

Lagrangian techniques and on-axis rotational transform

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Vacuum field energy for coil design

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Outline

- ▶ Second variation of magnetic field action enables to recover Mercier's formula.
- ▶ Second variation - discrete approach - ι as an eigenvalue problem.
- ▶ Coil design - introducing a new penalty: Vacuum field energy \mathcal{E} .
- ▶ Issues encountered in the coil-design problem.

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1. Magnetic field action yields on-axis rotational transform
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Magnetic field line action

- ▶ **Magnetic field line action:** Provided a closed curve \mathcal{C} and \mathbf{A} , with $\mathbf{B} = \nabla \times \mathbf{A}$:

$$\mathcal{S} := \oint_{\mathcal{C}} \mathbf{A} \cdot d\mathbf{l}. \quad (1)$$

- ▶ The first variation with respect to a change in the curve geometry $\delta\mathbf{x}$, is

$$\delta\mathcal{S} = \int_{\mathcal{C}} \mathbf{x}' \times \mathbf{B} \cdot \delta\mathbf{x} dl. \quad (2)$$

- ▶ Stationary integral curves are tangential to the magnetic field.
- ▶ To recover the on-axis ι , the **second** variation of the magnetic action $\delta^2\mathcal{S}$ is needed.

Second variation yields on-axis ι

- ▶ Second variation:

$$\delta^2 \mathcal{S}[\delta \mathbf{x}] = \oint_{\mathcal{C}} \delta(\mathbf{x}' \times \mathbf{B} \cdot \delta \mathbf{x}) d\ell = \oint_{\mathcal{C}} d\ell \delta \mathbf{x} \cdot (\delta \mathbf{x}' \times \mathbf{B} + \mathbf{x}' \times \delta \mathbf{B})$$

- ▶ In tensor form:

$$\delta^2 \mathcal{S} = \oint d\ell \delta \mathbf{x}^i \frac{\delta^2 \mathcal{S}}{\delta \mathbf{x}^i \delta \mathbf{x}^j} \delta \mathbf{x}^j \quad (3)$$

where,

$$\frac{\delta^2 \mathcal{S}}{\delta \mathbf{x}^i \delta \mathbf{x}^j} = \epsilon_{ijk} \mathbf{B}^k + \epsilon_{imk} \mathbf{x}'^m \partial_j \mathbf{B}^k \quad (4)$$

Second variation yields on-axis ι

- ▶ Defining the operator $\overline{\overline{\mathcal{M}}}$:

$$\overline{\overline{\mathcal{M}}} \equiv \frac{\delta^2 \mathcal{S}}{\delta \mathbf{x} \delta \mathbf{x}} = -(\mathbb{I} \times \mathbf{B}) \frac{d}{d\ell} + \mathbf{x} \times (\nabla \mathbf{B})^\top. \quad (5)$$

- ▶ Null eigenvectors are of importance to recover ι :

$$\overline{\overline{\mathcal{M}}} \cdot \mathbf{v} = \mathbf{0}. \quad (6)$$

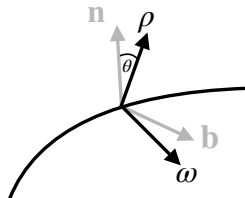
- ▶ For \mathbf{v} to be nontrivial we must have

$$\det(\overline{\overline{\mathcal{M}}}) = 0. \quad (7)$$

The second variation in Mercier coordinates

► Define Mercier coordinates:

- Start from Frenet - Serret frame($\mathbf{t}, \mathbf{n}, \mathbf{b}$)
- Rotation of θ : ($\mathbf{t}, \boldsymbol{\rho}, \boldsymbol{\omega}$)
- $(\rho, \omega = \theta + \int \tau d\ell, \ell)$ is an orthogonal coordinate system



