

Rectifier circuits for electromagnetic energy collection

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2. Wireless power transfer systems
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Energy harvesting is a fundamental technology for *smart environments* and the future of secure and reliable machinery [1, 2].

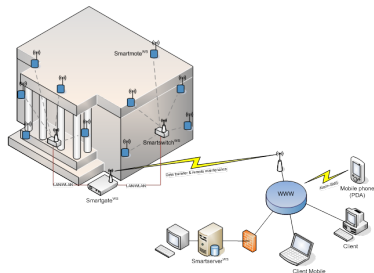
Wireless power transfer (WPT) guarantees energy availability by providing a constant power source [3].

INTRODUCTION

APPLICATIONS

The main applications of WPT are:

- ▶ Wireless sensor networks [4, 5].
 - ▶ RFID [6].
 - ▶ Medicine [4, 6].
 - ▶ Consumer electronics [7].
 - ▶ Automation, enterprise and domestic security.
- Variable monitoring.
 - Structural integrity.
 - Instantaneous variables.



INTRODUCTION

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 - ▶ RFID [6].
 - ▶ Medicine [4, 6].
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 - ▶ Automation, enterprise and domestic security.
- Transportation.
 - Inventory.
 - Localization.
 - Existence.



INTRODUCTION

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 - ▶ RFID [6].
 - ▶ Medicine [4, 6].
 - ▶ Consumer electronics [7].
 - ▶ Automation, enterprise and domestic security.
- People and equipment tracking.
 - patients monitoring and treatment.
 - Control of robotic prosthetics.

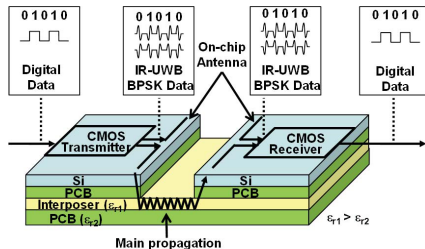


INTRODUCTION

APPLICATIONS

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 - ▶ RFID [6].
 - ▶ Medicine [4, 6].
 - ▶ Consumer electronics [7].
 - ▶ Automation, enterprise and domestic security.
- Short distance fast speed communications.
 - Electrical isolation in power stages.



INTRODUCTION

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- ▶ Automation, enterprise and domestic security.

The internet of things



WIRELESS POWER TRANSFER

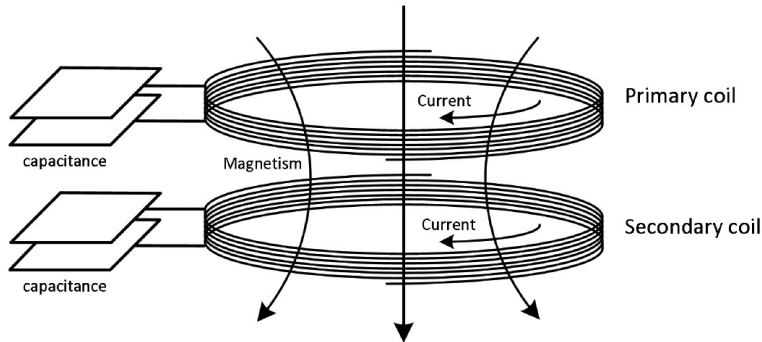
NEAR AND FAR FIELD

Wireless power transfer (WPT) is divided in 2 categories: near-field (inductive) transfer and far-field (electromagnetic) transfer [8].

Near-field is defined as [9]:

$$d < 0.62 \sqrt{\frac{D^3}{\lambda}}$$

d : transmission distance,
 D : maximum transmitter size,
 λ : wavelength.



Near Field power transfer.

WIRELESS POWER TRANSFER

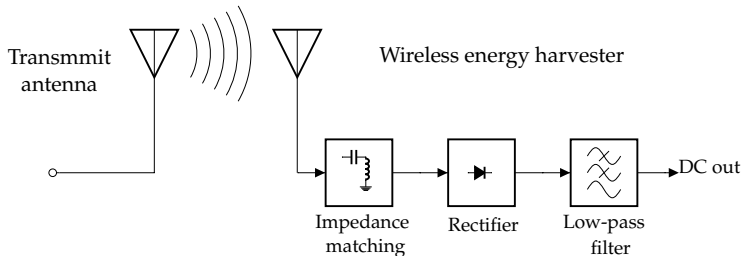
NEAR AND FAR FIELD

Wireless power transfer (WPT) is divided in 2 categories: near-field (inductive) transfer and far-field (electromagnetic) transfer [8].

Far-field is defined as [9]:

$$d > 2 \frac{D^2}{\lambda}$$

d : transmission distance,
 D : maximum transmitter size,
 λ : wavelength.

