184668 3.76963e+08
End 2 Forces (P V M): -270408 -184668 1.7704e+08

Element: 3 Type: ForceBeamColumn2d Connected Nodes: 3 4
Number of Sections: 5 Mass density: 6.36044
Lobatto
End 1 Forces (P V M): 1056.37 -50385 -1.75653e+08
End 2 Forces (P V M): -1056.37 50385 -1.77041e+08

In [2]:
```

IPython Console History

NONLINEAR DYNAMIC ANALYSIS RESULTS

PERIOD_01 : 1.32113890 - PERIOD_02 : 9.34380605
F: 1.843806048673832
Structure First Period: 1.3211389075865452
Structure Second Period: 9.343806261665975
Fmin: 1.843806261665975
Structure First Period: 1.3211389003907277
Structure Second Period: 9.34380583568142
Fmax: 1.8438058356814206
DF: -0.02129922771487713
DX: -86.56680295436094
IT: 1 - RESIDUAL: 86.56680295436094 - X: 586.5668029543609

Structure First Period: 1.2938764559626208
Structure Second Period: 7.81336791685246
PERIOD_01 : 1.29387646 - PERIOD_02 : 7.81336792
F: 0.3133679168524601
Structure First Period: 1.2938764587320013
Structure Second Period: 7.813368063685243
Fmin: 0.3133680636852434
Structure First Period: 1.2938764531932436
Structure Second Period: 7.8133677700197985