► Useful identities:

$$\mathbb{I} = \boldsymbol{\rho}\boldsymbol{\rho} + \boldsymbol{\omega}\boldsymbol{\omega} + \mathbf{t}\mathbf{t}, \quad \nabla = \boldsymbol{\rho}\partial_{\rho} + \frac{\boldsymbol{\omega}}{\rho}\partial_{\omega} + \frac{\mathbf{t}}{h}\partial_{\ell}$$

$$\boldsymbol{\rho}_{,\omega} = \boldsymbol{\omega}, \quad \boldsymbol{\rho}_{,\ell} = -\mathbf{t} \kappa \cos \theta, \quad \boldsymbol{\omega}_{,\omega} = -\boldsymbol{\rho}, \quad \boldsymbol{\omega}_{,\ell} = \mathbf{t} \kappa \sin \theta$$

$$\nabla \mathbf{t} = \mathbf{t}\mathbf{n}\frac{\kappa}{h}, \quad \nabla \boldsymbol{\rho} = \boldsymbol{\omega}\boldsymbol{\omega}\frac{1}{\rho} - \mathbf{t}\mathbf{t}\frac{\kappa \cos \theta}{h}, \quad \nabla \boldsymbol{\omega} = -\boldsymbol{\omega}\boldsymbol{\rho}\frac{1}{\rho} + \mathbf{t}\mathbf{t}\frac{\kappa \sin \theta}{h}$$

The second variation in Mercier coordinates

- Mercier coordinate system has the metric

$$ds^2 = d\rho^2 + \rho^2 d\omega^2 + h^2 d\ell^2, \quad h = 1 - \kappa\rho \cos \theta, \quad (8)$$

with κ the curvature.

- For the behavior near the magnetic axis: expansion in the parameter $\kappa\rho \ll 1$. To evaluate $\overline{\overline{\mathcal{M}}}$ to lowest order in $\kappa\rho$, we need to expand the magnetic field up to first order.
- We assume

$$\mathbf{B} = B_0(\ell)\mathbf{t} + \rho\mathbf{B}_1, \quad \mathbf{B}_1 = \left(B_1^\rho \boldsymbol{\rho} + B_1^\omega \boldsymbol{\omega} + B_1^t \mathbf{t} \right). \quad (9)$$

The second variation in Mercier coordinates

- Finally, $\overline{\overline{\mathcal{M}}}$ as given by Eq.(5) simplifies to

$$\begin{aligned}\overline{\overline{\mathcal{M}}} &\equiv \overline{\overline{\mathcal{M}}_1} \frac{d}{d\ell} + \overline{\overline{\mathcal{M}}_2} \\ \overline{\overline{\mathcal{M}}_1} &= (\boldsymbol{\rho}\boldsymbol{\omega} - \boldsymbol{\omega}\boldsymbol{\rho})B_0 \\ \overline{\overline{\mathcal{M}}_2} &= \kappa B_0 \mathbf{b}\mathbf{t} + (B_1^\rho \boldsymbol{\omega} - B_1^\omega \boldsymbol{\rho}) \boldsymbol{\rho} \\ &\quad + \boldsymbol{\omega}\boldsymbol{\omega} (\partial_\omega B_1^\rho - B_1^\omega) - \boldsymbol{\omega}\boldsymbol{\rho} (\partial_\omega B_1^\omega + B_1^\rho)\end{aligned}\tag{10}$$

- Remains to enforce constraints from MHD:

$$\nabla \cdot \mathbf{B} = 0 \quad \text{and} \quad \mathbf{J} = \nabla \times \mathbf{B} = J_0(\ell)\mathbf{t}.$$

MHD constraints

- ▶ Using dyadic algebra, we can express $\nabla \cdot \mathbf{B}$ and $\nabla \times \mathbf{B}$ from $\nabla \mathbf{B}$.
- ▶ Leads to the following components for \mathbf{B}_1 :

$$B_1^t = \kappa B_0 \cos \theta, \quad B_1^\rho = -\frac{1}{2}(B_0' + \partial_\omega b_1), \quad B_1^\omega = \frac{1}{2}J_0 + b_1,$$

- ▶ b_1 satisfies Laplace $(\partial_\omega^2 + 4)b_1 = 0$, and from [MEotEC87] it can be expressed as

$$\begin{aligned} b_1 &= b_{c2}(\ell) \cos(2u) + b_{s2}(\ell) \sin(2u), \\ u &= \theta + \delta(\ell) = \omega - \int \tau d\ell + \delta(\ell) \end{aligned} \tag{11}$$

- ▶ We get conditions on b_{c2} and b_{s2} , depending on $\delta(\ell)$ and $\eta(\ell)$ (eccentricity and rotation of flux surfaces).