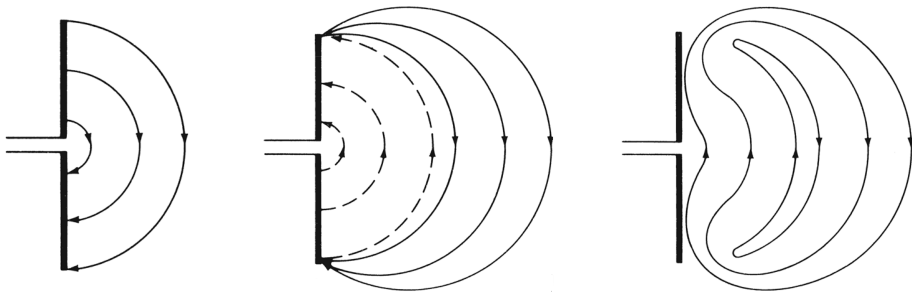


Far Field power transfer.

ANTENNA

RADIATION

Antennas allow the transduction of electric power into electromagnetic waves [9].



The transmission and reception characteristics are equal.

Friis' equation relates the transmitted and received power between 2 antennas.

$$\frac{P_r}{P_t} = e_{cdt}e_{cdr}(1 - |\Gamma_t|^2)(1 - |\Gamma_r|^2) \left(\frac{\lambda}{4 \pi R} \right)^2 D_r(\theta_r, \phi_r) D_t(\theta_t, \phi_t) |\hat{\boldsymbol{\rho}}_w \cdot \hat{\boldsymbol{\rho}}_a|^2$$

Radiation loss is $\propto \frac{1}{R^2}$ and represents the main cause of energy losses.

ANTENNA

FRIIS EQUATION

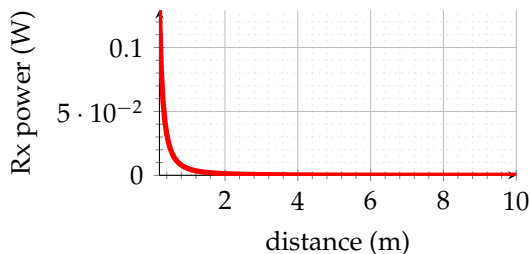
Friis' equation relates the transmitted and received power between 2 antennas.

$$\underbrace{\frac{P_r}{P_t}}_{\text{Tx power}} = \underbrace{e_{cdt}}_{\text{Tx eff}} \underbrace{e_{cdr}}_{\text{Rx eff}} \underbrace{(1 - |\Gamma_t|^2)}_{\text{Tx Z match}} \underbrace{(1 - |\Gamma_r|^2)}_{\text{Rx Z match}} \underbrace{\left(\frac{\lambda}{4\pi R}\right)^2}_{\text{Rad loss}} \underbrace{D_r(\theta_r, \phi_r) D_t(\theta_t, \phi_t)}_{\text{directivity loss/gain}} \underbrace{|\hat{\rho}_w \cdot \hat{\rho}_a|^2}_{\text{polarization loss}}$$

Radiation loss is $\propto \frac{1}{R^2}$ and represents the main cause of energy losses.

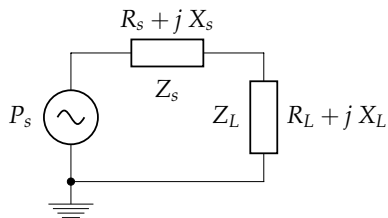
A simplified Friis' equation for practical purposes is:

$$P_r = EIRP_t e_{cdr} (1 - |\Gamma_r|^2) \left(\frac{\lambda}{4 \pi R} \right)^2 D_r(\theta_r, \phi_r) |\hat{\rho}_w \cdot \hat{\rho}_a|^2$$

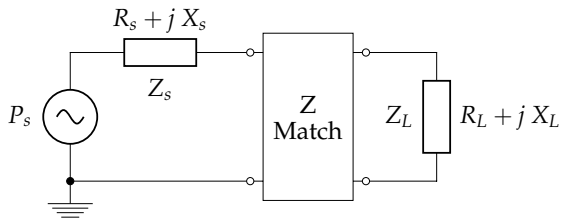


IMPEDANCE MATCHING

Maximum power will be transferred from a source to its load if the **load impedance equals the source impedance** [10].



$$R_s + jX_s = R_L + jX_L$$

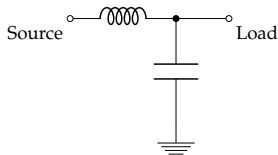


$$R_s + jX_s \neq R_L + jX_L$$

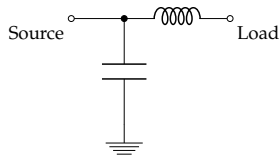
Matching networks are designed for a determined frequency and bandwidth.

IMPEDANCE MATCHING

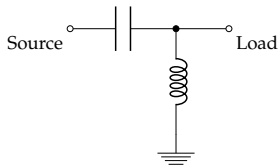
For low loss in RF harvesting systems the L matching network is the adequate choice [11].



