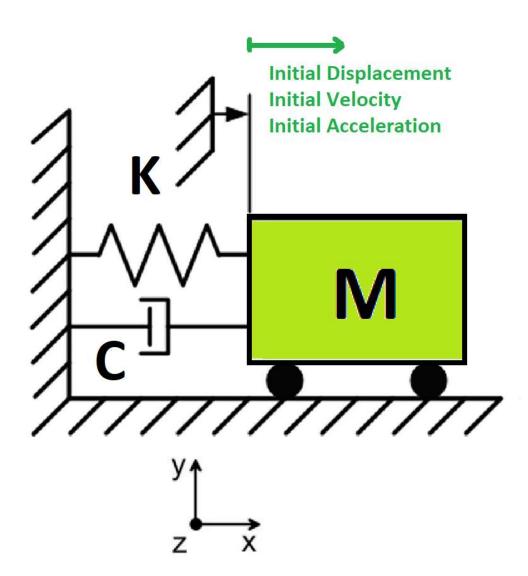
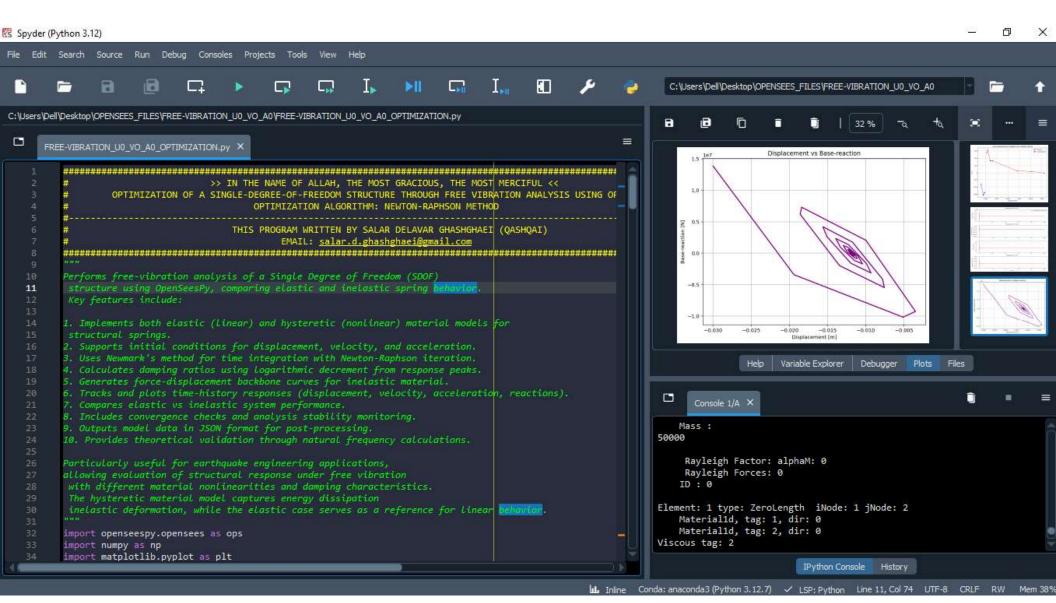
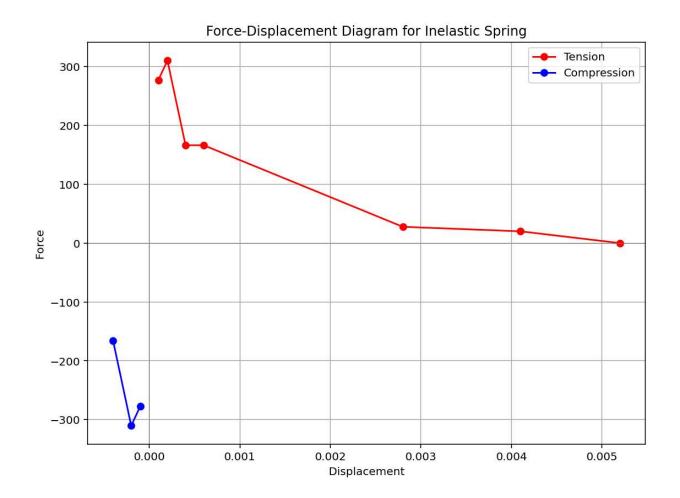
>> IN THE NAME OF ALLAH, THE MOST GRACIOUS, THE MOST MERCIFUL <<