Fmax: 0.31336777001979854
DF: -0.014683272242521637
DX: -21.34183114476149
IT: 2 - RESIDUAL: 21.34183114476149 - X: 607.9086340991224

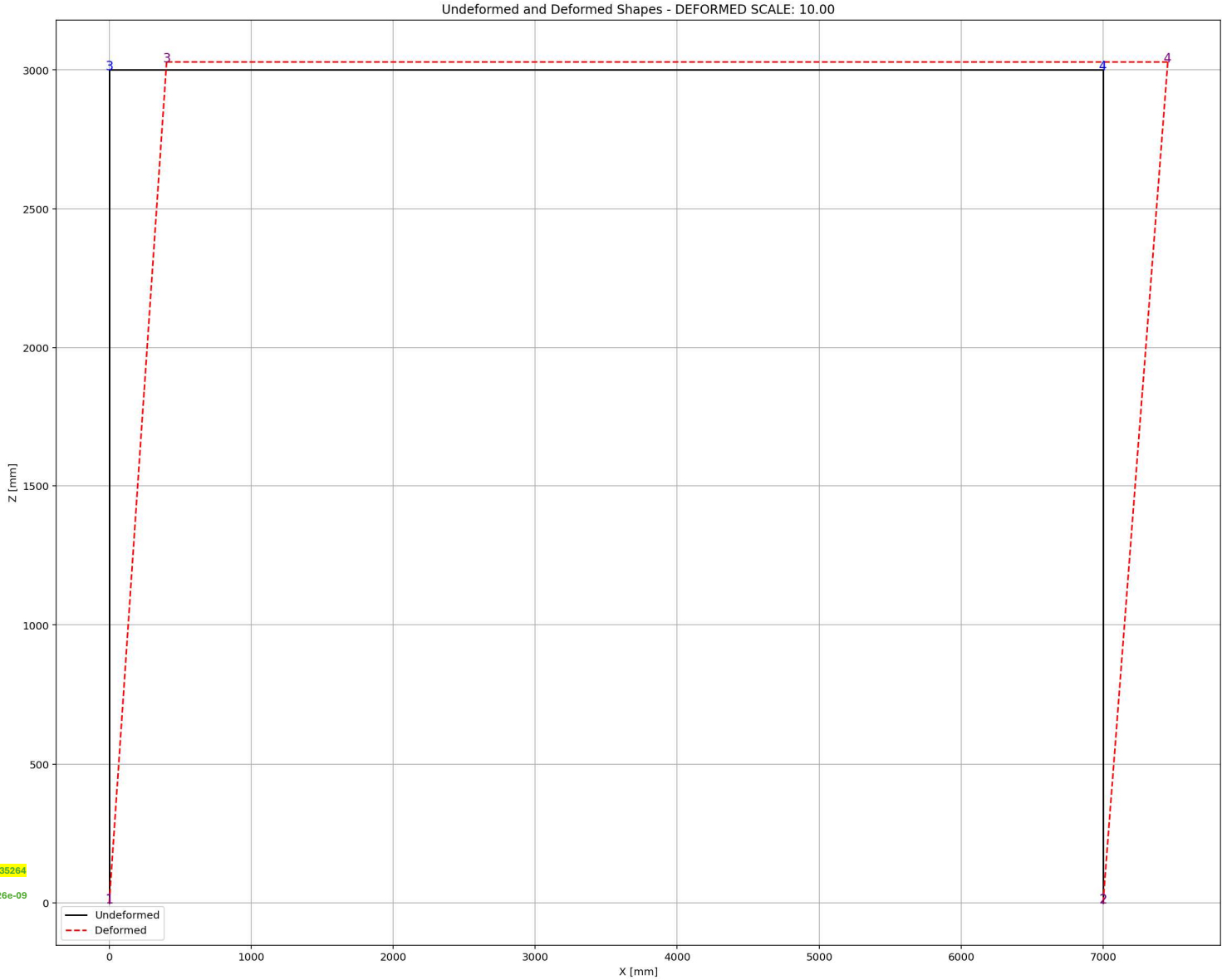
Structure First Period: 1.2881289006602148
Structure Second Period: 7.51251922775103
PERIOD_01 : 1.28812890 - PERIOD_02 : 7.51251923
F: 0.01251922775102976
Structure First Period: 1.2881289032798524
Structure Second Period: 7.5125193630900006
Fmin: 0.01251936309000623
Structure First Period: 1.2881288980405776
Structure Second Period: 7.51251909241217
Fmax: 0.012519092412169641