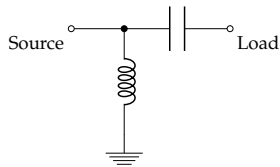
a) Low-pass, Higher Z



b) Low pass, Lower Z up



c) High pass, Higher Z



d) High pass, Lower Z

$$Q_s = Q_p = \sqrt{\frac{R_p}{R_s} - 1}$$

$$Q_s = \frac{X_s}{R_s}$$

$$Q_p = \frac{R_p}{X_p}$$

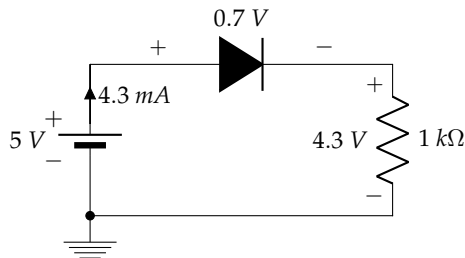
Subindex p represents parallel component and subindex s represents series component.

RECTIFIERS

DC NONLINEARITIES

Nonlinearities represents the main problem when analyzing rectifier circuits.

A basic analysis assumes a constant V_{th} .



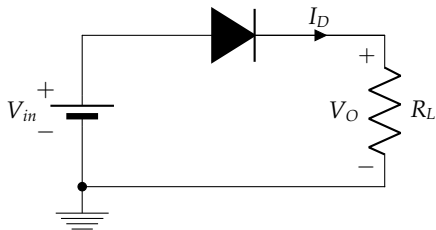
$$V_R = V_{in} - V_D$$

$$I = \frac{V_R}{R}$$

RECTIFIERS

DC NONLINEARITIES

A better approach would consider the diode current-voltage relationship.



$$I_D = I_S \left(e^{\frac{V_D}{n \frac{kT}{q}}} - 1 \right)$$

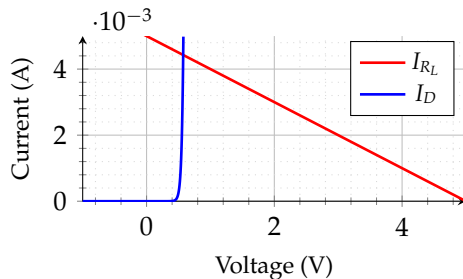
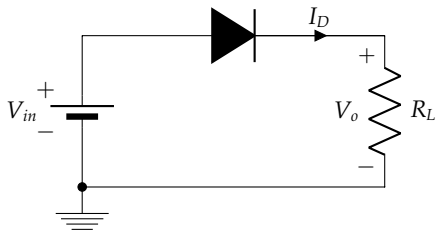
where:

- V_D diode voltage (V),
- I_D diode current (A),
- I_S diode saturation current (A),
- n ideality factor 1 - 2,
- k Boltzmann constant,
- T temperature (K),
- q electron charge

RECTIFIERS

DC NONLINEARITIES

The solution may be found with any numerical method.



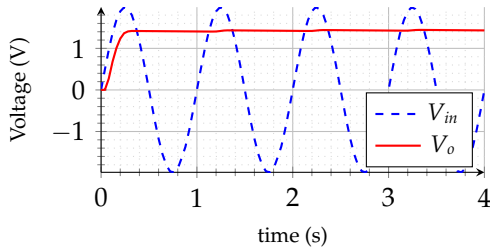
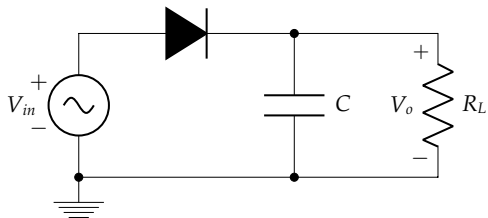
$$I_{R_L} = \frac{V_{in}}{R_L} - \frac{V_o}{R_L} = I_D = I_S \left(e^{\frac{V_{in} - V_o}{n \frac{kT}{q}}} - 1 \right)$$

A closed form solution is also possible [12].

RECTIFIERS

AC NONLINEARITIES

Considering an AC input requires frequency response considerations.



$$I_D \left(V_{in}(t) - V_o(t) \right) = C \frac{dV_o(t)}{dt} + \frac{V_o(t)}{R_L}$$

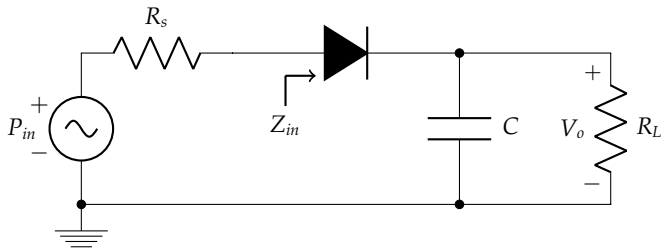
y

$$V_{in}(t) = V_p \sin(\omega t + \phi)$$

RECTIFIERS

AC NONLINEARITIES

A non-controlled power input complicates the problem even further.