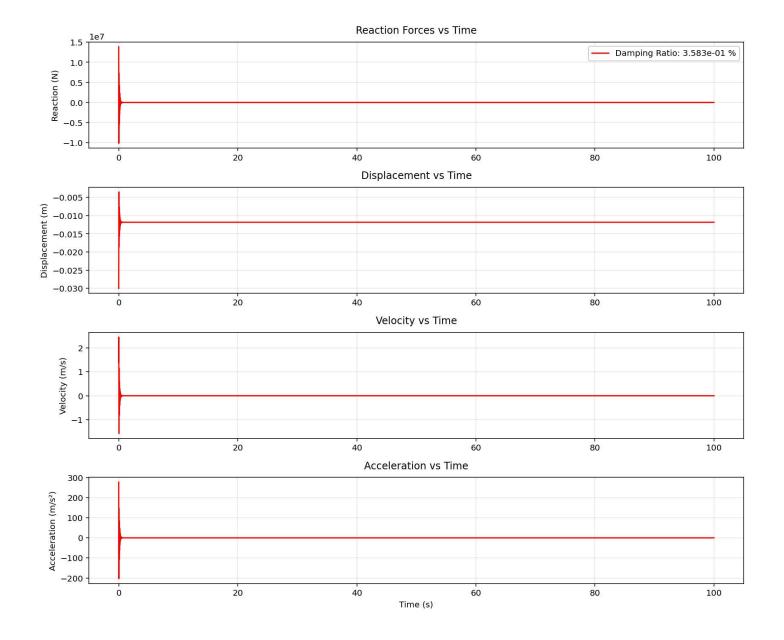
OPTIMIZATION OF A SINGLE-DEGREE-OF-FREEDOM STRUCTURE THROUGH FREE VIBRATION ANALYSIS USING OPENSEES

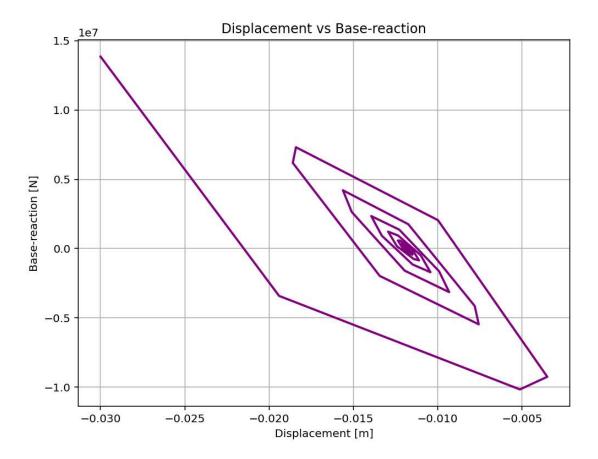
OPTIMIZATION ALGORITHM: NEWTON-RAPHSON METHOD
WRITTEN BY SALAR DELAVAR GHASHGHAEI (QASHQAI)











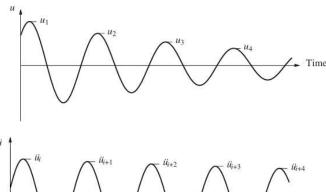
VISCOUSLY DAMPED FREE VIBRATION

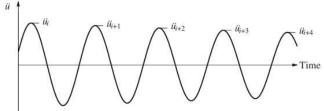
$$m\ddot{u} + c\dot{u} + ku = 0$$

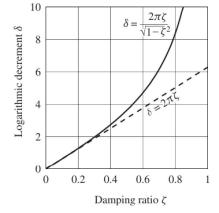
$$\ddot{u} + 2\zeta \omega_n \dot{u} + \omega_n^2 u = 0$$

$$\omega_n = \sqrt{k/m}$$
 $\zeta = \frac{c}{2m\omega_n} = \frac{c}{c_{cr}}$ $\omega_D = \omega_n \sqrt{1 - \zeta^2}$

$$u(t) = e^{-\zeta \omega_n t} \left[u(0) \cos \omega_D t + \frac{\dot{u}(0) + \zeta \omega_n u(0)}{\omega_D} \sin \omega_D t \right]$$