DF: -0.013533891829453635
DX: -0.9250279157532739
IT: 3 - RESIDUAL: 0.9250279157532739 - X: 608.8336620148757

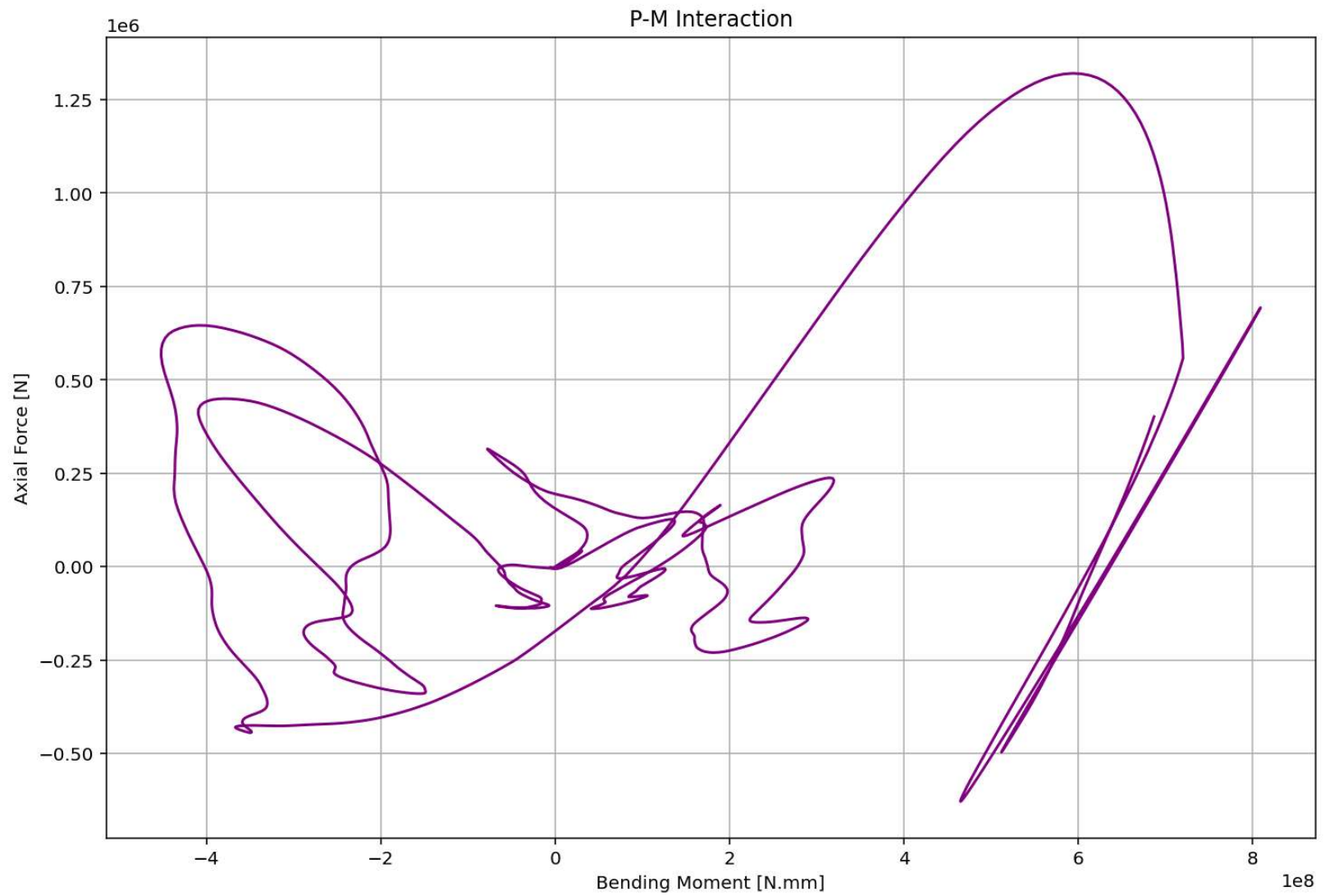
Structure First Period: 1.287886860074277
Structure Second Period: 7.500021607458597
PERIOD_01 : 1.28788686 - PERIOD_02 : 7.50002161
F: 2.1607458596584195e-05
Structure First Period: 1.287886862687799
Structure Second Period: 7.5000217423308575
Fmin: 2.1742330857499326e-05
Structure First Period: 1.287886857460755
Structure Second Period: 7.500021472586389
Fmax: 2.147258638895977e-05
DF: -0.013487223426977833