$$I_D \left(V_{in}(t) - V_o(t) \right) = C \frac{dV_o(t)}{dt} + \frac{V_o(t)}{R_L}$$

y

$$V_{in}(t) = V_p \sin(\omega t + \phi), \quad V_p = 2 \sqrt{2 R_s P_{in}} \frac{Z_{in}}{R_s + Z_{in}}$$

SPICE is the preeminent electronic circuit simulator. The analysis types for RF rectifiers are:

Time domain:

- ▶ Transient
 - ▶ AC
 - ▶ Harmonic Balance
 - ▶ Shooting Methods
- ▶ Uses the **Modified Nodal Analysis** method.
 - ▶ Provides the complete time-domain response of the circuit.
 - ▶ May be used to optimize the desired system response.
 - ▶ Computationally heavy for circuits with long stabilization periods.

SPICE is the preeminent electronic circuit simulator. The analysis types for RF rectifiers are:

► Transient

Frequency domain:

► AC

► Calculates the frequency response of the system.

► Harmonic Balance

► May be used to calculate the steady state linear transfer parameters (Z, Y, H, S).

► Shooting Methods

► Useful for obtaining the bandwidth of the system.

SPICE is the preeminent electronic circuit simulator. The analysis types for RF rectifiers are:

Frequency/Time domain:

- ▶ Transient
 - ▶ AC
 - ▶ Harmonic Balance
 - ▶ Shooting Methods
- ▶ Calculates the steady state response in the Fourier domain.
 - ▶ Fast, few harmonics provide a good approximation of the response.
 - ▶ Limited to sine signals (single or multi tone) and periodic responses.
 - ▶ Time to reach steady state not available.

SPICE is the preeminent electronic circuit simulator. The analysis types for RF rectifiers are:

► Transient

► AC

► Harmonic Balance

► Shooting Methods

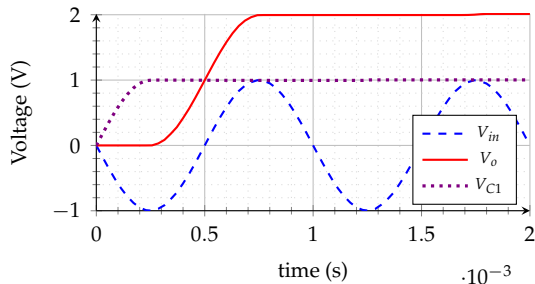
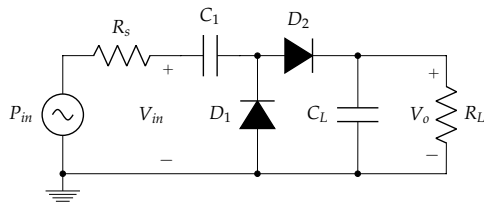
Time domain:

- *Shoots* a prediction of the steady-state conditions of the circuit and iterates.
- In practice is very similar to harmonic balance.

RECTIFIERS

HALF-WAVE VOLTAGE DOUBLER

The half-wave voltage doubler is the most ubiquitous type of RF rectifier.



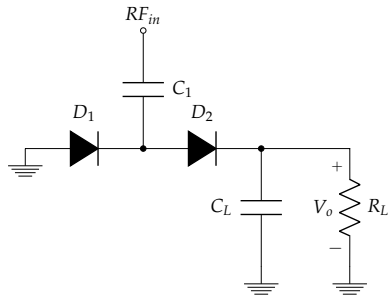
$$V_o = 2 V_{in} - V_{th1} - V_{th2}$$

Also known as the Greinacher multiplier, is mostly used in cases where information from the RF signal should be extracted.

RECTIFIERS

HALF-WAVE VOLTAGE DOUBLER

The half-wave voltage doubler is the most ubiquitous type of RF rectifier.



- ▶ Blocks DC components due to C_1
- ▶ Preserves the same GND terminal as the source, even for multiple stages.
- ▶ Ideal response time $\frac{3}{4}T$.

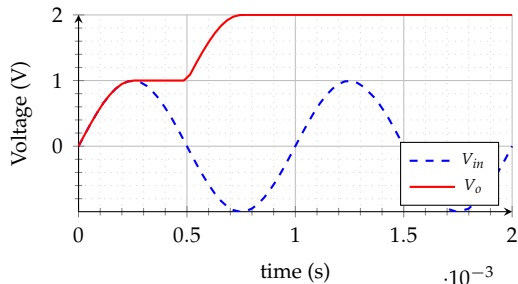
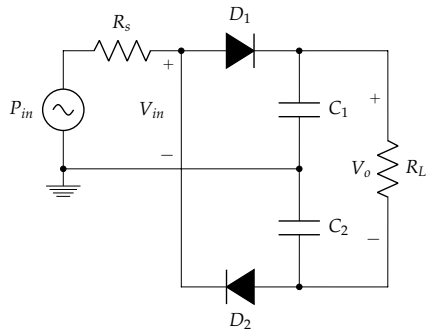
$$V_o = 2 V_{in} - V_{th1} - V_{th2}$$

Also known as the Greinacher multiplier, is mostly used in cases where information from the RF signal should be extracted.