MHD constraints

- ▶ Now let us solve for null eigenvector $\mathbf{v} = v^t \mathbf{t} + v^\rho \boldsymbol{\rho} + v^\omega \boldsymbol{\omega}$ of $\overline{\overline{\mathcal{M}}}$ such that $\overline{\overline{\mathcal{M}}} \cdot \mathbf{v} = 0$
- ▶ Developing $\overline{\overline{\mathcal{M}}} \cdot \mathbf{v} = 0$ using Eq.(10): only $\boldsymbol{\rho}$ and $\boldsymbol{\omega}$ components with derivatives of v_ρ, v_ω w.r.t. ℓ .
 \implies absorb v_t by redefining v_ρ and v_ω
- ▶ We set $v_t = 0$.
- ▶ Leads to the system:

$$\begin{cases} v'_\omega + \left(\frac{B'_0}{2B_0} - \frac{\partial_\omega b_1}{2B_0} \right) v_\omega - \left(\frac{J_0/2}{B_0} + \frac{b_1}{B_0} \right) v_\rho = 0 \\ v'_\rho + \left(\frac{B'_0}{2B_0} + \frac{\partial_\omega b_1}{2B_0} \right) v_\omega + \left(\frac{J_0/2}{B_0} - \frac{b_1}{B_0} \right) v_\omega = 0 \end{cases} \quad (12)$$

MHD constraints

- Therefore Eq.(12) can be written in matrix form:

$$\frac{d\tilde{\mathbf{v}}}{d\ell} = A(\ell)\tilde{\mathbf{v}}, \quad \tilde{\mathbf{v}} = (v_\rho, v_\omega). \quad (13)$$

- Floquet theory:

$$\tilde{\mathbf{v}} = U(\ell)e^{C\ell/L}, \quad (14)$$

- C is constant Hamiltonian matrix whose eigenvalues are the Floquet exponents, and are of the form $\nu = \pm i\nu$, $\nu \in \mathbb{R}$ near elliptic axis.

Other approach: use u -harmonics order

- ▶ Another approach: b_1 has only 2nd order harmonics in u : seek for solution with 1st order harmonics for $\tilde{\mathbf{v}}$
- ▶ We show that \exists solution with

$$\begin{pmatrix} v_\rho(\ell) \\ v_\omega(\ell) \end{pmatrix} = \begin{pmatrix} v_{\rho c}(\ell) \\ v_{\omega c}(\ell) \end{pmatrix} \cos u + \begin{pmatrix} v_{\rho s}(\ell) \\ v_{\omega s}(\ell) \end{pmatrix} \sin u \quad (15)$$
$$u = \omega - \int \tau d\ell + \delta(\ell).$$

- ▶ Equating $\sin(u)$ and $\cos(u)$ terms, the v_ω equation reads

$$v'_{\omega c} + \left(\frac{B'_0}{2B_0} - \frac{\eta'}{2} \right) v_{\omega c} + \frac{e^{+\eta}}{\cosh(\eta)} \left(\frac{J_0/2}{B_0} - \tau + \delta' \right) v_{\omega s} = 0$$
$$v'_{\omega s} + \left(\frac{B'_0}{2B_0} + \frac{\eta'}{2} \right) v_{\omega s} - \frac{e^{-\eta}}{\cosh(\eta)} \left(\frac{J_0/2}{B_0} - \tau + \delta' \right) v_{\omega c} = 0.$$