DX: -0.001602068706993009
IT: 4 - RESIDUAL: 0.001602068706993009 - X: 608.8352640835827

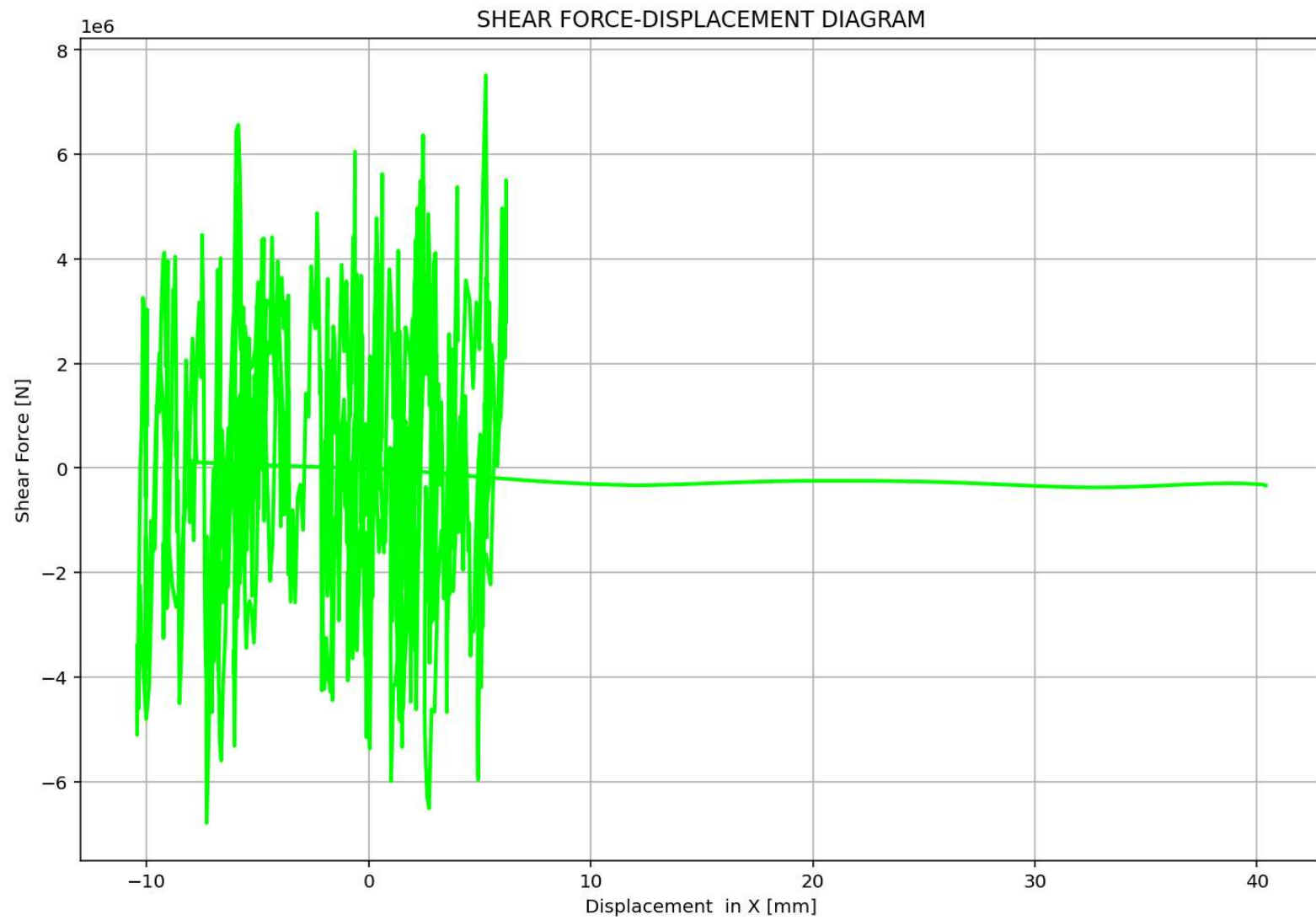
Structure First Period: 1.2878864413712046
Structure Second Period: 7.50000000080559
PERIOD_01 : 1.28788644 - PERIOD_02 : 7.50000000
F: 8.055867084522106e-11
Structure First Period: 1.2878864439847162
Structure Second Period: 7.500000134951995
Fmin: 1.3495199535640268e-07
Structure First Period: 1.2878864387576943
Structure Second Period: 7.49999865209172
Fmax: -1.3479082827672073e-07
DF: -0.013487141181656169