RECTIFIERS

FULL-WAVE VOLTAGE DOUBLER

The full-wave voltage doubler is an alternative to the half-wave doubler.



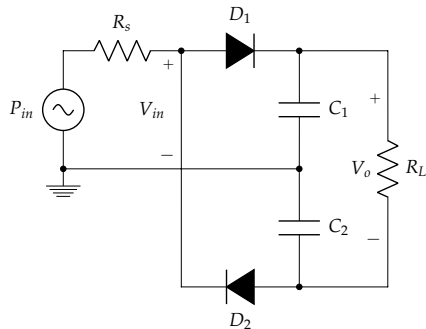
$$V_o = 2 V_{in} - V_{th1} - V_{th2}$$

In practice, this architecture has a smaller stabilization period compared to the half-wave doubler.

RECTIFIERS

FULL-WAVE VOLTAGE DOUBLER

The full-wave voltage doubler is an alternative to the half-wave doubler.



- ▶ DC components are not blocked
- ▶ GND terminal from source is changed in the output
- ▶ Ideal response time $\frac{3}{4}T$.

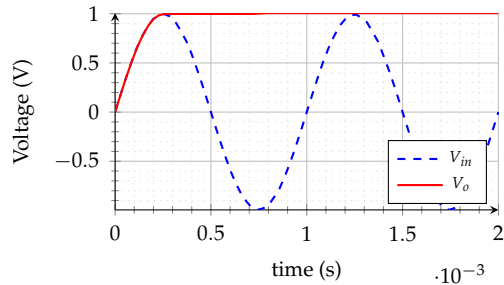
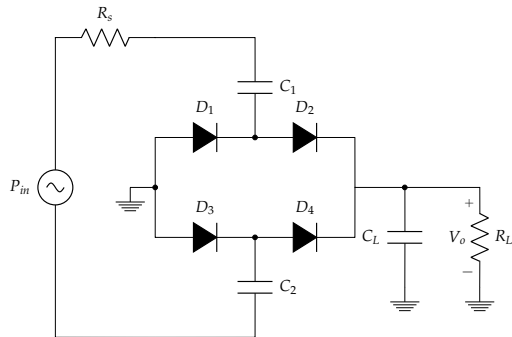
$$V_o = 2 V_{in} - V_{th1} - V_{th2}$$

In practice, this architecture has a smaller stabilization period compared to the half-wave doubler.

RECTIFIERS

VOLTAGE MULTIPLYING BRIDGE

The voltage multiplying bridge is mostly used in RFID applications.

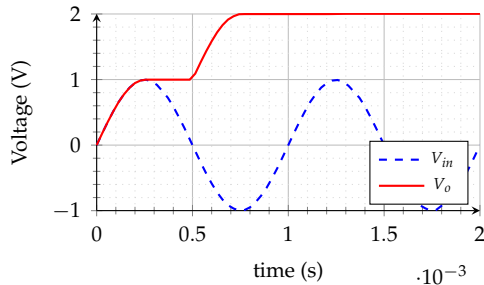
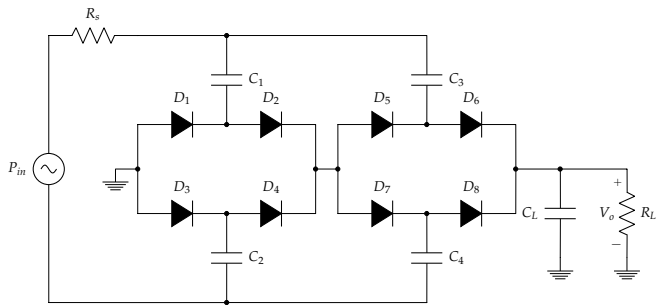


The “modular” characteristics makes it a versatile rectifier.

RECTIFIERS

VOLTAGE MULTIPLYING BRIDGE

Multiple stages are required for voltage multiplication.

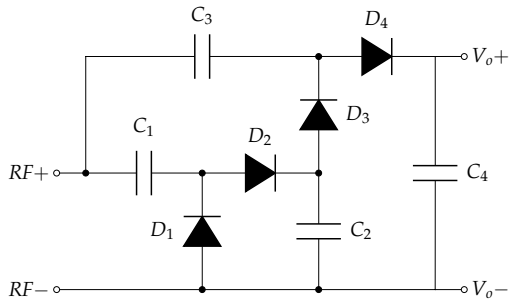


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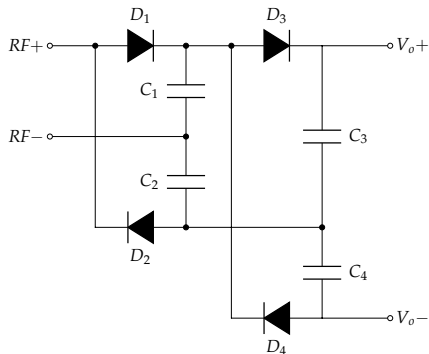
RECTIFIERS

MULTIPLE STAGES

Generally multiple stages are required to achieve useful power levels.



2 stage half-wave voltage multiplier.

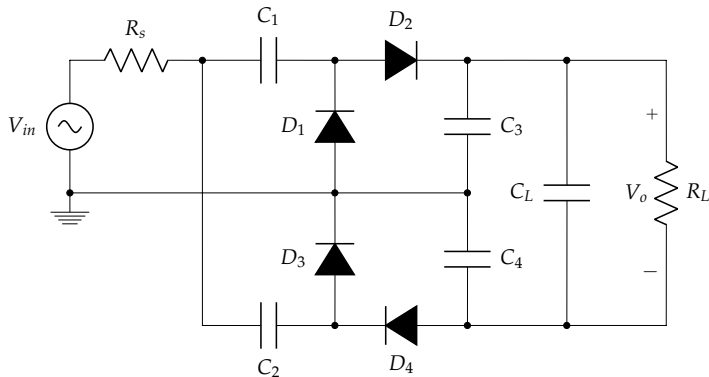


2 stage full-wave voltage multiplier.

RECTIFIERS

MIRROR-STACKED

The *mirror-stacked* configuration is an alternative to multi-staging rectifiers.



It can be used with multiple stages for additional voltage increase.

The two main parameters to measure the performance of a rectifier are:

Efficiency:

Is defined as the ratio of RMS AC input power and the DC power absorbed by the load.

$$\eta = \frac{P_{L,DC}}{P_{in,RMS}} = \frac{I_o \cdot V_o}{V_{in,rms} \cdot I_{in,rms}}$$

Transient values may be neglected depending on application.

Sensitivity:

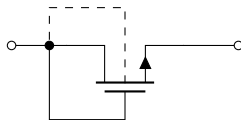
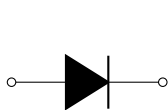
The minimum input power required to obtain a desired voltage/current output.

RECTIFIER

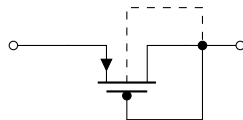
DIODE CONNECTED TRANSISTORS

The main source of energy losses in RF rectifiers is the threshold voltage of the active elements.

A threshold voltage (V_{th}) compensation is possible when MOS transistors are used as rectifiers.



NMOS



PMOS

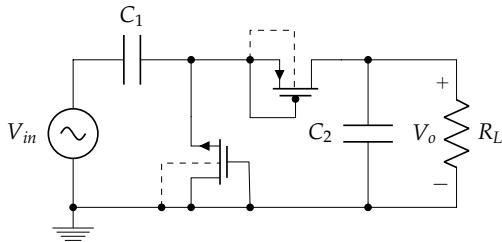
Diode-connected transistors.

The available power is in the range of -20 dBm to 0 dBm ($10\text{ }\mu\text{W}$ to 1 mW).

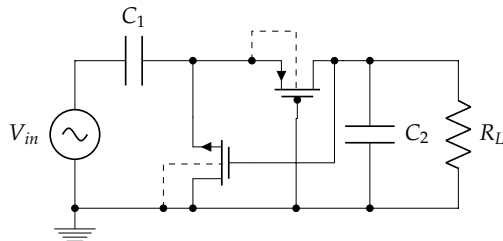
RECTIFIER

THRESHOLD VOLTAGE COMPENSATION

Self- V_{th} cancelation (SVC) scheme [13] is effective for low input power applications (≈ -10 dBm).



Rectifier without compensation.



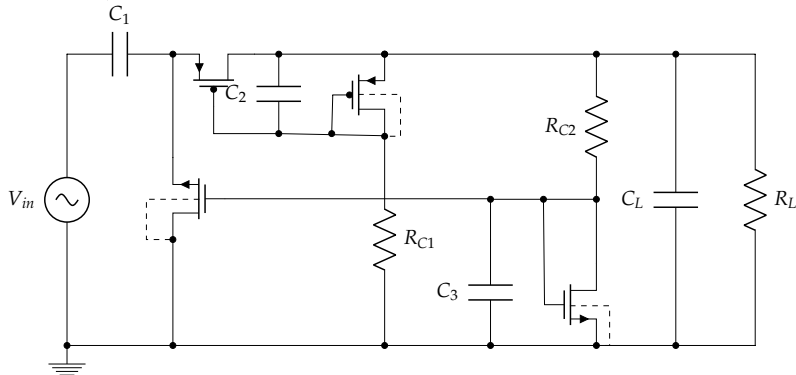
Rectifier with SVC scheme.