Other approach: use u -harmonics order

- Further reduce the system introducing new variables (X, Y) :

$$v_{\omega c} = \frac{1}{\sqrt{B'_0}} e^{+\eta/2} X(\ell), \quad v_{\omega s} = \frac{1}{\sqrt{B'_0}} e^{-\eta/2} Y(\ell) \quad (16)$$

- It becomes:

$$X' + \Omega_0(\ell)Y = 0, \quad Y' - \Omega_0(\ell)X = 0, \quad \Omega_0(\ell) = \frac{\frac{J_0/2}{B_0} - \tau + \delta'}{2 \cosh \eta}$$

- Using complex variable $Z = X + iY$: system reduces to complex ODE:

$$Z' - i\Omega_0 Z = 0 \quad \Rightarrow \quad Z(\ell) = Z_0 \exp \int_0^\ell i\Omega_0(s) ds \quad (17)$$

- ▶ Comparing Eq.(17) and Eq.(14), we identify the Floquet exponent:

$$\nu = \int_0^L \Omega_0(s) ds = \oint \frac{\frac{J_0(s)/2}{B_0(s)} - \tau(s) + \delta'(s)}{2 \cosh \eta(s)} ds \quad (18)$$

- ▶ Matches Mercier's formula!

Floquet Theory I

- Suppose one needs to solve the following linear system,

$$\dot{\mathbf{x}} = A(t)\mathbf{x} \quad \mathbf{x}(0) = \mathbf{x}_0, \quad (19)$$

where $A \in \mathcal{M}_{n \times n}$ is periodic in t with period T .

- Considering n solutions of Eq.(19) $\{\mathbf{x}_1, \dots, \mathbf{x}_n\}$: rewrite the system in the form of a matrix equation, defining the so-called fundamental matrix X by grouping the \mathbf{x}_i :

$$X(t, t_0) := \begin{pmatrix} \mathbf{x}_1; \mathbf{x}_2; \dots; \mathbf{x}_n \end{pmatrix} \quad (20)$$

$$\frac{d}{dt}X(t, t_0) = A(t)X(t, t_0), \quad X(t_0, t_0) = \mathbb{I}. \quad (21)$$

Floquet Theory II

- Fundamental matrix:

$$\det(X(t, t_0)) = \prod_{i=1}^n e^{\lambda_i T}, \quad (22)$$

where the λ_i are the Floquet exponents, which will be shown to be linked with the rotational transform. (Proof of thm. in [Mei07]). Note: $\exp(\lambda_i T)$ are called Floquet multipliers.

- Therefore Floquet multipliers are the eigenvalues of the fundamental matrix of the linear system Eq.(19).
- Main result: **Theorem (Floquet-Lyapunov)**. The fundamental matrix X solution of the system Eq.(21) is of the form

$$X(t, 0) = P(t)e^{tB} \quad (23)$$

where the matrix P is symplectic and T -periodic, and B is a constant hamiltonian matrix.

Discrete formalism: towards ι

- ▶ We follow MacKay and Meiss [MM83] for 1D Lagrangian.
- ▶ Discretize close curve \mathcal{C} with $n - 1$ curves \mathcal{C}_i

$$\begin{aligned}\mathcal{S} &= \sum_{i=1}^{n-1} \int_{\mathcal{C}_i} \mathbf{A} \cdot d\mathbf{l}, \\ &= \sum_{i=1}^{n-1} S(\mathbf{x}_i, \mathbf{x}_{i+1})\end{aligned}\tag{24}$$

- ▶ Notation:

$$\begin{aligned}\mathbf{S}_1^{[i,i+1]} &= \nabla_{\mathbf{x}_i} S^{[i,i+1]} := \nabla_{\mathbf{x}_i} S(\mathbf{x}_i, \mathbf{x}_{i+1}) \\ \mathbf{S}_2^{[i,i+1]} &= \nabla_{\mathbf{x}_{i+1}} S^{[i,i+1]} := \nabla_{\mathbf{x}_{i+1}} S(\mathbf{x}_i, \mathbf{x}_{i+1})\end{aligned}\tag{25}$$

Discrete formalism: towards ι

- Stationarity of the action for extremal curve

$$\begin{aligned}\delta S[\delta \mathbf{x}_i] &= \left[\nabla_{\mathbf{x}_i} S^{[i-1,i]} + \nabla_{\mathbf{x}_i} S^{[i,i+1]} \right] \cdot \delta \mathbf{x}_i = 0, \\ \iff \mathbf{S}_2^{[i-1,i]} + \mathbf{S}_1^{[i,i+1]} &= \mathbf{0}.\end{aligned}\tag{26}$$

- Total derivative of previous result

$$\begin{aligned}\delta \left(\mathbf{S}_2^{[i-1,i]} + \mathbf{S}_1^{[i,i+1]} \right) &= \overline{\overline{S}}_{12}^{[i-1,i]} \cdot \delta \mathbf{x}_{i-1} + \overline{\overline{S}}_{21}^{[i,i+1]} \cdot \delta \mathbf{x}_{i+1} \\ &\quad \left(\overline{\overline{S}}_{22}^{[i-1,i]} + \overline{\overline{S}}_{11}^{[i,i+1]} \right) \cdot \delta \mathbf{x}_i = \mathbf{0}, \\ 1 \leq i &\leq n-1.\end{aligned}\tag{27}$$

- Leads to tridiagonal-block matrix form.

Discrete formalism - ι as an eigenvalue problem

$$\begin{pmatrix} \left(\begin{array}{c} \overline{\overline{S}}_{22}^{[01]} + \overline{\overline{S}}_{11}^{[12]} \\ \overline{\overline{S}}_{21}^{[12]} \end{array} \right) & \overline{\overline{S}}_{12}^{[12]} & & & \lambda^{-1} \overline{\overline{S}}_{21}^{[01]} \\ & \left(\begin{array}{c} \overline{\overline{S}}_{22}^{[12]} + \overline{\overline{S}}_{11}^{[23]} \\ \overline{\overline{S}}_{21}^{[23]} \end{array} \right) & \overline{\overline{S}}_{12}^{[23]} & & \\ & & \ddots & \ddots & \\ & & \ddots & \ddots & \overline{\overline{S}}_{12}^{[n-1,n]} \\ \lambda \overline{\overline{S}}_{12}^{[n,n+1]} & & & \overline{\overline{S}}_{21}^{[n-1,n]} & \left(\overline{\overline{S}}_{22}^{[n-1,n]} + \overline{\overline{S}}_{11}^{[n,n+1]} \right) \end{pmatrix} \cdot \begin{pmatrix} \delta \mathbf{x}_1^T \\ \delta \mathbf{x}_2^T \\ \vdots \\ \vdots \\ \delta \mathbf{x}_{n-1}^T \\ \delta \mathbf{x}_n^T \end{pmatrix} = \mathbf{0}$$

- Recover the same form (discrete this time) as previously for our operator equation:

$$\iff \overline{\overline{M}}(\lambda) \cdot \delta \mathbf{x} = \mathbf{0}, \quad (28)$$

Discrete formalism - ι as an eigenvalue problem

- For such a matrix form, exists formula for determinant [Mol08]

$$\det(M(\lambda)) = \frac{(-1)^{mn}}{(-\lambda)^m} \det(T_S - \lambda \mathcal{I}_6) \det\left(\prod_{i=1}^n \overline{\overline{S}}_{12}[i, i+1]\right)$$

- Requires to define the so-called transfer matrix T_S

$$T_S = \prod_{i=1}^n \begin{pmatrix} -\overline{\overline{S}}_{12}^{-1[i, i+1]} (\overline{\overline{S}}_{22}^{[i-1, i]} + \overline{\overline{S}}_{11}^{[i, i+1]}) & -\overline{\overline{S}}_{12}^{-1[i, i+1]} \overline{\overline{S}}_{12}^{[i-1, i]} \\ \mathcal{I}_3 & 0 \end{pmatrix}.$$

Discrete formalism - a necessary condition

- ▶ MacKay and Meiss use what they call a convexity condition on their Lagrangian: $-L_{12} > 0$, which is similar to the so-called *true angle-dynamics* from [HS14].
- ▶ We propose a generalized criterion: imposing that the upper diagonal matrices are negative definite

$$\mathbf{x}^T \overline{\overline{S}}_{12}^{[i,i+1]} \mathbf{x} < 0, \quad \mathbf{x} \in \mathbb{R}^3, \quad 1 \leq i \leq n. \quad (29)$$

- ▶ Finally, $\det(M(\lambda)) = 0$ yields the following eigenvalue equation:

$$(-\lambda)^{-m} \cdot \det(T_S - \lambda \mathcal{I}) = 0. \quad (30)$$

- ▶ Exponents λ are eigenvalues of transfer matrix.

Discrete formalism - an example: piecewise linears

- One way to discretize: use **segments**

$$\begin{aligned}\mathcal{S} &= \sum_{i=1}^{n-1} S(\mathbf{x}_i, \mathbf{x}_{i+1}), \\ S(\mathbf{x}_i, \mathbf{x}_{i+1}) &= \int_0^1 \mathbf{A}\left(\zeta(\mathbf{x}_{i+1} - \mathbf{x}_i) + \mathbf{x}_i\right) \cdot (\mathbf{x}_{i+1} - \mathbf{x}_i) d\zeta \\ &= \int_0^1 \mathbf{A}(\mathbf{v}(\mathbf{x}(\zeta))) \cdot \mathbf{u} d\zeta,\end{aligned}\tag{31}$$

with $\mathbf{x}(0) = \mathbf{x}_i$ and $\mathbf{x}(1) = \mathbf{x}_{i+1}$, and the vector field \mathbf{v} defined as follows:

$$\mathbf{v}(\zeta, \mathbf{x}_i, \mathbf{x}_{i+1}) = \zeta(\mathbf{x}_{i+1} - \mathbf{x}_i) + \mathbf{x}_i\tag{32}$$

Discrete formalism - an example: piecewise linear

- For the transfer matrix T_S to be implemented, need the second derivatives of the action $\bar{\bar{S}}_{ij}$:

$$\begin{aligned}\bar{\bar{S}}_{12}^{[i-1,i]} &= \int_0^1 d\zeta \zeta \left[(1 - \zeta) \nabla_{\mathbf{v}} J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \cdot (\mathbf{x}_i - \mathbf{x}_{i-1}) - J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \right] \\ &\quad + (1 - \zeta) J_{\mathbf{A}}(\mathbf{v})\end{aligned}$$

$$\bar{\bar{S}}_{22}^{[i-1,i]} = \int_0^1 d\zeta \zeta \left[\zeta \nabla_{\mathbf{v}} J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \cdot (\mathbf{x}_i - \mathbf{x}_{i-1}) + (J_{\mathbf{A}}(\mathbf{v}) + J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v})) \right]$$

$$\begin{aligned}\bar{\bar{S}}_{21}^{[i,i+1]} &= \int_0^1 d\zeta (1 - \zeta) \left[\zeta \nabla_{\mathbf{v}} J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \cdot (\mathbf{x}_{i+1} - \mathbf{x}_i) + J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \right] \\ &\quad + \zeta J_{\mathbf{A}}(\mathbf{v})\end{aligned}$$

$$\begin{aligned}\bar{\bar{S}}_{11}^{[i,i+1]} &= \int_0^1 d\zeta (1 - \zeta) \left[(1 - \zeta) \nabla_{\mathbf{v}} J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v}) \cdot (\mathbf{x}_{i+1} - \mathbf{x}_i) \right. \\ &\quad \left. - (J_{\mathbf{A}}(\mathbf{v}) + J_{\mathbf{A}}^{\mathbf{T}}(\mathbf{v})) \right]\end{aligned}$$

Discrete formalism - an example: piecewise linears

- ▶ With vector potential \mathbf{A} provided, $T_{\mathcal{S}}$ can be easily implemented numerically.
- ▶ Model can be verified.
- ▶ Strength of this approach: In the limit $n \uparrow \infty$, even if the dimension of M is infinite, finding the exponents λ still reduces to finding the eigenvalues of a 6×6 matrix.