DX: -5.972986262581305e-09
IT: 5 - RESIDUAL: 5.972986262581305e-09 - X: 608.8352640895557

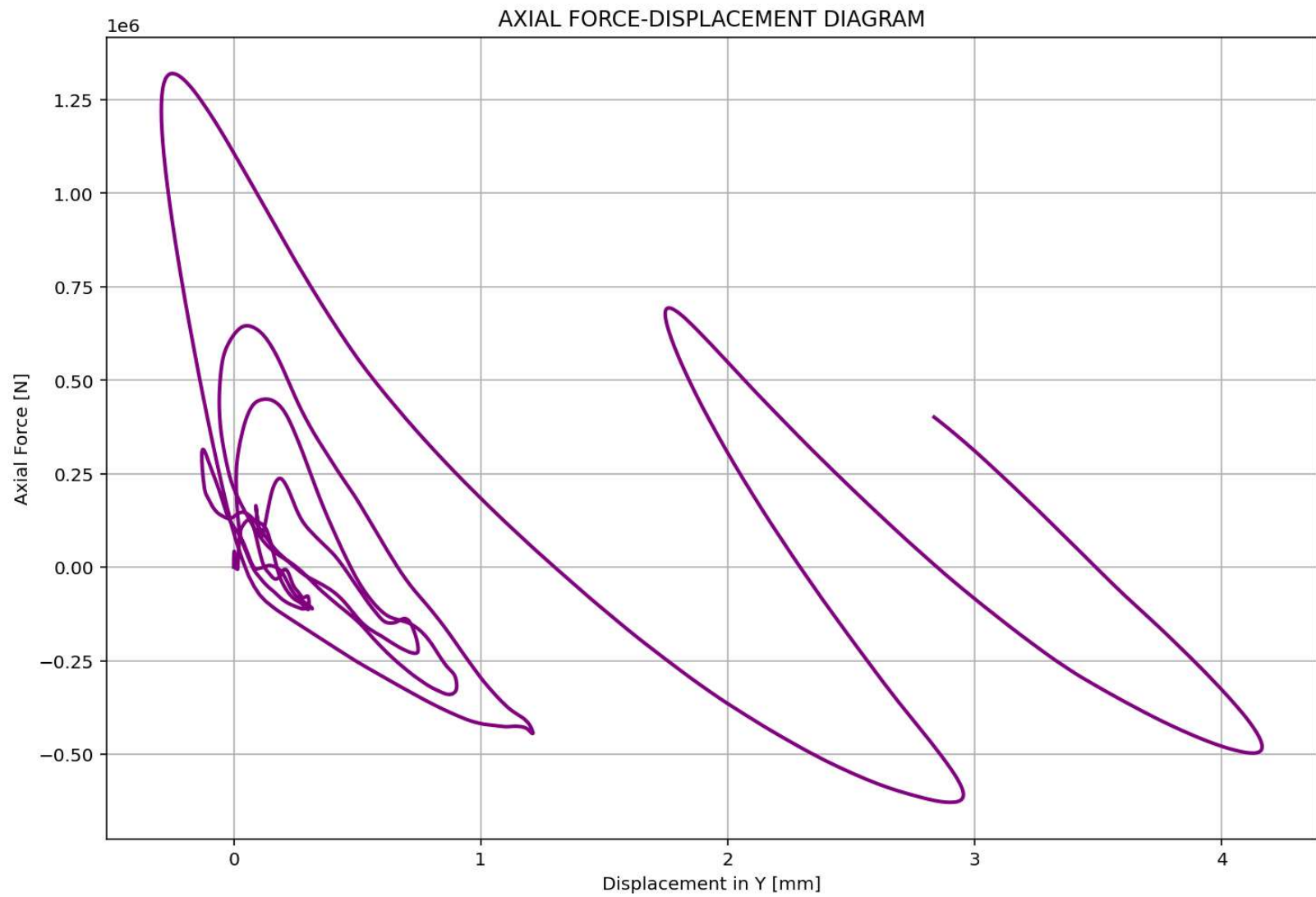
Optimum Column Section Depth : 608.835264
Iteration Counts: 5
Convergence Residual: 5.9729862626e-09

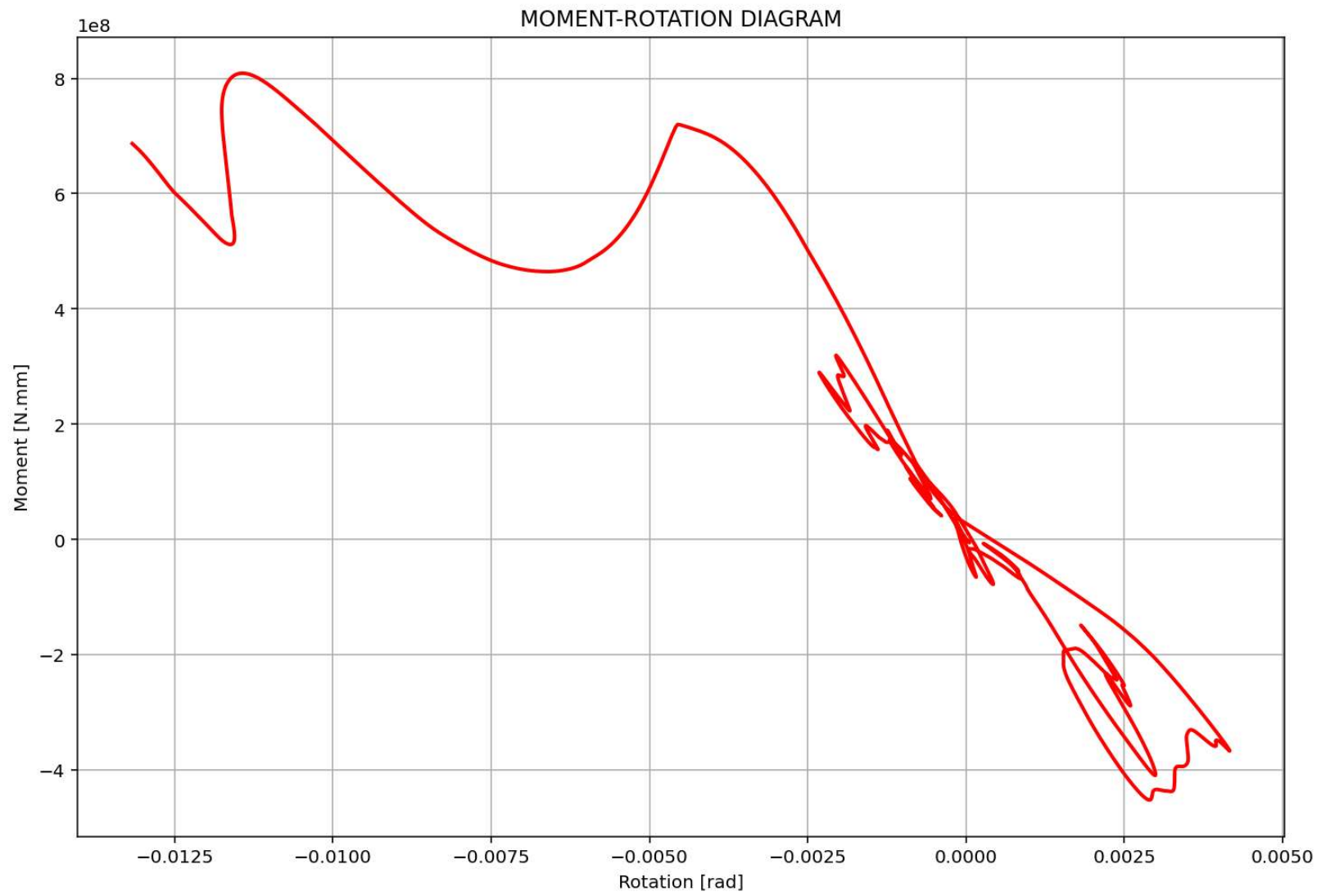
Total time (s): 12.8281



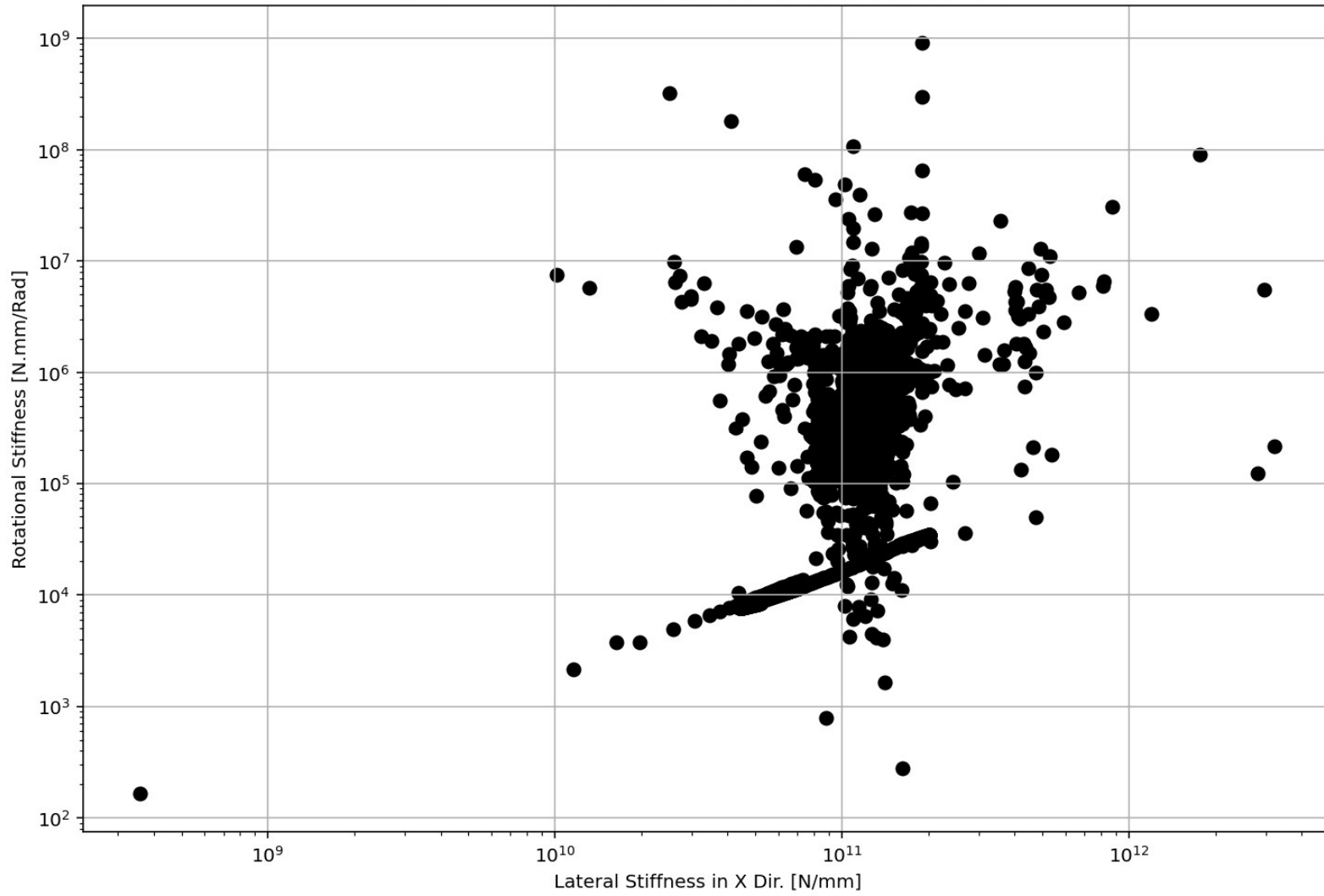




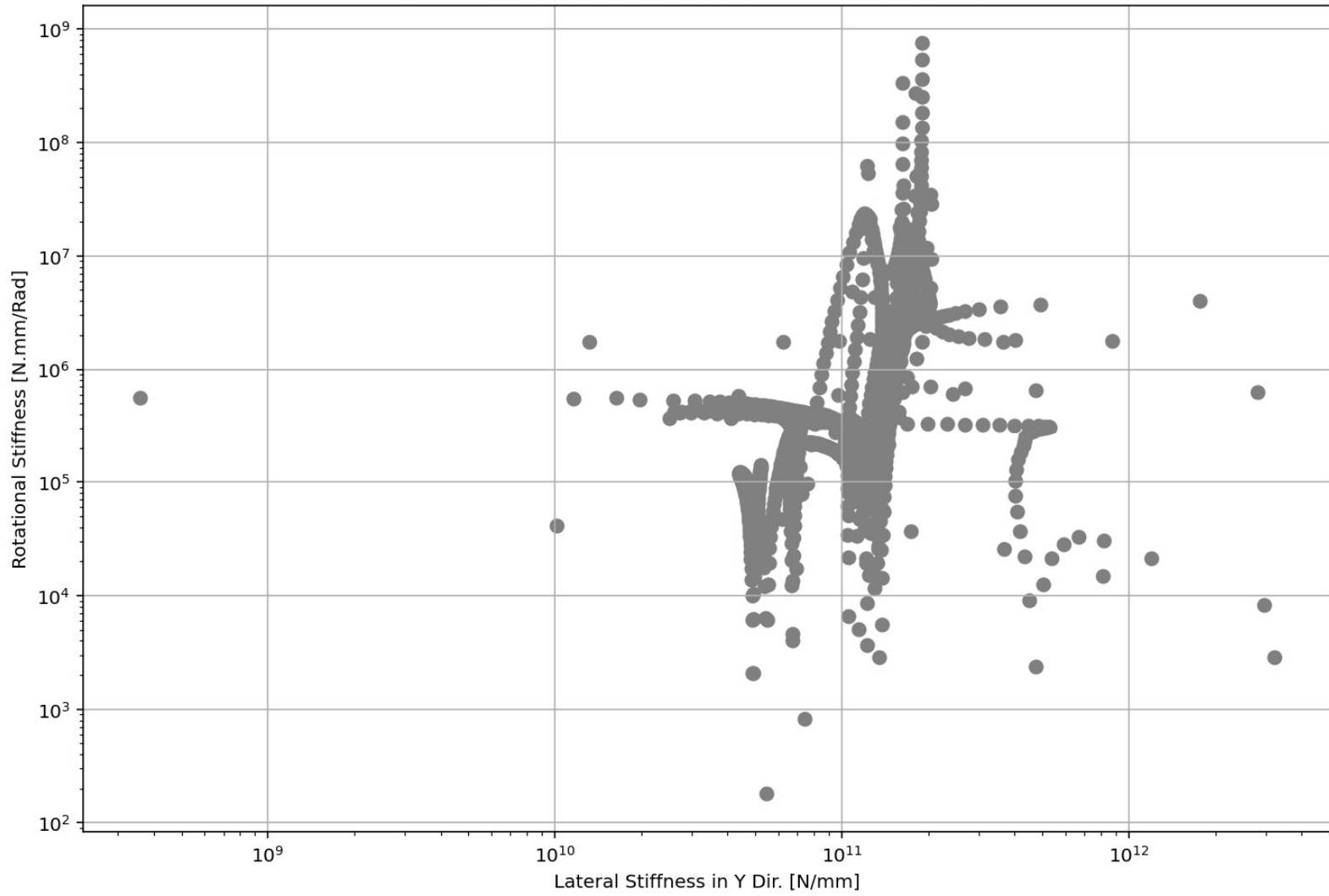


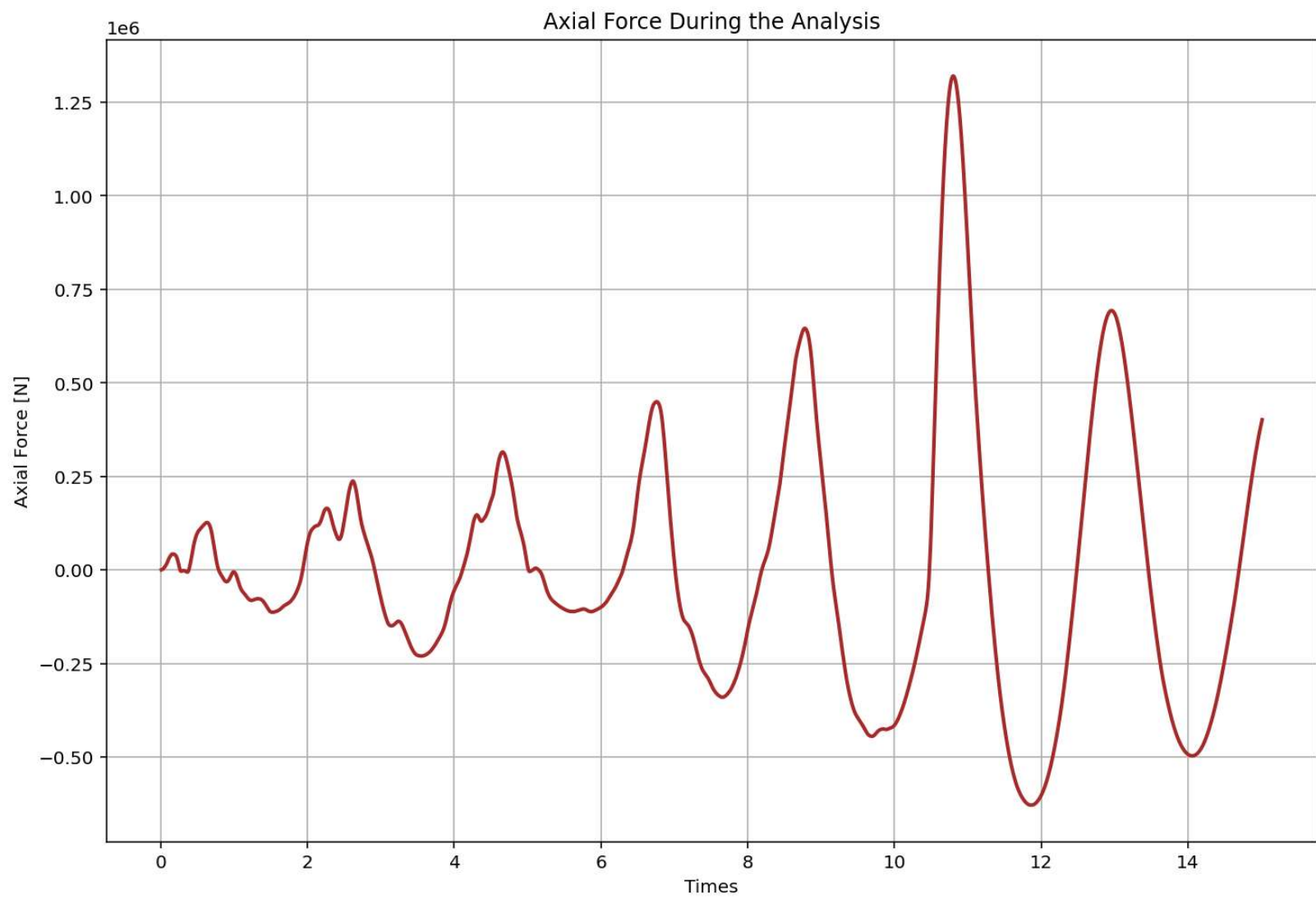


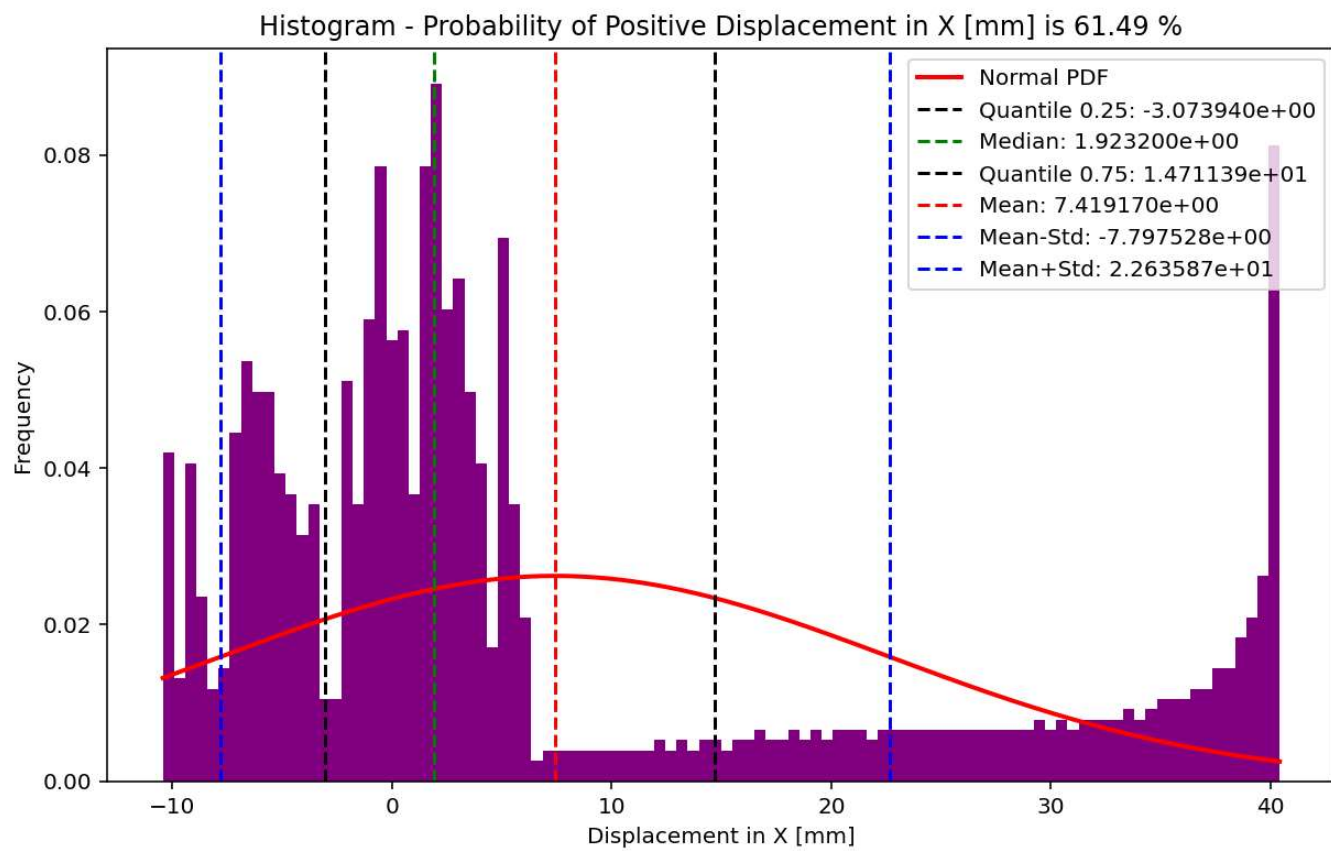
ROTATIONAL STIFFNESS-LATERAL STIFFNESS DIAGRAM

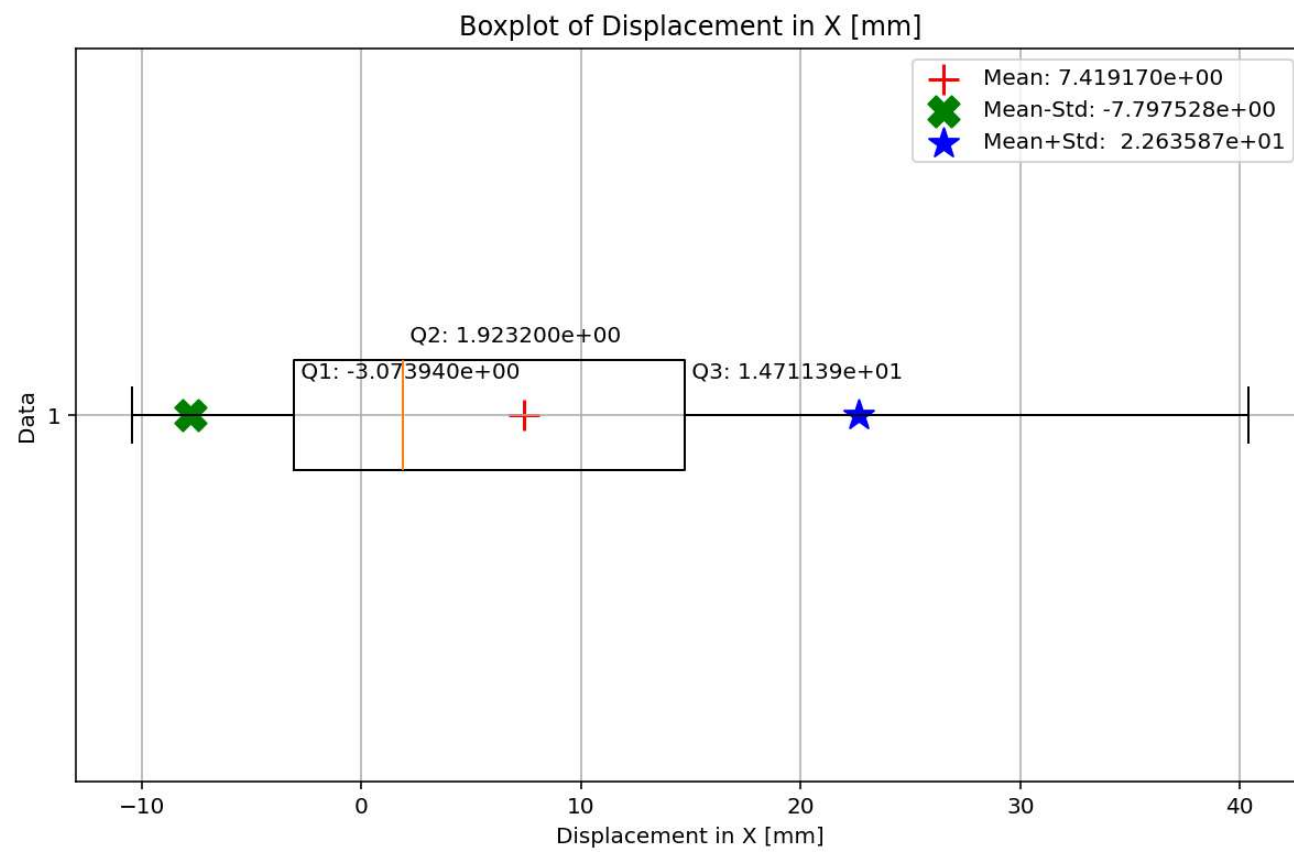


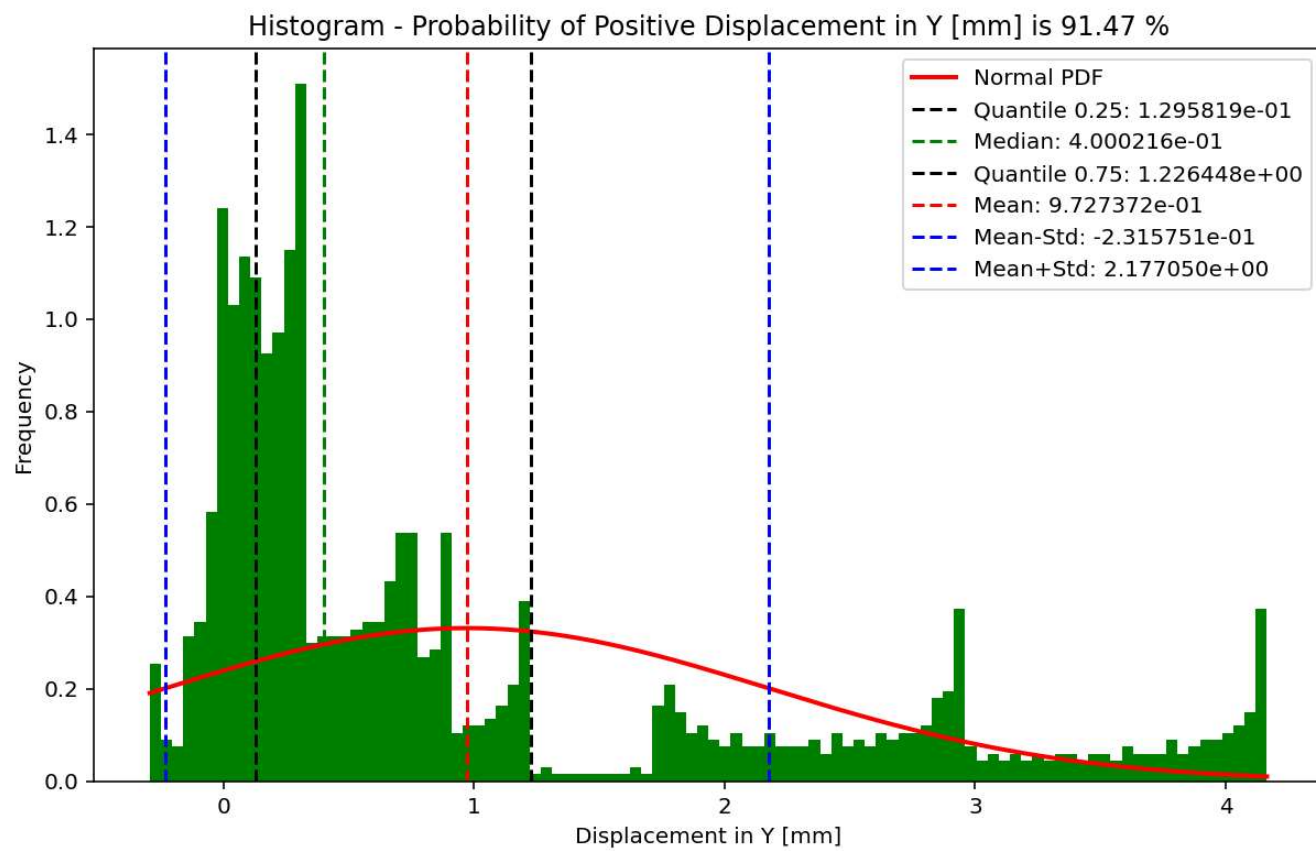
ROTATIONAL STIFFNESS-LATERAL STIFFNESS DIAGRAM

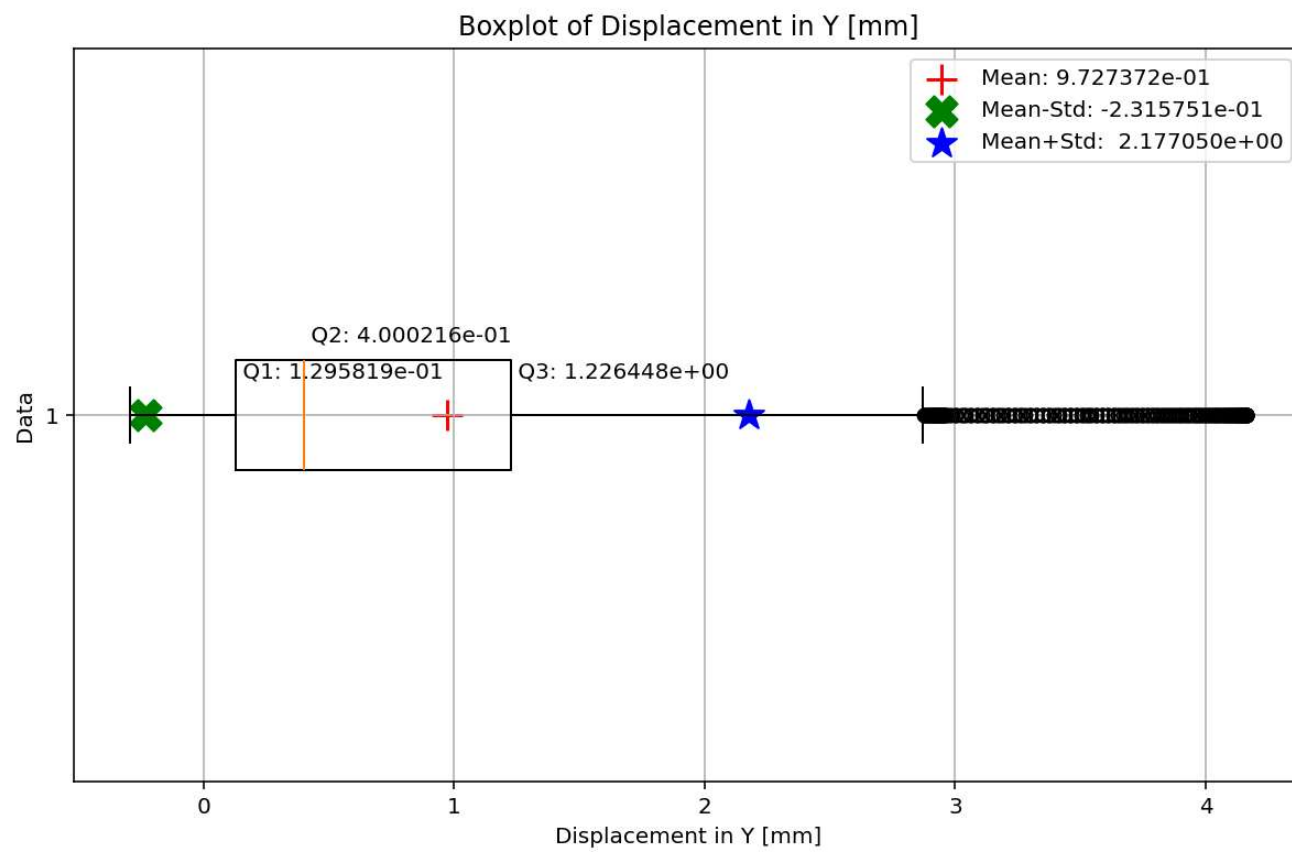


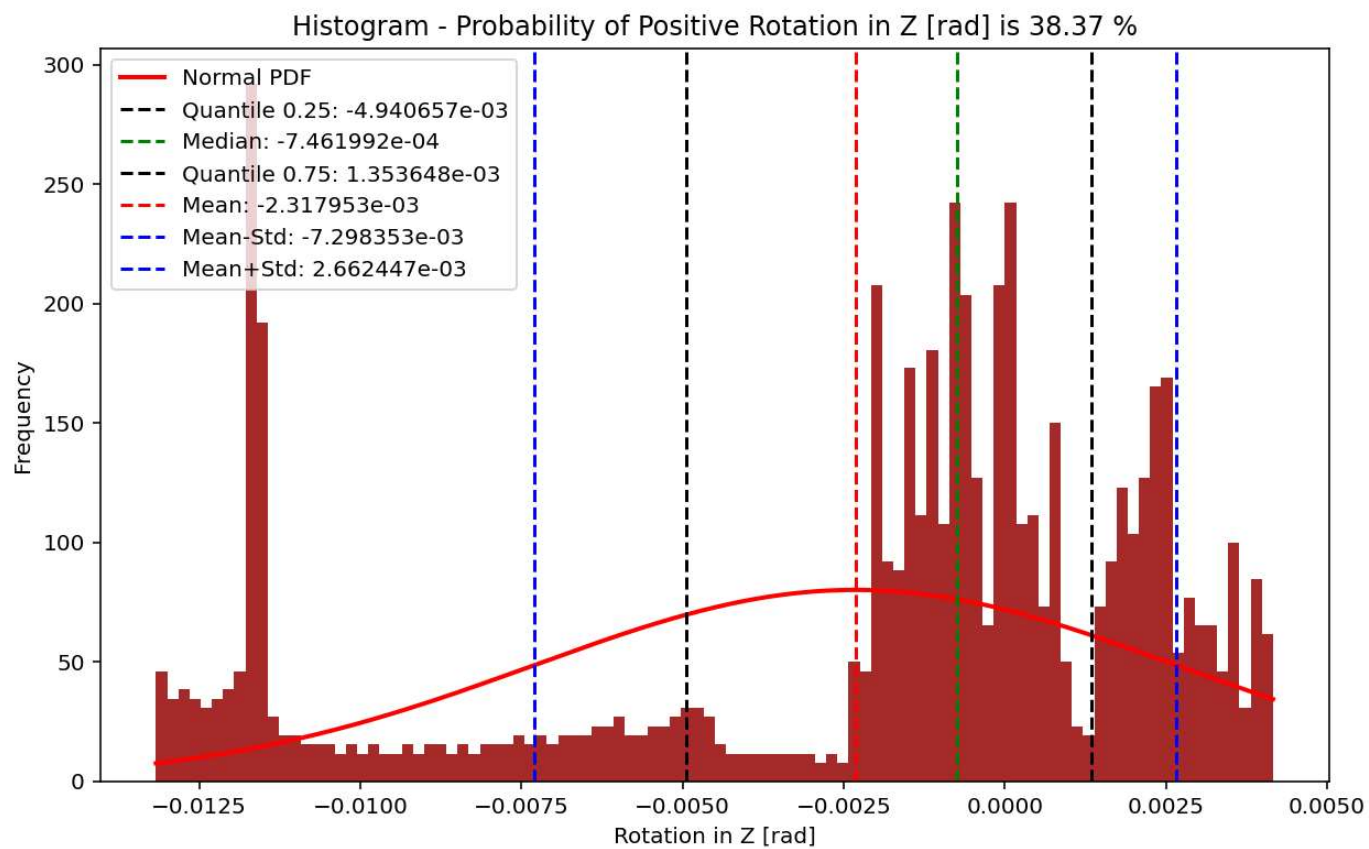


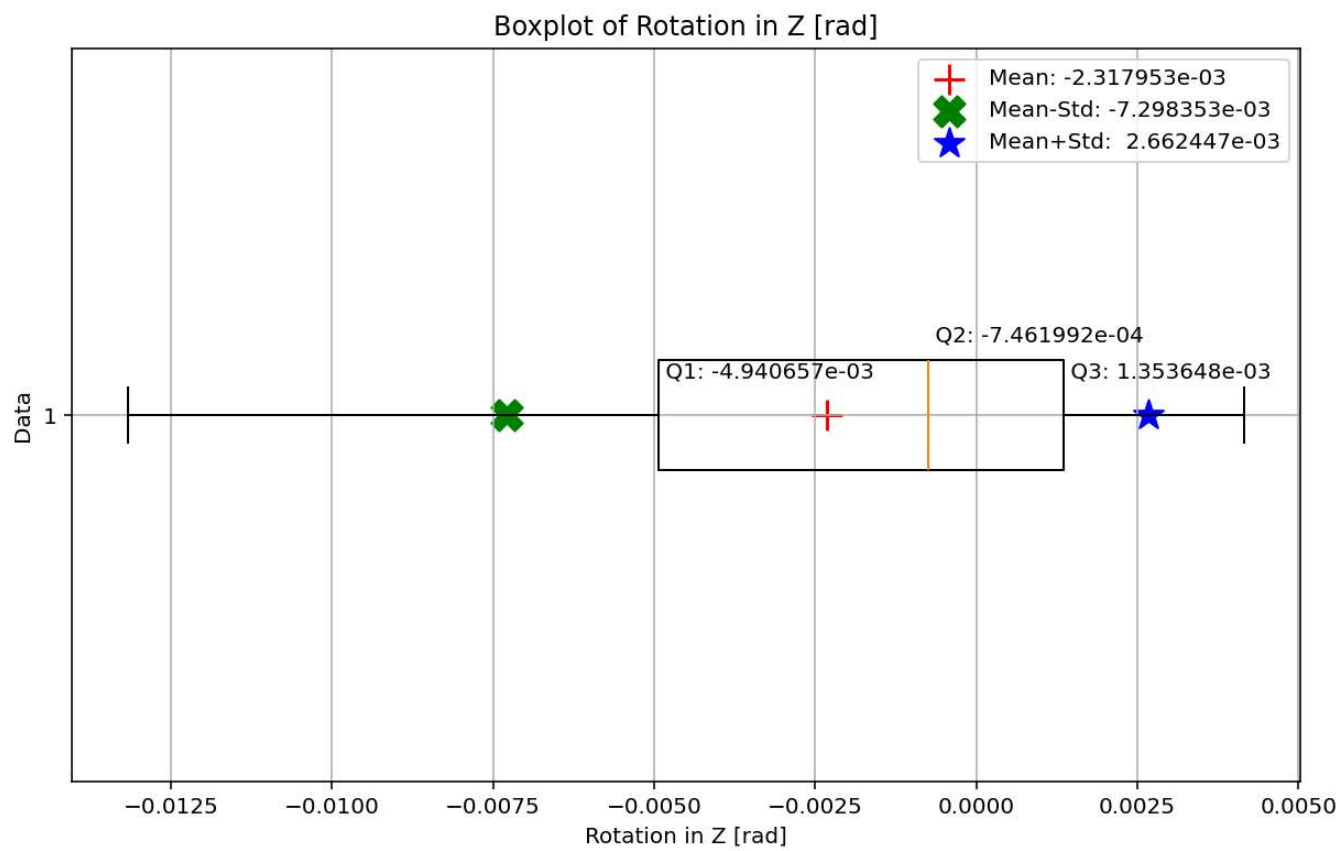


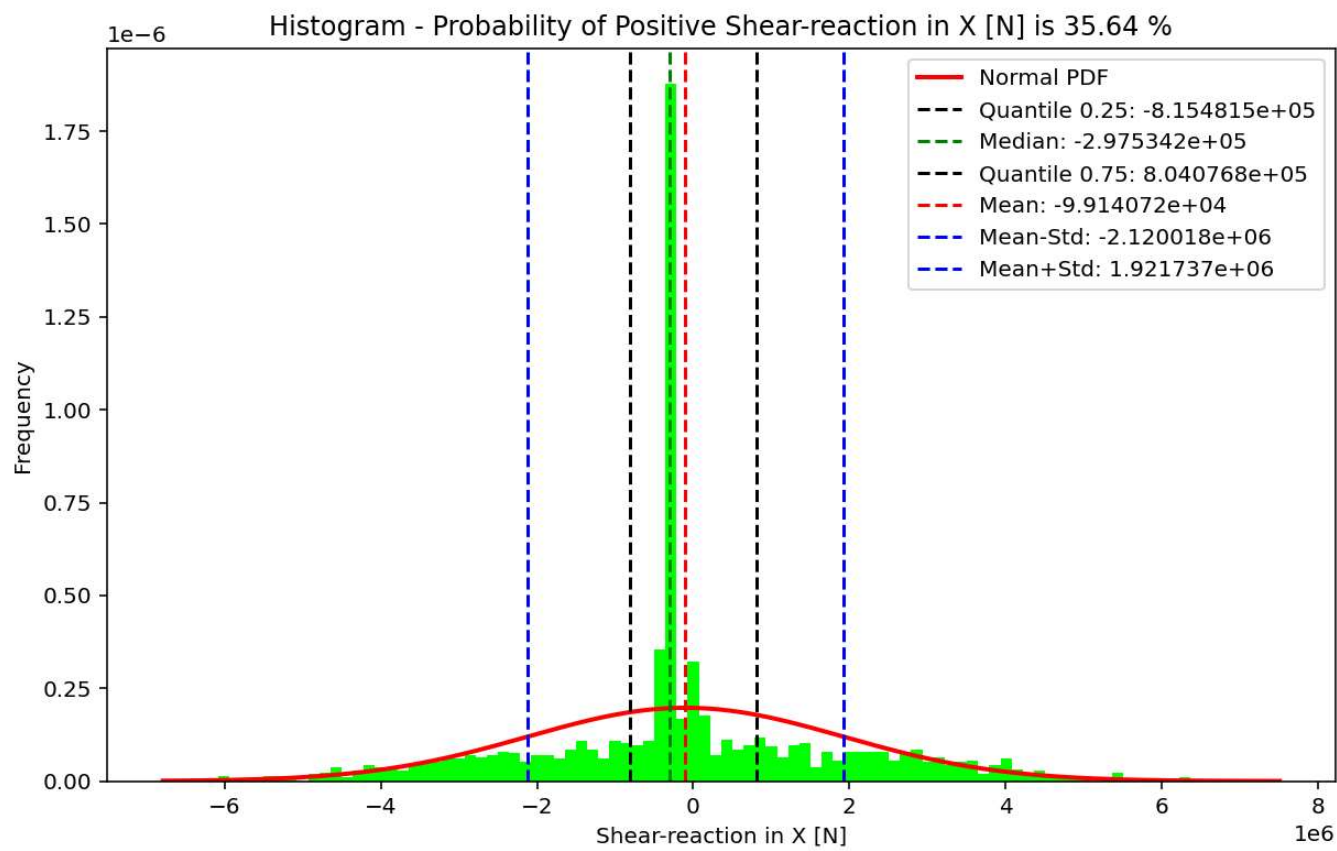


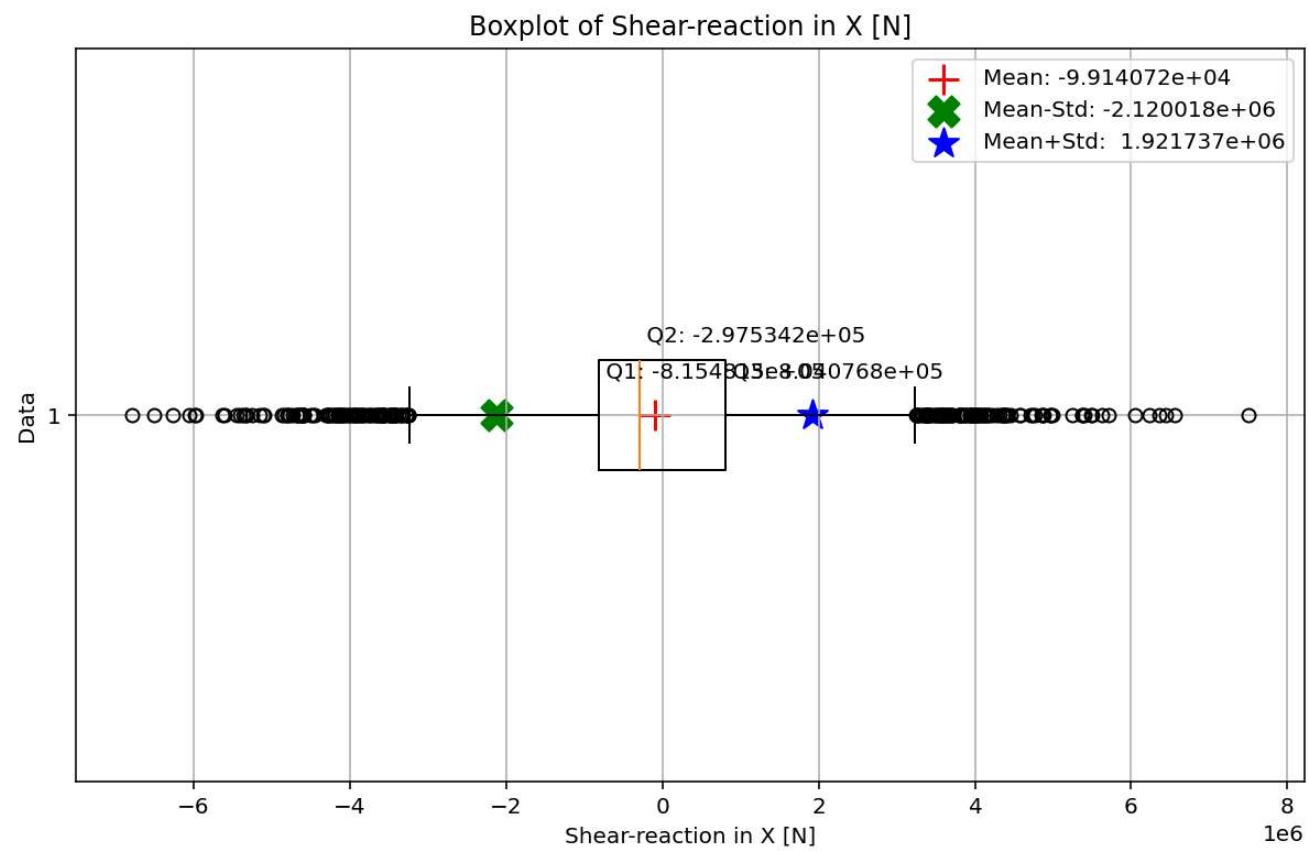


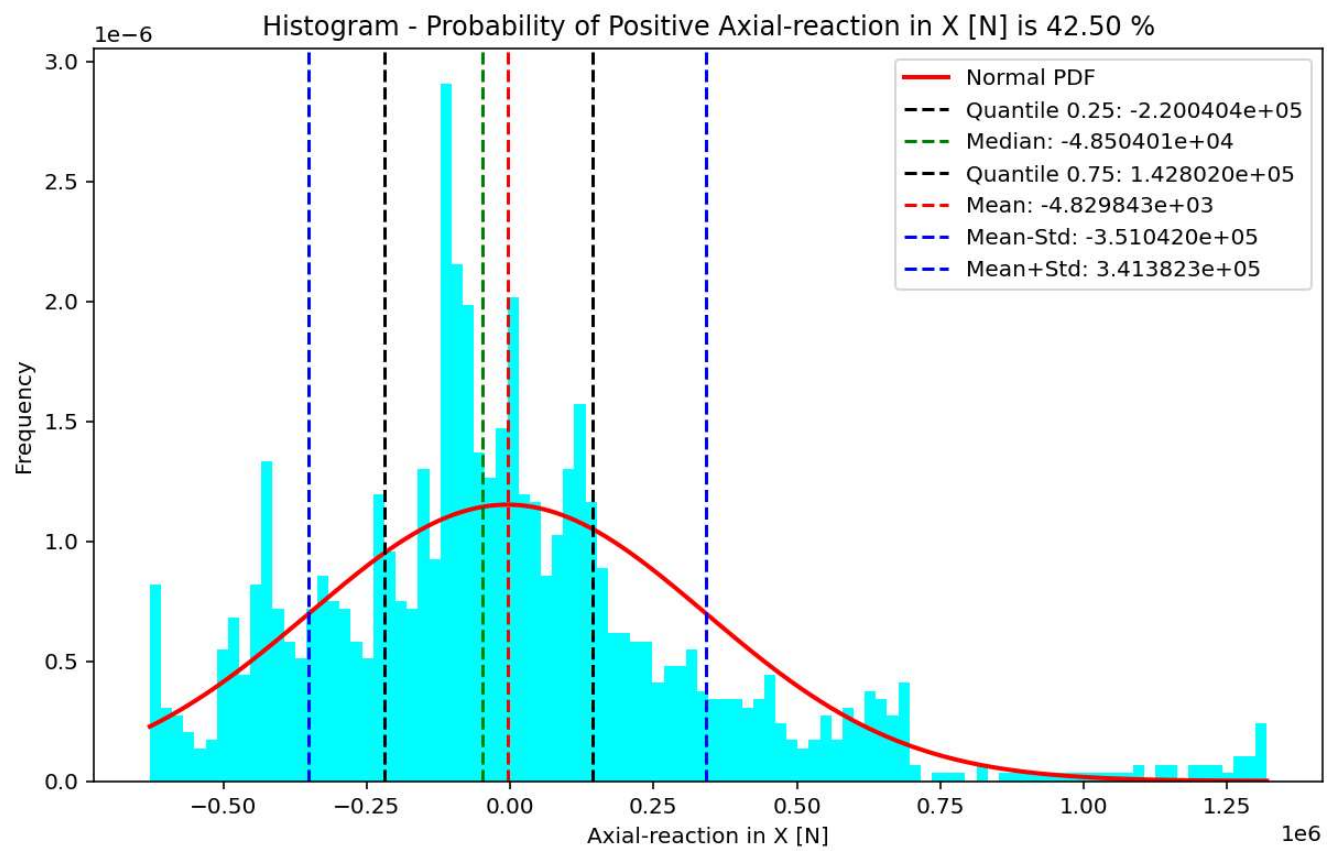


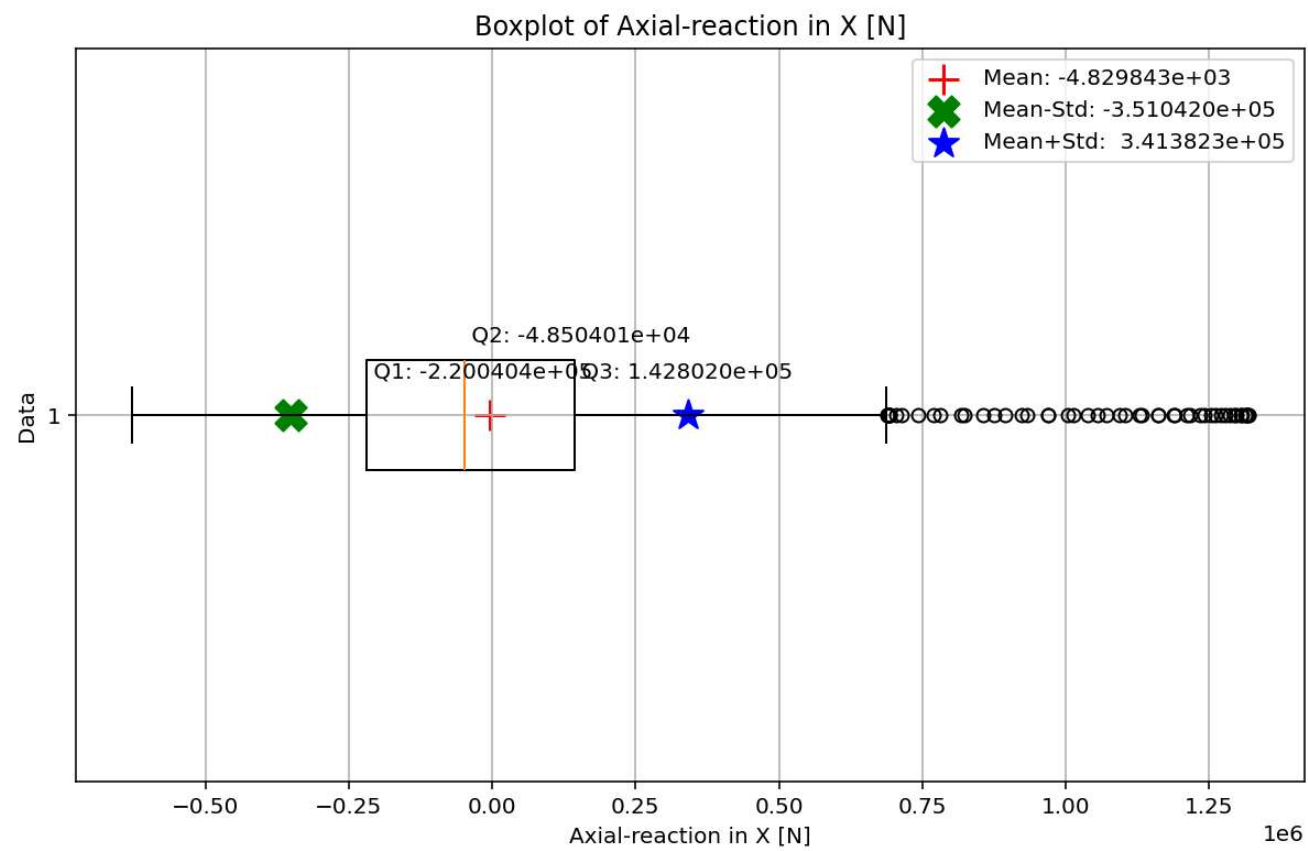


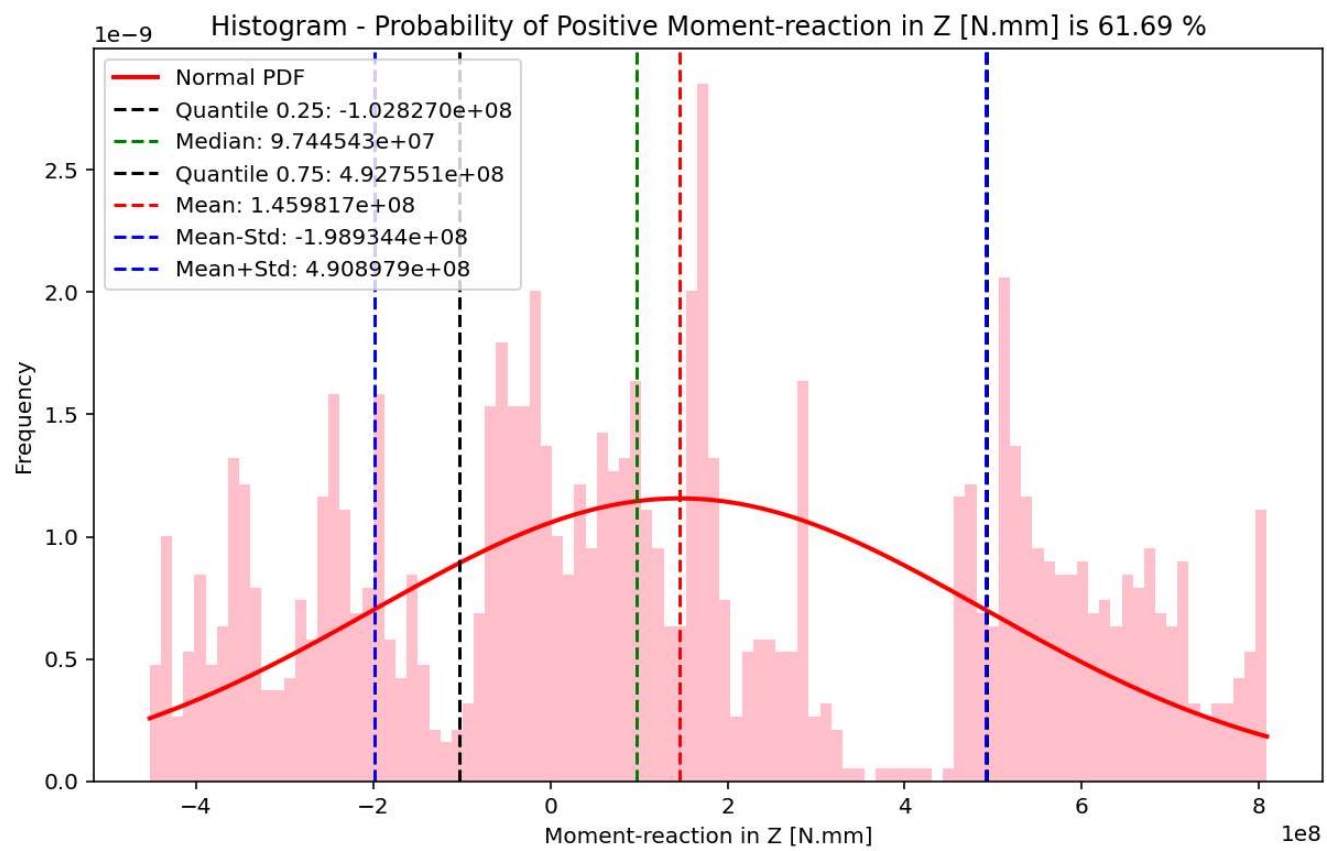


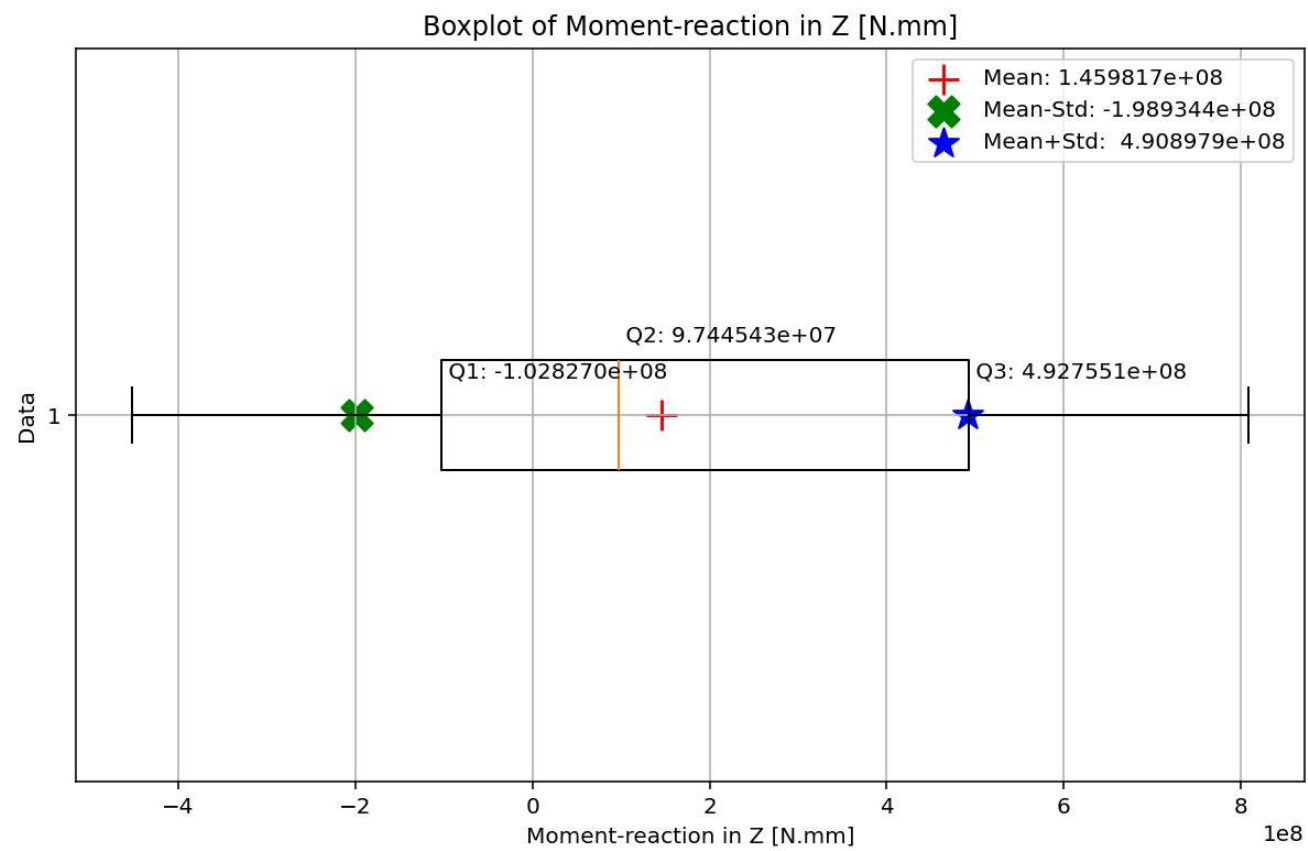


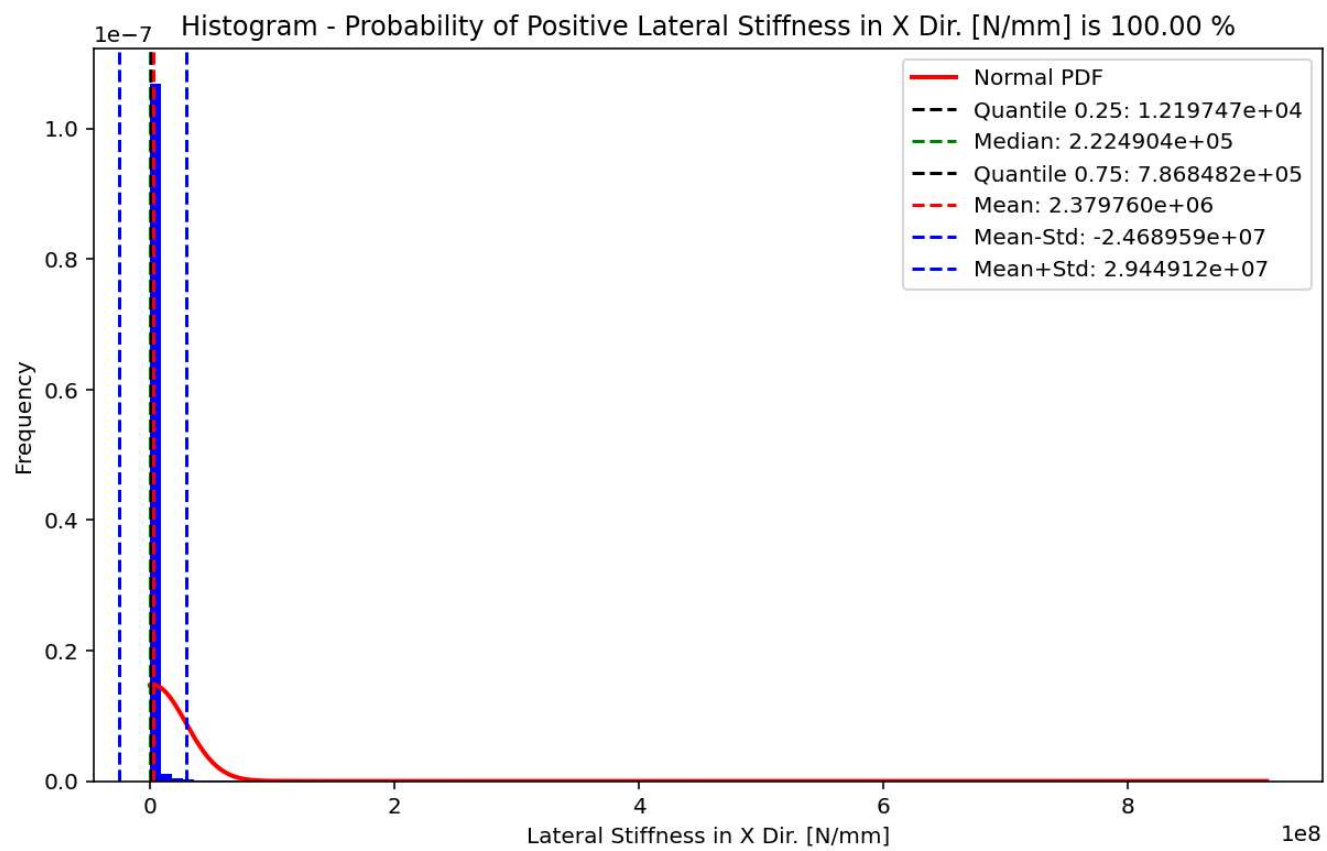




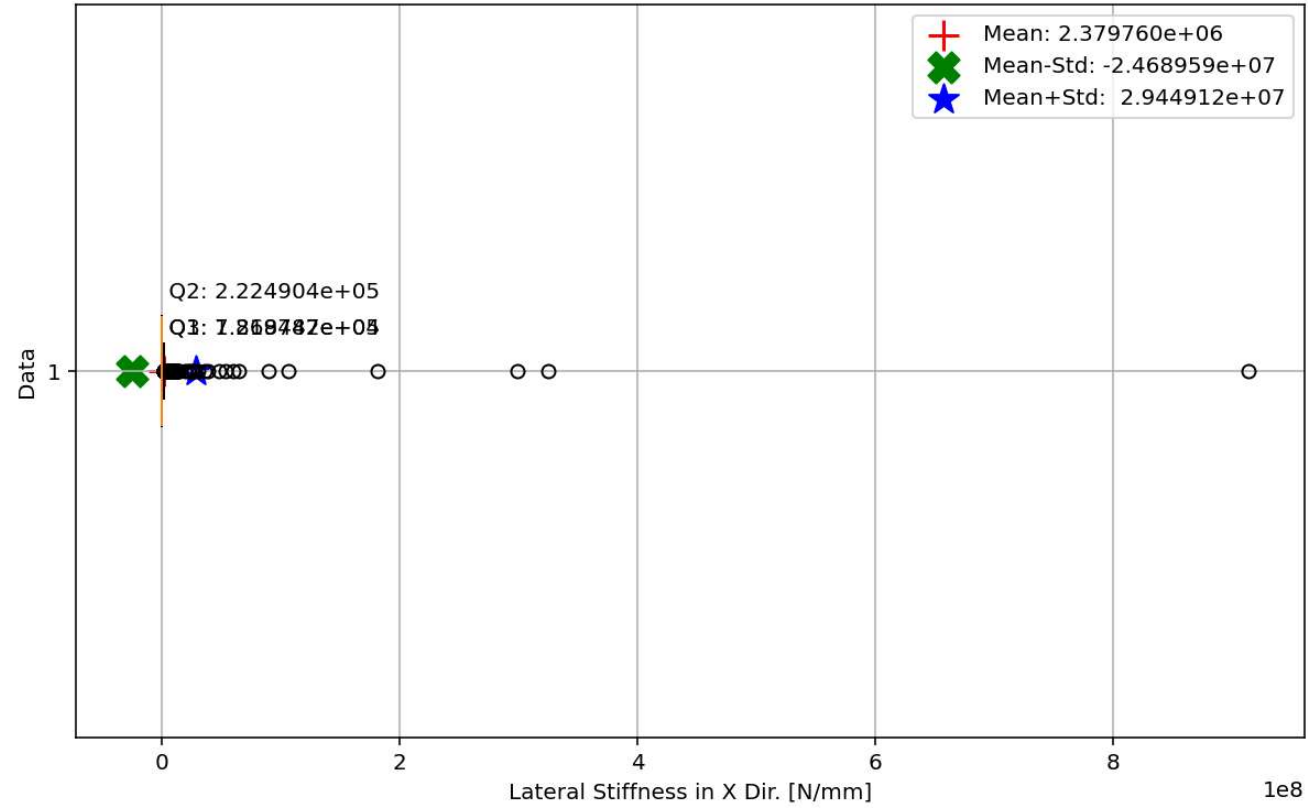


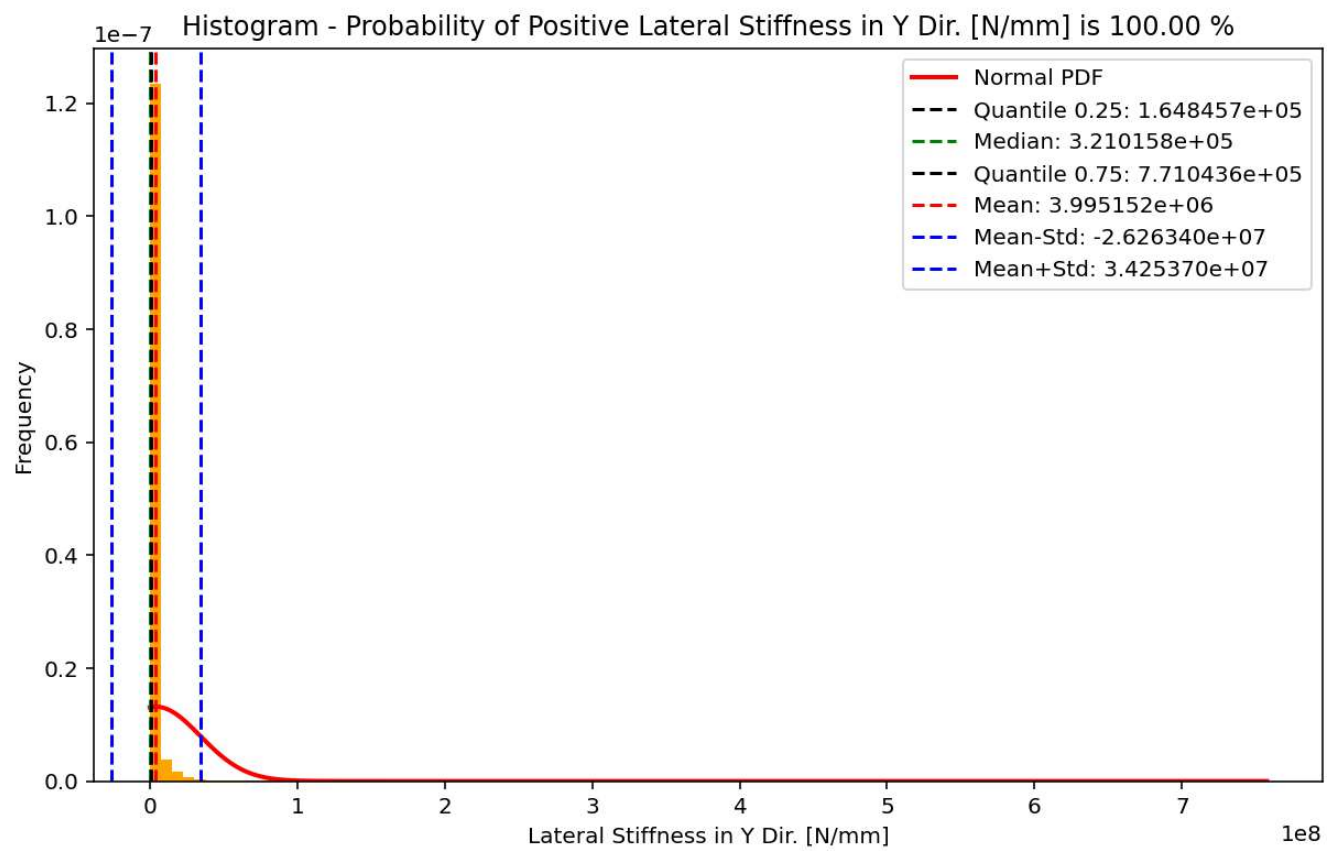




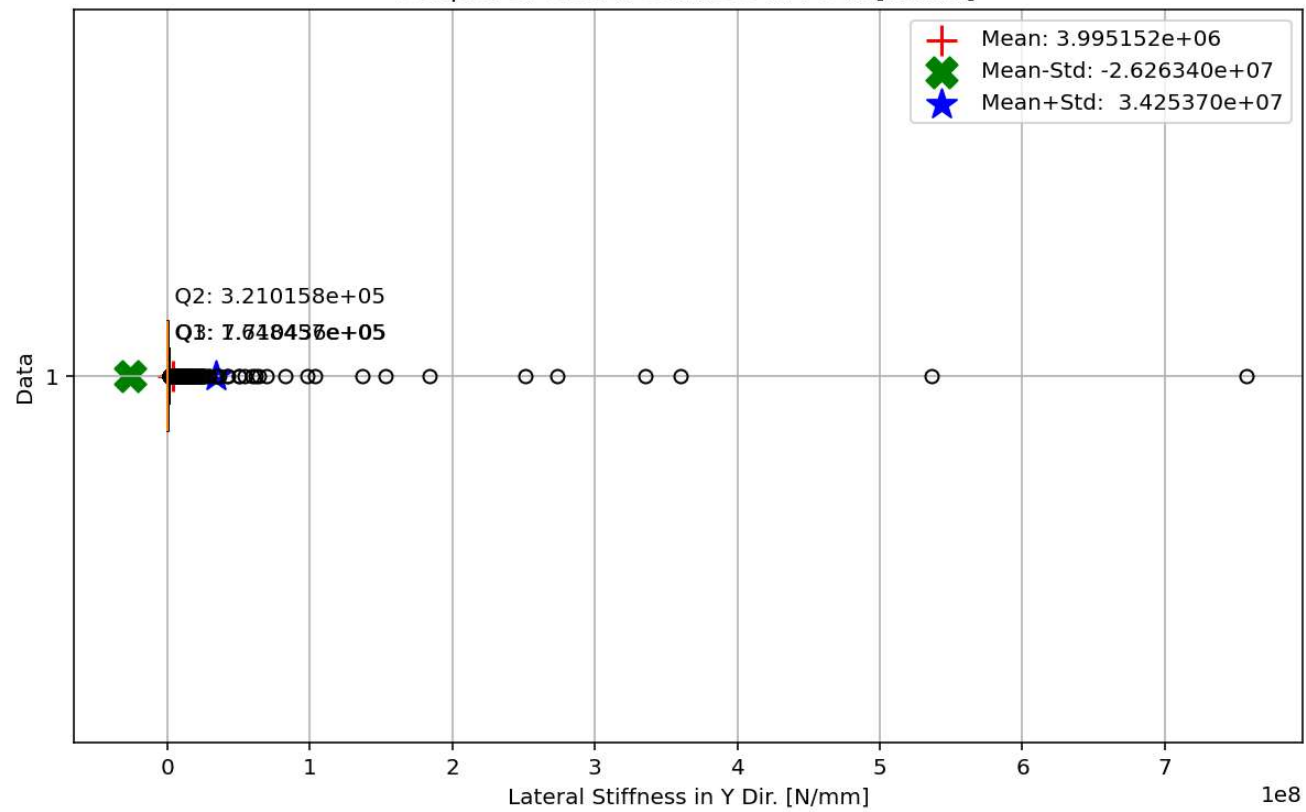


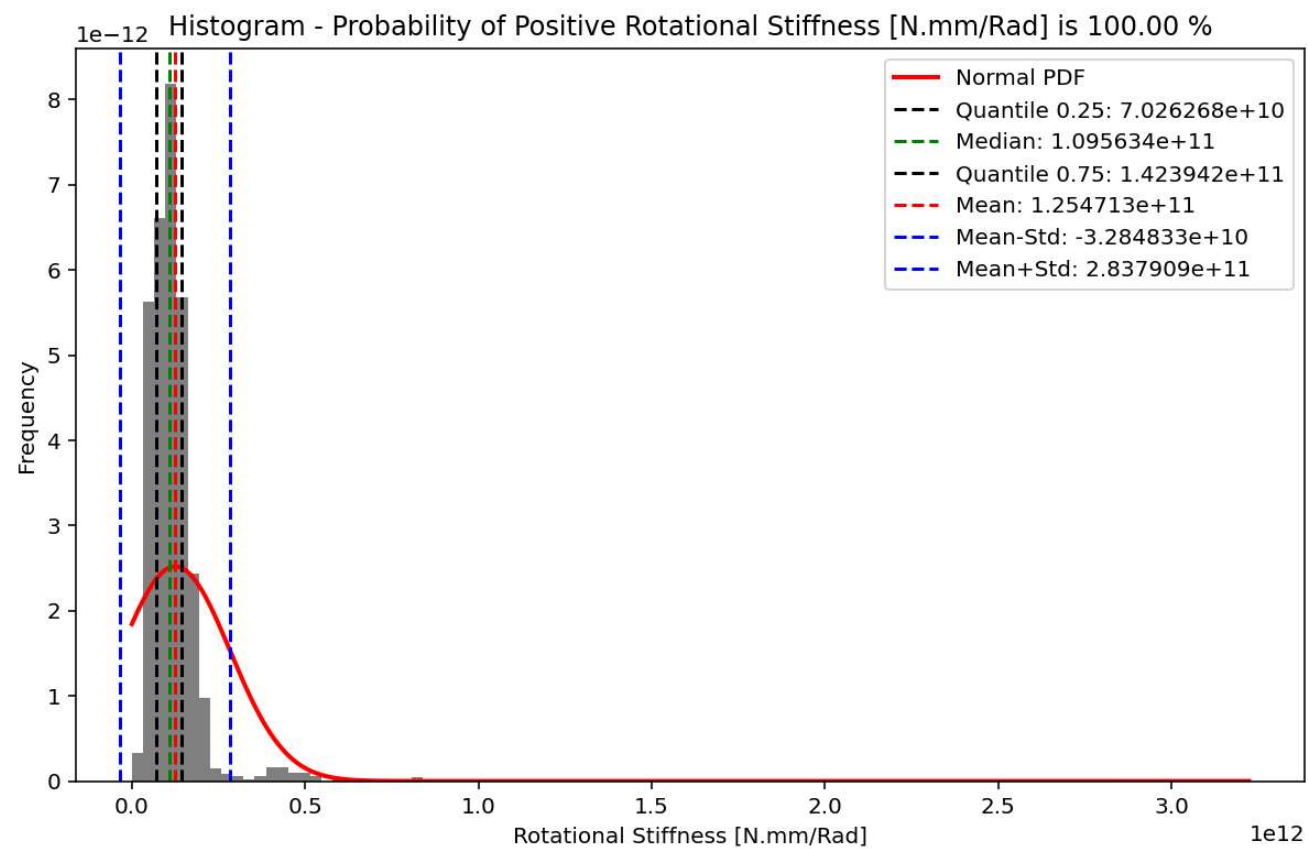
Boxplot of Lateral Stiffness in X Dir. [N/mm]

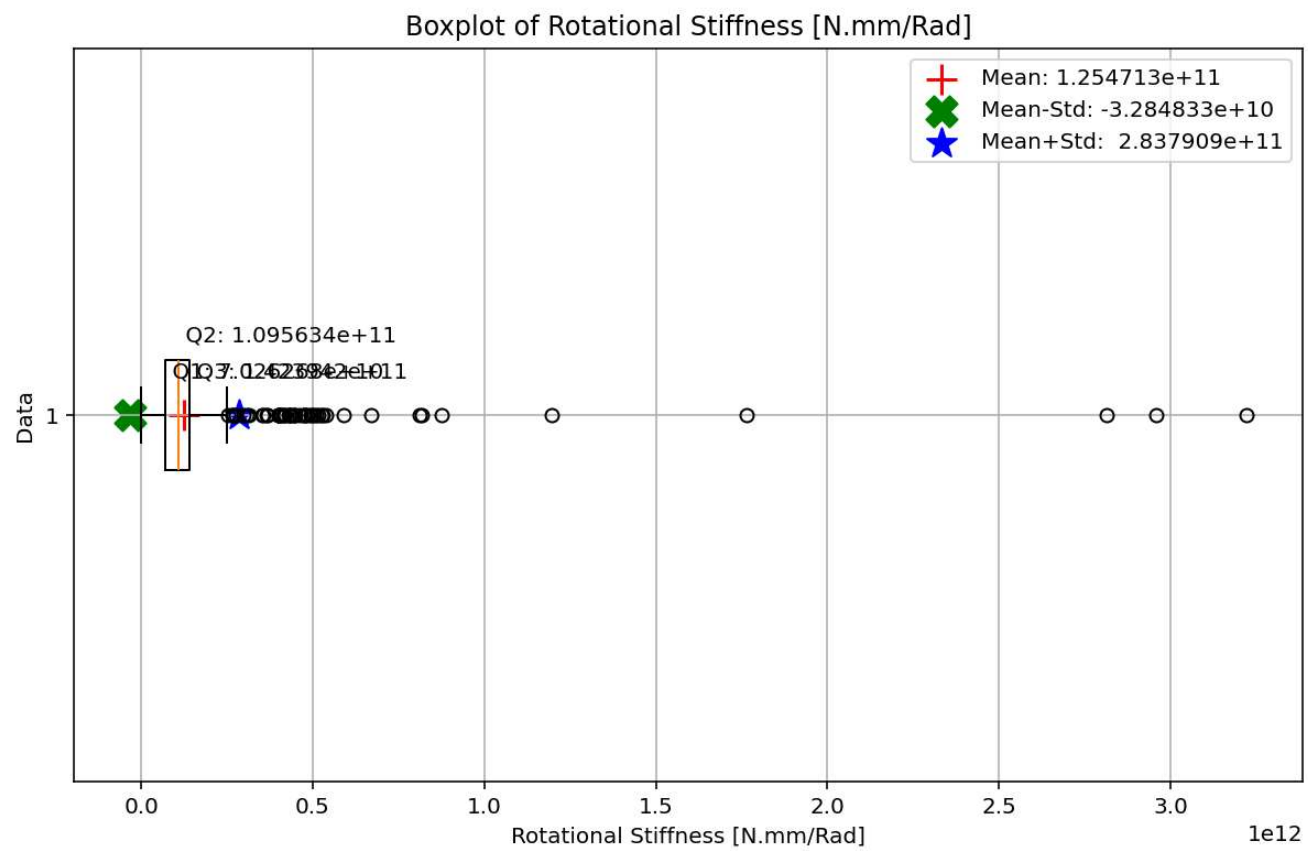




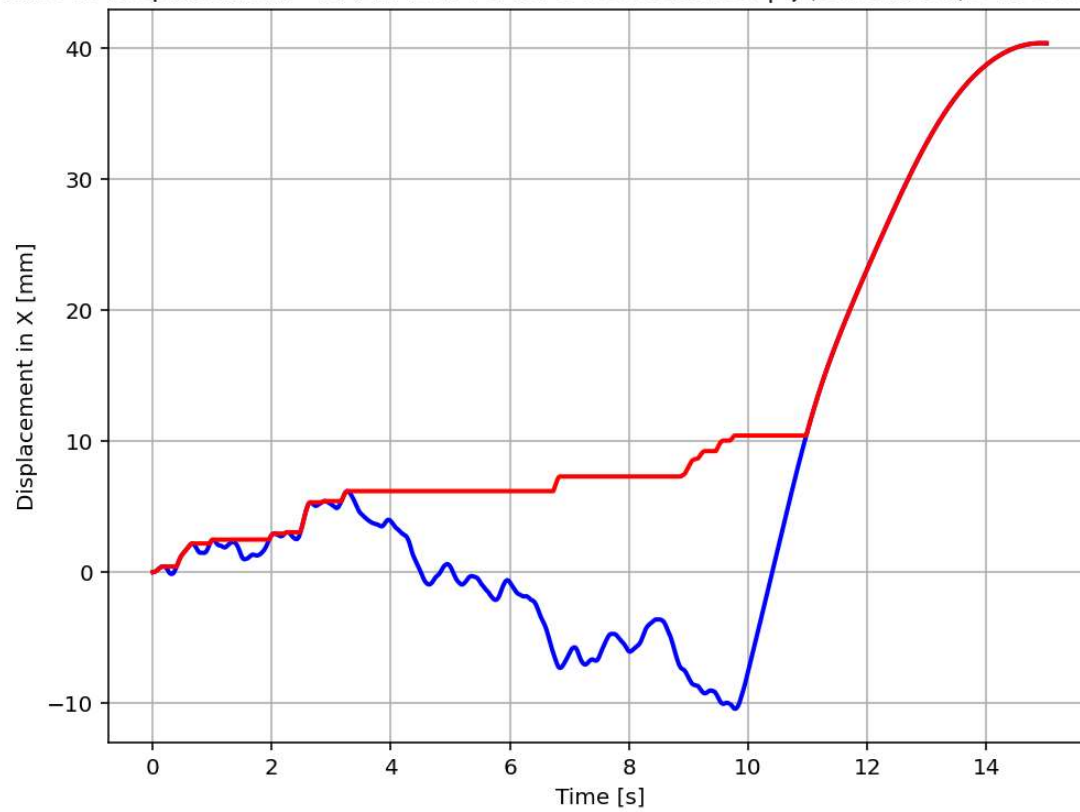
Boxplot of Lateral Stiffness in Y Dir. [N/mm]

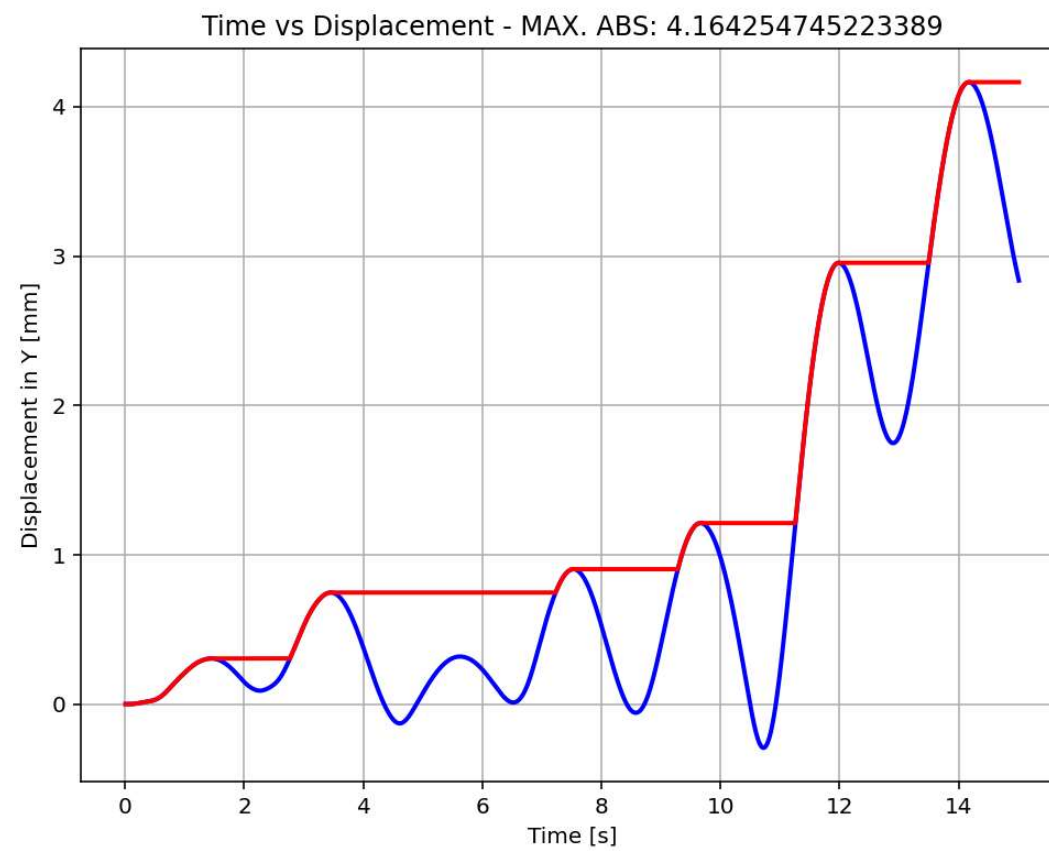


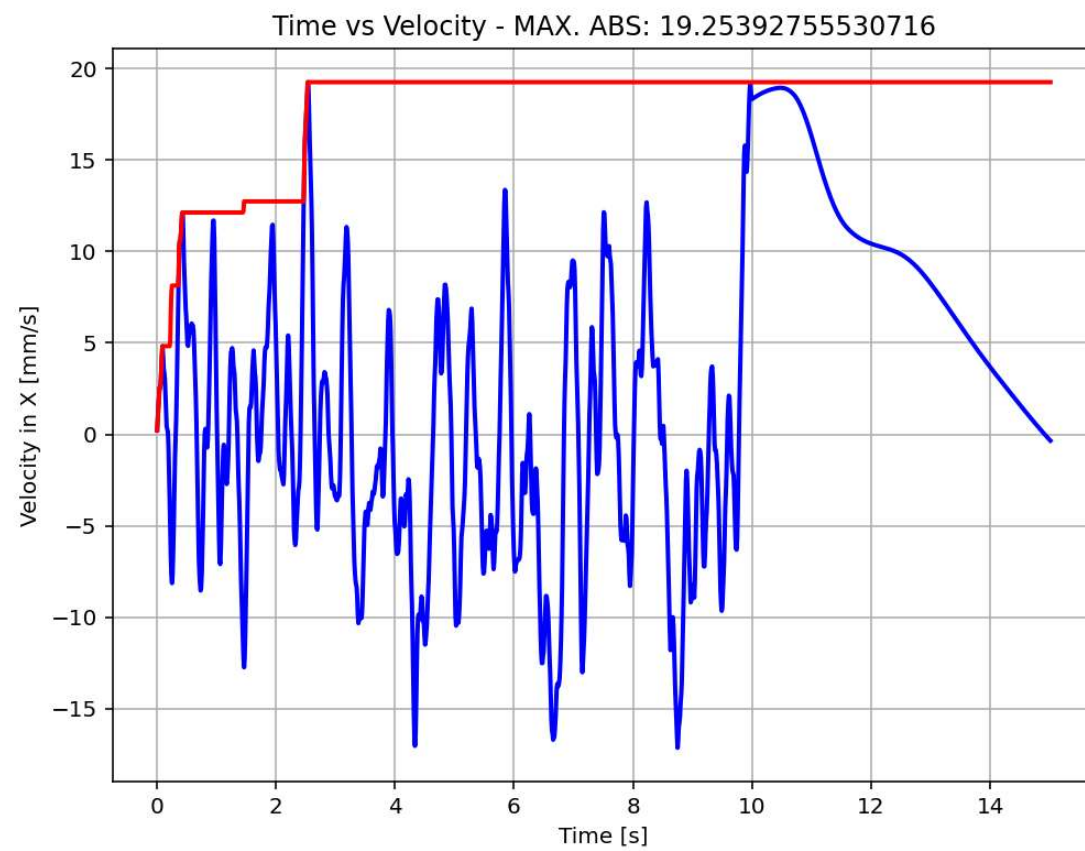




Time vs Displacement - MAX. ABS: 40.407545839972165 | ξ (Calculated): 1.00000e+02 %







Time vs Acceleration - MAX. ABS: 339.7025820125332