Decay of Motion

$$\delta = \ln \frac{u_i}{u_{i+1}} = 2\pi \zeta$$
 (approximate relation)

$$\delta = \ln \frac{u_i}{u_{i+1}} = \frac{2\pi \, \zeta}{\sqrt{1-\zeta^2}}$$
 (EXACT RELATION)

EXACT AND APPROXIMATE RELATIONS BETWEEN LOGARITHMIC DECREMENT AND DAMPING RATIO

SUPPLY: 0.04384989 F: 0.013849889675598415 Fmin: 0.013849889675612244 Fmax: 0.013849889675584585 DF: -1.3829215550487104e-09 DX: -10014949.600746213 TI: 1 - RESIDUAL: 10014949.600746213 - X: 10015049.600746213 SUPPLY: 0.01695705 F: -0.013042953880630502 Fmin: -0.0130429538806109 Fmax: -0.013042953880650104 DF: -1.9002375278537928-09 DX: 6653761.952466474 IT: 2 - RESIDUAL: 6653761.952466474 - X: 3361287.6482797386 SUPPLY: 0.03822344 F: 0.008223439438450754 Fmin: 0.008223439438471737 Fmiir: 0.008223439438477737 Fmax: 0.0082234394384329778 DF: -2.0979745718463505e-09 DX: -3919704.055904551 IT: 3 - RESIDUAL: 3919704.055904551 - X: 7280991.70418429 SUPPLY: 0.02635108 F: -0.0036489159704923835 Fmin: -0.0036489159704485227 Fmax: -0.0036489159705362477 DF: -4.386248309007357e-09 DX: 831899.088567141 IT: 4 - RESIDUAL: 831899.088567141 - X: 6449092.615617149 SUPPLY: 0.02968185 F: -0.00031814556011616063 Fmin: -0.00031814556007960654 Fmii: -0.00031814556017960654
Fmax: -0.0003181455601527078
DF: -3.655062363883132e-09
DX: 87042.44372404178
IT: 5 - RESIDUAL: 87042.44372404178 - X: 6362050.171893107 SUPPLY: 0.02999714 F: -2.8593443473050317e-06 Fmin: -2.859344311406664e-06 Fmax: -2.859344383206869e-06 DF: -3.593040352066694-06 DF: -3.590010233534002e-09 DX: 796.47247815511 IT: 6 - RESIDUAL: 796.47247815511 - X: 6361253.699414952 SUPPLY: 0.03000000 F: -6.043326949978223e-10 Fmin: -6.042968105079982e-10 Fmax: -6.043685829570933e-10 DF: -3.5886224547532204e-09 DX: 0.16840241697684538 IT: 7 - RESIDUAL: 0.16840241697684538 - X: 6361253.531012535 SUPPLY: 0.03000000 F: 5.608915508810640-14 Fmin: 9.1940422570708-14 Fmax: 2.01644258847544060-14 D: -3.588759271068180-09 DX: -1.58917749199535980-05 III: 8 - RESIDUAL: 1.56177494199535980-05 - X: 6361253.531028152 SUPPLY: 0.03000000 F: -6.938893903907228e-18 Fmin: 3.5887959271008185e-14 Fmax: -3.589489816491209e-14 DE: -3.5934604 (28779601)356-09
DX: 1.9333011116481393e-09
IT: 9 - RESIDUAL: 1.9333011116481393e-09 - X: 6361253.531028151

Total time (s): 8.3125

Iteration Counts: Convergence Residual: 1.9333011116e-09

Optimum Spring Area: