# Performance-based assessments for semiconductor circuit competencies

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The purpose of these assessments is for instructors to accurately measure the learning of their electronics students, in a way that melds theoretical knowledge with hands-on application. In each assessment, students are asked to predict the behavior of a circuit from a schematic diagram and component values, then they build that circuit and measure its real behavior. If the behavior matches the predictions, the student then simulates the circuit on computer and presents the three sets of values to the instructor. If not, then the student then must correct the error(s) and once again compare measurements to predictions. Grades are based on the number of attempts required before all predictions match their respective measurements.

You will notice that no component values are given in this worksheet. The *instructor* chooses component values suitable for the students' parts collections, and ideally chooses different values for each student so that no two students are analyzing and building the exact same circuit. These component values may be hand-written on the assessment sheet, printed on a separate page, or incorporated into the document by editing the graphic image.

This is the procedure I envision for managing such assessments:

- 1. The instructor hands out individualized assessment sheets to each student.
- 2. Each student predicts their circuit's behavior at their desks using pencil, paper, and calculator (if appropriate).
- 3. Each student builds their circuit at their desk, under such conditions that it is impossible for them to verify their predictions using test equipment. Usually this will mean the use of a multimeter only (for measuring component values), but in some cases even the use of a multimeter would not be appropriate.
- 4. When ready, each student brings their predictions and completed circuit up to the instructor's desk, where any necessary test equipment is already set up to operate and test the circuit. There, the student sets up their circuit and takes measurements to compare with predictions.
- 5. If any measurement fails to match its corresponding prediction, the student goes back to their own desk with their circuit and their predictions in hand. There, the student tries to figure out where the error is and how to correct it.
- 6. Students repeat these steps as many times as necessary to achieve correlation between all predictions and measurements. The instructor's task is to count the number of attempts necessary to achieve this, which will become the basis for a percentage grade.
- 7. (OPTIONAL) As a final verification, each student simulates the same circuit on computer, using circuit simulation software (Spice, Multisim, etc.) and presenting the results to the instructor as a final pass/fail check.

These assessments more closely mimic real-world work conditions than traditional written exams:

- Students cannot pass such assessments only knowing circuit theory or only having hands-on construction and testing skills they must be proficient at both.
- Students do not receive the "authoritative answers" from the instructor. Rather, they learn to validate their answers through real circuit measurements.
- Just as on the job, the work isn't complete until all errors are corrected.
- Students must recognize and correct their own errors, rather than having someone else do it for them.
- Students must be fully prepared on exam days, bringing not only their calculator and notes, but also their tools, breadboard, and circuit components.

Instructors may elect to reveal the assessments before test day, and even use them as preparatory labwork and/or discussion questions. Remember that there is absolutely nothing wrong with "teaching to

the test" so long as the test is valid. Normally, it is bad to reveal test material in detail prior to test day, lest students merely memorize responses in advance. With performance-based assessments, however, there is no way to pass without truly understanding the subject(s).

Competency: LED current limiting	Version:
Schematic	
V <sub>supply</sub> =	$R_{limit}$ $D_1$
Given conditions	
$V_{\text{supply}} = V_{\text{forward (LED)}} =$	$I_{forward(LED)} =$
Parameters	
$egin{aligned} egin{aligned} egin{aligned\\ egin{aligned} egi$	Predicted Measured
Analysis  Show how you calculated the ap	opropriate value for R <sub>limit</sub>
Draw the directions of both electron	on and conventional current
Sunnosa component   fails -	open other shorted

<u>file 04075</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 1

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Have students calculate the necessary current-limiting resistor for their LEDs based on measured values of  $V_{forward}$  for the LED (using a multimeter with a "diode-check" function). Let students research the typical forward current for their LED from an appropriate datasheet. Any LED should suffice for this activity.

Competency: Rectifying di	ode behavior		Version:
Schematic			
Forward-bia	sed	Rev	verse-biased
V <sub>supply</sub>	$R_1$ $D_1$	V <sub>supply</sub>	$R_1$ $D_1$
Given conditions			
$V_{\text{supply}} = $ (see multiple v	alues given bel	ow)	
$R_1 =$			
Parameters Forward-biase	ed		
Given	Pre	edicted	Measured
$V_{\text{supply}} = $	$V_{R1}$		
	$V_{D1}$		
Given	Pre	edicted	Measured
$V_{\text{supply}} = $	$V_{R1}$		
	$V_{D1}$		
Parameters Reverse-biase	∍d		
Given	Pre	edicted	Measured
$V_{\text{supply}} =$	$V_{R1}$		
	$V_{D1}$		
Given	Pre	edicted	Measured
$V_{\text{supply}} = $	$V_{R1}$		
	$V_{D1}$		

<u>file 01940</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 2

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). I recommend using one of the 1N400X series of rectifying diodes for their low cost and ruggedness.

Competency: Half-wave rectifier	Version:
Schematic	
Fuse 120 V / 12.6 V C.T. D <sub>1</sub>	$R_{load}$
Given conditions	
$V_{\text{secondary}} = (VAC \text{ RMS})$ $R_{\text{load}} =$	
Parameters	
Predicted Measured	
V <sub>load(DC)</sub> (Approximate of	only)
V <sub>ripple</sub>	
$ m f_{ripple}$	
Fault analysis	
Suppose component fails shorted	er
What will happen in the circuit?	

<u>file 01941</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 3

I recommend using 1N400X series rectifying diodes for all rectifier circuit designs. Make sure that the resistance value you specify for your load is not so low that the resistor's power dissipation is exceeded.

Watch out for harmonics in the power line voltage creating problems with RMS/peak voltage relationships. If this is a problem, try using a ferroresonant transformer to filter out some of the harmonic content. *Do not* try to use a sine-wave signal generator as an alternate source of AC power, because most signal generators have internal impedances that are much too high for such a task.

Competency: Full-wave center-tap rectifier	Version:
Schematic	
Fuse 120 V / 12.6 V C.T.	$D_1$ $R_{load}$
Given conditions	
$V_{\text{secondary}} = (VAC \text{ RMS})$	$R_{load} =$
Parameters	
Predicted Measured	
V <sub>load(DC)</sub> (Appro	ximate only)
V <sub>ripple</sub>	
$ m f_{ripple}$	
Fault analysis	
Suppose component fails shorted	other
What will happen in the circuit?	•

 $\underline{\mathrm{file}\ 01942}$ 

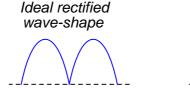
Use circuit simulation software to verify your predicted and measured parameter values.

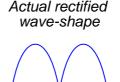
#### Notes 4

I recommend using 1N400X series rectifying diodes for all rectifier circuit designs. Make sure that the resistance value you specify for your load is not so low that the resistor's power dissipation is exceeded.

Watch out for harmonics in the power line voltage creating problems with RMS/peak voltage relationships. If this is a problem, try using a ferroresonant transformer to filter out some of the harmonic content. *Do not* try to use a sine-wave signal generator as an alternate source of AC power, because most signal generators have internal impedances that are much too high for such a task.

It is difficult to precisely calculate the DC load voltage from a rectifier circuit such as this when the transformer secondary voltage is relatively low. The diodes' forward voltage drop essentially distorts the rectified waveform so that it is not quite the same as what you would expect a full-wave rectified waveform to be:





Accurate calculation of the actual rectified wave-shape's average voltage value requires integration of the half-sine peak over a period less than  $\pi$  radians, which may very well be beyond the capabilities of your students. This is why I request approximations only on this parameter.

One approximation that works fairly well is to take the AC RMS voltage (in this case, half of the secondary winding's output, since this is a center-tap design), convert it to *average* voltage (multiply by 0.9), and then subtract the forward junction voltage lost by the diode (0.7 volts typical for silicon).

Competency: Full-wave bridge rectifier	Version:
Schematic	
Fuse 120 V / Fuse 12.6 V C.T.	$D_1$ $D_2$ $D_3$ $D_4$ $R_{load}$
Given conditions	
$V_{\text{secondary}} = (VAC RMS)$	$R_{load} =$
Parameters	
Predicted Measured	
V <sub>load(DC)</sub> (Ap	proximate only)
V <sub>ripple</sub>	
f <sub>ripple</sub>	
Fault analysis	
Suppose component fails show	
What will happen in the circuit?	iteu

 $\underline{\mathrm{file}\ 01943}$ 

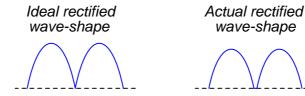
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 5

I recommend using 1N400X series rectifying diodes for all rectifier circuit designs. Make sure that the resistance value you specify for your load is not so low that the resistor's power dissipation is exceeded.

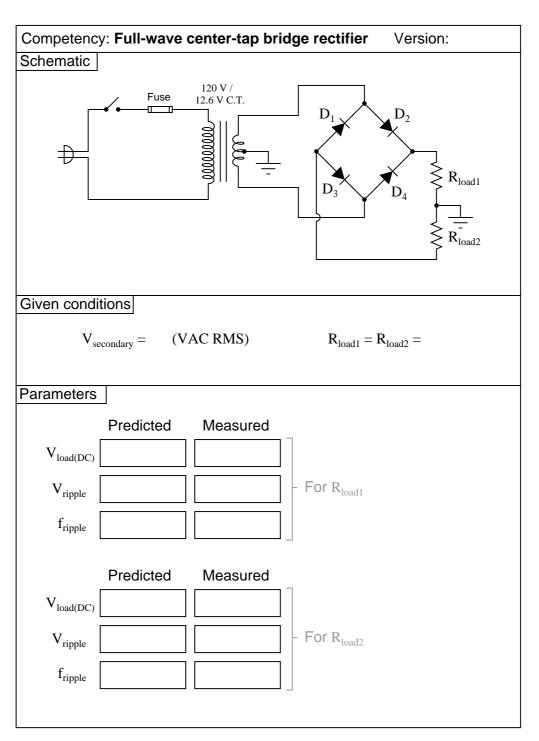
Watch out for harmonics in the power line voltage creating problems with RMS/peak voltage relationships. If this is a problem, try using a ferroresonant transformer to filter out some of the harmonic content. *Do not* try to use a sine-wave signal generator as an alternate source of AC power, because most signal generators have internal impedances that are much too high for such a task.

It is difficult to precisely calculate the DC load voltage from a rectifier circuit such as this when the transformer secondary voltage is relatively low. The diodes' forward voltage drop essentially distorts the rectified waveform so that it is not quite the same as what you would expect a full-wave rectified waveform to be:



Accurate calculation of the actual rectified wave-shape's average voltage value requires integration of the half-sine peak over a period less than  $\pi$  radians, which may very well be beyond the capabilities of your students. This is why I request approximations only on this parameter.

One approximation that works fairly well is to take the AC RMS voltage, convert it to *average* voltage (multiply by 0.9), and then subtract the total forward junction voltage lost by the diode (0.7 volts per diode typical for silicon, for a total of 1.4 volts).



<u>file 01944</u>

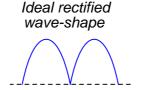
Use circuit simulation software to verify your predicted and measured parameter values.

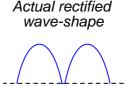
#### Notes 6

I recommend using 1N400X series rectifying diodes for all rectifier circuit designs. Make sure that the resistance value you specify for your load is not so low that the resistor's power dissipation is exceeded.

Watch out for harmonics in the power line voltage creating problems with RMS/peak voltage relationships. If this is a problem, try using a ferroresonant transformer to filter out some of the harmonic content. *Do not* try to use a sine-wave signal generator as an alternate source of AC power, because most signal generators have internal impedances that are much too high for such a task.

It is difficult to precisely calculate the DC load voltage from a rectifier circuit such as this when the transformer secondary voltage is relatively low. The diodes' forward voltage drop essentially distorts the rectified waveform so that it is not quite the same as what you would expect a full-wave rectified waveform to be:





Accurate calculation of the actual rectified wave-shape's average voltage value requires integration of the half-sine peak over a period less than  $\pi$  radians, which may very well be beyond the capabilities of your students. This is why I request approximations only on this parameter.

One approximation that works fairly well is to take the AC RMS voltage (in this case, half of the secondary winding's output, since this is a center-tap design), convert it to *average* voltage (multiply by 0.9), and then subtract the forward junction voltage lost by the diode (0.7 volts typical for silicon).

Competency	: Full-wave r	ectifier circuit	 Version:
Description			
Design and build a full-wave rectifier circuit of any configuration desired. It simply needs to output DC when energized by an AC source (provided by the instructor).			
Given conditi	ons		
$ m V_{supply(AC)}$	=	$f_{\rm supply} =$	
Schematic			
Parameters			
	Predicted	Measured	
$V_{ripple}$			
$\mathrm{f}_{\mathrm{ripple}}$			

 $\underline{\mathrm{file}\ 02296}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 7

I recommend using 1N400X series rectifying diodes for all rectifier circuit designs. Make sure that the resistance value you specify for your load is not so low that the resistor's power dissipation is exceeded.

Competency: AC-DC	power supply ci	rcuit	Version:
Description			
Build a "brute force" AC-DC power supply circuit, consisting of a step-down transformer, full-wave bridge rectifier, capacitive filter, and load resistor.			
Given conditions			
$V_{ m supply} =$	$C_{filter} =$	$R_{load} =$	
Schematic			
Davagastaga			
Parameters			
$V_{\text{out(DC)}}$ Predicted	Measured		
V <sub>out(ripple)</sub>			

<u>file 01622</u>

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 8

Use a Variac at the test bench to provide variable-voltage AC power for the students' power supply circuits.

Competency: Zener diode voltage regulator	Version:
Schematic	
V <sub>supply</sub>	$R_{load}$
Given conditions	
	$R_{series} =$
$ m V_{supply} =  m V_{zener} =$	$R_{ m load} =$
Parameters	
Predicted Measured  V <sub>load</sub> (nominal)  V <sub>supply</sub> (max)  V <sub>supply</sub> (min)	
Suppose component fails shorted  What will happen in the circuit?	other

The  $V_{supply}$  (min) parameter is the minimum voltage setting that  $V_{supply}$  may be adjusted to with the regulator circuit maintaining constant load voltage at  $R_{load}$ .  $V_{supply}$  (max) is the maximum voltage that  $V_{supply}$  may be adjusted to without exceeding the zener diode's power rating.  $V_{load}$  (nominal) is simply the regulated voltage output of the circuit under normal conditions.

<u>file 01623</u>

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 9

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard load resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.), and let the students determine the proper resistance values for their series dropping resistors.

I recommend specifying a series resistor value  $(R_{series})$  high enough that there will little danger in damaging the zener diode due to excessive supply voltage, but also low enough so that the normal operating current of the zener diode is great enough for it to drop its rated voltage. If  $R_{series}$  is too large, the zener diode's current will be too small, resulting in lower than expected voltage drop and poorer regulation (operating near the flatter end of the characteristic curve).

Values I have used with success are as follows:

- $R_{series} = 1 \text{ k}\Omega$
- $R_{load} = 10 \text{ k}\Omega$
- $V_{zener} = 5.1 \text{ volts (diode part number 1N4733)}$
- $V_{supply} = 12 \text{ volts}$

Measuring the minimum supply voltage is a difficult thing to do, because students must look for a point where the output voltage begins to directly follow the input voltage (going down) instead of holding relatively stable. One interesting way to measure the rate of output voltage change is to set a DMM on the AC voltage setting, then use that to measure  $V_{load}$  as  $V_{supply}$  is decreased. While turning the voltage adjustment knob on  $V_{supply}$  at a steady rate, students will look for an increase in AC voltage (a greater rate of change) at  $V_{load}$ . Essentially, what students are looking for is the point where  $\frac{dV_{load}}{dV_{supply}}$  begins to increase.

	Half-wave voltage doubler	Version:
Schematic		
	$V_{\text{supply}} \bigcirc D_1$	$V_{out}$ $C_2$
Given conditi	ons	
Olvoir coriaiti	0110	
$V_{\text{supply}} =$	$C_1 = C_2 =$	V <sub>F</sub> (typical) =
Parameters		
1 drameters		
	Predicted Measured	
$V_{C1}$		
$V_{C2}$		
V <sub>out</sub>		
Fault analysis		
Suppose co	mponent fails Ope	en other
What will ha	ppen in the circuit?	

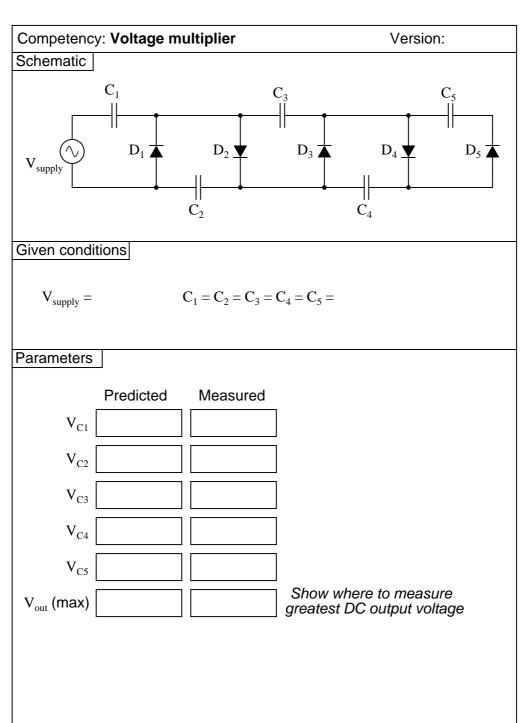
<u>file 01974</u>

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 10

I've used 47  $\mu$ F electrolytic capacitors and 1N4001 diodes with good success on a 10 volt AC (RMS) power supply. I recommend that students measure their own diodes to determine typical forward voltage  $(V_F)$ .

Don't forget to mention the polarity sensitivity of these capacitors! Electrolytic capacitors can explode violently if reverse-connected!



 $\underline{\mathrm{file}\ 02012}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 11

I've used 0.47  $\mu$ F capacitors and 1N4001 diodes with good success on a 10 volt AC (RMS) power supply. I recommend using low-capacity capacitors to minimize the amount of stored energy, since voltages in this circuit are potentially hazardous.

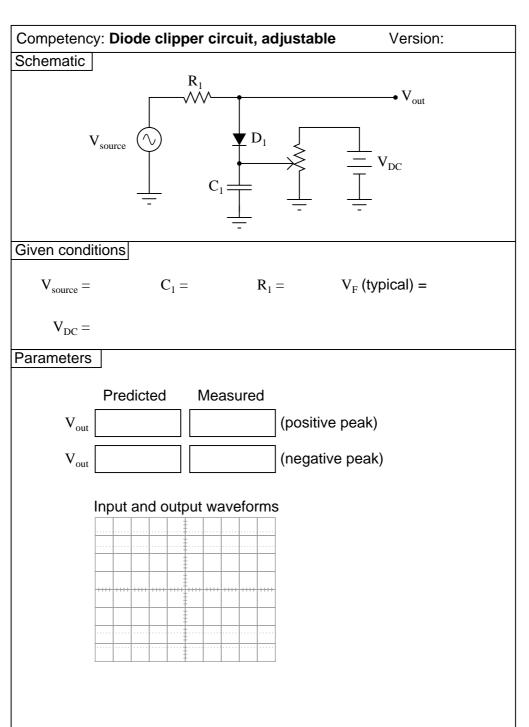
Competency: Diode clipper circuit	Version:
Schematic	
$V_{\text{supply}} \bigcirc D_1 $	▼ D <sub>2</sub>
Given conditions	
$ m V_{supply} =  m R_1 =  m$	V <sub>F</sub> (typical) =
Parameters	
Predicted Measured V <sub>out</sub>	Input and output waveforms
Sunnose component   Ifails -	oen other

<u>file 01979</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 12

Any diodes will work for this, so long as the source frequency is not too high. I recommend students set the volts/division controls on both channels to the exact same range, so that the slope of the clipped wave near zero-crossing may seen to be exactly the same as the slope of the input sine wave at the same points. This makes it absolutely clear that the output waveform is nothing more than the input waveform with the tops and bottoms cut off.



file 01986

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 13

Any diodes will work for this, so long as the source frequency is not too high. I have had good success with the following values:

- $V_{source} = 4 \text{ volts (peak)}$
- $f_{source} = 3 \text{ kHz}$
- $V_{DC} = 6$  volts
- $C_1 = 0.47 \ \mu \text{F}$
- $R_1 = 100 \text{ k}\Omega$
- Potentiometer =  $10 \text{ k}\Omega$ , linear
- $D_1 = \text{part number } 1\text{N}4004 \text{ (any } 1\text{N}400\text{x diode should work)}$

Competency: Zener diode clipper circu	lit Version:
Schematic	
$V_{\text{supply}}$ $D_1$ $D_2$	→ V <sub>out</sub>
Given conditions	
$V_{\text{supply}} = R_1 = V$	$V_{\rm F}$ (typical) = $V_{\rm Z}$ =
Parameters	
Predicted Measured Vout	Input and output waveforms
Sunnosa component   fails -	open other
What will happen in the circuit?	

<u>file 01980</u>

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 14

Be sure to use zener diodes with reasonably low breakdown voltages, and specify the source voltage accordingly.

Competency: BJT terminal identification	Version:	
Description		
Identify the terminals (emitter, base, and collector) of a bipolar junction transistor using a multimeter. Then, compare your conclusions with information from a datasheet or cross-reference book.		
Given conditions		
Part number =		
Parameters		
Measured  V <sub>bias(BE)</sub> V <sub>bias(BC)</sub>		
Terminal identification (Draw your own sketch if shown is not appropri		
Advertised Your conclusion  (Label)  (Label)		

<u>file 01921</u>

Contrary to what you might think, the datasheet or cross-reference is not the "final authority" for checking your meter-based conclusions! I have seen datasheets and cross-reference manuals wrong more than once!

# Notes 15

Identification of BJT terminals is a very important skill for technicians to have. Most modern multimeters have a *diode check* feature which may be used to positively identify PN junction polarities, and this is what I recommend students use for identifying BJT terminals.

To make this a really good performance assessment, you might want to take several BJT's and scratch the identifying labels off, so students cannot refer to memory for pin identification (for instance, if they remember the pin assignments of a 2N2222 because they use it so often). Label these transistors with your own numbers ("1", "2", etc.) so you will know which is which, but not the students!

Competency: Current-sourcing BJT switch Version:
Schematic
V <sub>supply</sub> = R <sub>load</sub>
Given conditions
$V_{supply} = R_{load} = \beta =$
Parameters
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Suppose component open other shorted  What will happen in the circuit?

<u>file 01931</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 16

Being able to design a circuit using a BJT as a switch is a valuable skill for technicians and engineers alike to have. The circuit shown in this question is not the only possibility, but it is the simplest.

Remind your students that the equation for calculating BJT power dissipation is as follows:

$$P_Q = I_C \left( V_{CE} + \frac{V_{BE}}{\beta} \right)$$

Competency: Current-sinking BJT switch	Version:	
Schematic		
V <sub>supply</sub>	$R_{load}$ $Q_1$	
Given conditions		
$V_{\text{supply}} = R_{\text{load}} =$	$\beta =$	
Parameters		
Predicted Measured  I <sub>load</sub>	Calculated β P <sub>Q1</sub>	
Suppose component open other shorted  What will happen in the circuit?		

 $\underline{\mathrm{file}\ 01932}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 17

Being able to design a circuit using a BJT as a switch is a valuable skill for technicians and engineers alike to have. The circuit shown in this question is not the only possibility, but it is the simplest.

Remind your students that the equation for calculating BJT power dissipation is as follows:

$$P_Q = I_C \left( V_{CE} + \frac{V_{BE}}{\beta} \right)$$

Competency: BJT swi	tch circuit	Version:
Description		
to turn o then turn or small only car	and build a circuit that use on a bipolar junction transions on a DC load such as a electric motor. The switcory enough current to activate not carry the full load cure.	stor, which a light bulb h must ate the BJT,
Given conditions		
$V_{ m supply} =$		
Schematic		
Parameters		
Measured	1	
I <sub>load</sub>	$\equiv$ Is $I_{load} >> I_{switch}$ ?	
I <sub>switch</sub>	load Switch	
	_	

 $\underline{\mathrm{file}\ 02319}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 18

Being able to design a circuit using a BJT as a switch is a valuable skill for technicians and engineers alike to have.

Competency: Buffered zener diode voltage regulator Version:
Schematic
$V_{\text{supply}} = D_1$ $R_{\text{load}}$
Given conditions
$V_{\text{supply}} = V_{\text{zener}} = R_{\text{series}} =$
Parameters
Predicted Measured  V_{load} (nominal)
What will happen in the circuit?

The  $R_{load}$  (max) and  $R_{load}$  (min) parameters are the maximum and minimum resistance settings that  $R_{load}$  may be adjusted to with the regulator circuit maintaining constant load voltage.  $V_{load}$  (nominal) is simply the regulated voltage output of the circuit under normal conditions.  $\frac{\text{file } 01945}{\text{file } 01945}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 19

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts.

I highly recommend specifying a large value for  $R_{series}$  and/or a high-wattage rated transistor and variable load resistor, so that students do not dissipate excessive power at either the transistor or the load as they test for  $R_{load}$  (min). Do not use a decade resistance box for  $R_{load}$  unless you have made sure its power dissipation will not be exceeded under any circuit condition!

Competency: Darlington-buffered zener voltage regulator Version:		
Schematic		
$V_{\text{supply}} = D_1$ $Q_1$ $Q_2$ $R_{\text{load}}$		
Given conditions		
$V_{\text{supply}} = V_{\text{zener}} = R_{\text{series}} =$		
Parameters		
Predicted Measured		
V <sub>load</sub> (nominal)		
R <sub>load</sub> (max)		
$R_{load}$ (min) $\boxed{\hspace{1cm}}$ $While still regulating V_{load}$		
Be sure to calculate transistor power dissipation before		
loading the circuit with $R_{load}$ (min) and measuring $V_{load}$ , to		
ensure there will be no damage done to the circuit.		
Fault analysis		
Suppose componentfails open other		
What will happen in the circuit?		

The  $R_{load}$  (max) and  $R_{load}$  (min) parameters are the maximum and minimum resistance settings that  $R_{load}$  may be adjusted to with the regulator circuit maintaining constant load voltage.  $V_{load}$  (nominal) is simply the regulated voltage output of the circuit under normal conditions.  $\underline{\text{file } 2010}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 20

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts.

I highly recommend specifying a large value for  $R_{series}$  and/or a high-wattage rated transistor and variable load resistor, so that students do not dissipate excessive power at either the transistor or the load as they test for  $R_{load}$  (min). Do not use a decade resistance box for  $R_{load}$  unless you have made sure its power dissipation will not be exceeded under any circuit condition!

Competency: Current mirror	Version:	
Schematic R <sub>1</sub>	V <sub>CC</sub> R <sub>load</sub>	
Given conditions		
$V_{CC} = R_1 =$	$R_{load}$ (max) =	
Parameters		
Predicted Measured		
I <sub>R1</sub>		
I <sub>load</sub>	(R <sub>load</sub> set to mid-value)	
R <sub>load(max)</sub>	(Maximum R with $I_{load}$ stable)	
R <sub>load(min)</sub>	(Minimum R with $I_{load}$ stable)	
Fault analysis	onen Oother	
Suppose component open other shorted		
What will happen in the circuit?		

<u>file 01938</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 21

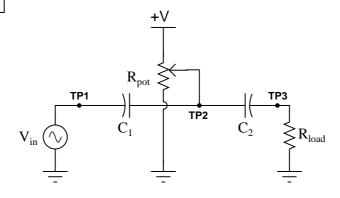
I recommend a 47 k $\Omega$  resistor for  $R_1$  and a 100 k $\Omega$  potentiometer for  $R_{load}$ .

Question 22

# Competency: Signal biasing/unbiasing network

Version:

Schematic



## Given conditions

$$V_{in} =$$

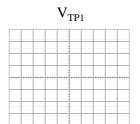
$$C_1 = C_2 =$$

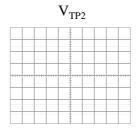
$$R_{load} =$$

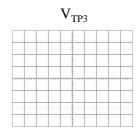
$$R_{pot} =$$

**Parameters** 

With potentiometer set to its \_\_\_\_% position:







Explanation

What effect, if any, does the potentiometer position have on the voltage measured at each test point?

Explain how you could measure the effects of the potentiometer's position *without* using an oscilloscope.

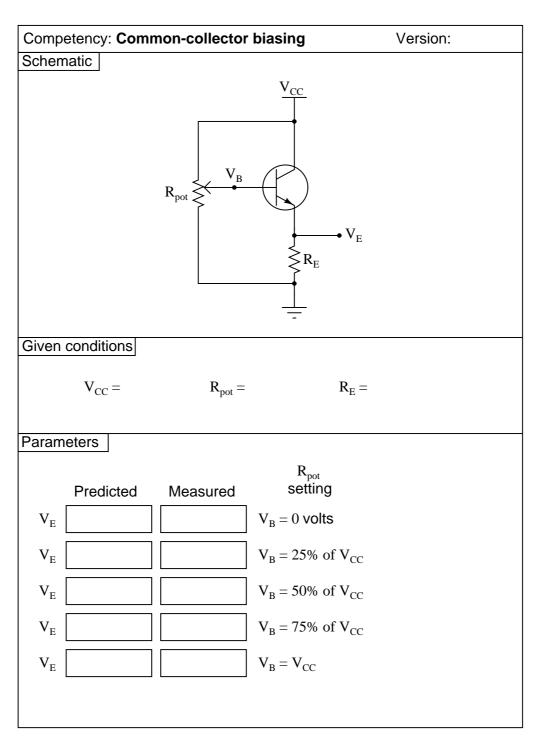
file 01946

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 22

The purpose of this exercise is to get students to understand how AC signals are mixed with DC voltages ("biased") and also how these DC bias voltages are removed to leave just an AC signal. This is important to understand for the purpose of analyzing BJT amplifier circuits.

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal.

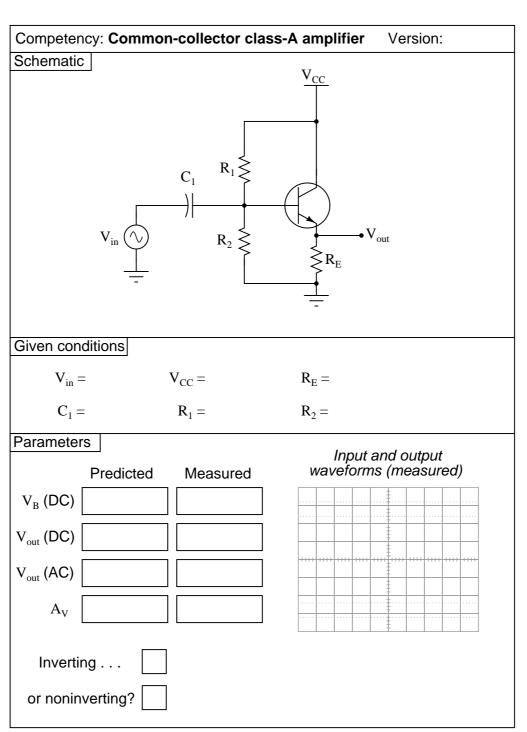


 $\underline{\mathrm{file}\ 01977}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 23

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).



 $\underline{\mathrm{file}\ 01967}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

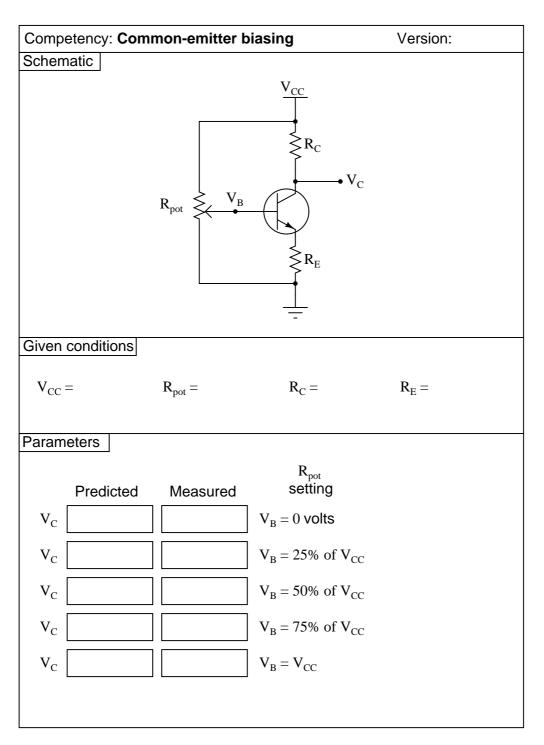
#### Notes 24

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{CC} = 9$  volts
- $V_{in} = 1$  volt RMS, audio frequency
- $R_1 = 10 \text{ k}\Omega$
- $R_2 = 10 \text{ k}\Omega$
- $R_E = 27 \text{ k}\Omega$
- $C_1 = 10 \ \mu \text{F}$

Question 25

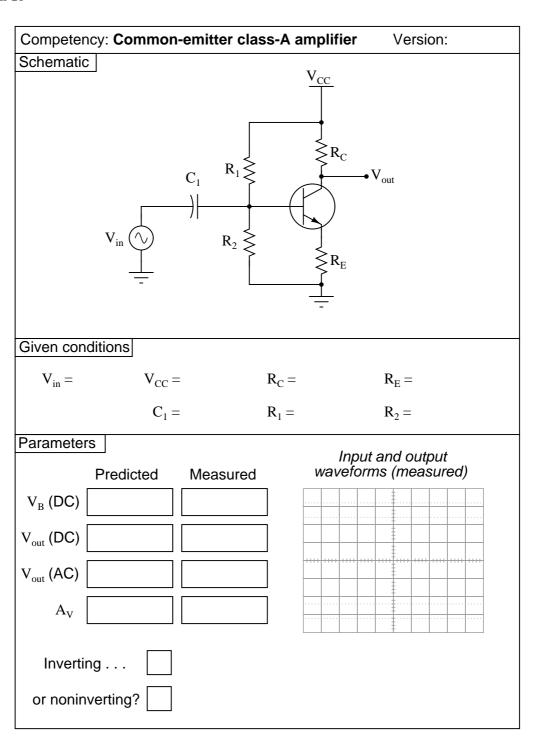


 $\underline{\mathrm{file}\ 01978}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 25

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).



<u>file 01966</u>

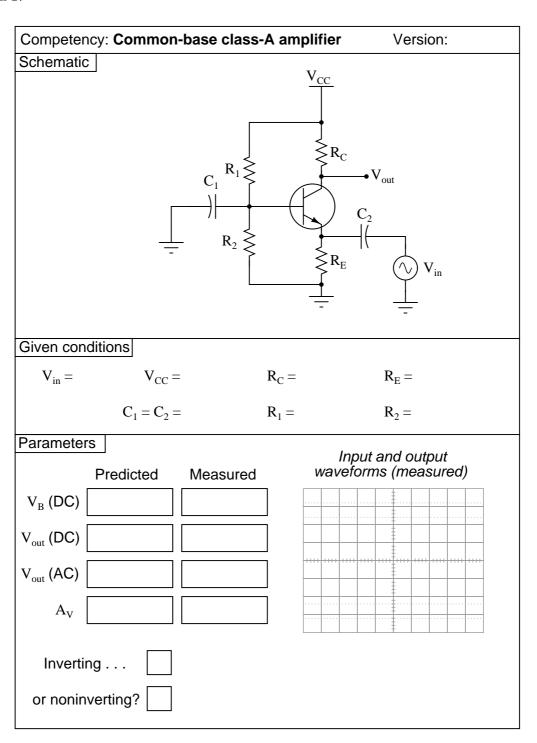
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 26

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{CC} = 9$  volts
- $V_{in}$  = audio-frequency signal, 0.5 volt peak-to-peak
- $R_1 = 220 \text{ k}\Omega$
- $R_2 = 27 \text{ k}\Omega$
- $R_C = 10 \text{ k}\Omega$
- $R_E = 1.5 \text{ k}\Omega$
- $C_1 = 10 \ \mu \text{F}$



 $\underline{\mathrm{file}\ 01981}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 27

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

The voltage gain of this amplifier configuration tends to be very high, approximately equal to  $\frac{R_C}{r_e'}$ . Your students will have to use fairly low input voltages to achieve class A operation with this amplifier circuit. I have had good success using the following values:

- $V_{CC} = 12$  volts
- $V_{in} = 20 \text{ mV}$  peak-to-peak, at 5 kHz
- $R_1 = 1 \text{ k}\Omega$
- $R_2 = 4.7 \text{ k}\Omega$
- $R_C = 100 \ \Omega$
- $R_E = 1 \text{ k}\Omega$
- $C_1 = 33 \ \mu \text{F}$

Your students will find the actual voltage gain deviates somewhat from predicted values with this circuit, largely because it is so dependent on the value of  $r'_e$ , and that parameter tends to be unpredictable.

Competency: Variable-bias, common-emitter BJT amp Version:
Schematic
$V_{\text{CC}}$ $R_{\text{C}}$ $V_{\text{out}}$ $V_{\text{in}}$ $R_{\text{C}}$ $R_{\text{E}}$
Given conditions
$V_{in} = V_{CC} = R_C = R_E =$
Parameters
Predicted Measured  A <sub>V</sub>
Suppose component open other shorted  What will happen in the circuit?

 $\underline{\mathrm{file}\ 03919}$ 

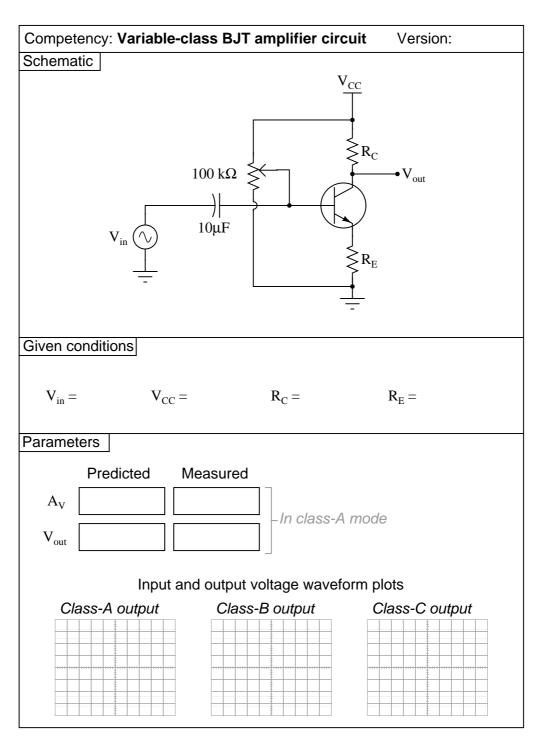
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 28

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, about 0.5 volts AC (peak).

Resistor values I have found practical are 10 k $\Omega$  for  $R_C$  and 2.2 k $\Omega$  for  $R_E$ . This gives a voltage gain of 4.545, and quiescent current values that are well within the range of common small-signal transistors.

An important aspect of this performance assessment is that students know what to do with the potentiometer. It is their responsibility to configure the circuit so that it operates in Class-A mode, and to explain the importance of proper biasing.



 $\underline{\mathrm{file}\ 01624}$ 

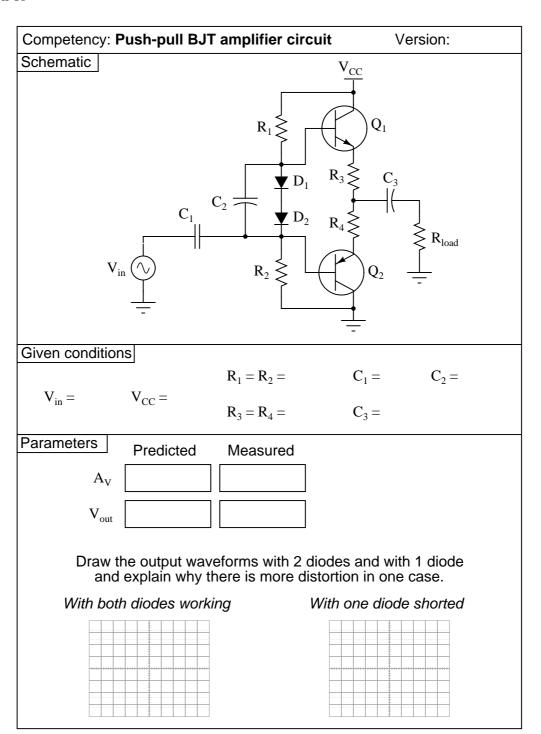
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 29

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, about 0.5 volts AC (peak).

Resistor values I have found practical are 10 k $\Omega$  for  $R_C$  and 2.2 k $\Omega$  for  $R_E$ . This gives a voltage gain of 4.545, and quiescent current values that are well within the range of common small-signal transistors.

An important aspect of this performance assessment is that students know what to do with the potentiometer. It is their responsibility to configure the circuit so that it operates in each mode (Class-A, Class-B, and Class-C).



<u>file 01994</u>

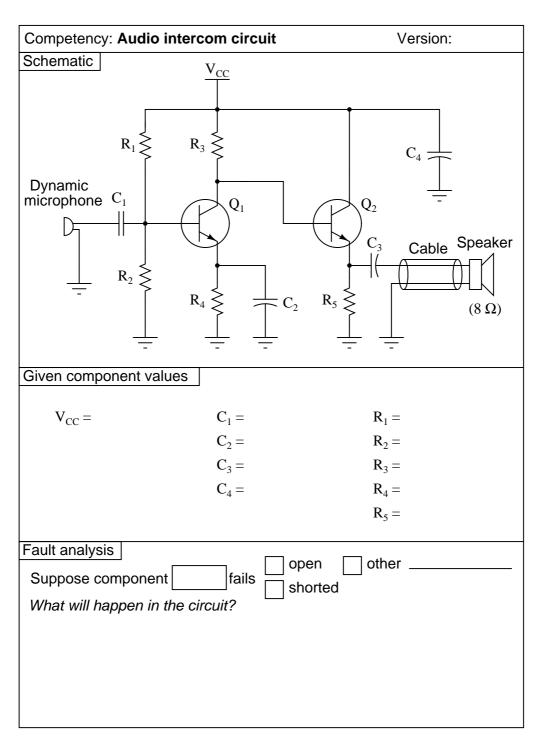
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 30

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{CC} = 6$  volts
- $V_{in} = 1$  volt (peak)
- $R_1 = R_2 = 10 \text{ k}\Omega$
- $R_3 = R_4 = 10 \ \Omega$
- $C_1 = 0.47 \ \mu \text{F}$
- $C_2 = 10 \ \mu \text{F}$
- $C_3 = 47 \ \mu \text{F}$
- $D_1 = D_2 = \text{part number } 1\text{N}4001$
- $Q_1 = \text{part number } 2\text{N}2222$
- $Q_2 = \text{part number } 2\text{N}2907$



 $\underline{\mathrm{file}\ 01937}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 31

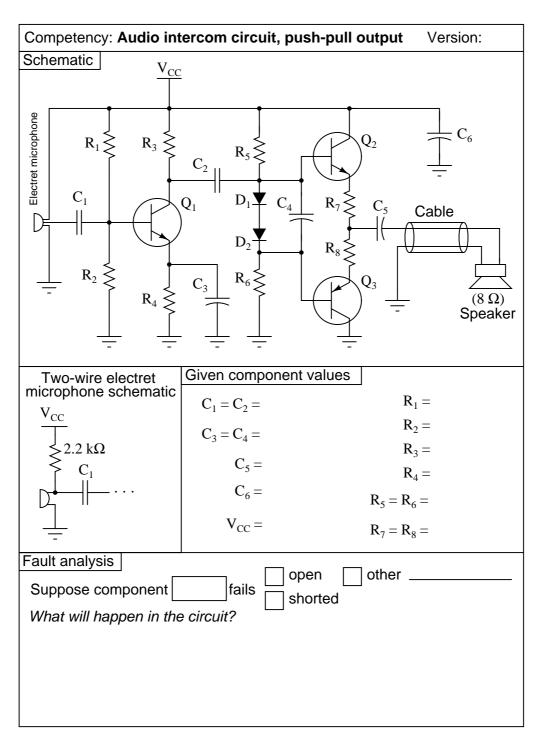
I've experienced good results using the following component values:

- $V_{CC} = 12$  volts
- $R_1 = 220 \text{ k}\Omega$
- $R_2 = 27 \text{ k}\Omega$
- $R_3 = 10 \text{ k}\Omega$
- $R_4 = 1.5 \text{ k}\Omega$
- $R_5 = 1 \text{ k}\Omega$
- $C_1 = 0.47 \ \mu \text{F}$
- $C_2 = 4.7 \ \mu \text{F}$
- $C_3 = 33 \ \mu \text{F}$
- $C_4 = 47 \ \mu \text{F}$
- $Q_1$  and  $Q_2 = 2N3403$

Students have a lot of fun connecting long lengths of cable between the output stage and the speaker, and using this circuit to talk (one-way, simplex communication) between rooms.

One thing I've noticed some students misunderstand in their study of electronic amplifier circuits is their practical purpose. So many textbooks emphasize abstract analysis with sinusoidal voltage sources and resistive loads that some of the real applications of amplifiers may be overlooked by some students. One student of mine in particular, when building this circuit, kept asking me, "so where does the signal generator connect to this amplifier?" He was so used to seeing signal generators connected to amplifier inputs in his textbook (and lab manual!) that he never realized you could use an amplifier circuit to amplify a real, practical audio signal!!! An extreme example, perhaps, but real nevertheless, and illustrative of the need for practical application in labwork.

In order for students to measure the voltage gain of this amplifier, they must apply a steady, sinusoidal signal to the input. The microphone and speaker are indeed practical, but the signals produced in such a circuit are too chaotic for students to measure with simple test equipment.



 $\underline{\mathrm{file}\ 01995}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 32

Use a variable-voltage, regulated power supply to supply a DC voltage safely below the maximum rating of the electret microphone (typically 10 volts). Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{CC} = 6$  volts
- $R_1 = 68 \text{ k}\Omega$
- $R_2 = 33 \text{ k}\Omega$
- $R_3 = 4.7 \text{ k}\Omega$
- $R_4 = 1.5 \text{ k}\Omega$
- $R_5 = R_6 = 10 \text{ k}\Omega$
- $R_7 = R_8 = 10 \ \Omega$
- $C_1 = C_2 = 0.47 \ \mu \text{F}$
- $C_3 = C_4 = 47 \ \mu \text{F}$
- $C_5 = 1000 \ \mu \text{F}$
- $C_6 = 100 \ \mu \text{F}$
- $D_1 = D_2 = \text{part number } 1\text{N}4001$
- $Q_1 = \text{part number } 2\text{N}2222$
- $Q_2 = \text{part number } 2\text{N}2222$
- $Q_3 = \text{part number } 2\text{N}2907$

Question 33

Competency: Class-A BJT amplifier w/specified gain Version:

## Description

Design and build a class-A BJT amplifier circuit with a voltage gain (A<sub>V</sub>) that is within tolerance of the gain specified.

You may use a potentiometer to adjust the biasing of the transistor, to make the design process easier.

Given conditions

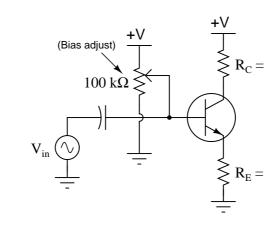
$$V_{in} =$$

$$+V = A_V =$$

$$A_{\rm v} =$$

$$\mathsf{Tolerance}_{\mathsf{A}_\mathsf{V}} =$$

Schematic



Parameters

Measured Calculated  $V_{in}$  $\mathsf{Error}_{\mathsf{A}_\mathsf{v}}$ 

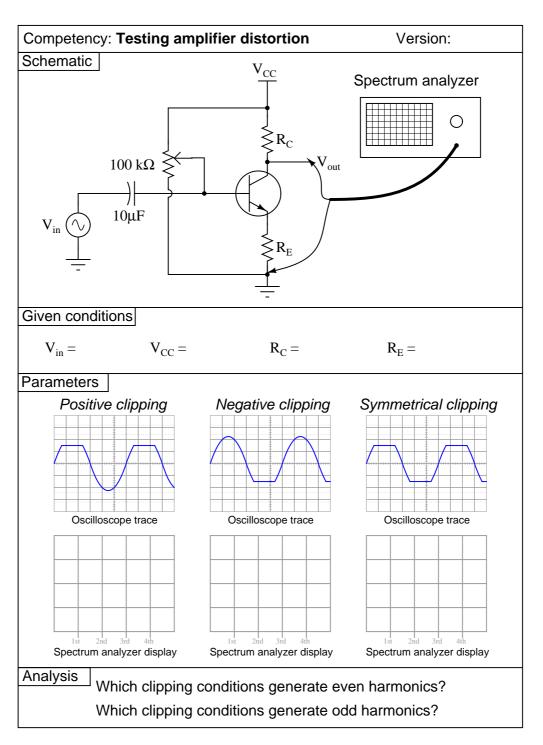
 $\underline{\mathrm{file}\ 01935}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 33

Students are allowed to adjust the bias potentiometer to achieve class-A operation after calculating and inserting the resistance values  $R_C$  and  $R_E$ . However, they are not allowed to change either  $R_C$  or  $R_E$  once the circuit is powered and tested, lest they achieve the specified gain through trial-and-error!

A good percentage tolerance for gain is +/- 10%. The lower you set the target gain, the more accuracy you may expect out of your students' circuits. I usually select random values of voltage gain between 2 and 10, and I strongly recommend that students choose resistor values between 1 k $\Omega$  and 100 k $\Omega$ . Resistor values much lower than 1 k $\Omega$  lead to excessive quiescent currents, which may cause accuracy problems ( $r'_e$  drifting due to temperature effects).



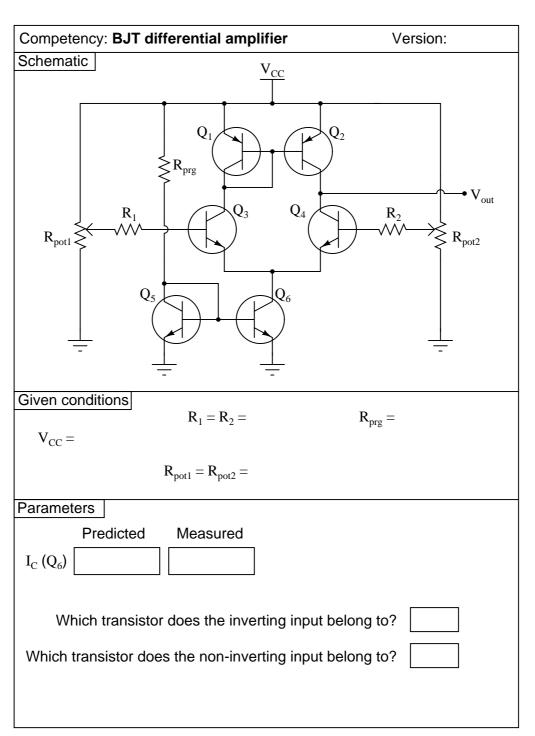
 $\underline{\mathrm{file}\ 01996}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 34

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal.

If you lack a spectrum analyzer in your lab, fear not! There are free software packages in existence allowing you to use the audio input of a personal computer's sound card as a (limited) spectrum analyzer and oscilloscope! You may find some of these packages by searching on the Internet. One that I've used (2002) successfully in my own class is called WinScope.



file 01997

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 35

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

I suggest using ordinary (general-purpose) signal transistors in this circuit, such as the 2N2222 and 2N3403 (NPN), and the 2N2907 and 2N3906 (PNP) models, operating with a  $V_{CC}$  of 12 volts. When constructed as shown, this circuit has sufficient gain to be used as a crude operational amplifier (connect the inverting input to the output through various feedback networks).

These values have worked well for me:

- $V_{CC} = 12$  volts
- $R_1 = 10 \text{ k}\Omega$
- $R_2 = 10 \text{ k}\Omega$
- $R_{prg} = 10 \text{ k}\Omega$
- $R_{pot1} = 10 \text{ k}\Omega$
- $R_{pot2} = 10 \text{ k}\Omega$

I recommend instructing students to set each potentiometer near its mid-position of travel, then slightly adjusting each one to see the sharp change in output voltage as one input voltage crosses the other. If students wish to monitor each of the input voltages to check for a condition of crossing, they should measure right at the transistor base terminals, not at the potentiometer wiper terminals, so as to not incur error resulting from current through protection resistors  $R_1$  or  $R_2$ .

Competenc	y: JFET terminal identification	Version:			
Description					
	Identify the terminals (emitter, base, and collector) of a junction field-effect transistor using a multimeter. Then, compare your conclusions with information from a datasheet or cross-reference book.				
Given condi	itions				
Part nur	mber =				
Parameters					
$ m V_{gate ext{-}channel}$ $ m V_{channel}$	Measured				
Terminal ide	entification (Draw your own sketch if shown is not appropri				
Advertis	sed Your conclusion				

file 01930

Contrary to what you might think, the datasheet or cross-reference is not the "final authority" for checking your meter-based conclusions! I have seen datasheets and cross-reference manuals wrong more than once!

# Notes 36

Identification of JFET terminals is a very important skill for technicians to have. Most modern multimeters have a *diode check* feature which may be used to positively identify PN junction polarities, and this is what I recommend students use for identifying JFET terminals.

To make this a really good performance assessment, you might want to take several JFET's and scratch the identifying labels off, so students cannot refer to memory for pin identification (for instance, if they remember the pin assignments of a J309 because they use it so often). Label these transistors with your own numbers ("1", "2", etc.) so you will know which is which, but not the students!

Competency	: Current-sourcing JFET switch	Version:
Schematic		
	$V_{\text{supply}} \stackrel{R_1}{=} V_{\text{probe}}$	Q <sub>1</sub> LED $R_{dropping}$
Given condit	ions	
$V_{ m supply} =$	$R_1 = R_d$	ropping =
Parameters		
${ m I_{LED}}$ (max) ${ m iggl[}$	Predicted Measured	
$V_{GS(off)}$	Advertised Measured F	Calculated P <sub>Q1</sub>
Schematic	(Draw a schematic diagram is necessary to turn the tran	

<u>file 01972</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 37

I strongly recommend a value for R1 of 1 M $\Omega$  or more, to protect the JFET gate from overcurrent damage. The students will calculate their own dropping resistor value, based on the supply voltage and the LED ratings.

This exercise lends itself to experimentation with static electricity. The input impedance of an average JFET is so high that the LED may be made to turn on and off with just a touch of the probe wire to a charged object (such as a person).

Using only the components shown, students may not be able to get their JFETs to completely turn off. This is left for them as a challenge to figure out!

I expect students to be able to figure out how to calculate the transistor's power dissipation without being told what measurements to take!

Competency	/: Current-sinking JFET switch	Version:
Schematic		
	$V_{\text{supply}} {{=}} \stackrel{\text{Probe}}{{=}} \stackrel{R_1}{{\swarrow}}$	LED  R <sub>dropping</sub> Q <sub>1</sub>
Given condit	ions	
		D.
$V_{\text{supply}} =$	$R_1 =$	$R_{dropping} =$
Parameters	I	
1 arameters	J	
	Predicted Measured	
I <sub>LED</sub> (max)		
LED ( / [		
	Advertised Measured	Calculated
<b>3</b> 7	Advertised Weasured	
$V_{GS (off)}$		P <sub>Q1</sub>
Schematic	Draw a schematic diagra	m showing what
	is necessary to turn the ti	
	•	, ,

<u>file 01973</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 38

I strongly recommend a value for R1 of 1 M $\Omega$  or more, to protect the JFET gate from overcurrent damage. The students will calculate their own dropping resistor value, based on the supply voltage and the LED ratings.

This exercise lends itself to experimentation with static electricity. The input impedance of an average JFET is so high that the LED may be made to turn on and off with just a touch of the probe wire to a charged object (such as a person).

Using only the components shown, students may not be able to get their JFETs to completely turn off. This is left for them as a challenge to figure out!

I expect students to be able to figure out how to calculate the transistor's power dissipation without being told what measurements to take!

Competency: Current-sinking MOSFET switch Version:
Schematic
V <sub>supply</sub> = R <sub>dropping</sub> $Q_1$
Given conditions
$V_{supply} = R_{bleed} = R_{dropping} =$
arameters
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
ault analysis open other
Suppose component fails shorted  What will happen in the circuit?

 $\underline{\mathrm{file}\ 02425}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 39

I recommend a value for R1 of 1 M $\Omega$  or more, to show that the bleed resistor need not be very conductive to do its job well. The students will calculate their own dropping resistor value, based on the supply voltage and the LED ratings.

Students predict the LED current (approximately 20 mA) and the switch current (0 mA), and then calculate the transistor's "on" channel resistance and power dissipation after taking additional measurements. I expect students to be able to figure out how to calculate both these parameters without being told what measurements to take!

Competency:	MOSFET switch circuit	Version:
Description		
	Design and build a circuit that uses a switch to turn on an E-type MOSFET, which then turns on a DC load such as a light bulb or small electric motor. The switch must carry zero current, with the transistor carrying 100% of the load current.	
Given condition	ons	
$V_{supply} =$		
Schematic		
Parameters		
ľ	Measured	
$I_{load}$		
I <sub>switch</sub>	Is $I_{\text{switch}} = 0 \text{ mA}$ ?	

 $\underline{\mathrm{file}\ 02424}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 40

Being able to design a circuit using a MOSFET as a switch is a valuable skill for technicians and engineers alike to have.

Competency: JFET cur	rent regulato	r Version:			
Schematic					
$\frac{V_{DD}}{R_{load}}$					
Given conditions					
	$R_1 =$	R <sub>load</sub> (max) =			
Parameters					
Predicted	Measured				
$I_{R1}$					
I <sub>load</sub>		(R <sub>load</sub> set to mid-value)			
$R_{load(max)}$		(Maximum R with $I_{load}$ stable)			
$R_{load(min)}$		(Minimum R with $I_{load}$ stable)			

file 01948

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 41

Competency: Co	ommon-dra	ain class-A a	amplifie	r	Ve	rsior	ո:	
Schematic								
			$\frac{V_{DD}}{I}$					
		$C_1$						
				<b>)</b> <sub>1</sub>				
			<b>\</b>	,	7			
	$V_{in} \left( \bigcirc \right)$	$R_G \geqslant$	> <sub>D</sub>		V <sub>out</sub>			
	<u> </u>		$\geq$ R	S				
			<u> </u>					
Given conditions	3							
***	<b>T</b> 7	D	D			<b>C</b>		
$V_{in} =$	$V_{DD} =$	$R_{G} =$	K	s =		$C_1 =$	=	
Danamatana								
Parameters				Input	and c	utpu	ıt	
Pred	licted M	leasured	wav	eforn	ns (m	easu	red	)
V <sub>G</sub> (DC)					 			
V <sub>out</sub> (AC)					‡			
					<del>-</del>			
$A_V$					<u> </u>			
					‡			
Inverting								
or noninverting	g?							
·	<b>-</b> Ш							

<u>file 01992</u>

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 42

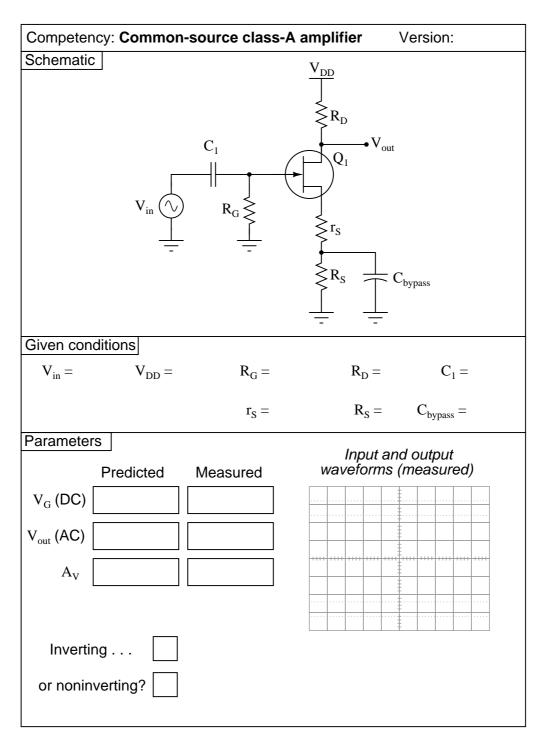
Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{DD} = 9$  volts
- $V_{in} = 1$  volt (peak), f = 2 kHz
- $R_G = 100 \text{ k}\Omega$
- $R_S = 10 \text{ k}\Omega$
- $C_1 = 0.47 \ \mu \text{F}$

Please note that the quiescent output voltage is impossible to precisely predict, as it depends on the particular characteristics of the JFET used ( $I_D$  versus  $V_{GS}$ ). The fact that this circuit uses self-biasing instead of voltage divider biasing makes the situation worse. Predicting quiescent gate voltage, however should be extremely easy (0 volts) if one understands how JFETs function.

An interesting parameter to explore in this circuit is the effect of the source resistor value on voltage gain. The theoretical voltage gain of a simple common-drain amplifier circuit is unity (1), but this may be approximated only with relatively large load resistor  $(R_S)$  values. Try substituting a 1 k $\Omega$  or less resistor for  $R_S$ , and notice what happens to the gain. Then, have your students explain why this happens!



 $\underline{\mathrm{file}\ 01993}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 43

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

I have had good success using the following values:

- $V_{DD} = 12$  volts
- $V_{in} = 0.5 \text{ volt (peak-to-peak)}, f = 2 \text{ kHz}$
- $R_G = 100 \text{ k}\Omega$
- $r_S = 2.2 \text{ k}\Omega$
- $R_S = 10 \text{ k}\Omega$
- $R_D = 10 \text{ k}\Omega$
- $C_1 = 0.47 \ \mu \text{F}$
- $C_{bypass} = 10 \ \mu F$

Please note that the quiescent output voltage is impossible to precisely predict, as it depends on the particular characteristics of the JFET used ( $I_D$  versus  $V_{GS}$ ). The fact that this circuit uses self-biasing instead of voltage divider biasing makes the situation worse. Predicting quiescent gate voltage, however should be extremely easy (0 volts) if one understands how JFETs function.

All quiescent circuit values depend on  $V_{DD}$ , so if things aren't biased the way you would like, simply adjust the power supply voltage to suit.

Competency: Class-A JFET amplifier w/specified phase Version:					
Description					
Design and build a class-A JFET amplifier circuit with the phase (inverting or noninverting) specified.					
Given conditions					
$V_{in} = +V =$	Inverting				
	Noninverting				
Schematic Show all component value	es!				
Parameters					
Does the amplifier invert the	e waveform or not?				

 $\underline{\mathrm{file}\ 03879}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 44

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

Competency: Class-A JFET amplifier w/specified gain Version:					
Description					
Design and build a class-A JFET amplifier circuit with a voltage gain $(A_{\rm V})$ that is within tolerance of the gain specified.					
Given conditions					
$V_{in}$ = $+V$ = $A_V$ = $Tolerance_{A_V}$ =					
Schematic Show all component values!					
Parameters					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					

 $\underline{\mathrm{file}\ 01936}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 45

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips at the specified gain.

Competency: Class-A transistor amplifier w/specified phase				
Description				
Design and build a class-A transistor amplifier circuit with the phase (inverting or noninverting) specified.				
Given conditions				
$V_{in} = +V =$	Inverting			
	Noninverting			
Schematic Show all component valu	es!			
Parameters				
Does the amplifier invert the	e waveform or not?			

 $\underline{\mathrm{file}\ 03884}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 46

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.). Use a sine-wave function generator to supply an audio-frequency input signal, and make sure its amplitude isn't set so high that the amplifier clips.

Competency: BJT mul	tivibrator circuit, astable	e Version:
Schematic		
$R_1$ $Q_1$	$V_{CC}$ $R_2$ $R_3$ $C_2$	$\mathbb{R}_4$ $\mathbb{Q}_2$
Given conditions		
$V_{CC} = R_1 =$	$R_2 =$	$C_1 =$ $C_2 =$
$R_4 =$	$R_3 =$	$C_2 =$
Parameters		
	edicted Measured	
Duty Cycle (at Q <sub>1</sub> collector)		Potentiometer turned fully clockwise
Fault analysis		
Suppose component What will happen in th	fails open shorted e circuit?	other

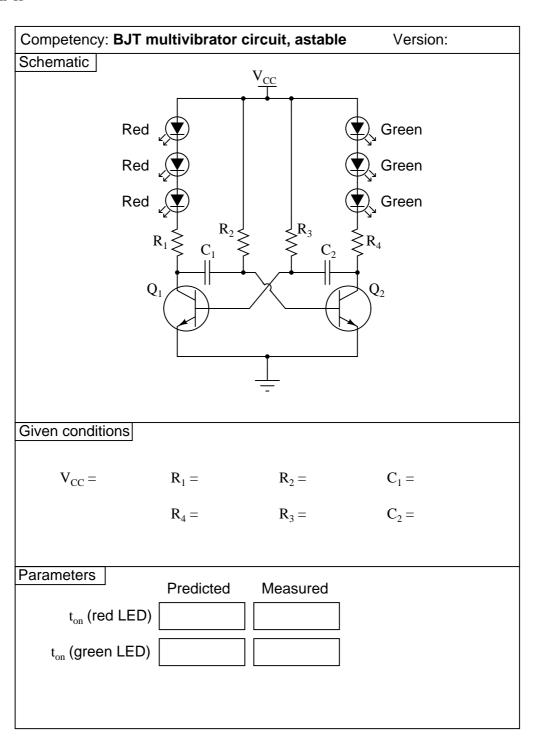
 $\underline{\mathrm{file}\ 01939}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 47

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than resistors  $R_2$  and  $R_3$ . This way,  $R_2$  and  $R_3$  dominate the capacitors' charging times, making calculation of duty cycle much more accurate. Component values I've used with success are 1 k $\Omega$  for  $R_1$  and  $R_4$ , 100 k $\Omega$  for  $R_2$  and  $R_3$ , and 0.1  $\mu$ F for  $C_1$  and  $C_2$ .



 $\underline{\mathrm{file}\ 01947}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 48

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than resistors  $R_2$  and  $R_3$ . This way,  $R_2$  and  $R_3$  dominate the capacitors' charging times, making calculation of duty cycle much more accurate. Component values I've used with success are 470  $\Omega$  for  $R_1$  and  $R_4$ , 270 k $\Omega$  for  $R_2$  and  $R_3$ , 4.7  $\mu$ F for  $C_1$  and  $C_2$ , and 6 to 14 volts for  $V_{CC}$ . The frequency of this circuit does vary with supply voltage, so don't expect perfect agreement between predicted and measured values.

By the way, this circuit works very well for holiday flashing lights – decorate your lab room accordingly with student-built light flashers!

	BJT multivi	brator w/ var	riable duty cyc	cle Version:
Schematic		$V_{CC}$		
	$R_1 \gtrsim Q_1$	<u>_</u>	$R_3$ $C_2$ $R_2$	
Given conditio	ns			
$V_{CC} =$	$R_1 =$	$R_2 =$	$\mathbf{R}_{\mathrm{pot}} =$	$C_1 =$
	$R_4 =$	$R_3 =$		$C_2 =$
Parameters				
	Predic	cted Meas	sured	
Duty Cycl (at Q <sub>1</sub> collec			Poten	tiometer turned ly clockwise
Fault analysis				L
Suppose con		fails	open oth	her

<u>file 01990</u>

Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 49

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than the combined resistance of resistors  $R_2$  and  $R_3$  and the respective potentiometer section resistances. This way,  $R_{pot}$ ,  $R_2$ , and  $R_3$  dominate the capacitors' charging times, making calculation of duty cycle much more accurate. Component values I've used with success are  $1 \text{ k}\Omega$  for  $R_1$  and  $R_4$ ,  $10 \text{ k}\Omega$  for  $R_2$  and  $R_3$ ,  $100 \text{ k}\Omega$  for  $R_{pot}$ , and  $0.001 \text{ }\mu\text{F}$  for  $C_1$  and  $C_2$ .

# Competency: BJT multivibrator w/ variable duty cycle Version: Schematic $V_{\underline{CC}}$ Given conditions $V_{CC} =$ $R_1 = R_2 =$ $R_{pot} =$ $R_4 = R_3 =$ Duty cycle (D) = Parameters Waveform at specified DMeasured Duty Cycle (at Q<sub>1</sub> collector)

file 02607

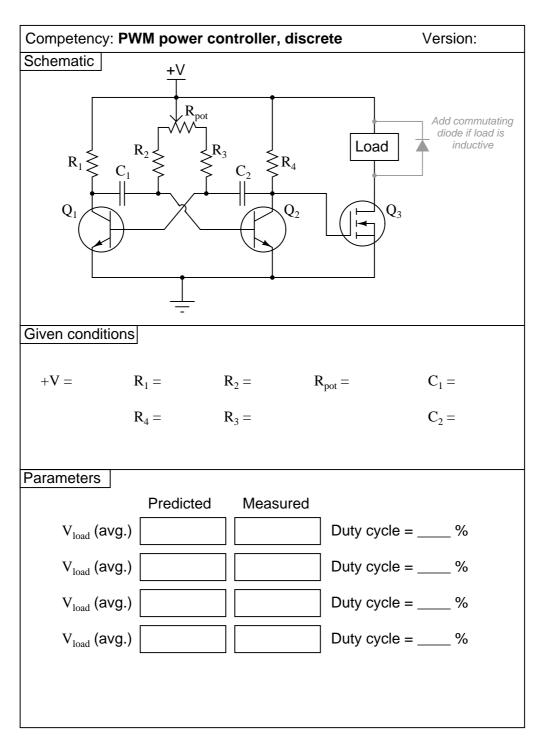
Use circuit simulation software to verify your predicted and measured parameter values.

## Notes 50

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than the combined resistance of resistors  $R_2$  and  $R_3$  and the respective potentiometer section resistances. This way,  $R_{pot}$ ,  $R_2$ , and  $R_3$  dominate the capacitors' charging times, making calculation of duty cycle much more accurate. Component values I've used with success are  $1 \text{ k}\Omega$  for  $R_1$  and  $R_4$ ,  $10 \text{ k}\Omega$  for  $R_2$  and  $R_3$ ,  $100 \text{ k}\Omega$  for  $R_{pot}$ , and  $0.001 \text{ }\mu\text{F}$  for  $C_1$  and  $C_2$ .

Question 51



 $\underline{\mathrm{file}\ 01991}$ 

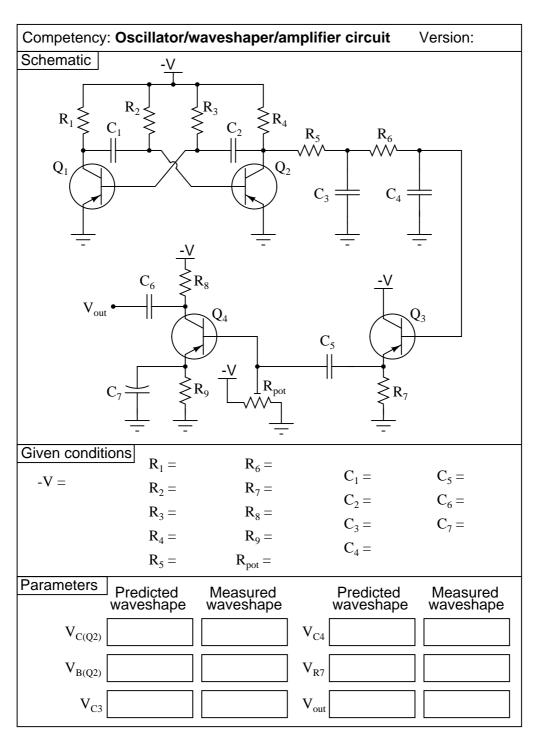
Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 51

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than the combined resistance of resistors  $R_2$  and  $R_3$  and the respective potentiometer section resistances. This way,  $R_{pot}$ ,  $R_2$ , and  $R_3$  dominate the capacitors' charging times, making calculation of duty cycle much more accurate. Component values I've used with success are  $1 \text{ k}\Omega$  for  $R_1$  and  $R_4$ ,  $10 \text{ k}\Omega$  for  $R_2$  and  $R_3$ ,  $100 \text{ k}\Omega$  for  $R_{pot}$ , and  $0.001 \mu\text{F}$  for  $C_1$  and  $C_2$ . In my prototype circuit, I used 2N2222 bipolar transistors and an IRF510 power MOSFET.

Although small DC motors work well as demonstrative loads, their counter-EMF may wreak havoc with measurements of average load voltage. Purely resistive loads work best when comparing measured average load voltage against predicted average load voltage. Also, motors and other inductive loads may cause the MOSFET to switch incorrectly (or not switch at all!) unless a commutating diode is installed to limit the voltage induced by the collapsing magnetic field every time the transistor turns off.



 $\underline{\mathrm{file}\ 02507}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 52

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

This circuit demonstrates the use of passive integrators to convert a square wave into a pseudo-sine wave output. The multivibrator portion produces nice, sharp-edged square wave signals at the transistor collector terminals when resistors  $R_1$  and  $R_4$  are substantially smaller than resistors  $R_2$  and  $R_3$ . Component values I've used with success are 1 k $\Omega$  for  $R_1$  and  $R_4$ , 100 k $\Omega$  for  $R_2$  and  $R_3$ , and 0.001  $\mu$ F for  $C_1$  and  $C_2$ .

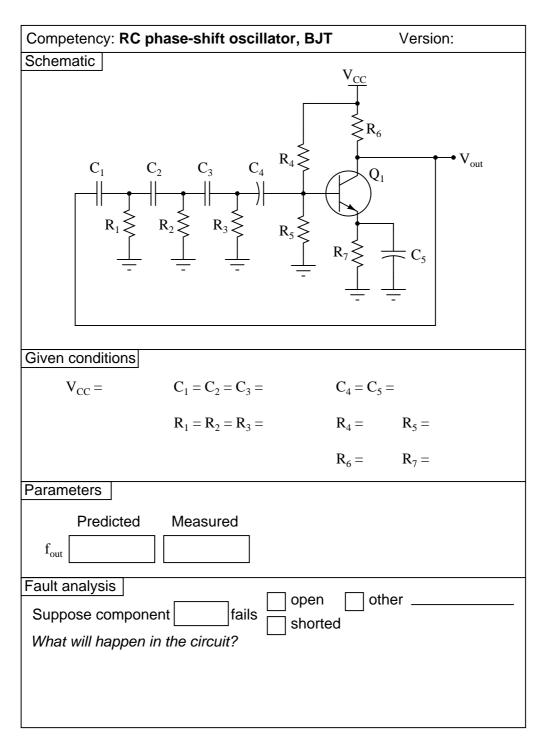
Resistors  $R_5$  and  $R_6$ , along with capacitors  $C_3$  and  $C_4$ , form a dual passive integrator network to re-shape the square-wave output of the multivibrator into a pseudo-sine wave. These components' values must be chosen according to the multivibrator frequency, so that the integration is realistic without the attenuation being excessive. Integrator component values that have worked well for the multivibrator components previously specified are 10 k $\Omega$  for  $R_5$  and  $R_6$ , and 0.1  $\mu$ F for  $C_3$  and  $C_4$ .

Transistor  $Q_3$  is just an emitter follower, placed there to give the amplifier section a high input impedance.  $Q_3$ 's emitter resistor value is not critical. I have used a 1 k $\Omega$  resistor for  $R_7$  with good success.

The last transistor  $(Q_4)$  is for voltage amplification. A "trimmer" style potentiometer (10 k $\Omega$  recommended for  $R_{pot}$ ) provides easy adjustment of biasing for different supply voltages. Using the potentiometer, I have operated this circuit on supply voltages ranging from -6 volts to -27 volts. Use a bypass capacitor  $(C_7)$  large enough that its reactance at the operating frequency is negligible (less than 1 ohm is good), such as 33  $\mu$ F. Resistor values I've used with success are 10 k $\Omega$  for  $R_8$  and 4.7 k $\Omega$  for  $R_9$ . Coupling capacitor values are not terribly important, so long as they present minimal reactance at the operating frequency. I have used 0.47  $\mu$ F for both  $C_5$  and  $C_6$  with good success.

You may find that the relatively high operating frequency of this circuit complicates matters with regard to parasitic capacitances. The fast rise and fall times of the strong square wave tend to couple easily to the sine-wave portions of the circuit, especially when the sine wave signal is so severely attenuated by the double integrators. One solution to this dilemma is to lower the operating frequency of the circuit, allowing a lower cutoff frequency for the double integrator (two-pole lowpass filter) section which in turn will improve the signal-to-noise ratio throughout. If you wish to try this, you may use these suggested component values:

- $R_1 = 1 \text{ k}\Omega$
- $R_2 = 100 \text{ k}\Omega$
- $R_3 = 100 \text{ k}\Omega$
- $R_4 = 1 \text{ k}\Omega$
- $R_5 = 100 \text{ k}\Omega$
- $R_6 = 100 \text{ k}\Omega$
- $R_7 = 1 \text{ k}\Omega$
- $R_8 = 10 \text{ k}\Omega$
- $R_9 = 4.7 \text{ k}\Omega$
- $R_{pot} = 10 \text{ k}\Omega$
- $C_1 = 0.047 \ \mu \text{F}$
- $C_2 = 0.047 \,\mu\text{F}$
- $C_3 = 0.1 \ \mu \text{F}$
- $C_4 = 0.047 \ \mu \text{F}$
- $C_5 = 1 \, \mu \text{F}$
- $C_6 = 1 \, \mu \text{F}$
- $C_7 = 33 \ \mu \text{F}$



 $\underline{\mathrm{file}\ 01950}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 53

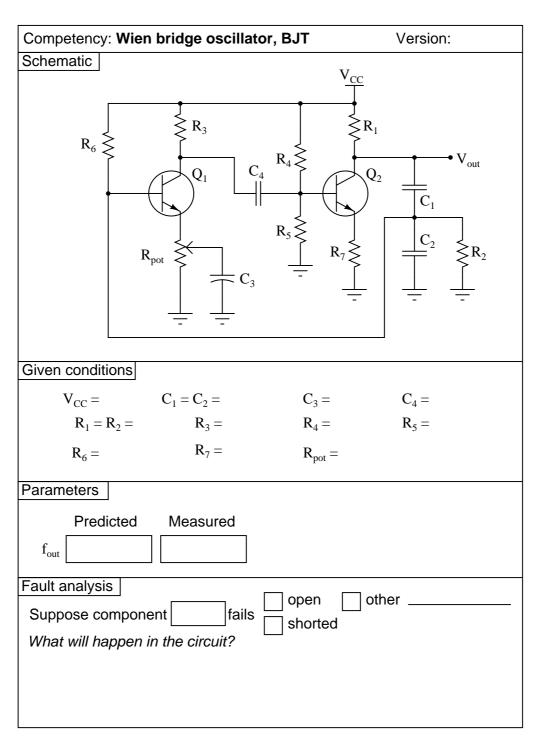
Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

I have had relatively good success with the following values:

- $V_{CC} = 9$  volts (from battery)
- $C_1$  through  $C_3 = 0.001 \ \mu F$
- $C_4$  and  $C_5 = 4.7 \ \mu \text{F}$
- $R_1$  through  $R_3 = 10 \text{ k}\Omega$
- $R_4 = 270 \text{ k}\Omega$
- $R_5 = 50 \text{ k}\Omega$  (two 100 k $\Omega$  resistors in parallel)
- $R_6 = 12 \text{ k}\Omega$  (you might want to make this resistor variable so students can experiment with  $A_V$ )
- $R_7 = 1 \text{ k}\Omega$
- $Q_1 = \text{part number } 2\text{N}3403$

One of the problems with the RC phase-shift oscillator circuit design is the loading of the phase-shift network by the transistor's biasing network ( $R_4$  and  $R_5$ ), which will offset the predicted oscillation frequency from what you might expect from the RC network alone. While it is possible to account for all the factors in this circuit, it is not a simple task for students just beginning to understand how the circuit is supposed to work.

I have also noticed that the frequency of this circuit is significantly reduced by the capacitance of any test leads connected to it. Beware of oscilloscope probe cables – the capacitance they add to the circuit will offset the oscillation frequency!



 $\underline{\mathrm{file}\ 01975}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 54

Use a variable-voltage, regulated power supply to supply any amount of DC voltage below 30 volts. Specify standard resistor values, all between 1 k $\Omega$  and 100 k $\Omega$  (1k5, 2k2, 2k7, 3k3, 4k7, 5k1, 6k8, 10k, 22k, 33k, 39k 47k, 68k, etc.).

 $R_{pot}$  serves the purpose of providing variable AC gain in the first amplifier stage to meet the Barkhausen criterion.

I have had good success with the following values:

- $V_{CC} = 12$  volts
- $C_1$  and  $C_2 = 0.001 \ \mu \text{F}$
- $C_3 = 47 \ \mu \text{F}$
- $C_4 = 0.47 \ \mu \text{F}$
- $R_1$  and  $R_2 = 4.7 \text{ k}\Omega$
- $R_3 = 4.7 \text{ k}\Omega$
- $R_4 = 39 \text{ k}\Omega$
- $R_5 = 22 \text{ k}\Omega$
- $R_6 = 27 \text{ k}\Omega$
- $R_7 = 3.3 \text{ k}\Omega$
- $R_{pot} = 10 \text{ k}\Omega$ , linear
- $Q_1$  and  $Q_2$  = part number 2N2222

0		<b>\</b> /
	pitts oscillator, BJT	Version:
Schematic	$V_{CC}$ $R_{2}$ $Q_{1}$	$V_{\text{out}}$ $C_1$
Given conditions		$C_2 =$
Given conditions		
$V_{CC} =$		$C_1 = C_3 $
Parameters		
Predicted $f_{out}$	Measured	
Fault analysis  Suppose compo	nent fails sh	en

<u>file 01952</u>

Use circuit simulation software to verify your predicted and measured parameter values.

### Notes 55

I have had great success with the following values:

- $V_{CC} = 7$  to 24 volts
- $C_1$  and  $C_2 = 0.22 \ \mu F$
- $C_3 = 0.47 \ \mu \text{F}$
- $L_1 = 100 \ \mu \text{H}$  (ferrite core RF choke)
- $R_1 = 22 \text{ k}\Omega$
- $R_2 = 1.5 \text{ M}\Omega$
- $Q_1 = \text{part number } 2\text{N}3403$

With these component values, the output waveform was quite clean and the frequency was very close to predicted:

$$f_{out} = \frac{1}{2\pi\sqrt{\frac{LC_1C_2}{C_1 + C_2}}}$$

You might want to quiz your students on the purpose of resistor  $R_2$ , since it usually only has to be present at power-up to initiate oscillation!

Competency: Hartley	oscillator, series	-fed BJT	Version:
Schematic			
$C_2 =$	$R_1$ $Q_1$ $C_1$ $Q_1$	V <sub>out</sub>	
Given conditions			
V <sub>CC</sub> =	$C_1 =$	$L_{primary} =$	
	$R_1 =$	$C_2 =$	
Parameters			
f <sub>out</sub>	Measured		
Fault analysis		onen Dotho	r
Suppose component open other shorted			
What will happen in the circuit?			

 $\underline{\text{file } 01965}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 56

I have had success with the following values:

- $V_{CC} = 12$  to 24 volts
- $C_1 = 0.47 \ \mu \text{F}$
- $C_2 = 0.47 \ \mu \text{F}$
- $T_1 = 1000:8 \Omega$  audio matching transformer (used as center-tap inductor)
- $R_1 = 1.5 \text{ M}\Omega$
- $Q_1 = \text{part number } 2\text{N}3403$

Capacitors  $C_1$  and  $C_2$  need not be equal value, since they serve entirely different purposes:  $C_1$  is the tank circuit capacitance, while  $C_2$  is merely a coupling capacitor. I just happened to be blessed with an abundance of 0.47  $\mu$ F capacitors when I prototyped this circuit, so I chose that value for both capacitors!

With these component values, the output waveform I measured was not very sinusoidal, but at least it was oscillating. The harmonic output of a Hartley oscillator is substantially greater than a Colpitts, primary because the two capacitors in the Colpitts design act as decoupling capacitances, shunting high-order harmonic signals to ground.

Of course, in order to predict the frequency of oscillation in this Hartley oscillator circuit, you must know the inductance of the audio transformer's primary winding!

You might want to quiz your students on the purpose of resistor  $R_1$ , since it usually only has to be present at power-up to initiate oscillation!

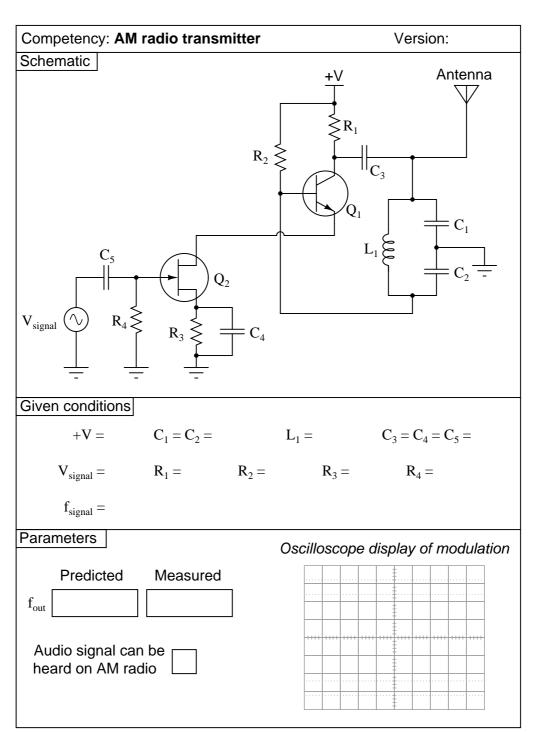
Competency: BJT oscillator w/specified frequency Version:			
Description			
Design and build a BJT oscillator circuit to output a sine-wave AC voltage at a frequency within the specified tolerance.			
Given condition	าร		
+V =	f =	Tolerance <sub>f</sub> =	
Schematic S	Show all compone	ent values!	
Parameters			
Measu	red	Calculated	
f	Error <sub>f</sub>	$f_{(actual)}$ -	$\frac{f_{\text{(ideal)}}}{100\%} \times 100\%$
1		$f_{(idea}$	× 100%

 $\underline{\mathrm{file}\ 01949}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 57

Students are free to choose any oscillator design that meets the criteria: sinusoidal output at a specified frequency.



 $\underline{\mathrm{file}\ 01953}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

#### Notes 58

I have had great success with the following values:

- $\bullet$  +V = 7 to 24 volts
- $C_1$  and  $C_2 = 0.001 \ \mu F$
- $C_3$ ,  $C_4$ , and  $C_5 = 0.47 \ \mu F$
- $L_1 = 100 \, \mu \text{H}$  (ferrite core RF choke)
- $R_1 = 22 \text{ k}\Omega$
- $R_2 = 1.5 \text{ M}\Omega$
- $R_3 = 6.8 \text{ k}\Omega$
- $R_4 = 100 \text{ k}\Omega$
- $Q_1 = \text{part number } 2\text{N}3403$
- $Q_2 = \text{part number MPF } 102$

With these component values, the carrier waveform was quite clean and the frequency was almost exactly  $700~\mathrm{kHz}$ :

$$f_{out} = \frac{1}{2\pi\sqrt{\frac{LC_1C_2}{C_1 + C_2}}}$$

Modulation isn't that great, due to the crude nature of the circuit, but it is certainly good enough to hear over an appropriately tuned AM radio. Setting  $V_{signal}$  and  $f_{signal}$  is a matter of experimentation, to achieve the desired degree of modulation and tone pitch.

Competency: SCR terminal identification	/ersion:	
Description		
Identify the terminals (emitter, base, and collector) of a silicon-controlled rectifier using a multimeter. Then, compare your conclusions with information from a datasheet or cross-reference book.		
Given conditions		
Part number =		
Parameters		
$\begin{array}{c} \text{Measured} \\ V_{\text{bias}(GK)} \end{array}$		
Terminal identification (Draw your own sketch if the	ne one	
shown is not appropriate	ie)	
Advertised Your conclusion		
(Label)		

<u>file 01922</u>

Contrary to what you might think, the datasheet or cross-reference is not the "final authority" for checking your meter-based conclusions! I have seen datasheets and cross-reference manuals wrong more than once!

# Notes 59

Identification of SCR terminals is a very important skill for technicians to have. Most modern multimeters have a *diode check* feature which may be used to positively identify PN junction polarities, and this is what I recommend students use for identifying SCR terminals.

This exercise may be made even more interesting if students must differentiate between SCR's with sensitive gates versus SCR's without sensitive gates!

To make this a really good performance assessment, you might want to take several SCR's and scratch the identifying labels off, so students cannot refer to memory for pin identification. Label these thyristors with your own numbers ("1", "2", etc.) so *you* will know which is which, but not the students!

Competency: SCR latch circuit	Version:
Schematic	
$V_{\text{supply}} \stackrel{}{=} \\ \hline \\  \\ SCR_1$	Mtr
Given conditions	
$V_{ m supply} =$	
Parameters	
$\begin{array}{c c} & \text{Predicted} & \text{Measured} \\ V_{\text{motor}}  (\text{on}) & & & & \\ I_{\text{supply}}  (\text{on}) & & & & \\ \end{array}$	
Calculated	
P <sub>SCR1</sub>	

<u>file 01987</u>

Use circuit simulation software to verify your predicted and measured parameter values.

### Notes 60

I have had good success using 12 volts DC for the supply voltage, an MCR8SN silicon-controlled rectifier, and a small brushless DC fan motor (80 mA running current) as the load. The MCR8SN is a "sensitive gate" SCR, which makes it easy to demonstrate static triggering (just *touch* the gate terminal with your finger to start the motor!). Some SCR's may be difficult to keep latched with low-current loads, so be sure to prototype your SCR/load combination before assigning part numbers to your students!

Competency: SCR late	h circuit		Version:
Description			
to turn it "latcl to a D	on a Silicones" in the Cload suc	ON state, ma	Rectifier so that intaining power small electric
Given conditions			
$V_{supply} =$			
Schematic			
Parameters			
Does the circuit latc	Yes	No	

 $\underline{\mathrm{file}\ 02345}$ 

Use circuit simulation software to verify your predicted and measured parameter values.

# Notes 61

# (Template)

Competency:	Version:
Schematic	
Given conditions	
Parameters	
Predicted Measured	

 $\underline{\mathrm{file}\ 01602}$ 

Here, you would indicate where or how to obtain answers for the requested parameters, but not actually give the figures. My stock answer here is "use circuit simulation software" (Spice, Multisim, etc.).

# Notes 62

Any relevant notes for the assessment activity go here.