The main purpose is to maintain the gates of PMOS and NMOS transistors to the lowest and highest (respectively) voltage available.

RECTIFIERS

THRESHOLD VOLTAGE COMPENSATION

Internal V_{th} cancellation scheme (IVC) [14] is effective for medium to large power inputs ($\approx -3 \text{ dBm}$).

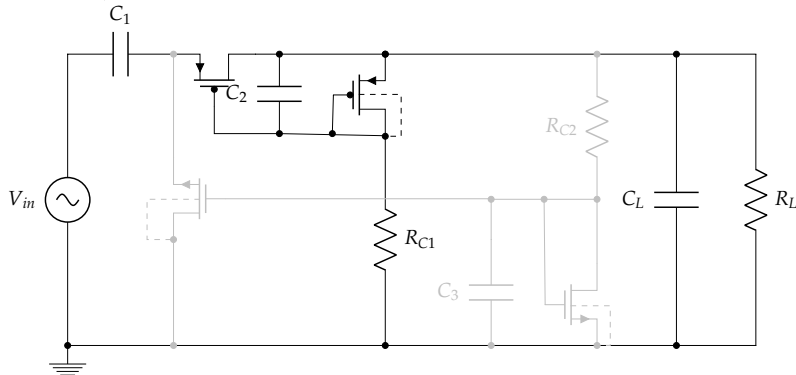


Resistors R_{C1} and R_{C2} are set at a high value (tens of $k\Omega$) to reduce losses.

RECTIFIERS

THRESHOLD VOLTAGE COMPENSATION

Internal V_{th} cancellation scheme (IVC) [14] is effective for medium to large power inputs ($\approx -3 \text{ dBm}$).

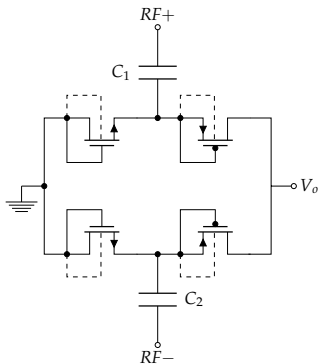


Resistors R_{C1} and R_{C2} are set at a high value (tens of $k\Omega$) to reduce losses.

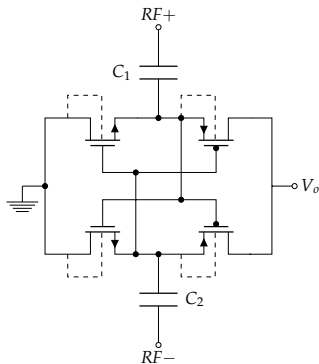
RECTIFIERS

THRESHOLD VOLTAGE COMPENSATION

The differential drive CMOS rectifier [15] is widely regarded as one of the most advanced rectifiers.



Without compensation

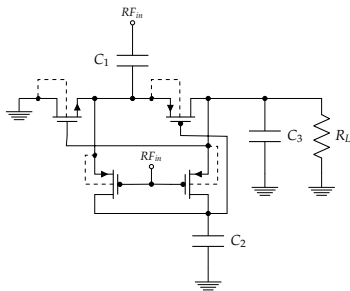


V_{th} compensated.

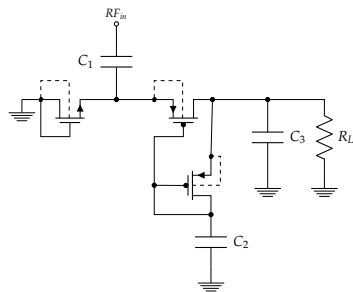
RECTIFIERS

LEAKAGE CURRENT COMPENSATION

Other techniques to increase the efficiency of rectifiers involve the reduction of the leakage current.



Threshold voltage and leakage current compensation [16].



Leakage current compensation [17].

DESIGN CONSIDERATIONS

ANTENNA

Operation frequency

- ▶ UHF band 850 *MHz* ($\lambda \approx 0.3527 \text{ m}$) [13, 14].
- ▶ ISM 433 *MHz*, 2.4 *GHz* and 5 *GHz*.

Antenna type

For WSN it is recommended to consider omni-directional antennas for Tx and directive antennas for Rx.



If the antenna is used below its resonant frequency the inductive effect may be used to ease impedance matching.

DESIGN CONSIDERATIONS

OPERATION MODE

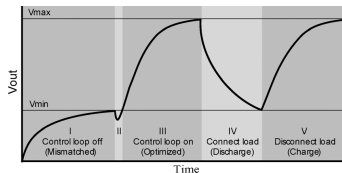
In general WPT may operate in 2 different modes [18]:

Continuous mode (duplex):

The system is design to maximize efficiency in **steady-state**. In general, the period to achieve steady state may be relatively large.

Charge-burst mode (sequential):

The system is optimized to reduce the **transient response** and only provide power to the load for a very short time [19].