2. Vacuum field energy for coil design

The filamentary coil description

- ▶ Coils are represented as filaments: **0 thickness**
- ▶ Coil: curve in 3D space $\mathcal{C} \subset \mathbb{R}^3$ + current $I_C \in \mathbb{R}_+$.
- ▶ **Degrees of freedom:** targeted by the algorithm to optimize for particular penalty involving the coils: Fourier modes (e.g. cartesian or cylindrical coordinates) + I_{C_i} .

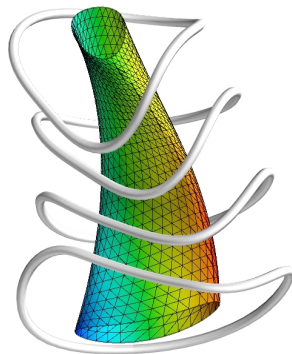


Figure: Filamentary coils for precise QA [LP22] configuration - penalty on \mathcal{L} .

Introduction of a new penalty

- ▶ $\mathbf{j} \times \mathbf{B}$ force is gradient of energy.
- ▶ Our guess: instead of minimizing force: minimize the "potential" that provokes it.
- ▶ Introduce the vacuum energy:

$$\mathcal{E} = \frac{1}{2\mu_0} \int_{\mathbb{R}^3} d\mathbf{x} B^2 = \frac{1}{2\mu_0} \int_{\mathbb{R}^3} d\mathbf{x} \mathbf{j} \cdot \mathbf{A}. \quad (33)$$

- ▶ Current constrained on set of coils $\{C_i\}$:

$$\mathcal{E} = \frac{1}{2\mu_0} \sum_{i=1}^{N_C} \oint_{C_i} I_i d\mathbf{l}_i \cdot \mathbf{A}(\mathbf{x}), \quad (34)$$

Introduction of a new penalty

- ▶ We can write $\delta\mathcal{E}$ in a shape gradient form:

$$\delta\mathcal{E}[\{\delta\mathbf{x}_i\}] = \sum_i I_i \oint_{C_i} dl \ (\delta\mathbf{x}_i \times \mathbf{t}) \cdot \mathbf{B}. \quad (35)$$

- ▶ Enables to express parameters derivatives to be implemented in Simsopt (w.r.t. Fourier modes for example) [LMW⁺21]

$$\begin{aligned} \frac{\partial\mathcal{E}}{\partial\Omega_k} &= \sum_i I_i \oint_{C_i} dl \ (\mathbf{t} \times \mathbf{B}) \cdot \frac{\partial\mathbf{x}_i}{\partial\Omega_k} \\ &= \sum_i \oint_{C_i} (\mathbf{j}_i \times \mathbf{B}) \cdot \frac{\partial\mathbf{x}_i}{\partial\Omega_k}, \end{aligned} \quad (36)$$

- ▶ \mathbf{B} can be expressed from Biot-Savart law

Limitations due to filamentary coils

- ▶ **B** is **singular** on the coils. Field generated by a filament and evaluated on the filament itself.
- ▶ Biot-Savart:

$$\mathbf{B}(\mathbf{x}) = \sum_{i=1}^{N_C} I_i \frac{\mu_0}{4\pi} \oint_{C_i} \frac{d\mathbf{l} \times (\mathbf{x} - \mathbf{x}_i)}{|\mathbf{x} - \mathbf{x}_i|^3}. \quad (37)$$

- ▶ The 0-thickness approx. works for objective functions such as integrated curvature, coil to coil separation etc. How can we overcome this singularity problem?