REFERENCES I

- [1] D. P. Harrop and M. R. Das, *Energy Harvesting and Storage for Electronic Devices 2011-2021*. IDTechEx, 2011.
- [2] C. Ó. Mathúna, T. O'Donnell, R. V. Martinez-Catala, J. Rohan, and B. O'Flynn, "Energy scavenging for long-term deployable wireless sensor networks," *Talanta*, vol. 75, pp. 613–623, may 2008.
- [3] G. Papotto, F. Carrara, and G. Palmisano, "A 90-nm CMOS threshold-compensated RF energy harvester," *IEEE Journal of Solid-State Circuits*, vol. 46, pp. 1985–1997, Sept 2011.
- [4] I. Akyildiz, W. Su, Y. Sankarasubramaniam, and E. Cayirci, "Wireless sensor networks: a survey," *Computer Networks*, vol. 38, no. 4, pp. 393 – 422, 2002.
- [5] W. C. Wilson and P. D. Juarez, "Emerging needs for pervasive passive wireless sensor networks on aerospace vehicles," in *International Conference on Emerging Ubiquitous Systems and Pervasive Networks*, vol. 37, pp. 101 – 108, 2014.
- [6] M. M. Aung, Y. S. Chang, and J.-U. Won, "Emerging RFID/USN applications and challenges," *International Journal of RFID Security and Cryptography*, vol. 1, no. 1 - 4, pp. 3 – 8, 2012.
- [7] K. Oh, S. Sankaran, H.-T. Wu, J.-J. Lin, M. Hwang, and K. Kenneth, "Full-duplex crystalless CMOS transceiver with an on-chip antenna for wireless communication in a hybrid engine controller board," *Solid-State Circuits, IEEE Journal of*, vol. 48, pp. 1327–1342, June 2013.

REFERENCES II

- [8] X. Lu, P. Wang, D. Niyato, D. I. Kim, and Z. Han, “Wireless charging technologies: Fundamentals, standards, and network applications,” *IEEE Communications Surveys & Tutorials*, vol. 18, no. 2, pp. 1413–1452, 2016.
- [9] C. A. Balanis, *Antenna Theory: Analysis and Design*. Wiley, 4 ed., 2016.
- [10] C. Bowick, *RF Circuit Design*. Elsevier Science, 2011.
- [11] Z. Hameed and K. Moez, “Design of impedance matching circuits for RF energy harvesting systems,” *Microelectronics Journal*, vol. 62, pp. 49–56, apr 2017.
- [12] Y. Wu, J. Linnartz, H. Gao, M. K. Matters-Kammerer, and P. Baltus, “Modeling of RF energy scavenging for batteryless wireless sensors with low input power,” in *2013 IEEE 24th Annual International Symposium on Personal, Indoor, and Mobile Radio Communications (PIMRC)*, pp. 527–531, Sept 2013.
- [13] K. Kotani and T. Ito, “High efficiency CMOS rectifier circuit with self-V_{th}-cancellation and power regulation functions for UHF RFIDs,” in *2007 IEEE Asian Solid-State Circuits Conference*, pp. 119–122, Nov 2007.

REFERENCES III

- [14] H. Nakamoto, D. Yamazaki, T. Yamamoto, H. Kurata, S. Yamada, K. Mukaida, T. Ninomiya, T. Ohkawa, S. Masui, and K. Gotoh, "A passive UHF RF identification CMOS tag IC using ferroelectric RAM in 0.35- μm technology," *IEEE Journal of Solid-State Circuits*, vol. 42, pp. 101–110, jan 2007.
- [15] K. Kotani, A. Sasaki, and T. Ito, "High-efficiency differential-drive CMOS rectifier for UHF RFIDs," *IEEE Journal of Solid-State Circuits*, vol. 44, pp. 3011–3018, nov 2009.
- [16] M. Rastmanesh and E. El-Masry, "A high efficiency 90-nm CMOSRF to DC rectifier," in *2013 IEEE 56th International Midwest Symposium on Circuits and Systems (MWSCAS)*, pp. 705–708, Aug 2013.
- [17] S. S. Chouhan and K. Halonen, "Internal V_{th} cancellation scheme for RF to DC rectifiers used in RF energy harvesting," in *2014 21st IEEE International Conference on Electronics, Circuits and Systems (ICECS)*, pp. 235–238, Dec 2014.
- [18] H. Gao, M. Matters-Kammerer, D. Milosevic, and P. G. M. Baltus, *Batteryless mm-Wave Wireless Sensors*. Springer International Publishing, 2018.
- [19] M. Stoopman, S. Keyrouz, H. J. Visser, K. Philips, and W. A. Serdijn, "Co-design of a CMOS rectifier and small loop antenna for highly sensitive RF energy harvesters," *IEEE Journal of Solid-State Circuits*, vol. 49, pp. 622–634, mar 2014.