Overcome singularity limitations

- ▶ Introduce thickness: probably most relevant solution (see Matt's work)
- ▶ Define a *ghost*-curve: displace the filament in an arbitrary direction (e.g. normal) by a distance ϵ to evaluate the field here.
- ▶ Obvious limitations to the ghost-curve:
 1. Assumes smooth behavior of the field around the curve.
 2. Depends on behavior of \mathbf{n} , \mathbf{b} along the filament.
 3. Need for additional numerical parameter: ϵ , adds arbitrariness to the model.

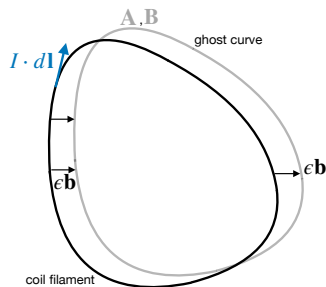


Figure: Filamentary coil curve (black) and ghost curve defined by binormal displacement.

Ghost-curves

- ▶ One issue with ghost curves: behavior of \mathbf{n} might be not smooth with abrupt changes in direction
- ▶ Solution (?): \mathcal{E} as an average of integral over 4 ghost curves at $\pm\epsilon\mathbf{n}$ and $\pm\epsilon\mathbf{b}$

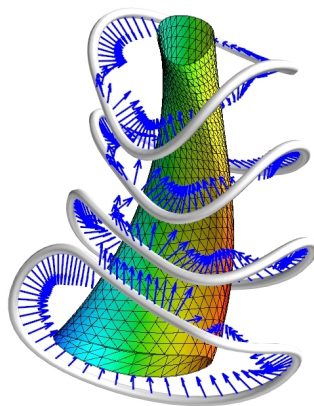


Figure: Same coils as in Fig.(28) with \mathbf{n} plotted in blue.

Results I

- ▶ Goal 1: recover configuration (here precise QA from Landreman-Paul [LP22]) minimizing quadratic flux Φ_2 .
- ▶ Need penalty to prevent coils length going to ∞ .
- ▶ Can we replace length penalty by vacuum-energy penalty?

$$\mathcal{F} = \int_S (\mathbf{B} \cdot \mathbf{n})^2 dS + \rho \mathcal{L} + \omega \mathcal{E} \quad (38)$$

- ▶ Goal 2: see if coils resulting from penalizing the energy have lower (inter-coil) forces.

Results II

- ▶ Penalty on energy not sufficient to constraint the coils lengths: need additional length penalty to prevent the coils from linking.
- ▶ The coils shapes are not regular.
- ▶ $\max\{C_i\} |\mathbf{j} \times \mathbf{B}|$ is higher.

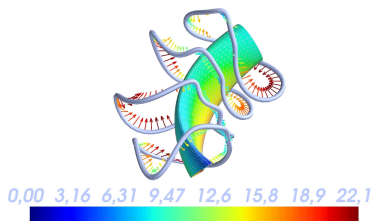
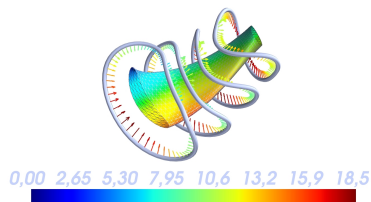


Figure: Up: Φ_2 and \mathcal{L} - Down: same $+\mathcal{E}$

What could cause these "errors"?

- ▶ Our intuition could be wrong.
- ▶ The implementation approach might not be correct:
 - ▶ Ghost curve not a good-enough tool.
 - ▶ Simsopt needs the objective function $\mathcal{E}.J()$ which is technically infinite for filamentary coils. Here it scales with ϵ^{-1} , and so do the derivatives. Hence the weight has to be $\propto \epsilon \rightarrow$ huge gap between energy weight and other weights.
 - ▶ In general: such discrepancies between variables that are combined are not good.
- ▶ The whole implementation of the energy in itself might contain errors.

Conclusion

- ▶ The vacuum-field energy still remains a promising quantity to minimize in order to reduce inter-coil forces, as long as we haven't found the proper way to implement it in the more general framework of non-linear optimization for coil-design.
- ▶ Probably need to give non-zero thickness to the coils?
- ▶ To sum things up: we need to think more!

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